# A provenance study of Upper Jurassic hydrocarbon source rocks of the Flemish Pass Basin and Central Ridge, offshore Newfoundland, Canada

By Matthew William Scott

A thesis submitted to the School of Graduate Studies in partial fulfillment of the requirements for the degree of Master of Science

Department of Earth Sciences

Memorial University of Newfoundland

May 2018

St. John's

Newfoundland and Labrador

#### <u>Abstract</u>

This project is a provenance study of Upper Jurassic source and reservoir rocks from the Flemish Pass Basin and Central Ridge, offshore Newfoundland, Canada. It is aimed at adding a new dataset to contribute to our understanding of the geology of this area, where a number of recent hydrocarbon discoveries have been made, but limited geological information is available. A primary goal of the project is to determine the provenance and paleodrainage patterns of the Upper and Lower Kimmeridgian Source Rock and Upper and Lower Tempest Sandstone of the Flemish Pass Basin and the Central Ridge. It is likely that the source rock and reservoir units increase in thickness toward their source terranes and this provenance study would thus help define where thicker sequences of hydrocarbon source rocks and reservoir units are located in the region. In total, sixty samples of both mudstones and sandstones were acquired, processed and analyzed from four wells (Baccalieu I-78, Panther P-52, South Tempest G-88 and Lancaster G-70) to determine provenance. A combination of detrital zircon geochronology, whole rock geochemistry, and heavy mineral proxies were used to decipher provenance. In addition, core logging and thin section descriptions were completed to gain an understanding of the depositional environment. This analysis indicates a basinal setting with sediment being delivered by turbidity currents. The Upper Kimmeridgian Source Rock, Lower Kimmeridgian Source Rock and the Rankin Formation are interpreted to be composed of detritus from the Avalon Zone, Central Mobile Belt, and underlying basement. Detritus would have been derived from the northeast, and thicker sequences of these units would be expected in the northeastern portions of the Flemish Pass Basin and Central Ridge. The Upper Tempest and Lower Tempest Sandstone are also characterized by material from the Avalon Zone. However, some of the detritus from these units is also interpreted to be derived from Iberia to the east. In addition, the Upper

Tempest Sandstone contains Mesozoic zircons, which helped constrain the depositional age of this unit. Mesozoic zircons were not found in samples from the other units. The Tempest Sandstone units are interpreted to be derived from the east, which means thicker sequences of this unit would be expected towards the eastern edges of the Central Ridge and Flemish Pass Basin. Knowledge of where the thickest packages of these units exist may be an important consideration for petroleum exploration in the region.

In addition to these provenance findings, another important conclusion is that although provenance analysis methods such as detrital zircon geochronology are more common in sandstones, it is evident that using these techniques to analyze fine-grained sedimentary rocks is indeed feasible and useful. Additionally, the detrital zircon distributions in interbedded sandstone and mudstone beds were compared. These distributions suggested provenance of these pairs is very similar, an important implication for future use of this method in mudstones.

#### Acknowledgements

First of all, I would like to thank my two thesis supervisors, Dr. Paul Sylvester and Dr. Derek Wilton. Working on this project was a great opportunity for me and I benefited greatly from your expertise. I appreciate having your guidance when necessary but also the freedom to work independently. I would also like to thank Dr. Richard Hiscott for his insightful and thorough input.

Financial support for this project was provided by the Research and Development Corporation of Newfoundland and Labrador in the form of an Ocean Industries Student Research Award and is gratefully acknowledged. The MITACS Accelerate program also contributed to this project financially and is certainly appreciated.

There are many others who have helped and contributed to the completion of this project in some way. Although I can't name them all, those working at the CREAIT Network at Memorial University such as Dylan Goudie, David Grant, Sarah Jantzi and Pam King were extremely helpful to me with guidance and timely analyses for the various methods undertaken. My officemates Michelle English, Marie-Eve Lajoie and Nico Kastek were a great sounding board and were always there for support if needed. Additional support from geoscientists at Suncor Energy in St. John's including Michael Livingstone, Jody Hodder, and Eric Albrechtsons was certainly appreciated. I would also like to thank the C-NLOPB, particularly David Mills and Jason Newell, for access to the core and sample materials. Kate Souders and Angela Norman helped significantly by teaching me sample preparation methods as well as helping with analytical techniques. I am very grateful for all your help. Finally, I would like to express my gratitude to my family. To my parents and brother, I thank you for the constant support, guidance, and belief in my abilities. To my fiancé, Emily-Ann, I thank you for the support, patience and understanding you have shown me. I am exceptionally grateful to you all.

# Table of Contents

Chapter 1 – Introduction and Geological Setting	1
1.1 - Introduction and Purpose	1
1.2 - Regional Mesozoic Geological and Tectonic Setting	3
1.3 - Flemish Pass Basin Geological Overview	10
1.4 - Central Ridge Geological Overview	17
1.5 – Grand Banks Kimmeridgian Source Rock	19
1.6 - Pre-Mesozoic Basement Geology	24
1.6.1 - Introduction	24
1.6.2 - Avalon Zone	25
1.6.3 - Meguma Zone	29
1.6.4 - Central Mobile Belt	
1.6.5 - Carboniferous Sedimentary Basins	
1.6.6 - Mesozoic Igneous Rocks	
1.6.7 - Irish Conjugate Margin	
1.6.8 - Iberian Conjugate Margin	
Chapter 2 – Methods, Wells Studied & Sampled Intervals	
2.1 - Introduction	
2.2 – Sample Collection	
2.3 – Analytical Methods	
2.3.1 - Introduction	
2.3.2 - Optical Petrography of Thin Sections	
2.3.3 – Sample Preparation for Detrital Zircon Geochronology	
2.3.4 - MLA-SEM Imaging for Detrital Zircon Geochronology	40
2.3.5 - LAM-ICP-MS for Detrital Zircon Geochronology	42
2.3.6 - Sample Preparation and MLA/SEM for Evaluation of Heavy Mineral Ratios	45
2.3.7 - X-Ray Fluorescence for Whole Rock Lithogeochemistry	46
2.3.8 - ICP-MS for Whole Rock Lithogeochemistry	47
2.4 - Wells Studied	
2.4.1 - Baccalieu I-78	
2.4.2 - Lancaster G-70	52

2.4.3 - South Tempest G-88	54
2.4.4 - Panther P-52	55
Chapter 3 – Core Logging and Sedimentary Petrology	58
3.1 - Introduction	58
3.2 - Baccalieu I-78 – Kimmeridgian Rankin Formation	58
3.3 - Panther P-52 – Kimmeridgian Lower Tempest Sandstone	61
3.4 - South Tempest G-88 Lower Kimmeridgian Source Rock	63
3.5 - South Tempest G-88 Lower Tempest Sandstone	65
3.6 - South Tempest G-88 – Upper Kimmeridgian Source Rock	67
3.7 - Core Interpretation	70
3.8 - Thin Section Petrography (Introduction and Methodology)	72
3.9 – Mudstone Petrographic Interpretations	75
3.9.1 - Introduction	75
3.9.2 - Baccalieu I-78 – Rankin Formation	76
3.9.3 - South Tempest G-88 – Upper & Lower Kimmeridgian Source Rock	77
3.10 - Petrographic Interpretations of Siltstones and Sandstones	82
3.10.1 - South Tempest G-88 – Upper Kimmeridgian Source Rock	82
3.10.2 - Baccalieu I-78 – Rankin Formation	83
3.10.3 - Panther P-52 – Lower Tempest Sandstone	83
3.10.4 - South Tempest G-88 – Lower Kimmeridgian Source Rock	85
3.11 - Petrographic Interpretations and Implications for Provenance	
3.11.1 - Mudstones	
3.11.2 - Sandstones	91
3.11.3 - Summary	92
Chapter 4 – Whole Rock Geochemistry	93
4.1 - Introduction	93
4.2 - Major Elements	94
4.2.1 - Introduction	94
4.2.2 - CIA Results	95
4.3 - Trace Element Data	98
4.3.1 - Introduction	98
4.3.2 - Element Mobility	

4.3.3 – Introduction to Trace Element Provenance Plots	102
4.3.4 - Zr/Sc vs. Th/Sc Plot	
4.3.5 - Sc – Th – Zr Ternary Plot	104
4.3.6 – Th-La-Sc Ternary Plot	
Chapter 5 – Heavy Mineral Concentrate Data	
5.1 – Introduction	
5.2 – Heavy Mineral Analysis Methods	
5.3 - Results	114
5.3.1 - Upper Kimmeridgian Source Rock	114
5.3.2 - Lower Kimmeridgian Source Rock	
5.3.3 - Rankin Formation	
5.3.4 - Upper Tempest Sandstone (Panther P-52)	
5.3.5 - Lower Tempest Sandstone (Panther P-52)	
5.4 - Heavy Mineral Ratio Diagrams	126
5.4.1 - Observations	
Chapter 6 – Detrital Zircon Geochronology	130
6.1 – Introduction	
6.2 – Quantitative/Qualitative Approaches	131
6.3 – Data Presentation	133
6.4 – Baccalieu I-78: Upper Kimmeridgian Source Rock	134
6.4.1 – Results	134
6.4.2 – Interpretations	139
6.5 – South Tempest G-88: Upper Kimmeridgian Source Rock	139
6.5.1 – Results	139
6.5.2 – Interpretations	144
6.6 – Lancaster G-70 – Rankin Formation	146
6.6.1 – Results	146
6.6.2 – Interpretations	151
6.7 – Baccalieu I-78 – Rankin Formation (Mudstone Interval)	153
6.7.1 – Results	153
6.7.2 – Interpretations	156
6.8 – Baccalieu I-78 – Rankin Formation (Sandstone Interval)	157

6.8.1 – Results	157
6.8.2 – Interpretations	
6.9 – Panther P-52 – Upper Tempest Sandstone	162
6.9.1 – Results	162
6.9.2 – Interpretations	167
6.10 – South Tempest G-88 – Lower Tempest Sandstone	169
6.10.1 – Results	169
6.10.2 – Interpretations	174
Chapter 7 - Provenance Interpretations	
7.1 - Interpretations of Geochemical Plots – Weathering Diagrams	
7.2 – Interpretations of Trace Element Diagrams	
7.2.1 - Zr/Sc vs. Th/Sc Plots	
7.2.2 - Sc-Th-Zr Plot	179
7.2.3 – Th-La-Sc Ternary Plot	180
7.3 – Geochemical Provenance Interpretations	181
7.3.1 - Introduction	
7.3.2 - Rankin Formation, Upper Kimmeridgian Source Rock, Lower Kimmeridgian Source	Rock
7 2 3 Lower Tompest Sondstone	101
7.4 Provenance Interpretations of Heavy Mineral Date	102
7.4 1 Introduction	201
7.4.2 Upper Kimmeridgien Source Beak, Lower Kimmeridgien Source Beak, Bankin Form	105
7.4.2 – Opper Kininendgian Source Kock, Lower Kininendgian Source Kock, Kankin Form	
7.4.3 – Upper Tempest Sandstone and Lower Tempest Sandstone	
7.4.4 - Summary	185
7.5 - Provenance Interpretations of Geochronological Data – Upper Kimmeridgian Source Roc	k 186
7.5.1 - Introduction	
7.5.2 - Late Neoproterozoic Grains	
7.5.3 - > 1 Ga Grains	
7.5.4 - Cambrian – Devonian Grains	190
7.5.5 - Middle Neoproterozoic Grains	192
7.6 – Provenance Interpretations of Geochronological Data - Upper Tempest Sandstone	193

7.6.1 - Introduction	
7.6.2 – Constraints on depositional ages	
7.6.3 - Identified Grains	
7.6.4 - Carboniferous – Permian Grains	
7.6.5 - Jurassic Grains	
7.7 - Provenance Interpretations of Geochronological Data - Lower Tempest Sandstone	
7.7.1 - Overview	
7.8 – Provenance Interpretations of Geochronological Data - Rankin Formation	
7.8.1 - Overview	
7.8.2 – Lancaster G-70 Sample	
7.9 - Late Jurassic Provenance Model	
7.9.1 - Upper Kimmeridgian Source Rock	
7.9.2 - Rankin Formation and Lower Kimmeridgian Source Rock	
7.9.3 - Rankin Formation Exception – Lancaster G-70 Sample	
7.9.4 - Upper Tempest Sandstone	
7.9.5 - Lower Tempest Sandstone	
7.9.6 - Provenance of Interbedded Sandstone and Mudstone	
7.10 - Conclusions	
References Cited	

# List of Tables

Table 2.1 – List of samples and types of analyses performed	.51
Table 5.1 - Average grain sizes of monazite, zircon, rutile and chromite as computed by MLA.	
Monazite/zircon size (M/Z size), rutile/zircon size (R/Z size), and chromite/zircon size (C/Z size also	
listed	.112

# List of Figures

Figure 1.1: Regional location and geology of the Newfoundland Grand Banks. Line shows location of cross-section in later figures. BP=Bonavista Platform; CGFZ=Charlie-Gibbs Fracture Zone; CR=Central Ridge; CRFZ=Cumberland Ridge Fault Zone; FC=Flemish Cap; OK=Orphan Knoll; WOB=West Orphan Basin; EOB=East Orphan Basin; JDB=Jeanne d'Arc Basin; CB=Carson Basin; WB=Whale Basin; FPB=Flemish Pass Basin; AU=Avalon Uplift. Wells: P-52=Panther P-52; I-78=Baccalieu I-78; G-70=Lancaster G-70; G-88=South Tempest G-88; Mizzen L-11, Kyle L-11; O-85=Harpoon O-85; C-78=Bay du Nord C-78; B-55=Cumberland B-55; E-63=Linnet E-63. Modified from Lowe (2009) and Enachescu (1987)
Figure 1.2: Cross-section from west to east across the Jeanne d'Arc Basin, Central Ridge, Flemish Pass
Basin, Beothuk Knoll, Flemish Graben, and Flemish Cap.; from Enachescu (1988); modified by Lowe (2009)
Figure 1.3: General stratigraphy of the Jeanne d'Arc Basin (broadly applicable to the Flemish Pass Basin). Primary reservoir units are the Jeanne d'Arc, Hibernia, and Ben Nevis/Avalon formations; from Enachescu (2012); originally modified from Sinclair (1993). The primary regional source rock is the Egret Member of the Rankin Formation. It is noted in this chart as a thin shale unit near the top of the Rankin Formation
Figure 1.4. Generalized stratigraphy of the Flemish Pass Basin. Kimmeridgian source rocks fall within
the MS1-50 sequence: modified from Foster & Robinson (1993)
Figure 1.5: Seismic character map for the MS1-50 Sequence from Foster & Robinson (1993)
Figure 1.6 - Summary chart of major ages of potential source terranes. Ages of time periods from Cohen
et al. (2013)
Figure 1.7 - Pre-Mesozoic basement geology of the Grand Banks and surrounding regions; modified from Lowe et al. (2011). Basement geology compiled from Haworth & Lefort (1979), Barrs et al. (1979), Priem & den Tex (1984), King et al. (1986), Capdevila & Mougenot (1988), Bell & Howie (1990), and Johnson et al. (2001). Black lines represent boundaries between terranes as well as modern day coastline. Study area is the Grand Banks of Newfoundland, eastern Canada. NL – Newfoundland; NS – Nova Scotia; OB – Orphan Basin; JDB – Jeanne d'Arc Basin; FPB – Flemish Pass Basin; IB – Iberian
Peninsula
Figure 2.1 - Image of approximately 50 g cuttings sample from the Baccalieu I-78 well (5000 m)
Figure 2.2 - Combined gamma ray, stratigraphic, and biostratigraphic log for the Baccalieu I-78 well50 Figure 2.3 - Combined gamma ray, lithostratigraphic, and biostratigraphic log for the Lancaster G-70 well
Figure 2.4 - Combined gamma ray, lithostratigraphic, and biostratigraphic log for the South Tempest G-
88 well
Figure 2.5 - Combined gamma ray, lithostratigraphic, and biostratigraphic log for the Panther P-52 well.
Figure 3.1: Core Log for the Kimmeridgian Rankin Formation from the Baccalieu I-78 well
Figure 3.2: Core log for the Lower Tempest Sandstone from the Panther P-52 well
Figure 3.3: Core log for the Lower Kimmeridgian Source Rock from the South Tempest G-88 well
Figure 3.4: Core log for the Lower Tempest Sandstone from the South Tempest G-88 well
Figure 3.5: Core log for the Upper Kimmeridgian Source Rock from the South Tempest G-88 well 68

Figure 3.6: Photographs of various Kimmeridgian cores. Canadian one-dollar coin for scale (diameter = 2.5 cm) (A) Scour marks in the Baccalieu I-78 Rankin Formation core. (B) Granules and small pebbles in a sandstone matrix in Baccalieu I-78 Rankin Formation core. (C) Dark grey laminated mudstone in the South Tempest G-88 Lower Kimmeridgian Source Rock core. (D) Clastic dike in the South Tempest G-88 Lower Tempest Sandstone. (E) Soft sediment deformation in the South Tempest G-88 Upper Kimmeridgian Source Rock. (F) Carbonaceous debris in the Upper Kimmeridgian Source Rock of the Figure 3.7: Sandstone classification diagram from Pettijohn (1975). Classification is based on modal abundances of quartz grains (Q), feldspar grains (F), and lithic grains (L), as well as the amount of detrital Figure 3.8: Mudstone Classification diagram from Macquaker & Adams (2003). (A) Silt-dominated mudstone; (B) Silt-rich mudstone; (C) Sand-bearing, silt-rich mudstone; (D) Sand and clay-bearing, siltrich mudstone; (E) Clay-bearing, silt-rich mudstone; (F) Clay-dominated mudstone; (G) Clay-rich mudstone; (H) Silt-bearing, clay-rich mudstone; (I) Sand-bearing, clay-rich mudstone; (J) Sand and siltbearing clay-rich mudstone; (K) Silt and clay-bearing mudstone; (L) Sand and clay-bearing mudstone; (M) Sand and silt-bearing mudstone; (N) Sand, silt and clay-bearing mudstone. (1) Baccalieu I-78 Rankin Formation sample; (2) South Tempest G-88 Upper Kimmeridgian Source Rock sample; (3) South Tempest G-88 Lower Kimmeridgian Source Rock sample......79 Figure 3.9: Photomicrographs of mudstone samples under crossed polars. (A) Baccalieu I-78 Rankin Figure 3.10: Modal Mineralogy (weight %) of three mudstone samples from MLA-SEM analysis. Figure 3.11: False-color images of mudstone samples. Identification of individual minerals here is difficult, but the images demonstrate how the MLA software fully classifies minerals in these fine-grained rocks. (A) Baccalieu I-78 (4142.2m). (B) South Tempest G-88 (3843.5m). (C) South Tempest G-88 Figure 3.12: Photomicrographs of sandstone samples. (A) Sandstone from the South Tempest G-88 Upper Kimmeridgian Source Rock under plane polarized light; (B) Sandstone from the Upper Kimmeridgian Source Rock from South Tempest G-88 under crossed polars; (C) Sandstone from the Rankin Formation of Baccalieu I-78 under crossed polars; (D) Sandstone from Panther P-52 in the Lower Tempest Figure 3.13: Modal mineralogy (weight %) of five sandstone samples from MLA-SEM analysis. Minerals Figure 3.14: False-colored images of sandstone samples. (A) South Tempest G-88 (3837.3m). (B) Baccalieu I-78 (4135.29m). (C) Panther P-52 (3754.95m). (D) Panther P-52 (3757.7m). (E) South Figure 4.4 - Mobility diagrams for trace elements of Upper Jurassic sandstones and mudstones. Samples are from the Upper Kimmeridgian Source Rock, Lower Kimmeridgian Source Rock, Rankin Formation, and Lower Tempest Sandstone stratigraphic units from wells Baccalieu I-78, Panther P-52, and South  Figure 4.5 – Mobility diagrams for trace elements Th and Zr for sandstones (A) and mudstones (B). Samples are from the Upper Kimmeridgian Source Rock, Lower Kimmeridgian Source Rock, Rankin Formation, and Lower Tempest Sandstone stratigraphic units from wells Baccalieu I-78, Panther P-52, Figure 4.6 - Trace element provenance diagrams for Upper Jurassic mudstone samples. Samples from this study include four samples from the Lower Kimmeridgian Source Rock unit; one sample from the Upper Kimmeridgian Source Rock unit; nine samples from the Rankin Formation; nine samples from the Lower Figure 4.7 - Trace element provenance diagrams for Upper Jurassic sandstones samples. Samples from this study include five samples from the Upper Kimmeridgian Source Rock unit; two samples from the Lower Tempest Sandstone unit; one sample from the Lower Kimmeridgian Source Rock unit......106 Figure 5.1 - Pie charts of detrital heavy mineral proportions of samples from the Upper Kimmeridgian Figure 5.2 - Authigenic apatite grains from samples of the Lancaster G-70 well. Arrows point to interpreted authigenic apatite grains. The image on the left shows an apatite grain with crude concentric layering. The image on the right shows an apatite grain with secondary porosity and nodular forms. .... 118 Figure 5.3 - Examples of rutile grains imaged in this study that possess characteristics suggesting a detrital origin. This is based on their overall homogeneity, lack of secondary pores, inclusions and crude Figure 5.4 - Pie charts of detrital heavy mineral proportions of sample of the Lower Kimmeridgian Source Rock from Lancaster G-70, Panther P-52, South Tempest G-88 and Baccalieu I-78......121 Figure 5.5 - Pie charts of detrital heavy mineral proportions of samples of the Rankin Formation from Figure 5.6 - Pie charts of detrital heavy mineral proportions of samples from the Upper Tempest Sandstone from Panther P-52 and South Tempest G-88......125 Figure 5.7 - Pie charts of detrital heavy mineral proportions of sample from the Lower Tempest Figure 5.8 - Plots of heavy mineral ratios. (A) MZi vs. RZi, (B) CZi vs. RZi, (C) MZi vs. CZi, (D) ZTR. Figure 5.9 - Plots of heavy mineral ratios with standard error bars (1 SE) for the average heavy mineral index value from each formation. (A) MZi vs. RZi, (B) CZi vs. RZi, (C) MZi vs. CZi, (D) ZTR. Samples with authigenic apatite removed from ZTR ratio diagram......129 Figure 6.1 - SEM images of zircons demonstrating potential sources of error in classifying zoning types. Grains shown are small and do not display zoning or display insufficient zoning to assess zoning type. 133 Figure 6.2 - Graphs for detrital zircons of the Baccalieu I-78 (4500 m) sample. (A) Concordia diagram with detrital zircon ages. (B) Detrital zircon age histogram. (C) Age vs. Th/U. (D) Zircon grain Figure 6.3 - SEM images of detrital zircon grains from each identified age group in the Baccallieu I-78 Figure 6.4 - Graphs for detrital zircons of the South Tempest G-88 (3837.3 m) sample. (A) Concordia diagram with detrital zircon ages. (B) Detrital zircon age histogram. (C) Age vs. Th/U. (D) Zircon grain 

Figure 6.5 - SEM images of detrital zircon grains from each identified age group in the South Tempest G-
88 (3837.3 m) sample. The 20 µm circle represents location grain was ablated
Figure 6.6 - Graphs for detrital zircons of the Lancaster G-70 (4405 m) sample. (A) Concordia diagram
with detrital zircon ages. (B) Detrital zircon age histogram. (C) Age vs. Th/U. (D) Zircon grain
morphology. (E) Age vs. Surface Area. (F) Age vs. Aspect Ratio
Figure 6.7 - SEM images of detrital zircon grains from each identified age group in the Lancaster G-70
(4405 m) sample. 20 µm circle represents location grain was ablated
Figure 6.8 - Graphs for detrital zircons of the Baccalieu I-78 (4142.2 m) sample. (A) Concordia diagram
with detrital zircon ages. (B) Detrital zircon age histogram. (C) Age vs. Th/U. (D) Zircon grain
morphology. (E) Age vs. Surface Area. (F) Age vs. Aspect Ratio
Figure 6.9 - SEM images of detrital zircon grains from each identified age group in the Baccalieu I-78
(4142.2 m) sample. 20 µm circle represents location grain was ablated
Figure 6.10 - Graphs for detrital zircons of the Baccalieu I-78 (4135.29 m) sample. (A) Concordia
diagram with detrital zircon ages. (B) Detrital zircon age histogram. (C) Age vs. Th/U. (D) Zircon grain
morphology. (E) Age vs. Surface Area. (F) Age vs. Aspect Ratio
Figure 6.11 - SEM images of detrital zircon grains from each identified age group in the Baccalieu I-78
(4135.29 m) sample. 20 µm circle represents location grain was ablated
Figure 6.12 - Graphs for detrital zircons of the Panther P-52 (3210 m) sample. (A) Concordia diagram
with detrital zircon ages. (B) Detrital zircon age histogram. (C) Age vs. Th/U. (D) Zircon grain
morphology. (E) Age vs. Surface Area. (F) Age vs. Aspect Ratio
Figure 6.13 - SEM images of detrital zircon grains from each identified age group in the Panther P-52
(3210 m) sample. 20 μm circle represents location grain was ablated
Figure 6.14 - Graphs for detrital zircons of the South Tempest G-88 (4195.8 m) sample. (A) Concordia
diagram with detrital zircon ages. (B) Detrital zircon age histogram. (C) Age vs. Th/U. (D) Zircon grain
morphology. (E) Age vs. Surface Area. (F) Age vs. Aspect Ratio
Figure 6.15 - SEM images of detrital zircon grains from each identified age group in the South Tempest
G-88 (4195.8 m) sample. 20 µm circle represents location grain was ablated
Figure 7.1 – Comparison of detrital zircon age peaks from this study, Lowe et al. (2011) and Pollock et al.
(2009). For this study, all grains were plotted (n=310). All grains from Lowe et al. (2011) (n=335) and
Pollock et al. (2009) (n=278) were also plotted. Data from Lowe et al. (2011) are from Mesozoic
sedimentary rocks offshore Newfoundland while samples from Pollock et al. (2009) are from
Neoproterozoic to Cambrian sedimentary rocks of the Avalon Zone onshore Newfoundland
Figure 7.2 - Interpreted large scale drainage routes during deposition of the Upper & Lower
Kimmeridgian Source Rock, and the Rankin Formation. Based on results from detrital zircon
geochronology, whole rock geochemistry and heavy mineral ratios. Black lines trace terrane boundaries
as well as modern day landmasses (NL- Newfoundland; NS- Nova Scotia; IB- Iberian Peninsula; JDB-
Jeanne d'Arc Basin; OB- Orphan Basin; FPB- Flemish Pass Basin). Arrows show interpreted drainage
routes. Figure modified from Lowe et al. (2011)
Figure 7.3 - Interpreted basin entry points and areas of abundant and restricted sediment supply during
deposition of the Upper & Lower Kimmeridgian Source Rock, and the Rankin Formation. Black lines
represent major taults. Figure modified from Cody et al. (2011)
Figure 7.4 - Spatial variation in the Kimmeridgian Source Rock on the Grand Banks. From Magoon et al.
(2005)

### List of Appendices

Appendix A – Geochemical Data	
XRF – Major Elements	
XRF – Trace Elements	
ICP-MS (Trace Elements)	
Appendix B – Heavy Mineral Data & Grain Size Distributions	
Appendix C – Detrital Zircon U-Pb Data	
Baccalieu I-78 (4500 m) Sample	
South Tempest G-88 (3837.3 m) Sample	
Lancaster G-70 (4405 m) Sample – Uncorrected Data	
Lancaster G-70 (4405 m) Sample – Andersen (2002) Corrected Data	
Baccalieu I-78 (4142.2 m) Sample	
Baccalieu I-78 (4135.29 m) Sample	
Panther P-52 (3210 m) Sample	
South Tempest G-88 (4195.8 m) Sample	
U/Pb data for Reference Standards	
91500 zircon	
02123 zircon	
OG-1 zircon	
Plesovice zircon	
Concordia Diagrams – All Data	
Baccalieu I-78 (4500 m) sample	

South Tempest G-88 (3837.3 m) sample	
Lancaster G-70 (4405 m) sample – uncorrected Concordia	
Lancaster G-70 (4405 m) sample – Andersen corrected	
Baccalieu I-78 (4142.2 m) sample	
Baccalieu I-78 (4135.29 m) sample	
Panther P-52 (3210 m) sample	
South Tempest G-88 (4195.8 m) sample	
Concordia Diagrams and Calculated Ages – Reference Standards	
91500 Zircon	
02123 Zircon	
OG-1 Zircon	
Plesovice Zircon	

### **Chapter 1 – Introduction and Geological Setting**

#### **<u>1.1 - Introduction and Purpose</u>**

The prolific Kimmeridgian source rocks of the Grand Banks of Newfoundland (Figure 1.1) have received considerable attention as they are the primary oil source rock for this significant petroleum district. The Egret Member, the Kimmeridgian source rock of the Jeanne d'Arc Basin has been studied in detail there, where there are three producing fields and a fourth is scheduled to commence production in 2017. Nearby basins such as the Flemish Pass Basin and Orphan Basin (Figure 1.1) contain similar geology and structures, and are thought to hold significant potential for hydrocarbon discoveries. These nearby basins, however, have been studied in a more limited fashion.

The Flemish Pass Basin, in particular, has had significant hydrocarbon discoveries at the Mizzen area in 2009, and the Harpoon and Bay du Nord areas in 2013, spurring industry exploration (Enachescu, 2014). The region has been the focus for academic research as well (Lowe et al., 2011). The Flemish Pass Basin is separated from the Jeanne d'Arc Basin by a topographic high called the Central Ridge (Figure 1.1), where hydrocarbon discoveries have also been made. Tithonian-aged sandstone, consisting of four siliciclastic intervals interbedded with shale, is the primary oil reservoir at Mizzen (Cody et al., 2012). The primary source for the oil is considered to be a Kimmeridgian organic-rich shale, likely equivalent to the Egret Member in the Jeanne d'Arc Basin (Fowler et al., 2007). The Egret Member (Figure 1.3) consists of brown to grey shale of marine origin, with interbedded marlstone/limestone, and fine-grained sandstone and siltstone (Bateman, 1995).

Previous work on the Upper and Lower Kimmeridgian Source Rocks in the Flemish Pass has focused on the organic geochemistry and hydrocarbon source potential of the units (McCracken et al., 2000; Creaney & Allison, 1987). This study will present new mineral data that contribute to the understanding of this important interval within the basin. As very little information is available on this unit in the area of interest, detailed core and thin section descriptions have been completed to help define the mineralogy and interpret the depositional environment of the source rocks.

The goal of this study is to determine the provenance and paleodrainage patterns that supplied detritus to the Kimmeridgian source rocks as well as interbedded Tempest Sandstones within the Flemish Pass Basin and Central Ridge. Lowe et al. (2011) determined provenance patterns within the coarse-grained reservoir intervals within the basin using detrital zircon geochronology as well as geochemistry of detrital tourmaline. For this project, detrital zircon geochronology, major and trace element geochemistry, and heavy mineral analyses will be applied to help predict where the thickest accumulations of fine-grained, organic-rich source rocks are located. All of the information gathered will enable a more accurate prediction of prospective areas for hydrocarbon exploration.



Figure 1.1: Regional location and geology of the Newfoundland Grand Banks. Line shows location of cross-section in later figures. BP=Bonavista Platform; CGFZ=Charlie-Gibbs Fracture Zone; CR=Central Ridge; CRFZ=Cumberland Ridge Fault Zone; FC=Flemish Cap; OK=Orphan Knoll; WOB=West Orphan Basin; EOB=East Orphan Basin; JDB=Jeanne d'Arc Basin; CB=Carson Basin; WB=Whale Basin; FPB=Flemish Pass Basin; AU=Avalon Uplift. Wells: P-52=Panther P-52; I-78=Baccalieu I-78; G-70=Lancaster G-70; G-88=South Tempest G-88; Mizzen L-11, Kyle L-11; O-85=Harpoon O-85; C-78=Bay du Nord C-78; B-55=Cumberland B-55; E-63=Linnet E-63. Modified from Lowe (2009) and Enachescu (1987).

## **1.2 - Regional Mesozoic Geological and Tectonic Setting**

Mesozoic rocks of offshore Newfoundland are restricted to a series of interconnected northeast-trending rift basins. These basins are typically half-graben structures separated by Precambrian and Paleozoic basement highs and include the Jeanne d'Arc, Flemish Pass, East Orphan, and West Orphan basins (Figure 1.1). A cross section across the Jeanne d'Arc Basin, Central Ridge, and Flemish Pass Basin (Figure 1.2) highlights the deep crustal relationship between the two basins. These Mesozoic basins were formed by rifting associated with the break-up of Pangea, spanning from the Permo-Triassic to the mid-Cretaceous (Enachescu, 1987 & 1988; Tankard & Welsink, 1987). Rifting progressed from south to north during the Late Triassic to the Early Cretaceous, which provided the conditions necessary for basin formation on the continental margin of Newfoundland. From the mid-Cretaceous to the present day, the evolution of the basins has been controlled by North Atlantic seafloor spreading and passive margin sedimentation (Enachescu, 1987 & 1988; Tankard & Welsink, 1987). Of these basins, the Jeanne d'Arc Basin is the most prolific hydrocarbon province, with three producing fields and a fourth scheduled to begin production in 2017. The basin is adjacent to the main listric detachment, and it therefore possesses the thickest succession of sediment (22 km) and most complete syn-rift succession (14 km) (Keen et al., 1987; Enachescu, 1987; Tankard & Welsink, 1987; Tankard et al. 1989; Driscoll & Hogg, 1995). Although this thesis will focus on the Flemish Pass Basin and Central Ridge, the adjacent Jeanne d'Arc Basin has widespread well control, and has been studied by other workers in great detail. This makes it an excellent analogue for studies of Mesozoic basins elsewhere in offshore Newfoundland, and it is therefore reviewed in detail.

Three rifting stages, interpreted to have affected sedimentation in many of the North Atlantic Basins (Enachescu, 1987; Sinclair, 1988), are clearly important in both the Flemish Pass and Jeanne d'Arc basins. The three rifting phases, according to Sinclair (1988), include: 1) Triassic to Early Jurassic rifting during a period of NW-SE oriented extension, resulting in the break-up of Africa and North America; 2) Tithonian to early Valanginian rifting, during a period of E-W oriented extension, resulting in the break-up of Iberia and the Grand Banks; 3) Aptian-Albian rifting, during a period of NE-SW oriented extension, resulting in the break-up of Europe and North America. From the Late Cretaceous onwards, thermal subsidence was the dominant mechanism affecting the newly created continental margins. At this point, the Atlantic margin became a passive margin and hence associated passive margin sediments were deposited which continues to the present day.



Figure 1.2: Cross-section from west to east across the Jeanne d'Arc Basin, Central Ridge, Flemish Pass Basin, Beothuk Knoll, Flemish Graben, and Flemish Cap.; from Enachescu (1988); modified by Lowe (2009).

A generalized stratigraphy of the Jeanne d'Arc Basin is presented in Figure 1.3. This stratigraphic chart is also considered applicable to the Flemish Pass Basin, as both possess a common stratigraphy and evolutionary history (Enachescu, 2012). All ages presented in this section follow the absolute timescale of Cohen et al. (2013). Precambrian metamorphic and Paleozoic metasedimentary and igneous rocks comprise the pre-Mesozoic basement (Enachescu, 1987). These rocks are considered to be an offshore extension of the Avalon terrane of the Appalachian Orogenic Belt (Williams & Hatcher, 1983; Haworth & Lefort, 1979; King et al., 1985; 1986). Upper Triassic sediments unconformably overlie the pre-rift basement and are associated with NW-SE oriented extension and the first rifting stage that affected the Grand Banks. These sediments comprise continental red beds of the Eurydice Formation and evaporites of the Argo Formation, the latter a result of recurrent influxes of salt water from the Tethys Sea

(Tucholke et al., 1989; McAlpine, 1990). This syn-rift fill was followed by regional thermal subsidence, and marine transgression, depositing thick accumulations of shale and limestone. The marine transgression is well represented by the Iroqouis Formation, where anhydritic dolomite is overlain by limestone (Sinclair, 1988). Overlying the limestone, the Downing Formation is a continuous shale sequence deposited in low energy conditions from the Pliensbachian (190.8 to 182.7 Ma) to the Bathonian (168.3 to 166.1 Ma) (Sinclair, 1988). From the Bathonian to Callovian (166.1 to 163.5 Ma), Voyager Formation was deposited over the Downing Formation (Sinclair, 1988). The Voyager Formation consists of an interbedded succession of shale, sandstone and limestone (Sinclair, 1988). The Rankin Formation, which is Oxfordian (163.5 to 157.3 Ma) to Kimmeridgian (157.3 to 152.1 Ma) in age, was deposited near the end of the thermal subsidence phase. Organic-rich shales were deposited in the Kimmeridgian, which represent the regional oil and gas source rock, and are the focus of this thesis.

A second rifting phase occurred during the Tithonian (152.1 to 145.0 Ma) to Valanginian (139.8 to 132.9 Ma) which reactivated movement along major faults. The onset of this rifting caused broad regional warping, uplift of the Avalon Uplift to the South, and the appearance of the Central Ridge structure (Sinclair, 1988). The appearance of the Central Ridge, in particular, marks the first point in time when the Jeanne d'Arc Basin and the northern Flemish Pass Basin could be considered two separate basins (Sinclair, 1988). During the Tithonian, the primary reservoir target in the Terra Nova Field, the Jeanne d'Arc Formation, was deposited. The Jeanne d'Arc Formation is interpreted as being derived from north-south oriented fluvial systems which eroded limestone, metaquartzite, chert cobbles and silica sand from the underlying Rankin Formation and deposited them near the Jeanne d'Arc Basin's ancient shoreline (Sinclair, 1998).

The Terra Nova Formation is composed of sandstones, conglomerates, and shales (Sinclair, 1988). The boundary between the Rankin Formation and Jeanne d'Arc Formation represents an unconformity, with a significant time gap (Sinclair, 1988). At the end of the Tithonian, transgression resulted in marine silts and muds of the Fortune Bay Formation covering the Jeanne d'Arc Formation fluvial sands. During the Berriasian (145.0 to 139.8 Ma), the continuation of the second rifting phase caused continued uplift of sediment source regions, resulting in northward progradation of fluvio-deltaic sands of the Hibernia Formation into the Jeanne d'Arc Basin (Sinclair, 1988; Brown et al., 1989). The Hibernia Formation is the primary reservoir target for the Hibernia Field with the main reservoirs being medium- to very coarsegrained channel deposits and very-fine to medium-grained delta front sandstones. (Brown et al., 1989). Above the Hibernia Formation, the "B" marker Member oolitic, bioclastic limestone of the Whiterose Formation was deposited in the late Valanginian during the thermal sag phase of the second rifting episode and indicates a period of basin stability (Dearin, 2006; Sinclair, 1988). Overlying the "B" marker Member, the Catalina Member, composed of thinly interbedded shales and calcareous sandstones, was deposited (Sinclair, 1988). The thick, Hauterivian (132.9 to 129.4 Ma) shale sequence of the Whiterose Formation was deposited above the Catalina Member (Sinclair, 1988). In the Barremian (129.4 to 125.0 Ma), the "A" marker limestone, similar in composition to the "B" marker (Dearin, 2006), was deposited, as seen at both the Hibernia and White Rose fields.

In the Barremian, a coarsening upward succession of shales and sandstones known as the Avalon Formation prograded over the "A" marker limestone (Sinclair, 1988). This northward progradation is likely a result of rejuvenated uplift in the south (Avalon Uplift), which resulted in

7

the development of the Aptian-Albian (~ 113.0 Ma) unconformity (Sinclair, 1988). The deposition of the Avalon Formation represents a period of basin-wide regression (Sinclair, 1988).

Deposition of the Ben Nevis Formation was significantly affected by the third and final rifting episode to affect the Grand Banks Basins, which occurred during Aptian-Albian time (Sinclair, 1993). As with the older Hibernia and Jeanne d'Arc Formations, coarse sediments of the Ben Nevis Formation were deposited in fluvial systems draining from north-south (Sinclair, 1988). These coarse sediments possess a transgressive character, hence a fining upward sequence which is recognizable throughout the Jeanne d'Arc Basin (Sinclair, 1988). They are composed of predominantly back-barrier to shoreface sediments (Sinclair, 1993). Stratigraphic stacking patterns were significantly affected by faulting during deposition of the Ben Nevis Formation (Dearin, 2006). Additionally, faulting during this time created structures such as tilted fault blocks where the majority of hydrocarbons are found in the basin (Sinclair, 1988). In addition to fault activity, salt diapirism was also important during Aptian-Albian time, resulting in localized salt ridges and pillars (Enachescu et al., 2000). As the Ben Nevis Formation is a regressive succession, eventually the laterally equivalent Nautilus Formation, composed of offshore shales, transgressed over the Ben Nevis Formation (Sinclair, 1988).

In the Cenomanian (100.5 to 93.9 Ma), the lower Dawson Canyon Formation and Petrel Member lime mudstones were deposited during a period of subsidence and low clastic input (Dearin, 2006). The deposition of these units represents the initiation of the final thermal sag within the basin (Dearin, 2006). Coarse-grained sandstones of the Otter Bay and Fox Harbour members were deposited during the late Cretaceous (Sinclair, 1988). These sandstones mark an important change in sediment provenance within the basin as they are interpreted as being derived from easterly prograding deltaic systems with a westerly source (Sinclair, 1988).

8

However, previous reservoir units (Jeanne d'Arc, Hibernia, Ben Nevis Formations) are interpreted as being derived from the south (Sinclair, 1988). The rapid progradation of these sandstones corresponds with the rift moving into the drift phase of the Falvey (1974) rift model where exponentially slowing thermal subsidence and expanding of the continental shelf and slope take place (Sinclair, 1988).

The Base Tertiary unconformity marks the top of the Upper Cretaceous succession, and is marked in the western Jeanne d'Arc Basin by a thin, highly radioactive bed, equivalent to the iridium-rich bed, which occurs worldwide at the Cretaceous-Tertiary boundary (Alvarez et al. 1980; Sinclair, 1988). This unconformity represents a large regional drop in relative sea level, perhaps caused by a regional rebound of the Atlantic margin (Enachescu & Hogg, 2005). Throughout the Tertiary, a marine succession with little deformation was deposited as low sediment input and long term subsidence dominated (McAlpine, 1990). This is indicative of a passive margin setting bordering the spreading Atlantic Ocean (Deptuck et al., 2003).



Figure 1.3: General stratigraphy of the Jeanne d'Arc Basin (broadly applicable to the Flemish Pass Basin). Primary reservoir units are the Jeanne d'Arc, Hibernia, and Ben Nevis/Avalon formations; from Enachescu (2012); originally modified from Sinclair (1993). The primary regional source rock is the Egret Member of the Rankin Formation. It is noted in this chart as a thin shale unit near the top of the Rankin Formation.

## **1.3 - Flemish Pass Basin Geological Overview**

The Flemish Pass Basin is located on the continental shelf of the Grand Banks

approximately 400 km east of St. John's, Newfoundland. It covers an area of approximately

30,000 km<sup>2</sup> with water depths between 400 and 1100 m (Foster & Robinson, 1993; DeSilva,

2000). The basin is separated from the Jeanne d'Arc Basin to the southwest by the Central Ridge, bounded to the east by Beothuk Knoll and Flemish Cap basement high, to the north by the Cumberland High, and to the South by the Avalon Uplift (Enachescu, 1987; Foster & Robinson, 1993; DeSilva, 2000) (Figure 1.1).

The Flemish Pass Basin shares a similar stratigraphy and common evolutionary history with the Jeanne d'Arc Basin (Enachescu, 2012). The geological history and a seismic-stratigraphic interpretation of the Flemish Pass Basin were reviewed by Foster & Robinson (1993), the latter based on seismic profiles and data from seven wells that had been drilled in the basin at that time. The basin was divided into megasequences, which are defined by Hubbard (1988) as genetically-related sets of sequences bounded by regional unconformities. Kimmeridgian source rocks fall within the MS1 megasequence (Figure 1.4). Because of the burial depth of the MS1 megasequence and the lack of well control, the authors struggled to map and interpret this megasequence across the whole basin. However, it was subdivided into smaller sequences and the MS1-50 sequence, which contains Kimmeridgian source rocks, was mapped and interpreted across the whole basin.



Figure 1.4: Generalized stratigraphy of the Flemish Pass Basin. Kimmeridgian source rocks fall within the MS1-50 sequence; modified from Foster & Robinson (1993).

Sediments of the MS1-50 sequence are found in two separate subbasins oriented in an approximately east-west orientation and divided by an intervening high found northeast of the Gabriel C-60 well (Figure 1.5) (Foster & Robinson, 1993). The majority of the northern subbasin lies to the west of the Baccalieu I-78 well (Foster & Robinson, 1993). Sediments in this northern subbasin onlap the subbasin margins to the south and east while in the southern subbasin, sediments onlap the previously mentioned intervening high (Figure 1.5) (Foster & Robinson, 1993). Foster & Robinson, 1993). Foster & Robinson (1993) concluded that the MS1-50 unit thins to the south. They postulated that there is likely a facies change to limestone overlain by thick sandstone as seen in the Kyle L-11 well. The source rock facies are thought to be restricted to the central parts of the subbasins (Foster & Robinson, 1993). Foster & Robinson (1993) indicated that the source-rock facies itself is marine mudstone restricted to the lower part of the MS1-50 sequence. These mudstones grade upwards into marine or shoreline sandstones. These authors also suggested that the source rock facies is likely widespread in both subbasins as the seismic character of the unit is extremely uniform.



Figure 1.5: Seismic character map for the MS1-50 Sequence from Foster & Robinson (1993).

The overlying MS2 megasequence comprises sediments from the lower Berriasian to Aptian (Foster & Robinson, 1993). MS2 sediments were deposited in northeast-southwest trending subbasins: the southern Gabriel subbasin, and the Baccalieu subbasin to the North, between an intervening high (Foster & Robinson, 1993). The base of MS2 represents a major unconformity, and the onset of major faulting in the early Berriasian (Foster & Robinson, 1993). Deposition of deep water mudstones began at the base of MS2, as this boundary also corresponds to significant regional subsidence (Foster & Robinson, 1993). The top of MS2 is likely Aptian, although it is difficult to determine as most of the wells are drilled in areas where much of the MS2 sequence is absent due to erosion during MS3 deposition (Foster & Robinson, 1993). The major Aptian unconformity found in the Jeanne d'Arc Basin is also present in the Flemish Pass Basin (Jansa & Wade, 1975; Tankard & Balkwill, 1989).

Sediments of the MS3 megasequence are Aptian to Albian in age and were deposited in basins oriented northwest–southeast (Foster & Robinson, 1993). However, deposition during the MS2 megasequence was in basins oriented northeast–southwest, indicating a significant change in basin orientation at MS3 time (Foster & Robinson, 1993). Some areas that were depocenters during MS2 deposition formed highs during the Aptian-Albian, and vice-versa (Foster & Robinson, 1993). Renewed extension in the Aptian likely contributed to rejuvenated dextral strike-slip motion along major northeast-southwest-trending faults (Sinclair, 1988). This movement resulted in the rearrangement of subbasins within the Flemish Pass Basin with the base of MS3 as a major unconformity (Foster & Robinson, 1993). Due to the lack of well control, depositional environment interpretations are limited to seismic facies analysis, which indicate the presence of muddy sediments containing sand-grade turbidites deposited in a deep marine environment (Foster & Robinson, 1993). The top of the MS3 megasequence is synchronous with the end of active tectonism and faulting within the basin and represents an important unconformity (Foster & Robinson, 1993).

The final megasequence as described by Foster & Robinson (1993) was deposited from the Albian to the present day. The base of this sequence coincides with the conclusion of active faulting and units deposited in this megasequence are equivalent to those deposited in the Jeanne

15

d'Arc Basin at the same time such as the Petrel limestone (Foster & Robinson, 1993). The base of this sequence onlaps MS3 and older highs and fills in adjacent lows, while the upper portion of the sequence is primarily a regressive Cenozoic shelf system with sediment being derived from the northwest (Foster & Robinson, 1993). Deposition of this shelf system continues to the present day (Foster & Robinson, 1993).

The oil and gas potential of the Flemish Pass Basin has been of great interest, particularly in recent years, as several large discoveries have been made and the existence of mature Upper Jurassic source rocks (the focus of this thesis), as well as the presence of potential reservoir units of Late Jurassic and Early Cretaceous age, has been confirmed. Additionally, industry 3-D seismic mapping has identified numerous significant structural traps, particularly some large faulted extensional anticlines (DeSilva, 2000; Enachescu & Hogg, 2005). In 2004, the Canada-Newfoundland and Labrador Offshore Petroleum Board and the Geological Survey of Canada estimated that the Flemish Pass Basin contains 1.7 billion barrels of undiscovered petroleum resources (50% probability), with a range of field sizes from 528 to 44 million barrels (Enachescu, 2014).

The Kimmeridgian source rocks are the primary focus of this thesis and will be discussed in detail in the next section, but a brief overview of the source rock potential will be presented here. Mature Kimmeridgian source rocks were intersected in the Baccalieu I-78 well in the northern Flemish Pass. RockEval analysis of samples from this well from McCracken (2000) defined total organic carbon (TOC) values from 0.92 - 4.83% (average 2.1%), and hydrogen indeces (HI) ranging from 109 - 510 mg HC/g TOC (average 355 mg HC/g TOC), indicating type II, marine source rocks. Analyses of oil samples from sandstone reservoir intervals in Mizzen L-11 (Fowler, 2007) and Gabriel C-60 (Creaney & Alsion, 1987) indicated the source rock possessed characteristics similar to the Egret Member of the Jeanne d'Arc Basin, with a likely more terrestrial component to the organic matter. Excellent reservoir quality sandstones were intersected in the Mizzen L-11 well into Upper Jurassic sandstones as well as 5 m of noncommercial oil pay in Cretaceous sandstone (Enachescu, 2006). In 2009, StatoilHydro drilled the Mizzen O-16 well, and discovered 26 m of oil pay. They successfully tested the discovery and were able to secure a Significant Discovery License from the Canada-Newfoundland and Labrador Offshore Petroleum Board (Cody et al., 2012). Oil was found in the uppermost sand of the Tithonian, in a unit laterally equivalent to the Jeanne d'Arc sandstone of the Jeanne d'Arc Basin (Cody et al., 2012). This discovery in the North Flemish Pass Basin has demonstrated the existence of a proven petroleum system, and Statoil has continued their evaluation of this system with a series of regional projects (Cody et al., 2012). In addition to the O-16 well, Statoil made significant discoveries in both the Harpoon O-85 and Bay du Nord C-78 wells in 2013. In these wells, light, sweet oil was discovered in Tithonian fluvial sandstones (McDonough, 2014). The Bay du Nord prospect is estimated to contain over 300 million barrels of recoverable oil (McDonough, 2014). The data from these wells, however, remains classified at this time.

#### **<u>1.4 - Central Ridge Geological Overview</u>**

In addition to wells in the Flemish Pass Basin, samples for this thesis were also collected from two wells, Panther P-52, and South Tempest G-88, located in the adjacent Central Ridge (Figure 1.1 & Figure 1.2). The Central Ridge is a faulted intrabasinal high that separates the Jeanne d'Arc and Flemish Pass basins. The geological evolution of the Central Ridge is similar to that of the Flemish Pass Basin. Some of the wells drilled in the Central Ridge are mentioned by Foster & Robinson (1993) and included in their interpretation of the Flemish Pass Basin. Enachescu (1987, 1988) stated that the Central Ridge was a relatively high area during the initial Late Triassic rifting episode. It was likely in a relatively elevated position until the late Jurassic

17

(Enachescu, 1988). Sinclair (1988) demonstrated that the major appearance and uplift of the Central Ridge structure was predominantly Tithonian, and that this marks the initial isolation of the Jeanne d'Arc Basin from the northern Flemish Pass Basin. By the Early Cretaceous, the ridge reached its maximum elevation, and was exposed as an island chain or peninsula (Enachescu, 1988). Since the island chain or peninsula was subaerially exposed, some of the Upper Jurassic and Lower Cretaceous sediments were eroded and are missing (Enachescu, 1988). However, approximately 5 km of Upper Triassic to Upper Jurassic sediments remain a part of the succession at the Central Ridge (Enachescu, 1988).

There have been both oil and gas discoveries in the Central Ridge despite sparse drilling. Oil has been found in the South Tempest G-88 well, and gas at both North Dana I-43 and Trave E-87. High quality Kimmeridgian source rocks have been intersected in North Dana I-43, South Tempest G-88, and Panther P-52 and the ridge possesses a variety of structural trapping configurations (Enachescu, 2014; DeSilva, 1994). These include tilted fault blocks, and inversion structures, in addition to a number of stratigraphic trapping possibilities (DeSilva, 1994). Kimmeridgian Upper and Lower Tempest sandstone units are interbedded with shales and siltstones of the Upper and Lower Kimmeridgian Source Rock units. The Tempest sandstones are described as fine- to medium-grained sandstones interbedded with shales. They are interpreted as turbidite deposits (Sinclair 1988; McAlpine, 1990; DeSilva, 1994) and flowed oil and gas at rates up to 1250 bbl per day and 4.9 mmcf per day, respectively, in the South Tempest G-88 well (Canada-Newfoundland and Labrador Offshore Petroleum Board (CNLOPB), 1990). The North Dana I-43 well flowed 12 mmcf and 292 bbl per day of gas and condensate, respectively, from the equivalent Tempest sandstones (CNLOPB, 1990). The Tempest sandstones are interpreted as having been deposited from turbidity currents flowing to the north

as structurally high areas exist to the South (DeSilva, 1994). In addition to addressing the provenance of Kimmeridgian source rocks, this thesis will also investigate the provenance of interbedded Tempest sandstones, and determine whether heavy mineral data support the interpretation of a southerly provenance.

#### **1.5 – Grand Banks Kimmeridgian Source Rock**

This study is focused predominantly on Kimmeridgian source rocks of the Flemish Pass Basin and Central Ridge and numerous studies have investigated their source rock potential. These Kimmeridgian source rocks are divided into specific members of the Rankin Formation. The members are called the Upper Kimmeridgian Source Rock and Lower Kimmeridgian Source Rock although McCracken (2000) showed that the Rankin Formation itself also possesses great source rock potential. In the Jeanne d'Arc Basin, these studies have been focused on the Egret Member, the laterally equivalent Kimmeridgian source rock. Although not directly related to provenance, previous studies on the source rock geochemistry provide important information about the depositional environment of these units as well as the amount of clastic input in the area at this time. These factors are important to this study. Creaney & Allison (1987) studied the Egret Member in the Jeanne d'Arc Basin and Central Ridge and attempted to correlate the unit with rocks of the Flemish Pass Basin. Their aim was to quantitatively characterize the organic geochemistry of the source interval using oil chromatograms, high H indices, and H/C ratios. Their results indicated that oil from the Egret Member was derived from type II, marine, algaldominated organic matter. Creaney & Allison (1987) concluded that the source rock appears to be present in the centre of the basin as a thick, organic-rich mudstone where sedimentation was not affected by eustatic changes. However, at the basin margins, the Egret Member is thinner, and interbedded with reservoir sands and carbonates. They postulated that as sea level varied,

the oxic/anoxic boundary in the water column probably fluctuated accordingly. This led to interbedded source and non-source intervals in these areas.

Creaney & Alison (1987) examined one well (Gabriel C-60) in the Flemish Pass Basin. The well did not penetrate Kimmeridgian source rocks, but an oil sample was obtained from a reservoir interval at 3995 m depth. This Gabriel oil had a higher pristine/phytane ratio than the samples from the Jeanne d'Arc Basin indicating that the source rock in the Gabriel well was likely deposited in a somewhat more oxidizing environment (Creaney & Alison, 1987). Creaney & Alison (1987) suggested that the source rock at Gabriel was deposited in a more proximal environment in the Flemish Pass. This is consistent with Foster & Robinson's (1993) interpretations that the source rock at this location onlaps the basin margins to the east.

McCracken et al. (2000) were the first to analyze the organic geochemistry of samples from the Kimmeridgian source rocks in the Flemish Pass Basin. Samples for their study were collected from the Baccalieu I-78 well in the northern Baccalieu subbasin. McCracken et al. (2000) confirmed, from geochemical and geophysical evidence, the existence of Upper Jurassic organic-rich source rocks that extend northeastward from the Jeanne d'Arc Basin into the northern Flemish Pass.

RockEval analysis results demonstrate TOC values from 0.92 – 4.83% (average 2.1%), and HI ranging from 109 – 510 mg HC (hydrocarbons)/g TOC with an average of 355 mg HC/g TOC (McCracken et al., 2000). HI is an abbreviation for the Hydrogen Index; which is derived from the ratio of Hydrogen to TOC (McCarthy et al., 2011). It is often used as a maturation indicator for source rocks. McCracken et al. (2000) classified most of the samples as Type II, marine source rocks, similar to those in the Jeanne d'Arc Basin. Additionally, biomarker analyses
indicate that the samples are genetically similar to oils in the Jeanne d'Arc Basin (McCracken et al., 2000).

McCracken et al. (2000) noted a distinct gravity and magnetic anomaly near the Baccalieu well that continued into the Jeanne d'Arc Basin. McCracken et al. (2000) theorized that this anomaly corresponds to the regions in which the Upper Jurassic source-rock facies was deposited and remains preserved today.

Fowler et al. (2007) analyzed a small sample of oil from Upper Jurassic sandstone in the Mizzen L-11 well. For the most part, the sample possesses characteristics similar to oils from the Egret Member in the Jeanne d'Arc Basin (Fowler et al., 2007). Similarities include the saturate hydrocarbon and gasoline range characteristics, and terpane distributions (Fowler et al., 2007). However, pristane/phytane ratios of the Mizzen oil are elevated in comparison with those analyzed from Jeanne d'Arc Basin oils (Fowler et al., 2007). This indicates a potential terrestrial component to the organic matter (Fowler et al., 2007). This terrestrial component indicates potential changes in the depositional environment of the Upper Jurassic source rock in the Flemish Pass Basin (Fowler et al., 2007). Alternatively, it may reflect the mingling of hydrocarbons from multiple sources (Fowler et al., 2007); an interpretation supported by the presence of multiple source rock intervals in other nearby wells such as Panther P-52 (Enachescu, 2012).

Bateman (1995) completed a study on numerous wells intersecting the Egret Member in the Jeanne d'Arc Basin in which he analyzed the mineralogical and geochemical (organic and inorganic) compositions of the source rock unit. Several analytical techniques were used including X-ray diffraction, whole rock geochemistry, and Rock-Eval analysis. XRD analysis

revealed samples from the eastern side of the basin had elevated quartz contents whereas samples from the southern edge of the basin possessed high calcite contents (Bateman, 1995). The elevated quartz contents on the eastern side of the basin were attributed to the presence of a Late Jurassic delta complex which resulted in an influx of terrestrial-derived sediments in this area (Fowler & McAlpine, 1994; Bateman, 1995). The high calcite contents in the southern portion of the basin were attributed to being in close proximity to a nearby carbonate bank or shelf (McAlpine, 1990; Bateman, 1995). With respect to the clay mineralogy, Bateman (1995) suggested that the prevalence of illite and illite/smectite indicated that detritus in these source rock samples was likely delivered from source terranes composed of mica-rich granites and metamorphic rocks (Weaver, 1989). In addition, Bateman (1995) found that Egret Member shales possessed abundant quantities of kaolinite relative to other Mesozoic shales. Weaver (1960) stated that kaolinite is uncommon in marine offshore sediments. Bateman (1995) interpreted the increased abundances of kaolinite in Egret Member samples to indicate a detrital influx from weathered kaolinite-rich rocks. A similar interpretation was suggested by Hurst (1981) for North Sea Jurassic shales. Gradstein et al. (1990) reported that deposition of kaolinite-rich sediments in the Jurassic was common due to the humid, subtropical climate of that time. Bateman (1995) suggests that chlorite in the samples is derived from mica-rich granites and chlorite-bearing metamorphic rocks (Weaver, 1989).

Bateman's (1995) whole rock geochemistry of the Egret Member shales is consistent with the XRD data of varying quartz and calcite contents within the basin. In addition to these observations, a lower than expected  $P_2O_5$  concentration was noted in the Egret shales by Bateman (1995). This was attributed to samples containing minor amounts of apatite (Bateman, 1995). Apatite precipitation is uncommon under anoxic conditions (Ingall et al., 1993; Riediger

& Bloch, 1995). Bateman (1995) suggests that the low apatite content is indicative of anoxic bottom waters during Egret deposition. Bateman (1995) also evaluated the whole rock geochemistry of the Egret samples which allows for an evaluation of the C-Fe-S systematics of the depositional system. Results reveal elevated sulfur values, suggesting deposition in a euxinic environment (Leventhal, 1983).

Bateman (1995) compared Egret Member samples to PAAS (post Archean average shale from Taylor & McLennan (1985)) and BPS (Average British Paleozoic shale from Jones & Plant (1989)). Egret Member samples were found to contain less alkalis than the PAAS & BPS. Bateman (1995) attributed this to a lack of feldspars and chlorite in the Egret Member. Citing Norry et al. (1994), Bateman (1995) concluded that the Egret is likely a very mature sediment and that feldspar and chlorite have been lost through several sedimentary cycles.

Bateman (1995) described four main lithological facies within the Egret Member: 1) a dark brown laminated shale; 2) a grey to grey-brown shale; 3) a light brown marlstone/limestone; 4) a fine-grained sandstone and siltstone, and provided a depositional model to explain the origin of these units. According to the model, dark brown laminated shales were deposited during highstands via pelagic sedimentation of clays and marine organisms (Bateman, 1995). The grey to grey-brown unlaminated shales are interpreted to have been deposited in a shallower environment during periods of lower sea level (Bateman, 1995). The marlstones and claystones were likely deposited under oxic conditions during periods of low sea level (Bateman, 1995). Meanwhile, Bateman (1995) links sandstone deposition to turbidity currents that deposited sediments from more proximal environments into more distal, basinal environments.

# **<u>1.6 - Pre-Mesozoic Basement Geology</u>**

# **Introduction – 1.6.1**

Source areas supplying detritus to the Flemish Pass Basin and Central Ridge during the Kimmeridgian include pre-Mesozoic basement rocks from possibly both sides of the North Atlantic, including the North American Conjugate Margin as well as the Irish and Iberian conjugate margins. The geology of each potential source region will be reviewed here. To accompany the description of each individual region, isotopic age constraints are provided for the major rock units. This provides the foundation for correlations to detrital zircon U-Pb geochronology presented in this study in later chapters that will address the provenance of Kimmeridgian rocks using U-Pb detrital zircon geochronology. In addition, a summary chart is presented in Figure 1.6 with the major ages of each potential source terrane.



Figure 1.6 - Summary chart of major ages of potential source terranes. Ages of time periods from Cohen et al. (2013).

#### 1.6.2 - Avalon Zone

The pre-Mesozoic basement underlying the Grand Banks is composed of rocks of the Avalon Zone of the Appalachian Orogen (Haworth & Lefort, 1979; King et al., 1985, 1986; Williams et al., 1999) (Figure 1.7). The Avalon Zone in Newfoundland is a Late Precambrian succession of volcanic rocks with associated intrusive rocks. This volcanic succession is overlain by deep-marine, deltaic, and terrestrial sedimentation (King, 1988). Similar rocks can be found in the southern part of the British Caledonides, the Hercynides of France and Iberia, and on the northern and eastern margins of the West African shield (Rast et al., 1976; Rast, 1980; O'Brien et al., 1983). The entire Late Precambrian succession is relatively unmetamorphosed (King, 1990) and ranges in age from 760 – 540 Ma (Pollock et al., 2009). The rocks have been subject to two major deformation events: the late Precambrian Avalonian Orogeny and the mid-Paleozoic Acadian Orogeny (King, 1990).

The base of the Late Precambrian successions of the Avalon Zone on the island of Newfoundland comprise arc phase magmatic and volcanic igneous rocks such as the Marystown and Harbour Main groups and Holyrood Granite, with U-Pb zircon ages from 586 to 632 Ma (Krogh et al., 1987). Older units, such as the Wandsworth Gabbro of the Burin Group, Burin Peninsula, the Tickle Point Formation calc-alkaline rhyolite flows, and granites of the Furby's Cove Intrusive Suite were radiometrically dated at 767  $\pm$  2.2 Ma, 682.8  $\pm$  1.6 Ma, and 673  $\pm$  3 Ma, respectively (Krogh et al., 1987; Swinden & Hunt, 1991; O'Brien et al., 1996). Overlying the Neoproterozoic magmatic and volcanic rocks is a succession of clastic sequences including the Conception, Connecting Point, St. John's, Musgravetown and Long Harbour groups. Detrital zircons in the Conception Group and St. John's Group are predominantly 570 – 650 Ma with minor Mesoproterozoic and Paleoproterozoic input (Pollock et al., 2009). In parts of the onshore Newfoundland Avalon Zone, Cambrian – Ordovician marine-shelf sedimentary rocks unconformably overlie the Neoproterozoic clastic sequences (King, 1990). Detrital zircons from the Cambrian – Ordovician cover sequences are dominantly 500 - 680 Ma, but unlike Neoproterozoic rocks on the Avalon Peninsula, have larger quantities of Mesoproterozoic (1.0 - 1.6 Ga) and Paleoproterozoic (1.9 - 2.3 Ga), and also some Late Archean zircons (2.7 - 2.8 Ga) (Pollock et al. 2009).

Information about the offshore Avalon Zone is limited as, typically, exploration or petroleum wells rarely reach basement. However, magnetic anomalies indicate that the Avalon Zone extends as far east as the edge of the Grand Banks (Haworth & Lefort, 1979). Magnetic anomalies that can be traced from onshore also suggest that some of the basement is composed of arc-phase igneous rocks; however, Precambrian igneous basement has not been encountered offshore besides at the Flemish Cap (Haworth & Lefort, 1979; King et al., 1985). Samples of granodiorite from the Flemish Cap, a submarine knoll east of the Flemish Pass Basin, gave discordant U-Pb zircon ages with upper intercepts of 751 and 833 Ma (King et al., 1985). This suggests an age of intrusion sometime between ca. 750 and 830 Ma (King et al., 1985). The Flemish Cap granodiorite is thus interpreted to be part of the Avalon Zone, although it likely represents a much older part of the Avalon Terrane than what is seen further west on the island of Newfoundland (King et al., 1985).

The offshore subcrop extensions of the Neoproterozoic clastic sequences onshore are poorly constrained (Lowe, 2009). However, in the Virgin Rocks – Eastern Shoals area on the Bonavista Platform and on the Flemish Cap, Precambrian cover sequences have been drilled (Lilly, 1966; King et al., 1985). It is thought that these cover sequences extend over the eastern margin of the Bonavista Platform, the Central Ridge area, and beneath the shallow cover sequences of the Flemish Cap (King et al., 1985; Bell & Howie, 1990). Lower Paleozoic clastic cover sequences found offshore are considered equivalent to those of the Avalon Peninsula's Bell Island Group, and are thought to occur in the Avalon Uplift and Bonavista Platform areas, as well as on the shelf and slope area beneath the West Orphan Basin, the Northern Jeanne d'Arc Basin, and Flemish Pass Basin (King et al., 1986; Bell & Howie, 1990). These Lower Paleozoic clastic rocks have been drilled at both the Cumberland B-55 well and the Linnet E-63 well (Figure 1.1), where 400 m of Ordovician shales and siltstones, and 320 m of Lower Paleozoic shales and siltstones were encountered (CNLOPB, 2007). The Kyle L-11 (Figure 1.1) well in the Flemish Pass Basin drilled a significant section (700 m) of metasedimentary basement rocks (CNLOPB, 2013). However, the age of this sequence is not reported.



Figure 1.7 - Pre-Mesozoic basement geology of the Grand Banks and surrounding regions; modified from Lowe et al. (2011). Basement geology compiled from Haworth & Lefort (1979), Barrs et al. (1979), Priem & den Tex (1984), King et al. (1986), Capdevila & Mougenot (1988), Bell & Howie (1990), and Johnson et al. (2001). Black lines represent boundaries between terranes as well as modern day coastline. Study area is the Grand Banks of Newfoundland, eastern Canada. NL – Newfoundland; NS – Nova Scotia; OB – Orphan Basin; JDB – Jeanne d'Arc Basin; FPB – Flemish Pass Basin; IB – Iberian Peninsula.

#### 1.6.3 - Meguma Zone

The furthest outboard Appalachian terrane, the Meguma Zone, may have also been an important source for detritus to the Grand Banks during the Late Jurassic (Figure 1.7). The Meguma Zone is exposed onland in southern Nova Scotia, but extends over a much larger area off shore (Hutchinson et al., 1988; Keen et al., 1991; Pe-Piper & Jansa, 1999). The Cambrian – Ordovician Goldenville Group was deposited on a Gondwanan passive margin and is composed of the oldest exposed rocks of the Meguma Zone (van Staal, 2007). The Goldenville Formation was deposited on the slope to outer shelf (van Staal, 2007) and is overlain by the Halifax Group, a Lower Ordovician shallowing-upward succession (Schenk, 1997). The Annapolis Supergroup, composed of Upper Ordovician to Lower Devonian shallow marine siliciclastic rocks as well as Upper Ordovician – Lower Silurian (~442-438 Ma) rift-related bimodal volcanic rocks, disconformably overlies the Halifax Group (van Staal, 2007; Schenk, 1997; Keppie & Krogh, 2000; MacDonald et al., 2002). Unconformably overlying the Annapolis Supergroup are continental and shallow-marine, Upper Devonian - Lower Carboniferous sedimentary rocks (Martel et al., 1993). These are overlain by Upper Carboniferous continental sedimentary rocks. During the Acadian Orogeny (Middle to Late Devonian; 380 - 365 Ma), numerous metaluminous to peraluminous granites were emplaced in the Meguma Zone (Clarke et al., 1997; Kontak et al., 2004).

Krogh & Keppie (1990) analyzed detrital zircons from the Goldenville Formation of the Meguma Zone. They found major populations of late Neoproterozoic (550 - 750 Ma), Middle Paleoproterozoic (2.0 - 2.2 Ga), and Archean (2.8 - 3.0 Ga) zircon grains. White et al. (2008) analyzed detrital zircons from younger sequences of the Meguma Zone. Similar detrital zircon ages to the Goldenville Formation were found, except that Archean aged grains are absent and a small population of Mesoproterozoic (1.0-1.2 Ga) grains is present (White et al., 2008).

Magnetic anomalies in the basement rocks indicate offshore extensions of the Meguma Zone reach as far as the southern Grand Banks, and comprise the basement to the Avalon Uplift (Haworth & Lefort, 1979). The Collector Magnetic Anomaly represents the boundary between the Meguma and Avalon zones (Haworth & Lefort, 1979). Furthermore, rocks of the Meguma Zone have been encountered as basement in a number of offshore wells. In particular, the Jaeger A-49 well in the southern Grand Banks encountered granitic basement, which yielded a K-Ar whole-rock isotopic age of  $376 \pm 17$  Ma (Amoco Canada, 1973). This is indicative of the Meguma Zone as this zone is intruded by abundant Late Devonian granites (Kreuger Enterprises, 1972; Clarke et al., 1997; Kontak et al., 2004). Although Late Devonian intrusions also exist in Newfoundland, the Meguma Zone is characterized by abundant intrusions of this age, and represents a more likely correlative for this offshore extension. Pe-Piper & Jansa (1999) dated a number of plutonic rocks encountered in wells drilled offshore Nova Scotia and found predominantly Devonian intrusions.

## **1.6.4 - Central Mobile Belt**

Rocks of the Gander and Dunnage zones of the Newfoundland Central Mobile Belt are also potential important sources for detritus to the Grand Banks during the Kimmeridgian (Figure 1.7). Rocks in these zones are composed of the vestiges of the Iapetus Ocean, and are also present in the offshore as basement (Lowe, 2009). The Dunnage Zone consists of arc-related rocks and terranes that existed within the Iapetus Ocean (Stern & Bloomer, 1992) that have peri-Laurentian (further west) or peri-Gondwanan origins (further east) separated by a major suture. Rock types within the Dunnage Zone include arc-associated volcanic rocks and related sedimentary successions. The Gander Zone, however, represents a fragment of a Gondwanan passive margin (van Staal, 1994). Sedimentary rocks are important in the Gander Zone, but Silurian to Devonian granites are also common, as well as some metamorphic rocks. For the most part, magmatic rocks of the Gander and Dunnage zones range in age from Late Cambrian to Early Devonian, with some rare Late Devonian granites (Dallmeyer et al., 1981; Chorlton & Dallmeyer, 1986; Dickson, 1990; O'Neill, 1991; Currie, 1995; Dube et al., 1996; Valverde-Vaquero et al., 2003; Valverde-Vaquero et al., 2006). O'Neill (1991) analyzed detrital zircons from the Gander Zone's Jonathans Pond Formation and found zircons of Mesoproterozoic (1.0 - 1.3 Ga), Paleoproterozoic (2.0 - 2.2 Ga), and Archean ( $\sim 2.7$  Ga) ages, as well as an individual Early Cambrian ( $\sim 540$  Ma) grain. Pollock et al. (2007) analyzed the detrital zircons from Late Ordovician to Silurian sedimentary successions in the Dunnage Zone and revealed populations with abundant Ordovician to Late Neoproterozoic (450 - 550 Ma), Mesoproterozoic (1.0 - 1.5Ga), and Late Paleoproterozoic (1.6 - 1.8 Ga) grains, and minor Late Archean (2.7 - 2.5 Ga) grains.

## **1.6.5 - Carboniferous Sedimentary Basins**

Numerous Carboniferous sedimentary basins were developed atop the Appalachian Orogen in Newfoundland, the Northeast Newfoundland Shelf, and elsewhere in the Maritimes and may represent significant potential sources for Late Jurassic detritus to the Grand Banks (Figure 1.7). These Carboniferous Basins include the Deer Lake and Bay St. George basins on the island of Newfoundland, as well as offshore extensions of these Carboniferous basins in the St. Anthony, Magdalen, and Sydney basins. The Carboniferous rocks are predominantly continental clastic sedimentary rocks, and have been intersected by several offshore wells. For instance, a thick (1500 m) succession of Carboniferous red-brown sandstones and siltstones were drilled in the Hare Bay E-21 well, West Orphan Basin. Other Carboniferous clastic sequences were intersected in the southern Grand Banks area in wells Hermine E-94, Gannet O-54, and Sandpiper J-77 (Bell & Howie, 1990). Each of the drilled sequences have been considered equivalent to adjacent Horton, Windsor, Canso, Riversdale, or Pictou Groups onshore in Nova

Scotia (BP Canada, 1979; Bell & Howie, 1990). The Avalon Uplift, south of the Flemish Pass Basin, is also thought to be covered by equivalent Upper Paleozoic (Devonian – Pennsylvanian) sequences (Barrs et al., 1979, Bell & Howie, 1990). Detrital zircons from the Horton Group, mainland Nova Scotia, were analyzed by Murphy & Hamilton (2000) and exhibit major populations of Neoproterozoic (550 – 700 Ma), and Paleoproterozoic (2.0 – 2.2 Ga) grains with less significant Devonian (370 – 380 Ma) and Silurian (411 Ma) grains. On the island of Newfoundland, detrital zircons from sandstones of the Carboniferous Deer Lake and Bay St. George basins are predominantly Ordovician – Silurian in age and are thought to have been derived from volcanics of the Newfoundland Dunnage Zone (Sylvester, 2012). Some Mesoproterozoic grains are also present, likely derived from Grenvillian basement to the north and west (Sylvester, 2012).

## **1.6.6 - Mesozoic Igneous Rocks**

In addition to pre-Mesozoic basement, contemporaneous rift-related igneous rocks may also have been an important source for detritus to the Grand Banks in the Late Jurassic. Syn-rift igneous rocks have been identified onland in Newfoundland, as well as in offshore wells. In Central Newfoundland, a small ultramafic pluton called the Budgell Harbour Stock was dated and yielded a K-Ar biotite age of  $139 \pm 9$  Ma (Helwig et al., 1974). On the Avalon Peninsula of Newfoundland, diabase dikes along the trans-Avalon aeromagnetic lineament gave a Late Triassic age of  $201.1 \pm 2.6$  Ma (Hodych & Hayatsu, 1980). Offshore, in the West Orphan Basin, granite from the Bonavista C-99 well was dated at  $146 \pm 6$  Ma using the K-Ar whole-rock method (BP Canada, 1975). Yet to be dated Triassic-Jurassic basalts were drilled in both the Spoonbill C-30 & Cormorant N-83 wells (Amoco et al., 1973; Jansa & Pe-Piper, 1986). On the Southern Grand Banks, Upper Jurassic volcanic rocks were intersected at Brant P-87 and Twillick G-49. At Brant P-87, K-Ar dating revealed an age of  $135 \pm 6$  Ma for 55 m of basalt and pyroclastics and 123 m of diabase sills, while at Twillick G-49, K-Ar dating revealed an age of  $177 \pm 5$  Ma on a 15 m thick porphyritic diabase (Jansa & Pe-Piper, 1988).

## **1.6.7 - Irish Conjugate Margin**

During deposition of the Kimmeridgian source rocks, the Irish and Iberian conjugate margins were relatively close to the study area, and thus might be potential source areas (Lowe, 2009) (Figure 1.7). It is therefore necessary to review the major crustal ages of these margins that could help distinguish European sources from the east and North American sources from the west.

The Paleozoic basement geology of the Irish Conjugate Margin is similar to that of the Newfoundland Margin as the major crustal blocks resulted from the development and subsequent closure of the Iapetus Ocean . In particular, the Irish Margin is largely comprised of Lower to Middle Paleozoic sequences overlain by Carboniferous clastic rocks and carbonates. One of the dated basement exposures on the Irish mainland is the Annagh Gneiss which has a U-Pb zircon age of 963  $\pm$  8 Ma (Daly & Flowerdew, 2005). In addition, Lower Ordovician magmatic rocks have been dated from Northwestern Ireland, with ages ranging from 467  $\pm$  6 Ma to 474  $\pm$  5 Ma (Flowerdew et al., 2005). Upper Silurian to Lower Devonian plutons and batholiths have also been found. One of these is the Galway Granite, with U-Pb zircon ages between 395 and 405 Ma (Feely et al., 2004).

Less information is available about the Paleozoic basement offshore Ireland, although in the Porcupine Basin and Porcupine Ridge, it is likely a continuation of the crustal blocks of the Appalachian-Caledonian orogeny. Johnson et al. (2001) interpreted the Clare Lineament, a major feature that divides the Porcupine Basin from the Porcupine Seabight Basin, as the boundary between the Avalon and Central Mobile Belt crustal blocks, and as an extension of the CharlieGibbs Fracture Zone found offshore Newfoundland. It is likely that Carboniferous sedimentary rocks are present offshore Ireland as well as those found onshore. In the Porcupine Basin, reworked Carboniferous palynomorphs have been found in younger Mesozoic clastic rocks (Smith & Higgs, 2001). The Porcupine Median high is an igneous feature thought to be Early Cretaceous in age (Tate & Dobson, 1988). This feature represents a potential source of Mesozoic detrital zircons from offshore Ireland. However, it has not been sampled, making its proposed age speculative.

### **1.6.8 - Iberian Conjugate Margin**

The Iberian Margin is the direct conjugate margin to the Grand Banks (Figure 1.7), and extension from the Tithonian to Valanginian resulted in seafloor spreading between the two margins (Sinclair, 1988). The majority of basement rocks present on the Iberian Peninsula are Paleozoic granitoids and were produced in the Mississippian (330 – 320 Ma), Pennsylvanian (310 – 300 Ma), and Early Permian (290 – 280 Ma) (Priem & Tex, 1984). The rest of the basement of the Iberian Peninsula is composed of Lower Ordovician gneisses with U-Pb ages ranging from 460 Ma to 490 Ma (Priem & Tex, 1984; Valverde-Vaquero & Dunning, 2000).

The Paleozoic basement of offshore northern and central Iberia is likely represented by a continuation of the onshore Central Iberian Zone with Carboniferous–Permian granitoids (Priem & Tex, 1984; Capdevila & Mougenot, 1988) as well as equivalent lithologies to the onshore Ossa Morena Zone (Capdevila & Mougenot, 1988). The Ossa Morena Zone is composed of Neoproterozoic metasedimentary and volcanic and intrusive rocks, in addition to volcanic and intrusive igneous rocks which formed during the Cambrian to Early Ordovician, and Mississippian (Romeo et al., 2006; Sola et al., 2008).

Additional Iberian-related sources may include Hercynian foreland basin sedimentary rocks. This scenario was described in detail in Hiscott et al. (2008). By analyzing a combination of paleocurrent data, ages of detrital micas, and sediment composition, Hiscott et al. (2008) determined that post-rift sediments from the Grand Banks were likely derived from Hercynian foreland basin sediments. It is likely that the Hercynian orogenic belt was in close proximity to the Grand Banks during the Carboniferous/Permian. Therefore, the deformation front for this orogen was near the eventual dividing line between Iberia and the Grand Banks. The associated Hercynian foreland basin would have existed 200-300 km to the west of this orogenic front (Allen & Homewood, 1986; Hiscott et al., 2008). Given this information, it is likely that sediments of this foreland basin would have blanketed at least some of the Grand Banks, particularly in the region of the Avalon Uplift (Hiscott et al., 2008). These foreland basin sediments would have been deposited in the Late Carboniferous or Permian, and would have likely contained substantial quantities of Permo-Carboniferous zircons from the Iberian granitoids which would have subsequently been available for erosion and deposition into Mesozoic basins.

#### Chapter 2 – Methods, Wells Studied & Sampled Intervals

#### 2.1 - Introduction

This chapter describes the mudstone intervals sampled for analysis, and provides an overview of the wells in the study area. Additionally, sample preparation and analytical methods are reviewed.

Conventional cores and cuttings samples of Kimmeridgian source rocks were collected from four wells within the Flemish Pass and Central Ridge area. The wells chosen were Baccalieu I-78 (Figure 2.2), Lancaster G-70 (Figure 2.3), South Tempest G-88 (Figure 2.4), and Panther P-52 (Figure 2.5) because they all intersected Kimmeridgian source rocks, and because of their distribution in the basin. Baccalieu I-78 is within the northern Baccalieu subbasin, while Lancaster G-70 is located in the southern Gabriel subbasin. Panther P-52 and South Tempest G-88 are both within the Central Ridge. Collecting samples from these separate areas permits a more thorough interpretation of the provenance and paleodrainage patterns during this time. To ensure consistent sampling from different wells, biostratigraphic reports and lithostratigraphic picks were used. Although there are several distinct interpretations, there is a consensus on where Kimmeridgian source rocks (or Egret Member equivalent source rocks) occur. There are distinct interpretations because different microfossil assemblages were used by different authors as well as different terminologies. For example, in the biostratigraphic reports, several of the available publications have older terminology, no longer used by the International Commission on Stratigraphy (ICS). The older terminology creates confusion with respect to the length of the Kimmeridgian Stage. In 1990, the International Subcommission on Jurassic Stratigraphy voted to discontinue the use of the Kimmeridgian 'sensu Anglico' in favour of the Kimmeridgian 'sensu Gallico,' both with different zonal content and boundaries (Zeiss, 1991; 2003). Thus, reports using the current 'sensu Gallico' terminology are used in this thesis. Reports found using the older terminology were avoided as a late Kimmeridgian age using the '*sensu Anglico*' terminology would actually correspond in part to a Tithonian age using the '*sensu Gallico*' terminology.

#### <u>2.2 – Sample Collection</u>

The available cores and cuttings were logged and sampled at the CNLOPB Core Storage and Research Centre in St. John's, Newfoundland. Although samples from conventional cores are preferred for this study, the entire Kimmeridgian source rock interval was not cored. Thus, cuttings were sampled where cores were unavailable. With cores, samples were collected from a mudstone unit as well as within interbedded siltstones of the same section. This permits a comparison between heavy-mineral distributions of the finer and coarser grained intervals within the same section with likely the same source region, to ensure there is no sample bias from a specific size fraction.

### **2.3 – Analytical Methods**

### 2.3.1 - Introduction

Several different analytical methods were employed in this study. Polished thin sections were observed first using an optical microscope and then analyzed on a scanning electron microscope using mineral liberation analysis techniques (hereafter referred to as MLA-SEM) to identify minerals and determine mineral modes. For detrital zircon geochronology, MLA-SEM imaging was the first step, followed by laser-ablation microprobe (LAM) ICP-MS analysis. Techniques employed for whole rock geochemical analysis include X-Ray Fluorescence, and inductively coupled plasma mass spectroscopy (ICP-MS). An assessment of heavy mineral suites and provenance-sensitive heavy mineral ratios was also undertaken using the MLA-SEM.

## **2.3.2 - Optical Petrography of Thin Sections**

Thin sections from the sampled intervals were examined by transmitted light microscopy and MLA, to provide a better understanding of the petrology and provenance characteristics of the source rocks. The composition of the constituent detrital grains, as well as the mineralogical and textural maturity were assessed in order to determine provenance. Dickinson & Suczek (1979) demonstrated that the framework mineralogy of sandstone is a good proxy for provenance. Diagenetic overprints were also evaluated. For example, features such as grain dissolution that could affect the composition of the rock or the diversity of heavy mineral assemblage were analyzed. The source rock petrology was described and interpreted. The MLA was used to determine modal mineral abundances. The MLA-SEM is described in detail in Section 2.3.4. It is useful for the determination of exact mineral abundances and as well as mineral associations. In addition, it is useful for identifying rare and small heavy mineral grains. The descriptions and interpretations supplemented other assessments of source area composition, sedimentary recycling, and transport distances.

## 2.3.3 – Sample Preparation for Detrital Zircon Geochronology

Different methods were used to prepare samples for detrital zircon geochronology depending on whether the material in question was from a core or from cuttings. Where cores were available, it was only possible to obtain a small (5 x 3 x 3cm) sample because the detrital zircon analysis is destructive. With such a small sample, crushing and heavy liquid separation are not feasible as material would likely be lost through the sample preparation process. Therefore, numerous thin sections were made from each small sample. Even if heavy minerals are not abundant in the sample, there should be enough grains to evaluate if several thin sections are cut from the same interval. An initial assumption made with fine-grained sediments is that there are likely not any heavy minerals large enough (>20  $\mu$ m for LA-ICP-MS at Memorial University) to

separate and analyze. However, studies by Totten & Hanan (1998, 2007) indicate that heavy minerals can be just as abundant, if not more abundant, in shales than sandstones with some possessing sizes large enough to analyze.

For work on cuttings, approximately 50 g samples are available from the CNLOPB. The cuttings were taken from 5 m intervals and were unwashed. For the thesis work, the cuttings were gently disaggregated, cleaned, and wet sieved through a 15 µm mesh to remove the drilling mud and fine clays. Tap water was used for this process. This mesh size is considered appropriate because the ability of the LAM-ICP-MS to analyze zircons smaller than 15 µm is limited by the spot size of the laser. After the samples are cleaned, they were left to dry overnight and then sieved through a 180 µm mesh. This split the sample into two fractions: one 15 - 180  $\mu$ m and the other > 180  $\mu$ m. The 15 – 180  $\mu$ m fractions were used for analysis. For heavy mineral analysis, studies such as Lowe et al. (2011) analyzed the  $63 - 180 \mu m$  fraction, following procedures outlined in Morton & Hallsworth (1994). For heavy mineral analysis, this size fraction was chosen because all heavy minerals were thought by those authors to exist within this size fraction. Thus, bias based on the grain size distribution from the parent rocks and subsequent hydrodynamic sorting is likely diminished when comparing ratios of different heavy minerals (Morton & Hallsworth, 1994). Lowe et al. (2011) also considered this size fraction appropriate for detrital zircon geochronology. However, Totten & Hanan (2007) stated that the median grain size of heavy minerals within shales is approximately 25 µm less than in sandstones. Because this study analyzed fine-grained hydrocarbon source rocks, a lower limit on the particle size to be considered was set at 15  $\mu$ m rather than 63  $\mu$ m. Further details on the rationale for the grain size bracket used are presented in Section 5.2.

#### 2.3.4 - MLA-SEM Imaging for Detrital Zircon Geochronology

Once the cuttings had been cleaned and sieved, samples were prepared for imaging on the MLA-SEM. In the SEM lab, Bruneau Innovation Centre, Memorial University, the samples were mounted in epoxy, left to cure overnight, and polished the next day. Polishing cuts into the embedded sedimentary particles and removes scratches and bumps or ridges on the epoxy surface, which permits proper imaging by the SEM. Polishing exposes the cores of grains in order to remove the outer surfaces of grains, which are typically enriched in adsorbed uranium (Krogh, 1982). Care must be taken to ensure that none of the zircons are polished away or plucked out of the mounts. After polishing, the samples are ready for imaging on the SEM.

Unlike a traditional optical microscope, which collects light, the SEM collects emitted electrons and can image small specimens at 100 to 100,000x their actual size. The images produced possess an extreme and realistic depth of focus. The SEM is equipped with an energy dispersive X-ray (EDX) detector, an electron backscatter diffraction (EBSD) system and a cathode-luminescence (CL) detector. In addition, the SEM is equipped with MLA® (Mineral Liberation Analysis) software, which is capable of X-ray aided image analysis. The technique relies primarily on backscattered electron imaging (BEI), and energy-dispersive X-ray (EDX) analysis, which classify the grains as known minerals. The MLA software has the ability to spatially quantify mineral abundances, define associations of areas, and indicate sizes and shapes of minerals in a systematic fashion. The instrument used for this study is the FEI MLA 650F. In addition, the high throughput EDS (energy-dispersive X-ray spectroscopy) detector was advantageous in reducing run times where samples contained abundant (>100,000) grains. Further details on the MLA-SEM are available in Sylvester (2012).

During MLA runs, typical instrument settings included voltage set at 25 KeV, a beam current of 10 nA, a working distance of 13.5 mm, and a spot size of about 5.5 µm. Between 10,000 and 300,000 particles were identified and analyzed in each individual sample. Unknown mineral phases were identified based on matching their spectra to that of Mineral EDX spectra standards. This is completed using the MLA Image Processing Tool software. Minerals of interest from the sample (i.e., zircon) were then imaged manually using the MLA Viewer Software. This permits the user to image and choose only the zircons that are optimal for age dating (i.e., free of inclusions, cracks, or other imperfections that could influence the analysis). The MLA then outputs coordinates for the location of the imaged zircons within the thin section or grain mount.

It is worth noting that the abundances of several heavy mineral phases, such as garnet, allanite, and ilmenite were erroneous, as the MLA method was ineffective at distinguishing these minerals from finely disseminated clays, micas, pyrite, and carbonate material, which are common components in samples for this study. Due to the method in which mineral spectra are obtained through spot analysis, the EDX elemental peaks for both these finely disseminated grains as well as the mentioned heavy minerals appeared very similar, which led to some misclassifications. This problem was also encountered by Lowe (2009) in sandstones of the Flemish Pass Basin. The abundances of the affected heavy mineral grains, therefore, were not included in the analysis of heavy mineral assemblages in Chapter 5. This problem is also apparent in the identification of clay minerals. Due to the nature of the spot analysis, differentiation between this finely disseminated material is difficult and the acquired spectra often represented a mixture of a number of different minerals. It was therefore necessary to group these minerals into new categories that represent a combination of the mineral spectra.

These include blends of fine-grained quartz and clay, as well as a mixture of fine-grained silicate and carbonate. However, it was still possible to identify minor quantities of individual clay minerals.

Another complication encountered was the abundance of the mineral Barite (BaSO<sub>4</sub>). Barite was abundant in all heavy mineral fractions from cuttings samples, as it is used as an additive in drilling mud. The sample preparation process removes significant amounts of the barite, but it was not always possible to completely eliminate this contaminant. However, the naturally occurring abundances of other heavy minerals are not expected to be affected by the occurrence of barite since the barite in these samples is industrial, and is derived from evaporite deposits. The barite may be associated with minerals such as gypsum and anhydrite, but those minerals are unrelated to the clastic sediments analyzed in this study.

#### 2.3.5 - LAM-ICP-MS for Detrital Zircon Geochronology

LA-ICPMS U-Pb zircon geochronology was carried out at Memorial University of Newfoundland using a Thermo-Scientific ELEMENT XR magnetic sector, single-collector ICPMS coupled to a Lambda Physik ComPex Pro 110 ArF excimer GeoLas laser ablation system operating at a wavelength of 193nm and a pulse width of 20 ns. The laser was operated at an energy density of 5-7 J/cm<sup>2</sup> and a repetition rate of 4-5 Hz, with a spot diameter of 20 micrometers. The sample aerosol is transported from the sample cell to the ICP using a Hecarrier gas to reduce sample redeposition within the ablation cell, improving sample transport efficiency and resulting in more stable time-resolved signals.

Data acquisition for each analysis is about two minutes, with the first ~30 seconds used to measure the gas background followed by ~40 sec of laser ablation, and ~50 sec of wash out. Measurements are carried out in peak-jumping mode with one point measured per peak. Isotopes

measured are <sup>200</sup>Hg, <sup>202</sup>Hg, <sup>204</sup>Hg+Pb, <sup>206</sup>Pb, <sup>207</sup>Pb, <sup>208</sup>Pb, <sup>232</sup>Th, <sup>235</sup>U and <sup>238</sup>U from both the zircon and gas background. Intensities for <sup>235</sup>U were calculated from <sup>238</sup>U assuming a natural, present-day <sup>238</sup>U/<sup>235</sup>U ratio (137.88), as the measured <sup>235</sup>U intensities for many analyses were low and thus had large uncertainties.

Raw data are dead-time corrected and reduced off-line using the Iolite 2.5 software (Paton et al. 2011) with the VizualAge DRS (Petrus and Kamber 2012), which carries out background and signal interval selections, gas background subtraction, signal drift corrections, external calibration, and age and uncertainty calculations. The external calibration provides corrections for instrumental mass bias and laser-induced U/Pb fractionation. In this study, signal intensities of zircon of unknown age were calibrated against standard reference material 91500 zircon (1065  $\pm$  3 Ma; Wiedenback et al. 1995). Ages and 2-sigma uncertainties were calculated from the corrected <sup>207</sup>Pb/<sup>206</sup>Pb, <sup>207</sup>Pb/<sup>235</sup>U and <sup>206</sup>Pb/<sup>238</sup>U ratios. Age determinations were calculated using the decay constants of Jaffey et al. (1971). Final concordia diagrams, U-Pb age histograms and probability density plots were produced using the Isoplot/Ex3.75macro (Ludwig 2012).

Common Pb corrections were made where <sup>204</sup>Pb was detected above gas background using the the method of Andersen (2002) in the Iolite/VizualAge software. The Andersen method was preferred to the <sup>204</sup>Pb common Pb correction method because <sup>204</sup>Hg made up a majority of the total measured 204-peak in many analyses and thus uncertainties on the <sup>204</sup>Pb intensities were large.

In order to monitor the efficiency of the instrumental mass bias and laser-induced fractionation corrections, standard reference materials, 02123 zircon (295  $\pm$  1 Ma; Ketchum et al. 2001), Plesovice zircon (337.13  $\pm$  0.37 Ma; Slama et al. 2008) and OG-1 zircon (3465.4  $\pm$  0.6

Ma; Stern et al. 2009) were analyzed between every 8 unknown zircons during each analytical session. These standard measurements also monitor the accuracy and reproducibility of U-Pb analyses. The weighted mean  ${}^{206}\text{Pb}/{}^{238}\text{U}$  age for all analyses of 02123 is 294.63 ± 0.8 Ma (2 $\sigma$ , MSWD = 1.7; n = 203), for Plesovice is 342.4 ± 1.6 Ma (2 $\sigma$ , MSWD = 2.4; n = 85), and for 91500 is 1062.0 ± 1.6 Ma (2 $\sigma$ , MSWD = 0.78; n = 368) over the course of all the U-Pb analytical sessions. The weighted mean  ${}^{207}\text{Pb}/{}^{206}\text{Pb}$  age for all analyses of OG-1 is 3475.5 ± 2.5 Ma (2 $\sigma$ , MSWD = 1.7; n = 79) over the course of all the U-Pb analytical sessions. All data for reference standards is available in Appendix B.

For detrital zircon geochronology, the aim is to analyze as many zircons as possible to reduce the probability of missing an age population. Fedo et al. (2003) stated that the analysis of 59 randomly selected zircon grains from a sedimentary rock that has a normal abundance of zircon grains reduces the possibility of missing an age population to 5%. Similarly, Dodson et al. (1988) indicate at least 60 grains must be analyzed to reduce the possibility of missing an age population greater than 0.05 to 95%. However, Vermeesch (2004) states that to be 95% confident that no age population greater than 0.05 has been missed, 117 grains must be dated. However, this assumes that the sample has a perfectly uniform distribution where each age group has the same amount of grains (Vermeesch, 2004). This type of distribution is uncommon in naturally occurring populations. Therefore, Vermeesch (2004) states that if there is prior knowledge indicating the populations are not uniformly distributed, it is sufficient to date 95 grains to be 95% confident no age population greater than 0.05 has been missed. Vermeesch (2004) suggests that if fewer than 117 grains are dated per sample, the probability of missing at least one age fraction should be reported.

In this study, as many grains as possible were analyzed in each sample. However, as discussed in Section 2.3.3, since these samples are derived from core and cuttings from offshore wells, a limited amount of sample material is available. Where cuttings were used, only 50 g samples over 5 m intervals were available (Figure 2.1). Samples could have been combined to cover 10 m or greater intervals, but this would result in lower resolution for the provenance analysis and was therefore avoided. In samples where fewer grains were analyzed, it is important to note that it is possible that only the major age peaks were detected. However, given that this is the first study of this nature on the Kimmeridgian rocks offshore Newfoundland, the major age peaks will still provide unique datasets and important provenance information. For each sample, the probability that an age peak has been missed will be noted as suggested by Vermeesch (2004).



Figure 2.1 - Image of approximately 50 g cuttings sample from the Baccalieu I-78 well (5000 m).

2.3.6 – Sample Preparation and MLA/SEM for Evaluation of Heavy Mineral Ratios Heavy mineral ratios are assessed to determine the provenance fingerprint of the studied

units. Provenance sensitive heavy mineral ratios using zircon, monazite, titanite, chromite, and

rutile are considered useful for provenance discrimination and assessing sedimentary recycling. Cuttings are used for this portion of the project and the procedure for processing the samples and heavy mineral separation are similar to the methods used for detrital zircon geochronology discussed previously. These samples are mounted in epoxy and analyzed on the MLA-SEM. The ability of the MLA software to identify heavy minerals and demonstrate the sizes and shapes of grains permits for a meaningful comparison of the provenance fingerprints of different stratigraphic units of this study.

#### 2.3.7 - X-Ray Fluorescence for Whole Rock Lithogeochemistry

Samples for X-ray fluorescence were taken from conventional cores, and prepared in the crushing room in the Department of Earth Sciences at Memorial University. Sample preparation involves pulverizing the rock into a fine powder using the Siebtechnik grinding mill. Strict laboratory protocols were followed to prevent contamination throughout this process.

The X-ray fluorescence analysis was completed at the TERRA lab facilities, Memorial University. The XRF facility uses a Fisons/Applied Research Laboratories model 8420+ sequential wavelength-dispersive x-ray spectrometer which has the capability for qualitative and quantitative determination of elements. The detection system utilizes an argon/methane flow proportional counter and also a scintillation counter. A combination of fused glass beads and pressed pellets is used to obtain a full analysis of all, major, minor and trace elements. For the preparation of the pressed pellets, approximately 9 g of rock powder is weighed and mixed with 2.7 g of wax binder. This mixed powder is then put in a Herzog Pellet Press and pressed at 276 MPa for 10 seconds. The final preparation step is baking the pellet at 90°C for 15 minutes. The pressed pellet analysis for trace elements, Fe<sub>2</sub>O<sub>3</sub> and MnO is completed on a Bruker S8 Tiger

WDXRF using the Geo-Quant T package. Two geological reference standards (SGR-1B-1 and SDO-1-1) were analyzed with each group of 13 samples to confirm accuracy and precision for the results. These reference standards are of the Green River Shale and the Devonian Ohio Shale, respectively. The accepted values for the geological reference materials analyzed are also given with the results sheets. The reference materials are combined with a reagent blank to measure the reagent contribution to the values. XRF is considered an excellent and robust method for the determination of the major and more abundant trace elements in rock samples. It will provide additional information on the provenance of the Kimmeridgian mudstones.

## 2.3.8 - ICP-MS for Whole Rock Lithogeochemistry

The concentrations of certain elements, particularly Th, in the samples are below the limit of detection of the XRF instrument. To obtain a complete analysis, ICP-MS (inductively coupled plasma mass spectrometer) is used because of its precise nature and sensitivity in trace element analysis. ICP-MS analyses were carried out at the TERRA lab facilities at Memorial University. The data obtained were combined with the XRF data to produce a more complete geochemical analysis of the samples. For introduction of rocks into the ICP-MS as solutions, samples must be digested in acid before analysis. All results are given in ppm. The analytical procedure is as follows: 1) Initial digestion of a 0.1 g sample aliquot using HF/HNO<sub>3</sub> (also boric and oxalic acids); and 2) the resultant solution is analyzed using inductively coupled plasma mass spectrometry correcting for matrix effects using the method of standard addition. Full details of the procedure are given in Jenner et al. (1990). If any sample material is not dissolved fully in HF/HNO<sub>3</sub>, it is treated with HCl/HNO<sub>3</sub>. In some samples, some resistant phases, most notably zircon, may not always dissolve completely. In these cases, Zr, Hf, and HREE values should be considered minimum concentrations. For samples in this study, it was noted that Zr values from ICP-MS were significantly lower than those from the XRF analyses. Therefore, it is concluded

that the lower Zr values from ICP-MS are a result of zircon not completely dissolving. Zr values used in graphs and geochemical analysis in this study were consequently taken from the XRF analyses. For quality control, two geological reference standards (SGR-1B-1, and SDO-1-1) were prepared and analyzed with the other samples as outlined in Section 2.3.7.

In ICP-MS analysis, there are a number of inter-element interferences present. The instrument used has been optimized so that the interferences are at a low enough level that they can be corrected for most rock types. The most noteworthy of these interferences is a Ba molecular ion interference on Eu. A correction is applied, but the error in this correction can be significant, especially at very high Ba/Eu ratios. This Ba-Eu interference is not considered an issue for samples in this study as these elements were not used in provenance graphs or analysis.

## 2.4 - Wells Studied

#### 2.4.1 - Baccalieu I-78

Baccalieu I-78, drilled in 1985 in 1092.8 m water depth by an Esso Parex-led consortium, is an abandoned exploratory well located in the Northern Flemish Pass Basin (47° 57' 41.49" N, 46° 10' 46.76" W). The total depth of the well is 5134.5 m and it intersected approximately 600 m of Tertiary, 1500 m of Lower Cretaceous, and 1500 m of Upper Jurassic strata (Figure 2.2). Potential reservoirs were encountered in the Cretaceous section, where texturally mature sandstone was penetrated between 3195 and 3275 m. This reservoir is considered equivalent to the Hibernia Formation of the Jeanne d'Arc Basin. A more poor reservoir, thought to be equivalent to the Avalon Formation, was penetrated between 2030 and 2220 m. The Upper Jurassic Jeanne d'Arc Formation equivalent sandstone is encountered between 3715 and 3780 m (McAlpine, 1989; CNLOPB, 2011). Kimmeridgian source rocks were encountered between 4398 and 4804 m, and also from 4975 to 5135 m, designated as the Upper and Lower Kimmeridgian Source Rock units, respectively (CNLOPB, 2011). Samples were collected for provenance analysis from both Kimmeridgian Source Rock units, as well as samples from the Rankin Formation, which is interbedded with the source rock units (Table 2.1). In combination with the lithostratigraphic picks, biostratigraphic interpretations were also used to ensure sampling was focused on the intended Kimmeridgian interval. Biostratigraphic reports from both Esso Resources (1986) and Robertson Research (2002) place the majority of the sampled units with the Kimmeridgian Stage. A limited amount of conventional drill core is available from this well; therefore the majority of sampled units are drill cuttings. However, conventional core was available between 4135 and 4153 m, and several samples were acquired from this interval.

Depth	Gamma Ray	Stratigrap	ohic Units	Biostratigraphic Interpretation			
_	0 API 150	Banquereau	Banquereau				
		Shale	Shale	Eocene		Pliocene	
			Nautilus Shale	Aptian	Hauterivian	Aptian	
		Barremian Shales			Valanginian		
		onaics		Valanginian to Hauterivian		Barremian	
_		Augles Fre					
						Factor	
			se Shale			Hauterivian	
2500m		0			Middle to Late Berriasian Kimmeridgian		
		Shale	itero			n to ian	
		eso.	M				
		/hiter				iasia angir	
		5				Late Berr Early Val	
		Hibornia Em	Hibornia Em				
			Fortuno Bay		arly Kimmeridgian	9 c	
			Shale			asiar	
		Shale	Jeanne d'Arc	sian		lithor Berri	
_			Formation	Berrias		_ate	
		Jeanne d'Arc Fm					
			c			honia	
			natio		ш	tte Tit	
			Forn	gian		eT	
		Ę	Line Earet				
_		natio	Mbr				
4500		E E E		nerid		an to	
4500m		ankir Kimi e Rod		Kimr		gian honia	
		pper ource				nerid le Tit	
		⊃ o	Voyager Formation			Kimn Midd	
				Oxfordian			
<u> </u>		Lower Kimm.	Downing	Oxicitian			
			Formation	Callovian	-		
		(2007	(198	sources	1990)	(2002)	
	Core Location	OPB.	Alpine	so Res 386)	scoli (	bertson search	
		CNL	McA	(19 (19	¥.	Re	

Figure 2.2 - Combined gamma ray, stratigraphic, and biostratigraphic log for the Baccalieu I-78 well.

	Denth helow	Formation*			Lithology**		Sample Type		Type of Analysis***				
Well	KB (m)	UTS	UKSR	RF	LTS	LKSR	SS	MS	Core	Cuttings	GC	DZG	HMA
	3500-3505	x	onon		210	Liton	x		0010	X	00	DLO	x
	3600-3605	v						v		Y Y			v
	3700-3705	x						x		x			x
	3830.1	~	x				x	A	x	A	x		А
	3832.0		X				X		X		X		
	2822.0 (P)		v				x v		v		v		
	3832.0 (B)		A V				A V		л v		л	v	
	2020 4		A V				A V		A V		v	л	
	2020 4 (D)		A V				A V		A V		A V		
	3838.4 (B)		A				А	37	A		A		
	3843.4		X					X	X		X		
	3843.4 (B)		Х					Х	X		X		
	4000 - 4005			X						X			X
	4183.9				X			X	X		X		
South	4183.9 (B)				Х			Х	X		Х		
Tempest G-88	4185.1				Х			X	X		Х		
	4185.4				Х			Х	Х		Х		
	4188.1				Х		Х		Х		Х		
	4188.1 (B)				Х		Х		Х		Х		
	4195.8				Х		Х		Х			Х	
	4198.0				Х			Х	Х		Х		
	4325.4					Х		Х	Х		Х		
	4327.3					Х		Х	Х		Х		
	4327.6					Х		Х	Х		Х		
	4329.6					Х		Х	Х		Х		
	4330.0					Х	Х		Х		Х		
	4331.3					Х		Х	Х		Х		
	4495-4500					Х		Х		Х			Х
	4600-4605			х				Х		Х			Х
	3210.0	Х					Х			Х		Х	Х
	3400.0		Х					Х		Х			Х
	3500.0		Х					Х		Х			Х
	3600.0				Х			Х		Х			Х
Panther P-52	3754.0				Х			Х	Х		Х		
	3756.7				Х			Х	Х		Х		
	3757.0				Х			Х	Х		Х		
	3757.0 (B)				Х			х	х		Х		
	3950.0					х		X		х			х
	4135.3			х			х		х			х	
	4135.8			x				x	x		x		
	4138.5			x				x	x		X		
	4140.9			X				X	X		X		
	4140.9			x v				v	v		Λ	v	
	4142.2			A V				A V	A V		v	Λ	
	4145.9			A V				A V	A V		A V		
	4140.0			A V				A V	A V		A V		
Baccalieu I-78	4147.0			A V				A V	A V		A V		
	4148.3			X				A	A		A		
	4148.3 (B)			X				X	X		X		
	4151.8	<u> </u>	v	X				X	X	N/	Х	v	37
	4500-4505		X					X		X		Х	X
	4705-4710		X					Х		X			X
	4900-4905			X				X		X			X
	5000-5005					Х		Х		X			X
	5075-5080					X		Х		X			X
Lancaster G- 70	3305-3310	L	Х					Х		Х			Х
	3500-3505		Х				Х			Х			Х
	3715-3720		Х					Х		Х			Х
	4200-4205			Х				Х		Х			Х
	4405-4410			Х			Х			Х		Х	Х
	4740-4745					Х		Х		Х			Х
	4820-4825					Х		Х		Х			Х
*UTS=I	Jpper Tempest	Sandsto	ne, UKSR=	Upper k	Cimmeria	lgian Sou	ce Rock	RF=Rank	in Formati	on, LTS=I o	wer Temp	est Sandsto	ne,
LKSR=Lower Kimmeridgian Source Rock													
**SS=sandstone. MS=mudstone													
***(C=Whole rock major and trace element geochemistry DZC=detrial zircon geochronology HMA=heavy mineral analysis													

Table 2.1 - List of samples and types of analyses performed.

## 2.4.2 - Lancaster G-70

Lancaster G-70 is also an abandoned exploratory well drilled in 1986 in the Southern Flemish Pass Basin (47° 19' 22.34" N, 47° 09' 40.77" W). The well was drilled by Petro-Canada in a water depth of 726 m and to a total depth of 5701 m. The well encountered 2500 m of Tertiary, and 2500 m of Jurassic strata (Figure 2.3). The well was drilled on a Jurassic high, and therefore the Cretaceous section is missing. Reservoir sections encountered in this well were thin, as the more prospective Cretaceous section is missing; however, some thin to moderately thick sandstones were encountered in the Upper Jurassic section which had limited reservoir quality due to cementation (NL Dept. of Mines and Energy, 2003). Lower Tempest sandstones were penetrated from 3764 to 3789 m. Kimmeridgian source rocks were encountered between 3207 and 3761 m, and also from 4736 to 4856 m, designated as the Upper and Lower Kimmeridgian Source Rock units, respectively (CNLOPB, 2007). Samples from this well were taken from the Upper and Lower Kimmeridgian Source Rock units, as well as the interbedded Kimmeridgian Rankin Formation, and Lower Tempest sandstone (Table 2.1). The biostratigraphic reports available for this well are somewhat contradictory, but were used nonetheless to ensure sampling was concentrated on the Kimmeridgian section. Conventional core for this well is limited to the Middle Jurassic section; consequently all of the samples obtained consist of drill cuttings.



Figure 2.3 - Combined gamma ray, lithostratigraphic, and biostratigraphic log for the Lancaster G-70 well.

## 2.4.3 - South Tempest G-88

The South Tempest G-88 well was drilled in 1980 by Mobil and Petro-Canada and is located in the Central Ridge area of the Grand Banks (47° 07' 19.57" N, 47° 57' 26.49" W). It is considered an abandoned oil well and was drilled to a depth of 4675 m in a water depth of 158 m. The well penetrated approximately 2500 m of Tertiary, 500 m of Cretaceous, and 1500 m of Upper Jurassic strata (Figure 2.4). Good reservoir quality sandstones as well as light oil (41° API) are present within the Kimmeridgian Tempest sandstone. This reservoir flowed at 1250 bopd, but was later abandoned. The Tempest sandstones are interbedded with the Upper and Lower Kimmeridgian Source Rock units. These are found between 3730 and 3977 m and 4324 and 4585 m, respectively. Samples from this well were collected from both source rock units, as well as the Tempest sandstones and Rankin Formation (Table 2.1). Similar to the Lancaster G-70 well, biostratigraphic reports were somewhat conflicting with respect to the boundaries of Kimmeridgian and Tithonian stages within the Late Jurassic. Three separate conventional cores are available for this well, from 3828 to 3846 m, 4181 to 4199 m, and 4322 to 4332 m. This allowed for direct sampling of the Upper and Lower Kimmeridgian Source Rock, as well as the Lower Tempest sandstone. Additional samples from this well came from drill cuttings.

Depth	Gamma Ray	Strat	igr	aphic	Units	Biostratigraphic Interpretation			
	0 API 150	CNLOPB (2007)		Riley Geoscience (2005)	McAlpine (1989)	Riley Geoscience (2005)	arch (2002)	li (1990)	
2500m		Banquereau Formation	Banquereau Formation		Banquereau Formation	Tertiary	Robertson Rese	Asco	
		Fortune Bay Shale	Hibernia Formation	Whiterose Shale	Whiterose Shale	Cretaceous		Early Cretaceous Tithonian	
_			Jear	ine d'Arc Em	Fortune Bay Shale	araan	Early Cretaceous	ian	
		ation Kimm Upper Tempest Rock Sandstones	ation	Upper South Tempest	Jeanne d'Arc Formation	kimmeridgian	Late Tithonian	Kimmeridg	
		Rankin Forma Lower Temp. Sandstones	Rankin Form	Lower South Tempest	Rankin Form	Late P	Early to Middle Tithonian		
4500m		Lower Kimm. Source Rock		Lower Egret Member	Voyager Formation		Middle to Late Kimmeridgian		
	Core Location								

Figure 2.4 - Combined gamma ray, lithostratigraphic, and biostratigraphic log for the South Tempest G-88 well.

# 2.4.4 - Panther P-52

Panther P-52 is an abandoned exploration well drilled in 1985 by a Husky-led consortium. It is located at 47° 01' 53.01" N, 47° 37' 39.81" W with 191 m of water depth and a total depth of 4203 m. Intersected were approximately 2500 m of Tertiary, 200 m of Cretaceous, and 1400 m of Upper Jurassic strata (Figure 2.5). Potential reservoirs were not encountered in

the Cretaceous section, however two potential reservoirs were penetrated in the Jurassic section including the Upper Tempest Sandstone (2969 – 3256 m) and the Lower Tempest Sandstone (3576 – 3758 m). The Upper and Lower Kimmeridgian Source Rock units were encountered from 3256 to 3566 m, and 3794 to 4003 m, respectively. Samples from this well were collected from both source rock units as well as interbedded Tempest sandstones and Rankin Formation shales (Table 2.1). The majority of these samples were from drill cuttings; however, one section of conventional core was available from 3752 to 3758 m, and a number of samples were taken from this interval as well. Once again, biostratigraphic reports were contradictory regarding the boundaries of the Kimmeridgian and Tithonian stages. However, when combined with lithostratigraphic picks, it was possible to focus sampling on the Kimmeridgian section.


Figure 2.5 - Combined gamma ray, lithostratigraphic, and biostratigraphic log for the Panther P-52 well.

### **Chapter 3 – Core Logging and Sedimentary Petrology**

### 3.1 - Introduction

Prior to sampling, cores from the Upper Jurassic source rock intervals within the studied wells were logged and described. Very little information is available describing the source rocks in the Flemish Pass / Central Ridge area. Therefore, the core logging was completed to understand lithologic and facies variations within the source rocks, and to note any important sedimentary structures or trace and body fossils. Detailed interpretations of the depositional environment of the source rocks throughout the basin, however, were not made, in part due to the scarcity of cores and well coverage in the area, but also because interpretations of this nature are outside the scope of this study. However, the level of marine versus non-marine influence and interpretations of the depositional environment of individual cores will be made and may be useful for the development of provenance and depositional models.

### 3.2 - Baccalieu I-78 – Kimmeridgian Rankin Formation

A conventional core between 4135 and 4153 m was described (Figure 3.1). The basal five metres of the section (4153 - 4148.53 m) are composed predominantly of dark grey mudstones with fine siltstone interbeds. The interbedded siltstones range from about 0.5 to 3 cm thick and they compose about 30% of this basal section. Soft sediment deformation features are typical and scour marks (Figure 3.6A) and load casts are common at the base of the coarser-grained beds. Coarser intervals have abundant mud clasts and minor carbonaceous organic debris. The next two metres of the core (4148.53 - 4146.14 m) are similar to the basal section; however, this section contains two 3–10 cm thick ungraded beds that are dominated by very coarse detritus (Figure 3.6B). Numerous brown concretionary layers ranging from 2–4 cm thick are present here as well. The upper 11 m of the core (4146.14 – 4135 m) possess similar characteristics to the basal section; however, there is a higher proportion (60%) of silt and very fine sand layers. The

thickness of these layers is typically around 0.5 cm. The majority of the layers can therefore be considered laminae. The thickest layers are around 6 cm and are thus considered beds. The muddy interbeds also average about 0.5 cm thick with a maximum thickness of only 2 cm. This interval also contains beds of very coarse detritus as well as a number of concretionary layers. Trace fossils are absent in this core; only a couple of examples of potential burrows were found. Body fossils are also absent.



Figure 3.1: Core Log for the Kimmeridgian Rankin Formation from the Baccalieu I-78 well.

### 3.3 - Panther P-52 – Kimmeridgian Lower Tempest Sandstone

The only conventional core obtained from this well (3757.9 – 3752.4 m) was described (Figure 3.2). This core displays similar characteristics to that of Baccalieu I-78, although this core is slightly coarser grained overall. The basal section (3757.9 - 3756.25 m) is composed of interbedded mudstones and siltstones with about 60% of the beds being mudstones. All the laminae average about 0.5 cm thick, with the maximum bed thickness being about 5 cm. As seen in the Baccalieu I-78 core, abundant soft sediment deformation features were seen here as well as particles of terrestrial plant debris in coarse-grained sections. The overlying section from 3756.25 - 3753.9 m is composed of fine-grained sandstone. Overall, this interval has about 90% sandstone and 10% interbedded mudstone. The mudstone beds are typically less than a centimeter thick, while the sand beds are on average 10 - 15 cm thick. Numerous mud clasts were found within the sandstone intervals. From 3753.9 to 3753.55 m, there is an abrupt change to fine-grained sediments as seen in the basal section. The main difference is that in this interval there are a number of tensional features such as veins, and fractures and slickensides visible on some bedding planes in the shale. The overlying section from 3753.70 to 3752.7 m is composed of thickly bedded, featureless, medium-grained sandstone. A number of minor (~1 mm) veins run vertically through the sandstone. The top of this core (3752.7 - 3752.4 m) consists of interbedded mudstones and siltstones as seen in the basal section. Similarly to the Baccalieu I-78 core, trace and body fossils are not present.



Figure 3.2: Core log for the Lower Tempest Sandstone from the Panther P-52 well.

## 3.4 - South Tempest G-88 Lower Kimmeridgian Source Rock

Three conventional core samples were retrieved from the South Tempest G-88 well, the first being from 4332.0 to 4322.1 m (Figure 3.3). These cores are described by DeSilva (1994). This core is located in the Lower Kimmeridgian Source Rock stratigraphic unit. The basal section (4332.0–4328.9 m) consists of interbedded black mudstone, and grey siltstone to finegrained sandstone. The mudstone beds are typically about 1 cm thick, with a maximum of about 5 cm, and make up 80% of this section (Figure 3.6C). The siltstone and fine-grained sandstone laminae are on average 1-2 mm thick with a maximum of 1 cm. These beds made up about 20% of the interval. Soft sediment deformation is common here, as well as load casts. Near the top of the interval is a 2 cm thick concretionary layer. The overlying section from 4328.9 to 4326.6 m is similar to the basal section; however, the ratio of mudstone beds to siltstone and fine-grained sandstone beds is about 50/50. The average lamina thickness in this section is about 3 mm, with a maximum of 3 cm. From 4326.6 to 4323.9 m, the rock returns to a facies similar to the basal section with about 80% mudstone beds and 20% interbedded siltstone and fine-grained sandstone. The top of the core, from 4323.9 to 4322.1 m is similar to the middle section with a mudstone to siltstone and fine-grained sandstone ratio of 50/50. Trace and body fossils are not present in this core.

Grain Size				
Depth	Lithology	Mud Silt C C C	Description	Legend
4322.0m 4323.0m			- Same characteristics as 4328.9m - 4326.6m	Siltstone/Sandstone
— 4324.0m —		✓		Mudstone
— 4325.0m —			- Same as basal section	Concretion
— 4326.0m —				Conglomerate $\sim$ Convolute lamination
4327.0m			- Similar to basal section, with more abundant silty interbeds	<ul> <li>Carbonaceous organic material</li> </ul>
4328.0m			- Some terrestrial plant debris present within this interval	<ul> <li>Load cast/scour mark</li> <li>Concretion</li> </ul>
— 4329.0m — — — —		0 0	- Numerous soft sediment deformation features	Soft sediment deformation
— 4330.0m —			- Load casts as well as flute casts	
			- Concretionary layer	
— 4331.0m — — — —			- Silty layers slightly calcareous	
4332.0m		$\sim$		

Figure 3.3: Core log for the Lower Kimmeridgian Source Rock from the South Tempest G-88 well.

### 3.5 - South Tempest G-88 Lower Tempest Sandstone

The Lower Tempest Sandstone was cored from 4199.0 to 4180.6 m (Figure 3.4). Despite being formally termed a sandstone unit, this particular section was similar to the previously described fine-grained lithologies. The basal section of this core from 4199.0 to 4197.03 m is composed of interbedded mudstone (50%) and siltstone and fine-grained sandstone (50%). Soft sediment deformation is prevalent throughout the core, and load casts are common, as well as beds with erosive bases. In the siltstone and fine-grained sand beds, some carbonaceous debris is present. Several brown, 1 cm thick concretions are present in this section. At 4197.03 m, there is an abrupt change to fine- to medium-grained sandstone. The sandstone is slightly less than 5 m thick and continues until 4192.77 m. It has sub-rounded to rounded grains and is moderately well sorted with abundant visible quartz grains. Scattered muddy lenses ranging from 1 mm to 10 mm thick cut the sandstone. The overlying section from 4192.77 to 4186.87 m consists of interbedded siltstone (65%) and mudstone (35%). Fine-grained sandstone beds are uncommon in this section. The average thickness of silt beds is about 4 cm with the maximum thickness being 10 cm whereas mudstone beds are typically 1 cm thick but may reach 3 cm in thickness. Soft sediment deformation is very prevalent in this section with a 10 cm vertical clastic dike present (Figure 3.6D). The upper portion of the core (4186.87 to 4180.6 m) is more of a mud-dominated succession and has about 80% mudstone to 20% interbedded siltstone. The thickest mudstone beds are around 12 cm thick but average 5 cm thick, and the average silt laminae are 2-3 mm thick with a maximum thickness of about 1 cm. This upper interval possesses 2–3 cm-thick, brown concretionary layers and similar soft sediment deformation features to the previous sections. Trace and body fossils are absent from this whole core.

65



Figure 3.4: Core log for the Lower Tempest Sandstone from the South Tempest G-88 well.

### <u>3.6 - South Tempest G-88 – Upper Kimmeridgian Source Rock</u>

A portion of the Upper Kimmeridgian Source Rock unit was cored from 3845.7 to 3827.7 m (Figure 3.5). Despite being designated as the source rock unit, this core was actually the most coarse-grained of any cores examined. The base of the section from 3845.7 to 3844.38 m is composed of brown to grey fine- to medium-grained sandstone interbedded with thin (1 mm) muddy lenses. Abundant carbonaceous debris is present, as is some soft sediment deformation. The sandstone appears quartz-rich, with sub-rounded grains that are moderately sorted. The overlying interval from 3844.38 to 3842.75 m is defined by slightly finer-grained sediments. Siltstone (60%) is interbedded with abundant mudstone layers (40%). The majority of the beds average 1 cm in thickness but may reach 2-3 cm. Soft sediment deformation is prevalent here and creates confusion when trying to define bed thicknesses and original depositional features (Figure 3.6E). Some load casts are present, however, and a single, 5 mm-thick concretionary bed occurs near the middle of the section. Features from 3842.75 to 3837.1 m are similar to the basal section; however, there is about 40% siltstone, 40% sandstone, and 20% mudstone here, with abundant carbonaceous debris. The top section of the core is composed of fine- to mediumgrained sandstone interbedded with scattered, 1 mm muddy lenses. Carbonaceous debris is very abundant here (Figure 3.6F) and even forms a couple of 1-2 cm-thick coal layers. The sandstone is moderately sorted, with sub-rounded grains, and abundant quartz. Some less significant soft sediment deformation is present here as well. Trace and body fossils are once again absent.



Figure 3.5: Core log for the Upper Kimmeridgian Source Rock from the South Tempest G-88 well.



Figure 3.6: Photographs of various Kimmeridgian cores. Canadian one-dollar coin for scale (diameter = 2.5 cm) (A) Scour marks in the Baccalieu I-78 Rankin Formation core. (B) Granules and small pebbles in a sandstone matrix in Baccalieu I-78 Rankin Formation core. (C) Dark grey laminated mudstone in the South Tempest G-88 Lower Kimmeridgian Source Rock core. (D) Clastic dike in the South Tempest G-88 Lower Tempest Sandstone. (E) Soft sediment deformation in the South Tempest G-88 Upper Kimmeridgian Source Rock. (F) Carbonaceous debris in the Upper Kimmeridgian Source Rock of the South Tempest G-88 well.

## **<u>3.7 - Core Interpretation</u>**

A number of features are ubiquitous throughout the Kimmeridgian core samples from the Baccalieu I-78, Panther P-52, and South Tempest G-88 wells. Before interpreting these features, an understanding of the regional depositional setting is essential. McAlpine (1990) described the depositional setting of the proto-Atlantic Ocean in the Late Jurassic as a restricted, silled basin that was relatively shallow (<200 m).

Bateman (1995) created a depositional model for the laterally equivalent Egret Member in the Jeanne d'Arc Basin which related deposition of dark-brown, laminated, organic-rich shales of the Kimmeridgian Egret Member to high sea level, bottom water anoxia, and pelagic sedimentation of marine organisms. Other facies encountered within the Egret Member include unlaminated, grey-brown shales with lower organic contents, as well as some marlstones, claystones, and sandstones (Bateman, 1995). The unlaminated shales were interpreted to have been deposited during a lowering of sea level, in a more proximal environment (Bateman, 1995). The marlstones and claystones were interpreted to be deposited during lowstands, in an oxidizing environment, and the sandstones via turbidity currents which transported slope and shelf sediments into more basinal environments (Bateman, 1995). During periods of high sea level, while deposition of organic-rich shales took place in the basin centre, the other facies (such as the grey-brown shales or sandstones) may have been deposited near the basin margins (Bateman, 1995). When considering the interpretations of Bateman (1995), it is important to note that pelagic sedimentation of marine organisms cannot be the sole process responsible for the deposition of the organic-rich source rock facies. Since there are a significant proportion of detrital clay minerals within this facies, it would be more appropriate to call them hemipelagic deposits.

Kimmeridgian cores from the Flemish Pass Basin and Central Ridge seem to be slightly different than the facies described in the Jeanne d'Arc Basin by Bateman (1995). In all of the described cores, fine-grained mudstones are interbedded with siltstones and sandstones as well as rare coarser beds containing granules and fine pebbles. The presence of these coarse beds, locally interbedded with mudstones, indicates variable energy conditions. Other important features are the abundant scours, erosive bases, flute casts and load casts. In addition, soft sediment deformation is very common and bioturbation is absent. All of these features indicate these sediments were deposited by turbidity currents in a poorly oxygenated environment. The turbidite interpretation was also preferred by Sinclair (1988), McAlpine (1990) & DeSilva (1994) for the Kimmeridgian Tempest Sandstone. Furthermore, a basinal depositional setting is suggested based on the regional depositional setting (McAlpine, 1990; Bateman, 1995), the lack of bioturbation in described cores, as well as black, laminated shales in the described cores which likely represent background sedimentation between turbidity currents (Figure 3.6). A turbidity current model can account for the presence of sands and gravels in this more basinal environment. Boggs (2006) stated that "the single most important mechanism for transporting sands and gravels to deeper water are high-velocity turbidity currents generated on the shelf or upper slope." In addition, the base of turbidite sequences commonly possess sole markings such as flute and load casts and the turbidites themselves generally lack bioturbation (Boggs, 2006). These are characteristics that all of the described cores share, and therefore the turbidite interpretation is preferred. Soft sediment deformation and convolute lamination are abundant in the described cores and are most commonly found in turbidite successions (Boggs, 2006). These features are typical of high depositional rates (Allen, 1982) which would be expected in submarine fans and other turbidite systems.

Evidently, the depositional environment of these individual cores in the Central Ridge and Flemish Pass Basin is different from that of Kimmeridgian source beds in the Jeanne d'Arc Basin. The presence of turbidites was mentioned by Bateman (1995); however, the main source rock facies was interpreted to be deposited by pelagic sedimentation. It appears the source rock of the Flemish Pass Basin and Central Ridge has a different depositional environment than in the Jeanne d'Arc Basin, while still possessing excellent source rock potential (McCracken, 2000). The different depositional environment; however, appears to be reflected in the type of oil expelled by the source beds. Organic geochemistry (Creaney & Alison, 1987; Fowler et al. 2007) indicates that oils from within Flemish Pass Basin sandstones were derived from a source rock with a greater terrestrial component. This matches well with the abundant terrestrial carbonaceous debris observed in the cores, and the input of terrigenous detritus from turbidity currents originating on the shelf or upper slope. This terrigenous detritus would have diluted the marine component of the source rock, which was more important in the Jeanne d'Arc Basin. If the source rock in the Flemish Pass and Central Ridge is in fact more terrigenous in nature, this is an important consideration for interpreting potential provenance of the unit as well as the basin entry points. Presumably, being in closer proximity to the source terrane would supply more abundant, and more terrigenous, detritus to the basin. The depositional environment of the source rock is another important consideration for provenance, as is the influence of marine vs. nonmarine conditions, as well as the transport distances of the interpreted system that would be incorporated into a paleodrainage and depositional model.

# 3.8 - Thin Section Petrography (Introduction and Methodology)

Polished thin sections of mudstones and interbedded sandstones and siltstones were viewed in transmitted light using a petrographic microscope. Mudstones were classified using a classification diagram from Macquaker & Adams (2003). Sandstones and siltstones were

classified using a classification diagram from Pettijohn (1975) (Figure 3.7). The mudstone classification of Macquaker & Adams (2003) aims to first identify whether the sample is dominated by allochthonous (detrital), autochthonous (productivity-derived), or components with indeterminate origins. If components are predominantly clastic in origin, as are the samples from this study, the relative abundances of sand, silt, and clay are used for classification. According to Macquaker & Adams (2003), this nomenclature is thought to more accurately define the constituents of fine-grained sediments and can describe the variability found within fine-grained sedimentary successions with more precision than previous schemes. Provenance characteristics of mudstones may be difficult to detect due to the fine grain size, and abundant mineralogical changes from weathering, transport and diagenesis. Previous work linking modal composition of sediments to specific tectonic settings and source terranes has been focused on sand-sized sediments (Dickinson & Suczek, 1979; Dickinson & Valloni, 1980). This highlights the necessity when working with fine-grained rocks to evaluate in-situ geochronology as in this thesis as provenance characteristics may be more difficult to detect, and implementing techniques used in sand-sized sediments may not be feasible (i.e., point counting). Framework minerals, however, may give insight into source terranes, and textures or dissolution features may indicate the effect of diagenesis on the sediment composition.

The sandstone classification scheme of Pettijohn (1975) uses the relative percentages of quartz, feldspars, and lithics (QFL) as well as the amount of matrix present to classify sandstones. The QFL proportions are all normalized to 100% before plotting on a ternary classification diagram; proportions of authigenic minerals, pore space, heavy minerals, detrital carbonate grains, micas and matrix are not included. If the sand and mud fractions have similar sources, provenance characteristics may be more easily identifiable in the interbedded sandstone

73

units. First of all, textural and mineralogical maturity can provide information about degree of sedimentary recycling and transport distances. Additionally, the mineralogy of sandstones has been linked to the tectonic affinities of source areas (Dickinson & Suczek, 1979). In quartz-rich sands, however, discriminating between continental block and recycled orogeny affinities may be difficult because of variable inputs of sedimentary lithic grains (Dickinson et al., 1983; Cox and Lowe, 1995b). Furthermore, processes such as weathering, transport, and diagenesis may alter the composition of the sandstone significantly from that of its parent rock, and these factors might not be considered sufficiently in interpretations of tectonic affinity based on modal mineralogy (Cox & Lowe, 1995a; Weltje & Eynatten, 2004). Evidently, this method has its limitations, but may be useful to supplement provenance interpretations from U-Pb detrital zircon geochronology and whole rock geochemistry.



Figure 3.7: Sandstone classification diagram from Pettijohn (1975). Classification is based on modal abundances of quartz grains (Q), feldspar grains (F), and lithic grains (L), as well as the amount of detrital matrix present.

In addition to work with the petrographic microscope, all thin sections were viewed and analyzed on the MLA-SEM. Mineralogical data acquired from this method are also presented with the petrographic results for each sample. The MLA-SEM method is described in Section 2.3.4.

## 3.9 – Mudstone Petrographic Interpretations

## 3.9.1 - Introduction

Thin sections from Kimmeridgian mudstones and interbedded sandstones were analyzed from all available conventional cores. Unfortunately, conventional core is unavailable for a number of the important stratigraphic units. For example, the Baccalieu I-78 well has a conventional core within the Rankin Formation, but none within the Upper or Lower Kimmeridgian Source Rock stratigraphic units. Although this is unfortunate for petrographic work, in the following chapters, cuttings samples were used to provide additional heavy mineral data. Abundant sampling for the purpose of petrographic work was not undertaken since the purpose of this study is focused on heavy mineral and geochemical provenance, and also because of a scarcity of core material. However, the samples obtained are interpreted to be representative of the mudstones or sandstones within that individual core.

### <u>3.9.2 - Baccalieu I-78 – Rankin Formation</u>

A single thin section from a mudstone unit was examined from the Baccalieu I-78 well (4142.2 m depth) which is stratigraphically within the Rankin Formation (CNLOPB, 2011). Core samples from this well did not penetrate the Kimmeridgian Source Rock units. Although just a single mudstone sample is described, this sample is superficially similar to other mudstone beds within this core. As previously mentioned in Section 3.2, this core is composed of interbedded mudstones, siltstones, and fine-grained sandstones. The mudstone beds are dark grey, and laminated and possess similar features throughout the full section.

Although some minor carbonate cement is present (<5%), this thin section is classified as a sand- and clay-bearing, silt-rich mudstone (Macquaker & Adams, 2003; Figure 3.8). The sample is organized into 2 mm-thick silt and very fine sand laminae interlaminated with 2–7 mm-thick clay-rich layers (Figure 3.9A). There is approximately 15% very fine sand, 45% silt, and 40% clay sized material in the thin section. The 2 mm-thick silt and very-fine sand laminae are abundant in quartz and carbonate cement, as well as minor clay minerals and muscovite, minor organic matter, and trace amounts of opaque heavy minerals. Grains are typically subrounded to subangular with an average size of 0.1 mm with the largest grains around 0.2 mm. Muddy layers have abundant clay minerals and organic matter, with minor quartz grains and framboidal pyrite. Body fossils are absent in this thin section and there is no evidence of trace fossils or bioturbation.

MLA-SEM analysis indicates a mineralogy similar to that seen in the petrographic work with abundant quartz and muscovite, and common clay minerals, pyrite, calcite, and organic material (Figure 3.10A). The MLA identified illite and chlorite as two individual clay mineral groups present. As mentioned in Section 2.3.4, some complications exist in identifying finely disseminated grains due to the nature of the MLA spot analysis. However, it is possible to group these minerals into broader groups such as 'fine-grained qtz-clay', 'quartz-felds-mix', and 'finegrained-silicate-carbonate'. A false-colored image generated by the MLA is presented in Figure 3.11A. The false-colored image does not reveal much more than was previously recognized using petrographic techniques; however, the alternating clay-rich and quartz-rich laminae are quite distinct and the compositional differences in these layers are noticeable.

## 3.9.3 - South Tempest G-88 – Upper & Lower Kimmeridgian Source Rock

Mudstone samples from the South Tempest G-88 well were analyzed from two depths (3843.5 & 4322.75 m). These samples are from the Upper Kimmeridgian, and Lower Kimmeridgian Source Rock stratigraphic units, respectively, and are interpreted to be representative of the mudstones within these cores (i.e., mudstones show similar characteristics throughout both core sections). They are classified as silt-bearing, clay-rich mudstones and are similar to the mudstone described from Baccalieu I-78, with a lack of very-fine sand sized grains (Figure 3.8). The sample from 3843.5 m contained 60% clay sized grains and 40% silt sized grains. The sample was divided into 5–10 mm-thick clay-rich laminations and 2–3 mm-thick silty laminations (Figure 3.9B). The silty laminations are rich in quartz grains, muscovite, and

microcrystalline carbonate cement. These grains range from angular to subrounded. The muddy laminations are composed of abundant clay minerals and microcrystalline calcite cement with some organic matter and muscovite and infrequent opaque heavy minerals and quartz grains. The sample from 4322.75 m is very similar, with a mixture of muddy laminae (70%) interbedded with more silty laminae (30%). The sample is finely laminated into alternating ~5 mm-thick clay-rich and silt-rich laminae and possesses a similar mineralogy to the previous sample. The average grain size of the sample is in the clay size range, with the largest grains being about 0.01 - 0.02 mm.

SEM-MLA analysis of these two samples revealed a similar mineralogy to that interpreted from petrographic work (Figure 3.10B, 3.10C). However, although the mineralogy of both samples appeared similar petrographically, the MLA revealed a slight difference in the mineralogy of the finely agglomerated material. The fine-grained material of the Upper Kimmeridgian Source Rock sample is predominantly composed of a mixture of fine-grained quartz and clay, while the finely agglomerated material of the Lower Kimmeridgian Source Rock sample is composed of clay with a mixed silicate-carbonate second component. Illite and chlorite were identified as the most abundant clay minerals in both samples. The false colored images (Figure 3.11B, 3.11C) once again highlight the alternating clay-rich and silt-rich laminae and their compositional differences.



Figure 3.8: Mudstone Classification diagram from Macquaker & Adams (2003). (A) Silt-dominated mudstone; (B) Silt-rich mudstone; (C) Sand-bearing, silt-rich mudstone; (D) Sand and clay-bearing, silt-rich mudstone; (E) Clay-bearing, silt-rich mudstone; (F) Clay-dominated mudstone; (G) Clay-rich mudstone; (H) Silt-bearing, clay-rich mudstone; (I) Sand-bearing, clay-rich mudstone; (J) Sand and silt-bearing clay-rich mudstone; (K) Silt and clay-bearing mudstone; (L) Sand and clay-bearing mudstone; (M) Sand and silt-bearing mudstone; (N) Sand, silt and clay-bearing mudstone. (1) Baccalieu I-78 Rankin Formation sample; (2) South Tempest G-88 Upper Kimmeridgian Source Rock sample.



Figure 3.9: Photomicrographs of mudstone samples under crossed polars. (A) Baccalieu I-78 Rankin Formation; (B) South Tempest G-88 Upper Kimmeridgian Source Rock.



Figure 3.10: Modal Mineralogy (weight %) of three mudstone samples from MLA-SEM analysis. Minerals with less than 0.5 wt. % are not included.



Figure 3.11: False-color images of mudstone samples. Identification of individual minerals here is difficult, but the images demonstrate how the MLA software fully classifies minerals in these fine-grained rocks. (A) Baccalieu I-78 (4142.2m). Most abundant minerals in this sample are quartz, muscovite, a quartz-feldspar mix, and a fine-grained quartz-clay mix. (B) South Tempest G-88 (3843.5m). Most abundant minerals in this sample are a fine-grained quartz-clay mix, muscovite, quartz and a quartz-feldspar mix. (C) South Tempest G-88 (4322.75m). Most abundant minerals in this sample are a fine-grained quartz-clay mix, muscovite, quartz and a quartz-feldspar mix. (C) South Tempest G-88 (4322.75m). Most abundant minerals in this sample are a fine-grained silicate-carbonate mix, muscovite, quartz, and a fine-grained quartz-clay mix.

### 3.10 – Petrographic Interpretations of Siltstones and Sandstones

### 3.10.1 - South Tempest G-88 – Upper Kimmeridgian Source Rock

A single sample from the South Tempest G-88 well (3837.3 m) is an arkosic wacke based on the classification scheme of Pettijohn (1975) (Figure 3.7). Although just one sample was analyzed, it is macroscopically representative of the interbedded sandstones within this section of core. The sample is composed predominantly of quartz, carbonate cement, and a fine clay matrix (Figure 3.12A, Figure 3.12B). Also present are feldspars, lithic fragments, muscovite and minor pyrite and opaque minerals. Albite is the most abundant feldspar present, although some Kfeldspar is present as well. It must be noted, however, that no stain was applied to the thin sections. Therefore, only twin laws were used to distinguish K-feldspar from plagioclase. The grains are subangular to subrounded and moderately well sorted. The carbonate cement is fairly abundant (15 %), and appears to have formed early, as there is a significant amount of intergranular volume, as well as few indications of compaction before cementation such as sutured quartz grain contacts or deformed clay-rich lithic grains. The porosity of the sandstone appears very low (3-5%) due to the abundant cementation. Bioturbation from this sample is absent.

SEM-MLA analysis of this sample reveals a similar mineralogy to that described from petrographic observations (Figure 3.13A). In particular, the MLA revealed that the relative feldspar proportions (albite more abundant than K-feldspar) previously identified by petrography were indeed correct, despite no staining in the thin sections. Minerals identified by the MLA which were not observed petrographically include illite and chlorite. The false-colored image (Figure 3.14A) highlights the lack of laminations or bedding in this sample.

### 3.10.2 - Baccalieu I-78 – Rankin Formation

A representative sample of interbedded sandstone from the Baccalieu I-78 well (4135.29 m) was analyzed and also plots as an arkosic wacke using the classification scheme of Pettijohn (1975) (Figure 3.7). The sample is composed of quartz, carbonate cement, feldspars, and lithic fragments (chert and sedimentary rock fragments), with minor shell fragments, and a fine clay matrix (Figure 3.12C). Also present are opaque iron oxides and framboidal pyrite. Feldspars present include albite and K-feldspar, with albite being the dominant feldspar. The grains are subrounded to subangular and moderately sorted. Average grain size is 0.25 mm, but ranges from 0.1 - 0.5 mm. Similar to the G-88 sample, carbonate cement is fairly abundant (20%), occludes porosity, and appears to have formed early due to the lack of sutured grain contacts and preservation of significant intergranular minus-cement porosity. Shell fragments present here are likely remnants of bivalve shells with one example of a crinoid stem. Many are fractured, disaggregated or broken. Bioturbation is absent from this sample.

SEM-MLA analysis of this sample supports the mineralogical observations from petrography (Figure 3.13B). Quartz, carbonate cement (identified by the MLA as calcite), and feldspars are most important. Of the feldsaprs, albite is more abundant than K-feldspar. Illite and chlorite were two clay mineral types identified. The false colored image (Figure 3.14B) shows the lack of laminations or bedding in the sample.

### <u>3.10.3 - Panther P-52 – Lower Tempest Sandstone</u>

At 3754.95 m of the Panther P-52 core, a representative sandstone sample was analyzed and plots as a subarkose (Pettijohn, 1975) (Figure 3.7). The sample is the most coarse-grained of all those sampled. It is composed of quartz, carbonate cement, feldspars, lithic fragments (chert and sedimentary rock fragments), muscovite, and a minor clay mineral matrix (Figure 3.12D). As with the previous samples, albite is more abundant than K-feldspar, although both are present. Grains are subrounded to subangular and poorly sorted. In contrast to previous samples, many of the quartz grains in the sample are fractured. The grain size averages 0.4 mm but ranges from 0.1 - 0.8 mm. Carbonate cement is present at about 10%, although not as abundant as in the previous samples. The cement likely formed before significant compaction; however, minuscement porosity is lower than in previous samples, and long grain contacts indicate some compaction has taken place. Bioturbation is not present in this sample; however, a few minor shell fragments were noted as detritus.

An additional sandstone sample from 3757.5 m was analyzed and possesses a similar composition to the sandstone from 3754.95 m. This sample contains abundant quartz, feldspars (predominantly albite), muscovite, lithic fragments (mostly sedimentary rock fragments), calcite cement, and a clay mineral matrix. The matrix of this sample is greater than 15%, so it is therefore classified as an arkosic wacke (Pettijohn, 1975) (Figure 3.7). Grains present are angular to sub-rounded and range from 0.01 - 0.1 mm with an average of about 0.05 mm. This sample also possesses more abundant calcite cement than previous samples (20%), which is microcrystalline in nature. The cement appears to have preceded compaction and significantly occludes any porosity. No bioturbation is observed in this sample. A 2 cm-long, 0.5 mm-thick shell fragment is present.

Analysis of these two samples by MLA-SEM indicates a similar mineralogy to that observed petrographically, with abundant quartz, albite, carbonate cement (identified by the MLA as calcite), and muscovite (Figure 3.13C, 3.13D). The MLA identified chlorite as the most important clay mineral as well as the presence of some Fe-carbonate minerals such as ankerite and siderite that were less important in previous samples. The false-colored images (Figure 3.14C, 3.14D) help to emphasize the grain size contrast between the coarse-grained sample from 3754.95 m and the finer-grained sample from 3757.5 m. The absence of laminations or bedding is also observed.

## 3.10.4 - South Tempest G-88 – Lower Kimmeridgian Source Rock

The one sample, G-88 (4322.2 m), from the Lower Kimmeridgian Source Rock stratigraphic unit plots as a subarkose (Figure 3.7; Pettijohn, 1975). This sample contains abundant quartz, feldspars (mostly albite), muscovite, and lithic fragments. The lithic fragments are predominantly chert and minor sedimentary rock fragments. The grains are on average 0.05 mm with a maximum of 0.1 mm and are subangular to subrounded. Also present is a minor clay mineral matrix, and abundant microcrystalline calcite cement that makes up about 30% of the sample. The cement occludes any porosity, and appears to pre-date compaction. No bioturbation is present in this sample.

MLA-SEM analysis of this sample supported the mineralogy results from petrographic analysis as quartz, calcite cement, albite, and muscovite are important framework minerals (Figure 3.13E). The MLA identified the presence of ankerite as well as dolomite, and found chlorite to be the most abundant clay mineral. The false colored image (Figure 3.14E) does not reveal any previously unidentified features, although the fine-grained nature of the sample is evident from the image.



Figure 3.12: Photomicrographs of sandstone samples. (A) Sandstone from the South Tempest G-88 Upper Kimmeridgian Source Rock under plane polarized light; (B) Sandstone from the Upper Kimmeridgian Source Rock from South Tempest G-88 under crossed polars; (C) Sandstone from the Rankin Formation of Baccalieu I-78 under crossed polars; (D) Sandstone from Panther P-52 in the Lower Tempest Sandstone under crossed polars.



Figure 3.13: Modal mineralogy (weight %) of five sandstone samples from MLA-SEM analysis. Minerals with less than 0.5 weight % are not included.



Figure 3.14: False-colored images of sandstone samples. (A) South Tempest G-88 (3837.3m). Most abundant minerals in this sample are quartz, calcite, a quartz-feldspar mixture and a fine-grained quartz-clay mixture. (B) Baccalieu I-78 (4135.29m). Most abundant minerals in this sample are quartz, calcite, a quartz-feldspar mixture, and muscovite. (C) Panther P-52 (3754.95m). Most abundant minerals in this sample are quartz, albite, calcite, and a quartz-feldspar mixture. (D) Panther P-52 (3757.7m). Most abundant minerals in this sample are quartz, a quartz-feldspar mixture, calcite, and albite. (E) South Tempest G-88 (4322.2m). Most abundant minerals in this sample are quartz, a quartz-feldspar mixture, calcite, and albite. (E) South Tempest G-88 (4322.2m). Most abundant minerals in this sample are quartz.

### 3.11 - Petrographic Interpretations and Implications for Provenance

## 3.11.1 - Mudstones

Interpreting provenance characteristics from mudstone petrography is challenging due to the fine grain size, and abundant diagenetic mineralogical changes. However, several features in the samples studied were found to provide information about potential source terranes and provenance. Despite the abundant clay minerals, and organic matter in the mudstone samples, there are also silty layers with some detrital grains present. The detrital grains are predominantly quartz and muscovite, which are characteristic of an upper crustal or granitic source. The morphologies of grains, however, are highly variable. Many grains are rounded, but there were also subrounded, subangular, and angular grains as well. This indicates varying provenance and transport histories of the grains. It is difficult to determine whether the mudstone units were derived from previous sedimentary rocks, or are first-cycle crystalline detritus. Likely, these mudstones result from a combination of both recycled sedimentary and first-cycle sources, as the surrounding terranes described in Chapter 1 are composed of a mixture of sedimentary as well as intrusive and extrusive volcanic rocks. It is difficult to determine the level of sedimentary recycling undergone by the grains from these mudstones, as previous studies linking mineralogical maturity (ie. the predominance of quartz grains) to sedimentary recycling (Dickinson & Suczek, 1979; Critelli et al., 2003; Arribas & Tortosa, 2003) all deal with sandstones, and are not necessarily comparable to mudstones. It may also be difficult to link the quartz grain morphology to the level of sedimentary recycling. In sandstones, angular grains indicate a lack of prolonged abrasion, and potential input from first-cycle sources (Blatt & Christie, 1963; Suttner et al., 1981; Cox & Lowe, 1995a). However, in addition to transport distance and level of abrasion, the rate of rounding of quartz is also a function of the particle size (R. Hiscott, personal communication). Silt-sized quartz will always be more angular than sandsized quartz from the same source and with the same transport history (R. Hiscott, personal communication). Therefore, it is difficult to determine if the angularity of the quartz grains is a function of the level of sedimentary recycling, or if it is just a function of the fine-grain size of these samples. Evidently, it is difficult to quantify the proportion of recycled to first-cycle material in these mudstones; however, the following chapters focused on heavy mineral analyses and geochemistry will address the degree of sedimentary recycling.

In mudstones, the type of clay minerals present may also be indicative of source terrains (Weaver, 1989; Potter et al., 2005). Although XRD analyses were not undertaken for these samples, the MLA-SEM modal mineralogy of all samples indicates that illite and chlorite are the most common clay minerals. These clay minerals may be indicative of their original sources; however, due to the burial depth of these samples, it is possible that they are in part diagenetic products. Nonetheless, Potter et al. (2005) state that illite may be derived from igneous, sedimentary, or metamorphic rocks with various weathering intensities and chlorite may be derived from sedimentary or metamorphic rocks that have undergone various degrees of weathering. This, combined with the presence of abundant muscovite grains, indicates a detrital supply from a combination of igneous, metamorphic and recycled sedimentary sources. The presence of abundant muscovite in most samples suggests mica-rich granites were an important supplier of detritus. Rocks of this composition are ubiquitous in the basement terranes that surround the continental margin of Newfoundland such as the Avalon Zone, and Central Mobile Belt. However, rocks of the Meguma Terrane of Nova Scotia and those of the Iberian Peninsula are also characterized by abundant granitic rocks. Generally, these mudstone units appear to be composed of a mixture of recycled and first-cycle material that was sourced from an upper crustal source that undoubtedly includes granites. This terrane could correlate with a number of

90

surrounding basement blocks known in the Grand Banks area. Detrital zircon geochronology and heavy mineral data in the following chapters will address the question of which terrane these Kimmeridgian rocks were most likely derived from.

## 3.11.2 - Sandstones

The sandstone samples provide a significant amount of provenance information. Two of the samples are subarkoses, while the other three are arkosic wackes. In general, they possess similar mineralogies with quartz, feldspars, lithic fragments, muscovite, calcite cement, and a clay mineral matrix. Mineralogically, the samples can be considered submature, as feldspars and lithic fragments make up >10% of these samples. This mineralogy indicates erosion of first-cycle rocks (plagioclase and potassium feldspars) and also recycled sedimentary rocks (sedimentary lithic fragments). Texturally, these sandstones are submature as well. The samples generally have a significant portion of clay matrix and grains tend to be moderately sorted and range from angular to subrounded. This suggests a lack of significant abrasion of grains and a mixture of first-cycle and recycled sedimentary detritus. Shell fragments (bivalves and crinoid stem) are found in the sandstone samples. These fragments have features indicative of transport as they are often fragmented or fractured. Overall, similar to the mudstone units, the sandstones appear to result from the erosion of both first cycle and recycled sedimentary material. Potential source areas, such as the Avalon Zone and Central Mobile Belt of Newfoundland are characterized by a mixture of plutonic and volcanic igneous rocks, as well as abundant sedimentary cover sequences. It is therefore plausible to expect a mixture of recycled and first-cycle grains in the Kimmeridgian rocks of the Flemish Pass and Central Ridge. This would account for the presence of both plagioclase and potassium feldspar grains from first-cycle sources as well as the sedimentary lithic fragments from sedimentary rocks.

91

In terms of reservoir quality, the Kimmeridgian sandstones described here would be low quality reservoir rocks. Porosity is generally very low, and abundant clay material as well as carbonate cement occludes pore spaces. Preserving significant porosity is likely reliant on grain dissolution of feldspars or unstable minerals as the grain shape and sorting of the majority of grains in these samples is inconsistent with abundant primary or intergranular porosity.

### 3.11.3 - Summary

Both mudstone and sandstone units sampled from the various wells display similar provenance characteristics. They were likely derived from a mixture of first-cycle igneous rocks (especially granites), metamorphic rocks, as well as recycled sedimentary rocks. This type of source rock is reasonable given the proximity to the Avalon Zone and Central Mobile Belt of Newfoundland, and to Iberia, where these types of igneous rocks and sedimentary cover sequences are common. It is difficult to determine potential transport distances of the detrital material using the texture and composition as seen in thin sections, because weathering and diagenesis have a large effect on these features. Detrital zircon geochronology and heavy mineral data in subsequent chapters will address this issue more thoroughly.
### <u>Chapter 4 – Whole Rock Geochemistry</u>

#### 4.1 - Introduction

Whole rock geochemical analyses were completed on samples of Upper Jurassic source rocks from the Central Ridge and Flemish Pass Basin. Since a significant amount of core was available over the Late Jurassic interval, all samples were of conventional core. This is preferable as cuttings samples may possess unknown levels of contaminants from drill bit shavings or drilling mud.

Major and trace element geochemical analyses were undertaken to supplement the provenance interpretations as deduced from detrital zircon geochronology (next chapter). Changes in sediment provenance for mudstones can be reflected in their chemical compositions (Hurst and Morton, 2001). Although McLennan et al. (2002) state that a dominant control on the composition of a sedimentary rock is the composition of the source rock from which it was derived, there are additional factors that control the chemistry of a sedimentary rock such as the amount and type of weathering, hydraulic sorting, and diagenesis. These factors will all be addressed in this section.

A combination of both major element and trace element analyses was undertaken to interpret provenance of the Upper Jurassic source rocks studied in this project. Datasets are presented in Appendix B. Sampling and analytical methods are reviewed in Section 2.3.7 as well as 2.3.8. In total, 20 samples were analyzed from the South Tempest G-88 well, 9 from Baccalieu I-78, and four from the Panther P-52 well. The South Tempest G-88 samples were from the Lower Kimmeridgian Source Rock, Lower Tempest Sandstone, and Upper Kimmeridgian Source Rock stratigraphic units. The Baccalieu I-78 samples were all from the Rankin Formation, and the Panther P-52 samples are from the Lower Tempest Sandstone.

#### 4.2 - Major Elements

#### 4.2.1 - Introduction

Major elements are not as useful as trace elements for identifying provenance signatures because they are much more susceptible to post-depositional alteration. Major element suites are most useful in determining how much weathering, and the type(s) of weathering, that a particular sample has undergone (Potter & Maynard, 2005). Several indices, such as the CIA (chemical index of alteration), can be used to quantify the weathering effects.

The CIA is a quantitative measure and is most useful for determining the degree of chemical weathering (Nesbitt & Young, 1982; Fedo et al. 1995). During chemical weathering, labile cations such as Ca<sup>2+</sup>, Na<sup>+</sup>, and K<sup>+</sup> are more easily removed relative to more stable elements such as Al<sup>3+</sup>, and Ti<sup>4+</sup> (Nesbitt & Young, 1982). Elevated CIA values suggest the formation of fine-grained clay minerals such as illite and kaolinite. Conversely, low CIA values indicate an absence of chemical weathering with physical weathering dominant. Physical weathering is most common in cool or arid conditions where source rock degrades into finer-grained material, but in contrast to chemical weathering, the resulting sediment retains the mineralogical and geochemical signature of the source rock (Nesbitt & Young, 1982; 1996). CIA values of around 50 represent fresh, unweathered rock, whereas values between 50 and 100, represent variably chemically weathered rocks. Samples with abundant clay minerals will possess CIA values of 75 or higher (Nesbitt, 2003). Fedo et al. (1995) define the procedures for calculating the CIA. It should be noted that the contributions of CaO from calcite, dolomite, and apatite must be removed from the calculations. For samples in this study, the amount of CaO from silicate rocks became negligible, and therefore a value of 0 weight % was used for CaO.

A useful feature of the CIA ratio is the capability to plot it on a ternary plot and identify weathering trends; i.e., it may be possible to identify a trend from the least weathered to the most weathered samples in the data. Furthermore, by extrapolating such a trend, it may be possible to identify the original composition of the source rock. It may be possible to use this method to supplement provenance interpretations from detrital zircon geochronology for the Upper Jurassic source rocks.

#### 4.2.2 - CIA Results

CIA values were calculated for all 33 samples, of which 25 were fine-grained enough to be considered mudstones. The mudstone samples are from four different stratigraphic units: the Lower Tempest Sandstone, Lower Kimmeridgian Source Rock, Rankin Formation and Upper Kimmeridgian Source Rock. The other eight samples are of the more uncommon, coarsergrained, sandstone beds from the Upper Kimmeridgian Source Rock and Lower Tempest Sandstone stratigraphic units. Results are illustrated on Figures 4.1 and 4.2. The minimum CIA value observed is 73, whereas the maximum is 80; the average is 77. The mudstone samples possess an average CIA value of 77, and the sandstone samples exhibit an average CIA value of 76. Samples from different wells display similar CIA values, and samples from different stratigraphic units also display little variation. There is a slight difference in CIA values within different lithologies, and the mudstones tend to have slightly higher values than the sandstones. Evidently, all these samples underwent weathering in an environment dominated by chemical weathering, converting feldspars to clay minerals. Unfortunately, due to the lack of variation in CIA values, it is difficult to define any weathering trends. In the adjacent Jeanne d'Arc Basin, Dearin (2006) analyzed rocks from the Ben Nevis Formation and was able to identify the original source rock for these sandstones as having been granodioritic in composition using the weathering trends of the CIA diagram (Figure 4.3). Trace element diagrams in the next section

95

proved to be more helpful for the identification of source rock composition(s) for the Upper Jurassic units in this study.



Figure 4.1 - CIA Diagram for Upper Jurassic mudstone samples.



Figure 4.2 - CIA Diagram for Upper Jurassic sandstone samples.



Figure 4.3 - CIA diagram from Dearin (2006).

#### **4.3 - Trace Element Data**

#### 4.3.1 - Introduction

To help ascertain the composition of the source region(s) and determine provenance, a number of trace element plots were examined. Typically, the distribution of trace elements such as Ti, Mn, Zr, Hf, Nb, Sn, Cr, Ni, V, Co, La-Lu, Y, and Sc are sensitive to the nature of their source region (McLennan et al. 2003). These elements have less residence time in seawater and are less susceptible to mobilization during sedimentary processes (McLennan et al. 2003). The next section presents an analysis of the mobility for a number of trace elements, followed by a number of plots that are used to determine the nature of the source region.

## 4.3.2 - Element Mobility

A major issue in sediment provenance geochemistry is determining which elements are least mobile (Fralick, 2003). The composition of the source area can only be accurately estimated if elements present within the resulting sediment have not been significantly mobilized. The elements mentioned in the previous section are considered less susceptible to mobilization and are used where possible in the trace element analysis in this study. Other elements that can be mobilized in certain redox conditions, especially in organic-rich shales include U, Th, V, Mo, Ni and Cr (Quinby-Hunt & Wilde, 1994). MacLean (1990) developed a technique to help determine element mobility during alteration of volcanic rocks and suggests that the method can be used for sedimentary rocks as well. This technique may be useful to define the behavior of elements within the Upper Jurassic samples from the Flemish Pass Basin and Central Ridge. The method is based on the premise that as mobile elements are gained, or lost from the rock, immobile elements will exhibit apparent increases or decreases in concentration (Fralick, 2003). Therefore, when two immobile elements are plotted against one another, a linear trend will be defined with samples plotting progressively closer to, or further away from the origin, as the detritus is depleted in, or enriched in mobile elements (Fralick, 2003). Essentially, if both elements are immobile, the points will define an isochemical line with the origin because the mass loss or gain from the rocks should affect both elements identically (Fralick, 2003).

When this technique was applied to the samples from this study, the majority of trace elements appear to have been immobile to chemical weathering. For instance when Th is plotted vs. Sc, La, TiO<sub>2</sub>, Cr, Ni, and Nb linear trends are defined towards the origin (Figure 4.4A, 4.4B, 4.4C, 4.4D, 4.4E, 4.4F). These elements can therefore be considered to have been immobile, and their signatures within the detritus are likely the same as in their original source rock. The scatter on the plots may be associated with minor differences in provenance. It is also possible that the scatter is due to slight mobilization of these elements in certain samples. However, the degree of this mobilization is clearly not significant, as the general trend with the origin is maintained.

In Figure 4.4G, Th is plotted vs. Co, and a negative trend is defined which is to be expected when a mobile element on the y-axis is plotted vs. an immobile element on the x-axis (Fralick, 2003). Essentially, the mass loss or gain affects Th and Co in different ways. Since Th appears to be immobile based on previous plots, it is interpreted that Co behaved as a mobile element and it should therefore not be used to interpret provenance.

In Figure 4.4H, Th is plotted vs. Zr. There is considerable scatter in the data points, and the sandstone samples define a different trend from that of the mudstone samples. At first glance, this may appear to indicate mobile behavior of Zr. However, when the sandstone and mudstone populations are plotted separately (Figure 4.5A, 4.5B), they both define linear trends. The scatter of points (and the variation in trends between sandstone and mudstone) is interpreted to be a result of hydraulic sorting. This is because hydraulic sorting causes heavy minerals such as

zircon to be enriched in sands and sandstones (Pettijohn et al., 1973). The enrichment of zircon within the sandstone beds results in an enrichment of the element, Zr. Therefore, it is concluded that Zr was immobile, but may exist in higher concentrations in the sandstone beds due to sorting of the mineral zircon. These findings are of particular interest for provenance deductions, as Zr may be either enriched or depleted in interbedded sandstone and mudstone units due to sorting.



Figure 4.4 - Mobility diagrams for trace elements of Upper Jurassic sandstones and mudstones. Samples are from the Upper Kimmeridgian Source Rock, Lower Kimmeridgian Source Rock, Rankin Formation, and Lower Tempest Sandstone stratigraphic units from wells Baccalieu I-78, Panther P-52, and South Tempest G-88.



Figure 4.5 – Mobility diagrams for trace elements Th and Zr for sandstones (A) and mudstones (B). Samples are from the Upper Kimmeridgian Source Rock, Lower Kimmeridgian Source Rock, Rankin Formation, and Lower Tempest Sandstone stratigraphic units from wells Baccalieu I-78, Panther P-52, and South Tempest G-88.

# **4.3.3 – Introduction to Trace Element Provenance Plots**

Following documentation that most trace elements in the Upper Jurassic samples were immobile to chemical weathering, the samples are plotted on trace element plots to ascertain the composition of the principal source region(s). The mudstone (Figure 4.6) and sandstone samples (Figure 4.7) were plotted on separate diagrams due to the previously documented sorting differences.

# 4.3.4 - Zr/Sc vs. Th/Sc Plot

Figures 4.6A and 4.7A are adapted from McLennan et al. (1990) and further described by McLennan et al. (2003). The Zr/Sc vs. Th/Sc plot is used because it allows the distinction of felsic from more mafic detritus, as well as defining amounts of sedimentary recycling. The graph

plots Zr/Sc on the x-axis and Th/Sc on the y-axis. A simple relationship exists between the two ratios in detritus from active margins; the more felsic the detritus, the higher those ratios will be. This is because Th and Zr are both incompatible and thus both ratios will increase with igneous differentiation (McLennan et al. 2003). The plotted location of a sample is therefore a good indication of the type of source material (felsic or mafic). In passive margin settings, however, sedimentary recycling processes are much more important. These processes lead to an increase in the Zr/Sc ratio almost independently from the Th/Sc ratio as the heavy mineral zircon tends to be preferentially concentrated during sorting and sedimentary recycling (McLennan et al. 2003). If samples plot in this region of the diagram, it is likely they were deposited in a passive margin environment where sedimentary recycling processes were dominant. However, this feature may only be noticeable in sandstones, as sedimentary recycling and hydraulic sorting processes are much more important in sandstones (Section 4.3.2).

The mudstone samples in Figure 4.6A plot in the upper region of the diagram with elevated Zr/Sc and Th/Sc ratios, an area that matches an upper crustal composition. There is no significant variation between the plotted locations for samples from the different formations, although the Rankin Formation and Lower Kimmeridgian Source Rock samples exhibit a slightly enhanced upper crustal signature compared to the Lower Tempest Sandstone and Upper Kimmeridgian Source Rock samples, which possess a more mixed signature.

The sandstone samples in Figure 4.7A also plot in the upper region of the diagram with elevated Th/Sc ratios but even higher Zr/Sc ratios than the mudstone samples. Unlike the mudstone samples, these sandstones plot in the area associated with passive margin sedimentary rocks. This includes samples from the Upper Kimmeridgian Source Rock, Lower Kimmeridgian Source Rock, and Lower Tempest Sandstone.

103

## 4.3.5 - Sc - Th - Zr Ternary Plot

A ternary plot of Sc, Th, and Zr from Bhatia & Crook (1986) is also used to decipher provenance (Figure 4.6B, 4.7B). Although the plot is designed for sandstones, it may still be valuable in mudstone samples for detecting quantities of mafic or felsic detritus. However, as shown in the previous sample, significant hydraulic sorting is possible within sandstone samples. This may cause the sandstone and mudstones to plot in different regions of the plot.

In general, samples deposited in oceanic arc environments will typically plot in the field represented by "A" as these samples should contain more Sc than other tectonic environments (Figure 4.6B, 4.7B). Samples deposited in continental island arcs, or active continental margins, will typically plot in the "B" and "C" fields, respectively, as sediments derived from these environments generally contain more Th and Zr than oceanic arc environments. Finally, sediments deposited in passive margins typically exhibit higher Zr/Th ratios (Bhatia & Crook, 1986), plotting towards Zr represented by "D". This plot is based on the premise that the geochemical nature of sedimentary rocks reflects that of their source region and that their source regions contain rock types that are diagnostic of a particular tectonic environment.

The mudstone samples (Figure 4.6B) plot in the middle region of the diagram, mostly in the continental island arc field. The different formations do not display much variation; however, the Lower Kimmeridgian Source Rock and Rankin Formation samples plot further to the right (more Zr-rich) than the Lower Tempest Sandstone and Upper Kimmeridgian Source Rock samples.

The sandstone samples (Figure 4.7B) define a considerably different signature than the mudstone samples, plotting much further towards Zr on the ternary plot. Some of the samples plot in the continental island arc field, whereas a couple of others lie just outside the passive

margin field. There is minimal discrepancy in the plotted location of the different formations, although three samples from the Upper Kimmeridgian Source Rock plot much closer to Zr than any other samples.



Figure 4.6 - Trace element provenance diagrams for Upper Jurassic mudstone samples. Samples from this study include four samples from the Lower Kimmeridgian Source Rock unit; one sample from the Upper Kimmeridgian Source Rock unit; nine samples from the Rankin Formation; nine samples from the Lower Tempest Sandstone unit.



Figure 4.7 - Trace element provenance diagrams for Upper Jurassic sandstones samples. Samples from this study include five samples from the Upper Kimmeridgian Source Rock unit; two samples from the Lower Tempest Sandstone unit; one sample from the Lower Kimmeridgian Source Rock unit.

# 4.3.6 - Th-La-Sc Ternary Plot

The provenance plot presented as Figure 4.6C, 4.7C is from Bhatia & Crook (1986) and uses the fields defined by Cullers (1994). This plot is useful for distinguishing between upper crustal and more mafic detritus. Samples from mafic or amphibolite sources will plot towards the Sc pole. Samples from mixed sources will plot in the middle region of the diagram and samples with felsic sources will plot in the upper left region. Unlike the Sc-Th-Zr/10 ternary plot, this ternary diagram is not able to distinguish passive margin sediments.

The mudstone samples show a fair amount of scatter, with some samples plotting in the field suggesting mixed sources, while others plot in the region indicating metabasic or amphibolite sources (Figure 4.6C). The Upper Kimmeridgian Source Rock samples are scattered, but the Rankin Formation and Lower Kimmeridgian Source Rock samples consistently plot in the field suggesting mixed sources, close to the average composition of the upper continental crust. However, the Lower Tempest Sandstone samples almost all plot further towards the Sc pole, suggesting more mafic sources for this unit.

The sandstone samples almost all cluster in the area of the plot that indicates a mixed source for the detritus (Figure 4.7C). All the samples plot close to the area where the average composition of the upper continental crust plots. All the samples from the four different formations plot in the same area of the diagram.

### <u>Chapter 5 – Heavy Mineral Concentrate Data</u>

#### 5.1 – Introduction

This chapter provides an overview of detrital heavy mineral data for drill cuttings of the fine-grained, Upper Jurassic samples analyzed in this study. Provenance-sensitive heavy mineral ratios are the main focus, although for each sample, the entirety of the heavy mineral suite as well as their associated textures are also described. Data were collected using the Mineral Liberation Analyser – Scanning Electron Microscope (MLA-SEM) at Memorial University; sample preparation techniques and analytical methods are described in Chapter 2. Provenance-sensitive heavy mineral ratios of zircon, monazite, titanite, chromite, and rutile are considered useful for provenance discrimination and assessing sedimentary recycling.

## 5.2 – Heavy Mineral Analysis Methods

Methods for analyzing heavy minerals in this study follow the process outlined by Morton & Hallsworth (1994, 1999). This approach has been applied by numerous authors to sandstones (Hallsworth et al. 2000; Morton et al. 2002; Morton et al. 2005; Lowe et al. 2011) as it employs detrital heavy mineral ratios to "fingerprint" the provenance of a given sample. This "fingerprint" is useful for correlation with provenance signatures from other units and to detect changes in provenance over time. For the method to be effective, it must be shown that the minerals used in the ratios are indeed detrital and not authigenic. This will be demonstrated for the samples presented in this study, primarily based on textures of the heavy minerals. It is also necessary to use heavy minerals that are not significantly differentiated by hydraulic sorting during transport, and are not susceptible to dissolution during diagenesis. Minerals chosen for the ratios therefore have similar densities and are considered stable during burial diagenesis.

The types of ratios used in this study include the monazite-zircon index (MZi: 100 x monazite count/(total monazite + zircon)), the rutile-zircon index (RZi: 100 x rutile count/(total

rutile + zircon)), and the chromite-zircon index (CZi: 100 x chromite count/(total chromite + zircon)). One of the common indexes used (the apatite-tourmaline index) was not used in this study as tourmaline was too uncommon in the studied samples; 15 of the 23 analyzed samples possessed no tourmaline. It was therefore decided to omit this index as the sample size is too small to draw conclusions from, and other indexes could be used.

Another widely used ratio is the ZTR (zircon-tourmaline-rutile) index (Hubert, 1962). This index measures the percentage of zircon, tourmaline and rutile grains among all nonopaque and non-micaceous heavy minerals such as zircon, tourmaline, rutile, apatite, monazite, chromite, and titanite (ZTR= (Z+T+R)/(Z+T+R+A+Mz+Cr+Ti)\*100). The minerals in the denominator of the ZTR ratio are more susceptible to breakdown and dissolution during weathering and transport processes (Morton & Hallsworth, 1999). As the detritus is subject to progressively greater weathering and transport, it will become enriched in the more stable heavy minerals (chemically and mechanically) such as zircon, tourmaline and rutile compared to the unstable heavy minerals (Hubert, 1962). Therefore, this index is considered a great measure of sedimentary recycling (Hubert, 1962). This is the same principle as some of the plots from the bulk rock trace element geochemical data of Chapter 4, particularly the Zr/Sc vs. Th/Sc plot. The heavy mineral data dovetails well with the bulk rock geochemical data, and therefore will be useful in obtaining a thorough understanding of the nature of the detritus and source regions.

One consideration for this study with respect to the ZTR index is that the minerals used in the denominator do not include all of the possible non-opaque, non-micaceous heavy minerals as in the standard definition of the ZTR index. The excluded minerals (such as epidote and olivine) are more unstable under diagenesis and were not included in the denominator of the ZTR index in this study. Since the dissolution of unstable phases and the variable nature of the effects of

109

intrastratial solution are not well understood between these samples from different wells, it was important that only the diagenetically stable minerals listed in the previous paragraph were used for this study. These minerals have been shown to be diagenetically stable up to depths of 4 km (Morton, 1979; Smale & Morton, 1987; Milliken, 1988; Morton & Hallsworth, 1999). This allows for a reasonable comparison of maturity levels and contribution of first-cycle or recycled sources between samples. To ensure diagenetic processes had not significantly affected the heavy mineral suites, textures of the heavy mineral grains were also assessed to identify authigenic features.

Typically, heavy mineral counts for conventional ratios are completed using a fine sand size bracket (63-177 µm) (Lowe et al. 2011; Morton & Hallsworth, 1994). This grain size is typically chosen because within this range, all of the heavy minerals are considered to exist inherently (Morton & Hallsworth, 1994). A 63-177 µm size range is unsuitable for this study of fine-grained mudstones. Totten & Hanan (2007) stated that the median size of heavy minerals in shales is approximately 25 µm less than those found in sandstones. Therefore, placing the low end of the size bracket at 63 µm would eliminate a significant portion of the heavy minerals in the samples studied. In Macquaker & Adams (2003) mudstone classification chart, they indicate a mudstone is any rock with >50% of the grains that are  $<63 \mu m$ . Understanding hydraulic equivalency (Rubey, 1933), it is reasonable to expect heavy minerals within the mudstones and siltstones of this study to be significantly smaller than 63 µm. Therefore, the lower end of the size range used for these samples was 10 µm. Many of these samples were also analyzed for detrital zircon geochronology as well as heavy mineral ratios. Using the LA-ICP-MS method, larger zircons typically result in more accurate analyses as it is easier to avoid any cracks, inclusions or other imperfections in a particular grain. Therefore, to ensure no large zircon grains were eliminated in these samples, the maximum size range was set at 180  $\mu$ m. To determine whether this size bracket is appropriate, and if size sorting was important in the studied samples, the average sizes for each heavy mineral phase from each sample were calculated using MLA data. The average sizes are then expressed in a ratio corresponding to the heavy mineral ratio pairs. For example, the average monazite size is divided by the average zircon size  $(M/Z_{size})$ corresponding to the MZi ratio. If the ratios have values near 1, this means that there is little size difference between the two different mineral phases, and implies that overprints of size sorting are insignificant and that the size fraction used for analysis is appropriate. Ratios are presented in Table 5.1. For all samples, the average  $M/Z_{size}$  is  $0.79 \pm 0.55$ , which indicates monazite grains are generally smaller than zircon grains. However, this is not a significant size difference, and likely means overprints of size sorting are negligible. The same can be said for the R/Zsize (rutile/zircon size) as well as C/Z<sub>size</sub> (chromite/zircon size) ratios, which averaged  $0.97 \pm 0.23$ and  $1.16 \pm 0.42$  respectively. The R/Z<sub>size</sub> and C/Z<sub>size</sub> ratios, however, do not include values from one sample G-70 (4740m) which is considered anomalous with ratios of 10.7 and 3.7, respectively. This sample was therefore excluded from the analysis. It is concluded that the size fraction used  $(10 - 180 \mu m)$  can be considered appropriate. In addition to the table below, grain size distributions for heavy minerals from each sample are presented in Appendix B.

Sample	Formation	Average Msize (um)	Average Zsize (um)	Average Rsize (um)	Average Csize (um)	Sorting Effects (M/Zsize)	R/Z size	C/Zsize
G-70 (3305)	Upper Kimmeridgian Source Rock	26.00	15.50	22.00	15.00	1.68	1.42	0.97
G-70 (3500)	Upper Kimmeridgian Source Rock	26.00	28.00	25.00	29.00	0.93	0.89	1.04
G-70 (4740)	Lower Kimmeridgian Source Rock	-	10.00	107.00	37.00	-	10.70	3.70
G-70 (4820)	Lower Kimmeridgian Source Rock	14.00	17.00	21.00	20.00	0.82	1.24	1.18
G-70 (4200)	Rankin Formation	6.00	32.00	22.00	25.00	0.19	0.69	0.78
G-70 (3715)	Upper Kimmeridgian Source Rock	9.00	30.00	25.00	41.00	0.30	0.83	1.37
G-70 (4405)	Rankin Formation	9.00	37.00	30.00	30.00	0.24	0.81	0.81
P-52 (3600)	Lower Tempest Sandstone	14.00	40.00	40.00	33.00	0.35	1.00	0.83
P-52 (3950)	Lower Kimmeridgian Source Rock	6.00	33.00	22.00	23.00	0.18	0.67	0.70
P-52 (3210)	Upper Tempest Sandstone	21.00	37.00	29.00	30.00	0.57	0.78	0.81
P-52 (3400)	Upper Kimmeridgian Source Rock	37.00	41.00	52.00	45.00	0.90	1.27	1.10
P-52 (3500)	Upper Kimmeridgian Source Rock	54.00	29.00	27.00	38.00	1.86	0.93	1.31
G-88 (3600)	Upper Tempest Sandstone	15.00	25.00	18.00	25.00	0.60	0.72	1.00
G-88 (3700)	Upper Tempest Sandstone	7.00	21.00	20.00	26.00	0.33	0.95	1.24
G-88 (4000)	Rankin Formation	22.00	13.00	13.00	20.00	1.69	1.00	1.54
G-88 (3500)	Upper Tempest Sandstone	28.00	34.00	30.00	31.00	0.82	0.88	0.91
G-88 (4495)	Lower Kimmeridgian Source Rock	-	24.00	23.00	21.00	-	0.96	0.88
G-88 (4600)	Rankin Formation	28.00	24.00	31.00	37.00	1.17	1.29	1.54
I-78 (5000)	Lower Kimmeridgian Source Rock	20.00	12.00	10.00	22.00	1.67	0.83	1.83
I-78 (4500)	Upper Kimmeridgian Source Rock	7.00	26.00	26.00	23.00	0.27	1.00	0.88
I-78 (4705)	Upper Kimmeridgian Source Rock	6.00	7.00	10.00	17.00	0.86	1.43	2.43
I-78 (4900)	Rankin Formation	12.00	27.00	27.00	43.00	0.44	1.00	1.59
I-78 (5075)	Lower Kimmeridgian Source Rock	-	13.00	9.00	10.00	-	0.69	0.77
Average						0.79	0.97	1.16
Standard Deviation						0.55	0.23	0.42

Table 5.1 – Average grain sizes of monazite, zircon, rutile and chromite as computed by MLA. Monazite/zircon size (M/Z size), rutile/zircon size (R/Z size), and chromite/zircon size (C/Z size also listed.

A potential drawback of the heavy mineral ratio approach in this study is the inability of the analytical equipment to differentiate between rutile and other  $TiO_2$  minerals such as anatase and brookite. Morton & Hallsworth (1994) proposed that for heavy mineral ratios, only rutile grains be counted, excluding anatase and brookite grains. As the MLA method relies on chemistry for the identification of different mineral phases, it cannot differentiate between detrital rutile and other  $TiO_2$  phases. Therefore, MLA counts of rutile may also include some anatase and brookite. Another potential drawback with this method is that rutile, brookite and anatase can all be found as authigenic phases and are common in sedimentary rocks (Morad, 1986; Pe-Piper et al., 2011). Minerals such as ilmenite or biotite break down and provide Ti ions in solution which contribute to the formation of authigenic  $TiO_2$  minerals (Morad, 1986). The detrital  $TiO_2$  minerals may be difficult to distinguish from diagenetic phases as the detrital grains often have secondary porosity or inclusions. In addition, the authigenic grains may sometimes be fairly homogenous (eg. Morad, 1986; Pe-Piper et al., 2011), particularly when dealing with fine grain sizes such as in this study. Textures of several rutile grains were analyzed in each sample with the aim of identifying the presence of authigenic grains. However, given the caveats mentioned, it is possible that authigenic TiO<sub>2</sub> grains may not have been identified. This is a consideration for the analysis of provenance based on heavy mineral ratios.

Another potential drawback of this approach involves the use of detrital apatite for provenance. The abundance of apatite is affected by chemical weathering as well as provenance. It has been shown that a significant reduction of the proportions of detrital apatite takes place due to weathering during erosion, transport, and alluvial storage (Morton & Hallsworth, 1994). Therefore, ZTR values may be different for two different samples with the same provenance as a result of chemical weathering of apatite. Morton & Hallsworth (1999) suggest that environments with hot, humid climates, and low relief drainage are the most effective in the weathering and removal apatite. However, in arid or semi-arid climates, as well as marine environments, apatite weathering is considered to be less extensive. Samples from this study are interpreted to have been deposited in a marine environment. However, it is possible that apatite may have been depleted on land before being deposited in the marine environment. It is therefore a consideration that ZTR values may be affected by weathering of apatite. An additional issue with apatite is that it can form authigenically as noted by Pe-Piper & Weir-Murphy (2008) and Lowe et al. (2011). Authigenic apatite forms as nodular, porous cements or overgrowths and if present, could affect ratios in which it is included. The authigenic grains can be identified based on texture, and some representative grains from each sample will be noted in this study to ensure grains included in heavy mineral ratios are indeed detrital.

Some additional considerations include the amount of grains necessary for robust heavy mineral ratios as well as the size fraction analyzed. Morton & Hallsworth (1994) discussed the necessary amount of grains to produce accurate data for provenance interpretations and state that a minimum of 100 grains per mineral pair are necessary; although ideally 200 grains should be counted. As shown in Appendix B, significantly more than 200 grains were counted from each rutile-zircon pair for each sample of this study. However, less than 100 grains were counted in several samples from the chromite-zircon and monazite-zircon pairs. This will be taken into consideration when interpreting these ratios. Previous heavy mineral provenance studies (Lowe et al., 2011; Piper et al., 2012; Morton & Hurst, 1995) were focused on the 63-177 µm size fraction of sandstones. As seen in the diagrams in Appendix B, the grain size of heavy minerals from mudstones in this study typically range from 10 to a maximum of 100 µm. An interesting question for consideration in this section is whether the results yielded from mudstone samples are as effective for provenance discrimination as they are in sandstones. The feasibility of using provenance-sensitive heavy mineral ratios in mudstones will be assessed in this study.

### 5.3 - Results

#### 5.3.1 - Upper Kimmeridgian Source Rock

Counts of zircon, tourmaline, rutile, apatite, monazite, chromite, titanite, staurolite and epidote were obtained from seven 5 m thick cuttings intervals from the Upper Kimmeridgian Source Rock. Heavy mineral counts for all samples are shown in Appendix B. Three samples were from the Lancaster G-70 well, from depths of 3305m, 3500m, and 3715m, respectively. In addition, two samples were from the Panther P-52 well (3400 and 3500 m), and two samples from the Baccalieu I-78 well (4500 and 4705 m). A pie chart of proportions of heavy minerals in these samples is presented in Figure 5.1. Evidently, apatite is an important mineral, comprising 7-45% of the total heavy minerals in a given sample. However, in the samples from 3305m and 3715m from the Lancaster G-70 well, the apatite grains have features that indicate many of the grains are authigenic (Figure 5.2). The grains exhibit crude concentric layering (Figure 5.2A), nodular forms, and secondary pores (Figure 5.2B), which are distinctive features of authigenic apatite (Pe-Piper & Weir-Murphy, 2008; Lowe et al. 2011). This is an important consideration for the heavy mineral ratios. The proportion of authigenic to detrital apatite grains is unknown, as both varieties were not systematically counted. Both authigenic and detrital varieties must be present in these two samples, and thus the actual proportion of detrital apatite grains must be lower than the number of grains mapped by the MLA. The presence of authigenic grains may explain the greater proportion of apatite in the sample from 3715 m (Figure 5.1). Detailed investigations into diagenetic changes of these samples are outside the scope of this study, but Pe-Piper & Weir-Murphy (2008) noted that authigenic phosphorite is common in environments with abundant marine organic matter. Abundant P from marine organic matter can then be incorporated into diagenetic phosphorite or apatite. It is not surprising that some of the samples from the Upper Kimmeridgian Source Rock would possess authigenic apatite, as this unit is also rich in marine organic matter (Creaney & Alison, 1987; McCracken, 2000).

Rutile is generally the most abundant heavy mineral in these samples by far, at 40-74%. Based on the observed textures, all of the rutile grains appear detrital in nature; similar to the homogenous rutile grains in Figure 5.3 without any inclusions, secondary pores or crude zoning. However, given the caveats mentioned in Section 5.2, it is possible that authigenic rutile may share these features and may not have been identified here.

In addition to apatite and rutile, the heavy mineral fractions also contain zircon (3-17%), minor monazite (0-1%), minor chromite (0-6%), and minor titanite (1-9%). Tournaline is absent from all the Upper Kimmeridgian Source Rock samples except two samples from the Lancaster

G-70 well (3305m and 3500m), which contained 33% and 10% tourmaline, respectively. Apart from the apatite grains discussed above, all heavy mineral grains in these samples lack the features of authigenic grains such as inclusions, secondary porosity and concentric layering patterns and are thus considered detrital (i.e. Figure 5.3).

The G-70 (3305m) sample possesses an RZi of 93.65, an MZi of 30.91, and a CZi of 11.63. The sample from G-70 (3500m) possesses a similar RZi of 91.71, with slightly different MZi and CZi ratios of 12.94 and 2.63, respectively. The ZTR ratio from this sample is 81.45. The sample from G-70 (3715m) possesses an RZi of 89.70, an MZi of 13.89, and a CZi of 18.42. The ZTR ratios for both the G-70 (3305m) and G-70 (3715m) sample are not included because of the potential influence authigenic apatite may have had on these samples.

The P-52 (3400m) and P-52 (3500m) samples possess similar heavy mineral ratios. RZi ratios are 85.01 and 86.50, MZi ratios 10.53 and 7.34 and CZi ratios 14.53 and 36.48. The ZTR ratios of these samples are 63.18 and 74.73, respectively.

Both the I-78 (4500m) and I-78 (4705m) samples possess very similar heavy mineral ratios. The sample from 4500 m has an RZi of 82.75, an MZi of 6.90, a CZi of 5.26 and a ZTR of 89.94 whereas the 4705m sample has an RZi of 80.11, an MZi of 2.70, a CZi of 2.70 and a ZTR of 87.65.



Figure 5.1 - Pie charts of detrital heavy mineral proportions of samples from the Upper Kimmeridgian Source Rock of the Lancaster G-70, Panther P-52 and Baccalieu I-78 well.



Figure 5.2 - Authigenic apatite grains from samples of the Lancaster G-70 well. Arrows point to interpreted authigenic apatite grains. The image on the left shows an apatite grain with crude concentric layering. The image on the right shows an apatite grain with secondary porosity and nodular forms.



Figure 5.3 - Examples of rutile grains imaged in this study that possess characteristics suggesting a detrital origin. This is based on their overall homogeneity, lack of secondary pores, inclusions and crude zoning. Arrows point to the rutile grains.

#### 5.3.2 - Lower Kimmeridgian Source Rock

Several 5 m interval cuttings samples were collected of the Lower Kimmeridgian Source Rock including one sample from the Lancaster G-70 well (4820m), one sample from the Panther P-52 well (3950m), one sample from the South Tempest G-88 well (4495m) and two samples from the Baccalieu I-78 well (5000m and 5075m). Pie charts of the heavy mineral proportions for these samples are presented in Figure 5.4. Rutile is generally the most abundant heavy mineral, comprising 30-71%. However, in the sample from the P-52 well (3950 m), apatite is the most abundant heavy mineral (34%). In the other samples, apatite is common (7-23%). Titante comprises 2-20% of these samples, while zircon makes up 2-17%. Chromite and monazite are uncommon at 1-2% and 0-1%, respectively. Tourmaline is only present in two samples (G-70 (4820m) and P-52 (3950m)), but it is fairly common at 11% and 27%, respectively. All heavy mineral phases discussed are interpreted to be detrital in nature and exhibit features similar to those in Figure 5.3. However, as discussed in Section 5.2, it is possible authigenic rutile grains are present.

The sample from G-70 (4820m) has an RZi of 93.01, an MZi of 20.00, a CZi of 8.57 and a ZTR of 86.75. The sample from P-52 (3950m) possesses an RZi of 92.83, an MZi of 6.82, a CZi of 18. The ZTR for this sample is fairly low at 59.48. Additionally, the sample from G-88 (4495m) possesses an RZi index of 87.84, an MZi of 0.00, a CZi of 9.26 and a fairly low ZTR of 55.82. The samples from the Baccalieu I-78 well possess fairly similar heavy mineral ratios. The sample from 5000 m has an RZi of 80.41, an MZi of 2.53, a CZi of 5.52, and a ZTR of 87.63. The sample from 5075 m possesses an RZi of 80.61, an MZi of 0.65, a CZi of 7.88 and a ZTR of 88.49.



Figure 5.4 - Pie charts of detrital heavy mineral proportions of sample of the Lower Kimmeridgian Source Rock from Lancaster G-70, Panther P-52, South Tempest G-88 and Baccalieu I-78.

# 5.3.3 - Rankin Formation

Several 5 m interval cuttings samples were collected for analysis from the Rankin Formation. Two samples are from the Lancaster G-70 well from a depth of 4200 and 4405 m. An additional two samples are from the South Tempest G-88 well (4000m and 4600m) and one sample is from the Baccalieu I-78 well (4900m). The heavy mineral proportions in these samples are presented in Figure 5.5. All heavy minerals assessed possess features similar to those displayed in Figure 5.3, suggesting a detrital origin for all heavy mineral phases. There is some potential for the presence of authigenic rutile grains, as discussed in Section 5.2. For the most part, all of these samples show very similar heavy mineral proportions. Rutile is the most abundant mineral in all of the samples (61-68%), followed by apatite (10-17%). Other common heavy minerals include zircon (8-13%), and titanite (4-11%). Chromite comprises just 1% of the total heavy minerals in samples G-70 (4200m), G-88 (4000m) and G-70 (4405m). However, in samples G-88 (4600m) and I-78 (4900m), chromite comprises 10% and 5% of the total heavy minerals, respectively. Monazite comprises just 0-1% in all samples and tourmaline is absent in all of these samples.

The sample from G-70 (4200m) possesses an RZi of 86.93, an MZi of 6.12, a CZi of 9.80 and a ZTR of 77.19. The sample from G-70 (4405) m has an RZi of 88.28, an MZi of 14.77, a CZi of 7.41 and a ZTR of 75.50. The samples from the South Tempest G-88 well The G-88 (4000m) sample possesses an RZi of 83.42, an MZi of 5.95, a CZi of 4.24 and a ZTR of 81.73. The RZi for the G-88 (4600m) sample is 88.85, the MZi is 3.39, the CZi is 53.28 and the ZTR is 75.84. The I-78 (4900m) sample has an RZi of 88.87, an MZi of 10.94, and a CZi of 41.24. The ZTR for this sample is 68.67.



Figure 5.5 - Pie charts of detrital heavy mineral proportions of samples of the Rankin Formation from Lancaster G-70, South Tempest G-88 and Baccalieu I-78.

### 5.3.4 - Upper Tempest Sandstone (Panther P-52)

Heavy mineral counts were obtained from 5 m cuttings intervals of the Upper Tempest Sandstone from the Panther P-52 well (3210m) and the South Tempest G-88 well (3500m, 3600m, and 3700m). A pie chart of the heavy mineral proportions for these samples is available in Figure 5.6. Rutile is the most abundant heavy mineral in all samples except the Panther P-52 (3210m) sample. It comprises 65-75% of the South Tempest samples but only 34% of the Panther P-52 (3210m) sample. Zircon is the most abundant mineral in the P-52 (3210m) sample at 61%. It comprises 9-12% of the South Tempest G-88 samples. Other heavy minerals in all samples include apatite (3-15%), chromite (1-4%), monazite (0-1%) and titanite (<1-4%). Once again, all grains assessed possess features similar to those in Figure 5.3, suggesting the contribution of authigenic heavy minerals to these counts is negligible. However, the contribution of authigenic grains to rutile counts is possible as discussed in Section 5.2.

The heavy mineral ratios of the P-52 (3210m) sample include an RZi of 35.74, a MZi of 2.20, a CZi of 2.20, and a ZTR of 94.18. For the South Tempest G-88 well, the sample from 3500 m has an RZi of 86.12, an MZi of 2.53, a CZi of 6.76 and a ZTR of 86.71. The sample from 3600 m possesses an RZi of 88.89, an MZi of 10.71, a CZi of 21.88 and a ZTR of 83.03 while the sample from 3700 m possesses an RZi of 85.88, an MZi of 3.92, a CZi of 27.94 and a ZTR of 76.10.



Figure 5.6 - Pie charts of detrital heavy mineral proportions of samples from the Upper Tempest Sandstone from Panther P-52 and South Tempest G-88.

## 5.3.5 - Lower Tempest Sandstone (Panther P-52)

One 5 m interval cuttings sample was collected from the Lower Tempest Sandstone of the Panther P-52 well from a depth of 3600 m. A pie chart of the heavy mineral proportions is presented in Figure 5.7. All heavy minerals of this sample possess features similar to those shown in Figure 5.3, suggesting that detrital rutile is most important in this sample. As with other samples, there is a chance some authigenic rutile grains were not identified as discussed in Section 5.2. Rutile is the most abundant heavy mineral, representing 32% of the total heavy mineral counts. This is followed by apatite (23%), tourmaline (15%), titanite (4%), zircon (3%), chromite (2%), and monazite (<1%).

Heavy mineral ratios for this sample include an RZi of 93.01, an MZi of 12.20, a CZi of 46.27 and a ZTR of 63.14.



Figure 5.7 - Pie charts of detrital heavy mineral proportions of sample from the Lower Tempest Sandstone of the Panther P-52 well.

### 5.4 - Heavy Mineral Ratio Diagrams

Plots of heavy mineral ratios are presented in Figure 5.8. Figure's 5.8A, 5.8B, and 5.8C are scatter plots containing all combinations of RZi, MZi and CZi values, and Figure 5.8D is a plot of the ZTR index values for each sample arranged horizontally by formation. Figure 5.9 shows the same plots as Figure 5.8, but with averaged heavy mineral indexes from each formation with standard error bars. These plots are not intended to pinpoint precise source terranes, but are considered useful for provenance discrimination and providing a provenance "fingerprint" for a particular formation.

#### 5.4.1 - Observations

The first plot (Figure 5.8A) has the MZi (monazite-zircon index) on the x-axis and the RZi (rutile-zircon index) on the y-axis. Samples from all formations possess a fairly high RZi with most samples >80. MZi values tend to be more variable ranging from near zero up to about

30. Using standard errors (Figure 5.9A), none of the formations are really discriminated from one another as most of the standard errors overlap with one of the other formations. The one unit that possesses a slightly different signature is the Upper Tempest Sandstone, which has a much lower average RZi, and lower MZi values in general. However, this feature is the result of a single outlier sample with a very low RZi and MZi value which may not be representative of the formation as a whole. In addition, the standard error for the Upper Tempest Sandstone samples is fairly large, and does overlap with the other formations. It is difficult to draw any meaningful conclusions from the Lower Tempest Sandstone as only one sample was available from this unit. However, this one sample plots in a similar region to points for most other formations.

The next plot (Figure 5.8B) shows the CZi (chromite-zircon index) plotted vs. the RZi (rutile-zircon index). Similar to the MZi, CZi values are fairly variable, ranging from near zero to almost 60. Using the standard error plot (Figure 5.9B), all the formations have a broadly similar provenance signature as most of the standard errors overlap with one of the other formations. Once again, the Upper Tempest Sandstone appears to possess a slightly different signature, although this may be attributed to the influence of an outlier sample, and the standard errors for this formation overlap with the other units. The Lower Tempest Sandstone sample plots with a high CZi value, although it is difficult to draw meaningful conclusions as just one sample was available from this unit.

The MZi vs. CZi plot (Figure 5.8C) shows a large scatter. The standard error plot (Figure 5.9C) shows that most formations have similar values, and any individual formation has a standard error that overlaps with that of another. The Lower Tempest Sandstone is fairly anomalous here as the CZi value is much higher than that of any other formation. However, it is

127

once again difficult to say if this is part of a larger trend or if it is anomalous as just one sample was available from the Lower Tempest Sandstone.

The final plot (Figure 5.8D) shows the ZTR values of the various formations. Substantial scatter is present for the Upper and Lower Kimmeridgian Source Rock units, while the Upper Tempest Sandstone and Rankin Formation samples are better constrained. Once again, having only a single sample from the Lower Tempest Sandstone limits the significance of an interpretation of this interval. Overall, looking at the standard error plot (Figure 5.9D), it appears that most of the formations possess a similar average ZTR value in the range of 70-80. However, the average ZTR of the Upper Tempest Sandstone is slightly higher, at 85.



Figure 5.8 - Plots of heavy mineral ratios. (A) MZi vs. RZi, (B) CZi vs. RZi, (C) MZi vs. CZi, (D) ZTR. Samples with authigenic apatite removed from ZTR ratio diagram.


Figure 5.9 - Plots of heavy mineral ratios with standard error bars (1 SE) for the average heavy mineral index value from each formation. (A) MZi vs. RZi, (B) CZi vs. RZi, (C) MZi vs. CZi, (D) ZTR. Samples with authigenic apatite removed from ZTR ratio diagram.

### <u>Chapter 6 – Detrital Zircon Geochronology</u>

#### 6.1 – Introduction

The geochronological analyses for this study were undertaken to define detrital zircon ages for mudstone and interbedded sandstone beds from the Kimmeridgian units of the Central Ridge and Flemish Pass Basin, offshore Newfoundland. Many of the samples consisted of grain mounts of cuttings, whereas others were thin sections taken from conventional core samples. The data will provide direct indications of the age(s) and nature(s) of the source region(s) and may elucidate provenance questions that petrographic techniques are not able to address. Seven samples were analyzed from the Kimmeridgian rocks with approximately 30 to 80 detrital zircons analyzed per sample. The location of the wells sampled from is shown on Figure 1.1. In addition to ages of detrital zircon grains, features such as Th/U, grain sizes, and morphologies will also be described. Taken together these data will be useful for grouping zircon grain populations and interpreting source regions. Although important, zoning patterns were not used as a means of classification. Back scattered electron (BSE) images were taken using the SEM and the majority of grains imaged did not exhibit any zoning since many of the grains were actually just grain fragments or very fine-grained (Figure 6.1). The few grains that did exhibit zoning only possessed two or three different growth zones, which made it difficult to distinguish between types of zoning. Since these grains are detrital, the majority were likely broken in transport. A misinterpretation here would potentially lead to a misclassification of the grain origin. It was therefore decided to eliminate zoning as a means of grain classification. This study employs methods similar to Lowe et al. (2011), and the methods are described in detail in Chapter 2. Geochronological data are presented in Appendix A.

### 6.2 – Quantitative/Qualitative Approaches

U-Pb ages obtained from laser ablation inductively coupled plasma mass spectrometry (LA-ICP-MS) analysis alone can be very diagnostic of provenance, and are particularly useful for constraining paleogeography, and tectonic reconstructions (Fedo et al., 2003). Lowe et al. (2011) demonstrated that source terranes for Upper Jurassic and Cretaceous reservoir sandstones in the Flemish Pass Basin could be pinpointed using this method. This study will expand this previous work into the fine-grained, organic-rich, Kimmeridgian source rocks and Tempest sandstones.

The morphology of zircon grains can indicate the amount of sedimentary recycling that a grain has been subjected to (eg. Lowe et al, 2011; Piper et al, 2012). Grains in this study were classified as first-cycle, or polycyclic based on morphology. First-cycle zircons typically show euhedral to subhedral morphologies. Therefore, grains with angular, or euhedral crystal faces were interpreted as being first-cycle. Grains with rounded, subrounded, or subangular shapes, however, are interpreted to have been derived from older sedimentary rocks and thus are considered polycyclic. There are recognized uncertainties using this technique as rounded grains may also be of metamorphic origin (Hoskin & Schaltegger, 2003) and first-cycle zircons that have been transported long distances may present as rounded grains. In addition, it is possible that polycyclic grains that have not been subject to significant attrition or long distances of transportation may not appear rounded. This method does provide a preliminary means of classifying and distinguishing different zircon populations and, given evidence about the robustness of zircon (although there are exceptions), rounded grains are likely polycyclic.

Other features, such as Th/U, grain surface area, and grain aspect ratios are also important in distinguishing the parent rock type of detrital zircons. For example, igneous zircons typically have Th/U greater than 0.5, whereas metamorphic zircon grains are characteristically more rounded with lower Th/U, and irregular zoning (Lowe et al., 2011). Features such as subhedral morphologies, and high aspect ratios are diagnostic of volcanic zircons (Hoskin & Schaltegger, 2003). These features were recorded for each zircon grain dated to provide a thorough interpretation of the parent rocks and drainage patterns for the Kimmeridgian rocks of the Flemish Pass Basin and Central Ridge.

Grain surface area as well as aspect ratio are two features recorded by the MLA. As many of the samples in this study are polished grain mounts, the surface area recorded for a particular grain may be affected by how far the polishing process cut into the grain. However, to ensure grains were not significantly polished away or even removed, great care was taken in the sample preparation process and some of the aggressive polishing steps were scaled back. Therefore, the number of grains significantly affected by this is likely minimal. In addition, the aspect ratio recorded by the MLA will be affected by the orientation of the grain in the epoxy mount. However, the vast majority of grains would naturally lie along their long axis as opposed to standing on end. It is therefore unlikely that a significant number of grains were affected by this. Despite these caveats, surface area and aspect ratio may provide a useful means of distinguishing groups of zircons when combined with other grain features discussed.



Figure 6.1 - SEM images of zircons demonstrating potential sources of error in classifying zoning types. Grains shown are small and do not display zoning or display insufficient zoning to assess zoning type.

# 6.3 – Data Presentation

U-Pb zircon ages are presented on conventional Concordia plots, as well as, age vs. frequency cumulative probability histograms using the ISOPLOT/Ex program (version 4.15) of Ludwig (2012). Concordia plots, age vs. frequency histograms, Th/U plots, zircon grain surface area plots, and aspect ratio plots are presented with every individual sample. On the Concordia plots, only concordant results are shown, but in Appendix C, Concordia plots are presented that show all the data. Grains that are up to 10% discordant are considered acceptable for detrital studies. Therefore, any grains that were less than 10% discordant are considered concordant in the following text. These plots use <sup>206</sup>Pb/<sup>238</sup>U and <sup>207</sup>Pb/<sup>235</sup>U ages which are plotted with 2σ error ellipses. For the age vs. frequency cumulative probability histograms, if grains are younger than

1.2 Ga, the <sup>206</sup>Pb/<sup>238</sup>U age is plotted against the number of zircons for all concordant grains. If grains are older than 1.2 Ga, the <sup>207</sup>Pb/<sup>206</sup>Pb age is plotted against the number of zircons for all concordant grains. In addition, a cumulative probability curve is presented which helps define age peaks in the samples.

## 6.4 – Baccalieu I-78: Upper Kimmeridgian Source Rock

## 6.4.1 – Results

A cuttings sample from 4500 – 4505m yielded sufficient detrital zircons for analysis. Based on observations of the cuttings, this interval was dominated by fine-grained mudstones with some interbedded siltstone. The sample processing involved separating the sample into three grain size fractions for heavy mineral separation using the hydroseparator. The 48-100µm size fraction was used for the isotope analysis as the smaller size fraction contained very few zircon grains. Of the 37 zircon grains imaged, 33 were ablated and 27 yielded concordant U-Pb ages (Figure 6.2A, Figure 6.2B). Four grains were skipped as they were smaller than the laser spot size of 20 µm. With 27 dated grains, using the method of Vermeesch (2004), there is a 95% confidence that no fraction >0.16 was missed. The analyses are characterized by three primary age groups of zircon grains (Figure 6.2B). The first is a peak of eight Cambrian- to Devonianaged grains (507 - 363 Ma) that comprise 30% of the sample. The peak defined by the cumulative probability plot is at *ca*. 365 Ma (Figure 6.2B) but the mean of the  ${}^{206}$ Pb/ ${}^{238}$ U ages of this group is  $408 \pm 46$  Ma. The second is a major peak of 10 Neoproterozoic-aged grains (552 – 635 Ma) that comprise 37% of the sample. The peak as defined by the cumulative probability plot is *ca.* 625 Ma (Figure 6.1B), but the mean of the  ${}^{206}$ Pb/ ${}^{238}$ U ages of this group of grains is  $598 \pm 29$  Ma. The final major cluster of grains is a group of five zircon grains older than 1 Ga consisting of grains at  $1024 \pm 25$  Ma,  $1222 \pm 36$  Ma,  $1257 \pm 42$  Ma,  $1464 \pm 44$  Ma, and  $1749 \pm 25$  Ma,  $1222 \pm 36$  Ma,  $1257 \pm 42$  Ma,  $1464 \pm 44$  Ma, and  $1749 \pm 25$  Ma,  $1222 \pm 36$  Ma,  $1257 \pm 42$  Ma,  $1464 \pm 44$  Ma, and  $1749 \pm 25$  Ma,  $1222 \pm 36$  Ma,  $1257 \pm 42$  Ma,  $1464 \pm 44$  Ma, and  $1749 \pm 25$  Ma,  $1257 \pm 120$  Ma,  $1257 \pm 120$  Ma,  $1267 \pm 120$  Ma,  $1257 \pm 120$  Ma,  $1267 \pm 120$  Ma,  $1202 \pm 120$  Ma,

30 Ma which comprise 19% of the total sample. Four of the grains are Mesoproterozoic, with one older Paleoproterozoic grain (Figure 6.2B).

In addition, outlier grains of  $529 \pm 17$  Ma,  $661 \pm 18$  Ma,  $822 \pm 20$  Ma, and  $949 \pm 21$  Ma were also present.

Another notable aspect of the dated grains are the Th-U ratios, which range from 0.10 to 1.05 (Figure 6.2C). The Cambrian – Devonian group of grains possess Th/U ranging from 0.18 - 1.05 with an average of 0.47. Grains from the prominent late Neoproterozoic peak have Th/U values from 0.41 to 0.95 with an average of 0.62, while grains from the > 1 Ga group have much lower Th/U with values ranging from 0.10 - 0.50 with an average of 0.29.

The morphology of all dated grains was also documented and may be the most important feature for determining the level of sedimentary recycling and/or the transportation distance (Figure 6.2D). Subangular grains are the most abundant type of grain making up 41% of all those dated. The Cambrian – Devonian group of grains is composed of mostly subangular grains with minor angular, subrounded, and rounded grains present as well. The late Neoproterozoic group of grains are also mostly subangular, however, subrounded and rounded grains are more important here than in the younger Cambrian – Devonian group. In the >1 Ga group of grains, the majority of grains are subrounded and rounded, with only one subangular grain. Evidently, older grains appear to have more rounded morphologies than the younger, euhedral or angular grains. This is evidence that the older grains have been subject to potentially numerous cycles of sedimentation and have been therefore more mechanically abraded.

Surface area of dated grains range from  $854 - 6152 \ \mu m^2$  (Figure 6.2E). Grains from the Cambrian – Devonian group possess surface areas ranging from  $854 - 3178 \ \mu m^2$  with an average

surface area of 2191  $\mu$ m<sup>2</sup>. The late Neoproterozoic grains have surface areas ranging from 1283 – 6152  $\mu$ m<sup>2</sup>, averaging 2939  $\mu$ m<sup>2</sup>. The >1 Ga group of grains is composed of mostly smaller grains, with surface areas ranging from 1719 – 2840  $\mu$ m<sup>2</sup>, and averaging 2273  $\mu$ m<sup>2</sup>.

Aspect ratios of dated grains were also documented and range from 1.04 - 2.91 (Figure 6.2F). The Cambrian – Devonian grains have aspect ratios from 1.11 - 2.91 with an average aspect ratio of 1.62. The grains for the late Neoproterozoic group possess aspect ratios with an average of 1.34 and ranging from 1.04 - 2.04. Values for the > 1 Ga group of grains were similar to the late Neoproterozoic group, and ranged from 1.17 - 1.70 with an average of 1.37.



Figure 6.2 - Graphs for detrital zircons of the Baccalieu I-78 (4500 m) sample. (A) Concordia diagram with detrital zircon ages. (B) Detrital zircon age histogram. (C) Age vs. Th/U. (D) Zircon grain morphology. (E) Age vs. Surface Area. (F) Age vs. Aspect Ratio.



Figure 6.3 - SEM images of detrital zircon grains from each identified age group in the Baccallieu I-78 (4500 m) sample. The 20  $\mu$ m red circle represents location the grain was ablated.

# 6.4.2 – Interpretations

Three major clusters of zircon grains populate the cumulative probability histogram for this sample. The most abundant group of grains is late Neoproterozoic. These grains have morphologies that are angular to rounded, indicating a mixture of grains that are possibly both first-cycle and polycyclic. Variable Th/U, as well as a range of grain sizes also support a mixture of first-cycle and polycyclic sources for the late Neoproterozoic grains. The large grain size of a number of zircons from this group may indicate the importance of plutonic igneous rocks as a source.

The second largest cluster of zircons is the Cambrian – Devonian group. This group is characterized by a mixture of morphologies, with a higher proportion of angular grains than the late Neoproterozoic group. Therefore, polycyclic grains are interpreted to be less important in this group than in the late Neoproterozoic group. However, variable Th/U, and aspect ratios, suggest that there is a mixture of volcanic and plutonic igneous rocks, as well as recycled sedimentary rocks that comprise the source region for this group.

The final group (> 1 Ga grains) is characterized by more rounded morphologies, low Th/U, and smaller grain surface areas and aspect ratios. These characteristics are indicative of polycyclic grains, potentially with some grain input from metamorphic rocks. This is anticipated of older grains such as these, as they have likely been subject to significant reworking.

# 6.5 – South Tempest G-88: Upper Kimmeridgian Source Rock

#### <u>6.5.1 – Results</u>

Several thin sections were prepared from a core sample from the South Tempest G-88 well at 3837.3 m depth. This interval is considered to be within the Upper Kimmeridgian Source Rock (CNLOPB, 2007). This sample is defined as an arkosic wacke, as described in Chapter 3.

Zircons from three thin sections were imaged and dated. Of the 71 zircons imaged, 68 were ablated (three were rejected due to their small size), yielding 56 concordant U-Pb ages (Figure 6.4A, 6.4B). With 56 dated grains, using the method of Vermeesch (2004), there is a 95% confidence that no fraction >0.10 was missed. The zircon populations from this sample are similar to those in the previous sample from the Baccalieu I-78 well. Three major populations of zircons were present. The first was a peak of 11 Cambrian – Devonian aged grains (533 – 405 Ma) that comprises 20% of all dated grains. The cumulative probability plot categorizes a couple of probability peaks, with the larger at ca. 404 Ma and ca. 526 Ma (Figure 6.4B). The average of the  ${}^{206}\text{Pb}/{}^{238}\text{U}$  ages from this group is 476 ± 52 Ma. The second group is a major peak of 20 late Neoproterozoic-aged grains (626 - 544 Ma) which comprises 36% of all grains analyzed. The cumulative probability plot defines a peak at ca. 582 Ma (Figure 6.4B), and the mean of the  $^{206}$ Pb/ $^{238}$ U ages is 594 ± 29 Ma. The third group is composed of 19 grains > 1 Ga (2740 - 970 Ma) that make up 34% of the sample. One grain was actually dated as early Neoproterozoic (970  $\pm 21$  Ma), and although this is not >1Ga, it was included in this group due to its proximity to a group of grains that were dated near 1 Ga. There are six Mesoproterzoic grains in this group, as well as ten Paleoproterozoic grains, and two grains from the Neoarchean (Figure 6.4B). In addition to these main clusters, a couple of minor other groups were noted as well. Two grains were dated at  $281 \pm 8$  Ma and  $341 \pm 8$  Ma, respectively, forming a minor Carboniferous – Permian population. Three grains were dated at  $788 \pm 16$ ,  $789 \pm 18$  Ma, and  $841 \pm 19$  Ma, respectively, defining a minor population of Middle Neoproterozoic grains. A single outlier grain of  $941 \pm 26$  Ma was also dated.

The Th-U ratios vary from 0.11 - 1.24 (Figure 6.4C). The Cambrian – Devonian-aged grains have Th-U ratios ranging from 0.11 - 0.99, averaging 0.49. Grains from the prominent

late Neoproterozoic peak have Th-U ratios ranging from 0.21 - 1.24 with an average of 0.62, and grains from the older, > 1 Ga group have Th-U ratios ranging from 0.21 - 1.01 with an average of 0.61. It is noteworthy that the average of 0.61 for the >1 Ga group is significantly higher than the average for the previous sample from the Baccalieu I-78 well, where the average Th/U for the >1 Ga group was 0.29. The minor group of Carboniferous – Permian grains have Th-U ratios of 0.35 and 1.05, and the group of Middle Neoproterozoic grains has Th-U ratios of 0.24, 0.33, and 0.50.

The key feature of grain morphology is also assessed for the dated grains from this sample (Figure 6.4D). Of all the grains, a subangular morphology was most common as 39% of all dated grains were subangular in shape. Five Cambrian – Devonian grains are subrounded, with four subangular, and two angular grains as well. Late Neoproterozoic grains are predominantly subangular (11 grains), with four angular grains, two subrounded grains, and three rounded grains. The group of > 1 Ga grains are composed primarily of subrounded grains (10 grains), with five rounded and four subangular grains present as well. The two youngest grains dated (Permian – Carboniferous) were both angular and in the three Middle Neoproterozoic grains, two were subangular, and one angular in shape. The most notable feature observed is that grain morphologies are similar to those in the Kimmeridgian Source Rock sample from the Baccalieu I-78 well. The > 1 Ga grains appear to possess much more rounded shapes than the younger grains, indicating more abrasion than the younger grains, probably a reflection of recycling through a number of sedimentary cycles.

Surface areas of dated grains range from  $610 - 3604 \ \mu\text{m}^2$  (Figure 6.4E). Grains from the Cambrian – Devonian group have surface areas ranging from  $610 - 2909 \ \mu\text{m}^2$  with an average of 1651  $\mu\text{m}^2$ . Grains from the prominent late Neoproterozoic group have surface areas ranging from

 $866 - 3210 \ \mu\text{m}^2$  with a mean surface area of 1770  $\ \mu\text{m}^2$ . The group of >1 Ga grains have surface areas ranging from  $1046 - 3604 \ \mu\text{m}^2$  with an average of 1989  $\ \mu\text{m}^2$ . The two Carboniferous – Permian grains have surface areas of 1331 and 1762  $\ \mu\text{m}^2$  and the three Middle Neoproterozoic grains have surface areas of 954, 1015, and 1341  $\ \mu\text{m}^2$ .

Aspect ratios of all dated grains range from 1.04 - 2.73 (Figure 6.4F). The Cambrian – Devonian grains have variable aspect ratios ranging from 1.04 - 2.71 with an average of 1.51. Aspect ratios of grains of the late Neoproterzoic peak are very similar, and range from 1.08 - 2.73 with an average of 1.51. Grains from the > 1 Ga group had slightly smaller aspect ratios in general, with an average of 1.42. In addition, values were much less variable than the younger grains, as the values for the >1 Ga grains range from just 1.15 - 1.88. The two Carboniferous – Permian grains possess aspect ratios of 1.09 and 1.76, while the three Middle Neoproterozoic grains have aspect ratios of 1.42, 1.44 and 1.95.



Figure 6.4 - Graphs for detrital zircons of the South Tempest G-88 (3837.3 m) sample. (A) Concordia diagram with detrital zircon ages. (B) Detrital zircon age histogram. (C) Age vs. Th/U. (D) Zircon grain morphology. (E) Age vs. Surface Area. (F) Age vs. Aspect Ratio.



Figure 6.5 - SEM images of detrital zircon grains from each identified age group in the South Tempest G-88 (3837.3 m) sample. The 20  $\mu$ m circle represents location grain was ablated.

## 6.5.2 – Interpretations

Similar to the Kimmeridgian Source Rock sample from the Baccalieu I-78 well, this sample contains three main groups of detrital zircons. The most abundant grains, the late Neoproterozoic group, are characterized by predominantly subangular grains, variable Th/U, and

variable aspect ratios and surface areas. These features probably indicate a mixture of types of source rocks. These likely include some plutonic and volcanic igneous rocks (based on some high Th/U, and variable surface areas), as well as recycled sedimentary rocks (some rounded grains).

The second most abundant group of grains in this sample is the > 1 Ga grains. These grains have mostly subrounded and rounded shapes, variable Th/U, and surface areas, with small, well constrained aspect ratios. These characteristics indicate that recycled sedimentary rocks was probably an important source for the > 1 Ga group (rounded grain shapes, small aspect ratios). Metamorphic rocks may also have been source rocks, as there are some low Th-U ratios, and metamorphic zircons are known to be rounded as well. However, the Th-U ratios in this sample are considerably larger than those in the Baccalieu I-78 Kimmeridgian Source Rock sample, indicating more of an igneous component in the > 1 Ga grains analyzed in this sample.

The Cambrian – Devonian group of grains possess mostly subrounded and subangular morphologies. As with most other groups, the Th-U ratios are fairly variable, as well as the aspect ratios and overall grain surface areas. It is interpreted that these grains are likely derived from a mixture of igneous rocks (high Th/U, high surface area grains) and recycled sedimentary rocks (subrounded grains, low aspect ratio grains).

The two Carboniferous – Permian grains are both angular in shape, one with a high Th/U and aspect ratio, the other with a low Th/U and aspect ratio. Both grains are near the overall average in surface area. These grains are likely derived from igneous rocks based on their morphology, but not enough information is available on the group to draw conclusions about the Th/U, aspect ratio, or surface area.

Of the three Middle Neoproterozoic grains, two are subangular, and the other is angular in morphology. All of the grains possess Th/U values of 0.5 or below, aspect ratios below 2 and relatively small surface areas. As with the Carboniferous – Permian grains, it is difficult to draw conclusions from features such as the Th/U, aspect ratio, and surface area from relatively few grains, but the angular and subangular morphologies indicate a derivation from igneous rocks.

## 6.6 – Lancaster G-70 – Rankin Formation

#### <u>6.6.1 – Results</u>

A cuttings sample from the Rankin Formation at 4405 – 4410m contained sufficient detrital zircons to be analyzed. Observations from the cuttings indicated this interval was predominantly fine-grained, consisting of mudstones interbedded with minor siltstones and finegrained sandstones. This sample was separated into three grain size fractions for heavy mineral separation using the hydroseparator. The 20 - 48 and  $48 - 100 \mu m$  fractions were the size fractions analyzed as very few zircons were found in the other size fractions. Of the 70 zircon grains imaged, 62 were ablated (eight were rejected as they were less than 20 µm in size). Unfortunately, many of the grains contained abundant <sup>204</sup>Pb, and yielded discordant results. <sup>204</sup>Pb, also known as common lead, is a problem because its' presence in a zircon means that the calculated U-Th-Pb ratios, and hence calculated ages, no longer represent that of the crystallization age (Andersen, 2002). In this sample, of the 62 grains ablated, only 20 were less than 10% discordant. However, a common lead correction was applied to the grains, and many of the previously discordant grains plotted as concordant. The correction was completed using the VizualAge software within the Iolite program (Petrus & Kamber, 2012). Additional details of the correction itself are available in Andersen (2002). Essentially, the Andersen (2002) correction uses an algorithm that assumes that the time of lead loss (if any) can be determined, and that the U/Th ratio of the grain is undisturbed. This method is particularly useful when the measured

abundances of <sup>204</sup>Pb are not recorded or unreliable (Petrus & Kamber, 2012). This is often the case in LA-ICP-MS analyses due to the low natural abundance of <sup>204</sup>Pb and interference from <sup>204</sup>Hg (Petrus & Kamber, 2012). <sup>204</sup>Pb was measured in this study, but as mentioned above, may not provide the most reliable results in LA-ICP-MS analyses. This is likely why the Andersen (2002) correction was so effective in these samples, as this correction does not use the <sup>204</sup>Pb data. After applying the correction, 57 of the 62 ablated grains plotted concordantly. Of these 57 concordant grains, however, only 56 are included in the detrital zircon analysis (Figure 6.6A, 6.6B) as calculated date of the rejected grain was  $112 \pm 5$  Ma, inconsistent with the established Late Jurassic biostratigraphic age of this interval as defined by Robertson Research (2002), a discrepancy of around 40 Ma. Other biostratigraphic reports from Jenkins (1986) and BP Exploration (1991) also date this interval as latest Callovian to earliest Oxfordian (~160 Ma) and Early Kimmeridgian (~157 Ma), respectively. Although a divergence between the biostratigraphic and detrital zircon ages is possible, it is unlikely to be this large. Therefore, the result for this  $112 \pm 5$  Ma detrital zircon grain is discarded. Since this sample is from drill cuttings, it is likely that this zircon grain was derived from higher in the stratigraphic section, from cavings of Cretaceous or younger strata. This interpretation is preferred given that the age of the unit is well established and that only a single grain of  $112 \pm 5$  Ma was found. With 56 dated grains, using the method of Vermeesch (2004), there is a 95% confidence that no fraction >0.10 was missed.

The grains define five prominent clusters: The youngest group is composed of seven Late Devonian – Permian-aged grains (361 - 248 Ma) that make up 13% of all dated grains. These zircons comprise 13% of all dated grains and define two cumulative probability peaks at *ca*. 267 Ma and *ca*. 360 Ma, respectively (Figure 6.6B). The average of the  ${}^{206}$ Pb/ ${}^{238}$ U ages of grains in

this group is  $300 \pm 42$  Ma. Another group consists of 13 Cambrian to Silurian-aged zircons (532 – 431 Ma) which comprises 23% of the sample. This group forms a cumulative probability peak at *ca.* 456 Ma, although there is an additional peak at *ca.* 538 Ma (Figure 6.6B). The average  $^{206}$ Pb/<sup>238</sup>U ages of grains in this group is 488 ± 35 Ma. A group of 11 late Neoproterozoic grains (664 – 548 Ma) comprises 20% of all dated grains. The cumulative probability peak formed by this group is *ca.* 612 Ma (Figure 6.6B) and the average of the  $^{206}$ Pb/<sup>238</sup>U ages of grains in this group of three Middle Neoproterozoic grains (837 – 817 Ma) makes up 5% of the total sample. They form a cumulative probability peak at *ca.* 833 Ma (Figure 6.6B) and have an average  $^{206}$ Pb/<sup>238</sup>U age of 830 ± 9 Ma. The largest group is composed of 19 grains with ages > 1 Ga (2636 – 1017 Ma) and comprises 34% of all grains analyzed. In this group, there are 8 Mesoproterozoic grains, 8 Paleoproterozoic grains and 3 Neoarchean grains. (Figure 6.6B). Two other grains were dated with ages of 545 ± 22 Ma and 539 ± 27. Additionally, one Upper Jurassic grain was dated at 175 ± 9 Ma (Figure 6.6A, 6.6B).

The Th/U of grains from this sample range from 0.06 - 1.6 (Figure 6.6C). The Jurassic grain has a Th/U of 1.27. The Late Devonian to Permian grains have Th-U ratios ranging from 0.3 - 1.31, with an average of 0.75. The Cambrian to Silurian group has Th-U values ranging from 0.06 - 1.15 with an average of 0.64. The late Neoproterozoic grains have Th-U values ranging from 0.3 - 1.19 with an average of 0.64. The Middle Neoproterozoic grains have Th-U values values ranging from 0.29 - 1.12 with an average of 0.58. The > 1 Ga grains have much more variable Th-U values ranging from 0.15 - 1.60 with an average of 0.65.

The most common grain shape here is subangular, with 46% of the grains possessing this morphology (Figure 6.6D). The Jurassic grain is subangular, wheras the Late Devonian to Permian grains are characterized by three angular and four subangular grains. The Cambrian –

Silurian grains possess a wide range of morphologies, with three angular, six subangular, three subrounded and one rounded grain. The Late Neoproterozoic grains are characterized by one angular, five subangular, three subrounded, and two rounded grains. The Middle Neoproterozoic group is composed of one subangular and two subrounded grains. The group of >1 Ga grains is predominantly subrounded (nine grains), with two rounded grains, seven subangular grains, and one angular grain. This group, as was noted with previous samples, was probably subject to numerous sedimentary cycles to produce mostly subrounded and rounded grains. The two ungrouped grains are both subangular.

The surface area of all grains dated ranges from  $650 - 3930 \ \mu\text{m}^2$  (Figure 6.6E). The Jurassic grain possesses a surface are of 752  $\mu\text{m}^2$ . The Late Devonian to Permian grains have surface areas ranging from  $650 - 3863 \ \mu\text{m}^2$  with an average of 1448  $\mu\text{m}^2$ . The Cambrian to Silurian grains possess surface areas ranging from  $673 - 1571 \ \mu\text{m}^2$  with an average of 999  $\mu\text{m}^2$ . Late Neoproterozoic grains are characterized by surface areas ranging from  $886 - 2629 \ \mu\text{m}^2$  with an average of 1496  $\mu\text{m}^2$ . The Middle Neoproterozoic grains all range from  $1079 - 1107 \ \mu\text{m}^2$  with an average of 1094  $\mu\text{m}^2$  while the > 1 Ga grains had variable surface areas ranging from 725  $- 3930 \ \mu\text{m}^2$  with an average of 1618  $\mu\text{m}^2$ . The two ungrouped grains possess surface areas of 1315  $\mu\text{m}^2$  and 1656  $\mu\text{m}^2$ , respectively.

Aspect ratios of dated grains vary from 1.07 - 2.21 (Figure 6.6F). The Jurassic grain possesses an aspect ratio of 1.38. The Late Devonian – Permian grains are characterized by aspect ratios between 1.14 - 1.89 with an average of 1.55. The Cambrian – Silurian grains possess aspect ratios between 1.08 - 1.77 with an average of 1.31. The Late Neoproterozoic grains are characterized by aspect ratios between 1.1 and 1.77 with an average of 1.37 while the Middle Neoproterozoic grains possess aspect ratios ranging from 1.15 - 1.93 with an average of



1.47. The older, >1 Ga grains are characterized by aspect ratios ranging from 1.07 - 2.21 with an average of 1.46. The two ungrouped grains possess aspect ratios of 1.63 and 1.83, respectively.

Figure 6.6 - Graphs for detrital zircons of the Lancaster G-70 (4405 m) sample. (A) Concordia diagram with detrital zircon ages. (B) Detrital zircon age histogram. (C) Age vs. Th/U. (D) Zircon grain morphology. (E) Age vs. Surface Area. (F) Age vs. Aspect Ratio.



Figure 6.7 - SEM images of detrital zircon grains from each identified age group in the Lancaster G-70 (4405 m) sample. 20  $\mu$ m circle represents location grain was ablated.

## 6.6.2 – Interpretations

This sample is composed of five major zircon grain populations. The Late Devonian – Permian grains are characterized by angular and subangular morphologies, Th/U averaging greater than 0.75 and variable surface areas and aspect ratios. Based predominantly on the subangular and angular grain morphologies as well as fairly high Th/U, it is likely that these grains are derived from igneous rocks as first or second cycle sediments.

The Cambrian – Silurian grains are characterized by very variable Th/U and grain morphologies, but generally low aspect ratios and surface areas. Grains with more rounded morphologies, aspect ratios and surface areas are likely polycyclic, but other grains with high Th/U and more angular morphologies are likely first-cycle, and derived from igneous rocks.

Grains of the late Neoproterozoic group possess similar Th/U values to the Cambrian – Silurian grains, and variable grain morphologies, surface areas, and aspect ratios. This suggests a mixed origin for the late Neoproterozoic grains. Many of the grains with more rounded morphologies, low surface areas and aspect ratios are likely derived from sedimentary rocks. The grains with high Th/U and more angular morphologies are likely derived from igneous rocks.

The Middle Neoproterozoic grains are characterized by variable Th/U, two subrounded and one subangular grain, surface areas near  $1100 \ \mu m^2$  and variable aspect ratios. It is difficult to pinpoint the type of source rock based on only three grains; however the relatively small surface areas and subrounded grain morphologies indicate recycled sedimentary rocks are likely important sources of these Middle Neoproterozoic grains. One of the grains possesses a very high Th/U and is likely derived from igneous sources.

The abundant, >1 Ga grains are characterized by mostly subrounded grain morphologies, highly variable Th/U, as well as a wide range of aspect ratios and surface areas. Due to the abundance of rounded and subrounded grain morphologies, it is likely that many of these grains are polycyclic and derived from recycled sedimentary rocks. However, metamorphic rocks may also be important as a source because metamorphic zircon grains may also be rounded with low Th/U ratios.

### 6.7 – Baccalieu I-78 – Rankin Formation (Mudstone Interval)

#### <u>6.7.1 – Results</u>

A sample from conventional core at 4142.2m was used to make several thin sections, which contained sufficient detrital zircons for analysis. This sample was described in Chapter 3 as a sand- and clay-bearing, silt-rich mudstone. 23 zircons from this sample were imaged and ablated, and yielded 20 concordant analyses (Figure 6.8A, 6.8B). With 20 dated grains, using the method of Vermeesch (2004), there is a 95% confidence that no fraction >0.21 was missed. The 20 concordant analyses are defined by similar age abundance peaks as the G-70(4405m) sample. A group of 11 late Neoproterozoic grains are present (553 – 675 Ma) (Figure 6.8B) which comprise 55% of the total sample. This group forms a cumulative probability peak at *ca*. 570 Ma (Figure 6.8B), although the average  $^{206}$ Pb/<sup>238</sup>U age of all grains in this group is 603 ± 41 Ma. There is also a group of seven >1 Ga grains (1155 – 2060 Ma), which comprise 35% of all grains analyzed. Three of the >1 Ga grains are Mesoproterozoic, and the other four are Paleoproterozoic (Figure 6.8B). One Devonian grain (415 ± 17 Ma), and one Middle Neoproterozoic grain (814 ± 30 Ma) are also present (Figure 6.8B).

Th/U of all grains range from 0.13 - 1.24 (Figure 6.8C). The late Neoproterozoic grains have Th/U values ranging from 0.32 - 1.24 with an average of 0.67. The > 1 Ga grains have markedly lower Th/U which range from 0.13 - 0.66 with an average of 0.37. The Devonian grain has a Th/U of 0.43, and the Middle Neoproterozoic grain possess a Th/U of 0.58.

The most common grain morphology of the dated grains is subangular, as 45% of all the grains have this shape (Figure 6.8D). The late Neoproterozoic grains are predominantly subangular (four grains), however three angular grains, three subrounded grains, and one rounded grain is also present. The > 1 Ga grains are characterized by three subangular grains,

two subrounded grains and two rounded grains. It appears these grains have been subject to more attrition than the Neoproterozoic grains, although probably not as significant as the >1 Ga grains in previous samples, as subangular grains are most abundant in this particular sample. The Devonian grain as well as the Middle Neoproterozoic grain both possess subangular morphologies.

Surface areas of all dated grains range from  $589 - 2072 \ \mu\text{m}^2$  (Figure 6.8E). The late Neoproterozoic grains have surface areas ranging from  $589 - 1892 \ \mu\text{m}^2$  with an average of 1207  $\mu\text{m}^2$ . The > 1 Ga grains have slightly larger surface areas ranging from  $931 - 2072 \ \mu\text{m}^2$  with an average of 1438  $\mu\text{m}^2$ . The Devonian grain has a surface area of 826  $\mu\text{m}^2$  while the Middle Neoproterozoic grain possess a surface area of 1397  $\mu\text{m}^2$ .

Aspect ratios of all grains range from 1.04 - 2.17 (Figure 6.8F). The late Neoproterozoic grains are defined by variable aspect ratios ranging from 1.04 - 2.17 with an average of 1.67. Grains >1 Ga possess aspect ratios ranging from 1.15 - 2.11 with an average of 1.46. The Devonian grain has an aspect ratio of 1.31 and the Middle Neoproterozoic grain has an aspect ratio of 1.42.



Figure 6.8 - Graphs for detrital zircons of the Baccalieu I-78 (4142.2 m) sample. (A) Concordia diagram with detrital zircon ages. (B) Detrital zircon age histogram. (C) Age vs. Th/U. (D) Zircon grain morphology. (E) Age vs. Surface Area. (F) Age vs. Aspect Ratio.



Figure 6.9 - SEM images of detrital zircon grains from each identified age group in the Baccalieu I-78 (4142.2 m) sample. 20  $\mu$ m circle represents location grain was ablated.

### 6.7.2 – Interpretations

The most abundant group of zircons in this sample is this late Neoproterozoic group. These grains are characterized by variable Th/U, subangular grain morphologies, variable surface areas as well as a wide range of aspect ratios. As with the late Neoproterozoic grains from previous samples, there is likely a range of parent rock types for these zircons. Plutonic and volcanic rocks are likely important (high Th/U, angular grains) but recycled sedimentary rocks are likely also an important source based on the presence of some subrounded and rounded grains.

The >1 Ga grains are characterized by subangular to rounded grain morphologies, with low Th/U and variable surface areas and aspect ratios. These features are indicative of a derivation from recycled sedimentary rocks (rounded grain morphologies) as well as metamorphic rocks (low Th/U).

The two outlier grains (Devonian & Middle Neoproterozoic) both possess subangular morphologies. The Middle Neoproterozoic grain has a Th/U of 0.58, and was likely derived from an igneous source, while the Devonian grain has a Th/U of 0.43 and may be derived from a metamorphic source, or potentially a recycled sedimentary rock.

### 6.8 – Baccalieu I-78 – Rankin Formation (Sandstone Interval)

#### <u>6.8.1 – Results</u>

A sample was obtained from conventional core at 4135.29m, and several thin sections were made from this sample. The sample is described in Chapter 3, and is termed an arkosic wacke. This sample was analyzed, in addition to the mudstone sample at 4142.2m, because it is of interest to determine if detrital zircon populations are the same in both the fine-grained mudstone beds, as well as the coarser sandstone beds. An important topic in the study on mudstone provenance is the issue of whether interbedded mudstones and sandstones were both derived from the same source (Potter & Maynard, 2005; McLennan et al., 2003). Potter & Maynard (2005) ponder whether muds may be derived from a more distant source whereas sands and silts from a source much closer? McLennan (2003) suggested that this question has received inadequate study and that in deep sea turbidites, many sand-mud pairs within individual Bouma cycles show systematic differences in their trace element compositions which indicates different provenance. Hence, it was of interest for this study to determine if detrital zircons indicate a similar or different provenance for interbedded mud-sand pairs in the Kimmeridgian rocks from

offshore Newfoundland. Both the mudstone (from I-78 (4142.2m)) as well as this sandstone sample from I-78 (4135.29m) were examined to determine whether the detrital zircons indicate a common provenance. 47 zircons from this sample were imaged, and 37 were ablated. Ten were skipped because of their small size ( $<20 \ \mu m$ ). Of these grains, 34 yielded concordant analyses (Figure 6.10A, 6.10B). With 34 dated grains, using the method of Vermeesch (2004), there is a 95% confidence that no fraction >0.14 was missed. The zircon groups are similar to that of the mudstone sample from 4142.2m. The most abundant group of grains is late Neoproterozoic, and 15 grains of this age are present (546 - 674 Ma) comprising 44% of the sample (Figure 6.10B). They form a cumulative probability peak at ca. 598 Ma (Figure 6.10B), and the average of the  $^{206}$ Pb/ $^{238}$ U age of all grains in this group is 611 ± 33 Ma. The second most abundant group is the > 1 Ga grains, which is made up of 12 grains (1084 - 2130 Ma) comprising 35% of all dated grains (Figure 6.10B). The >1 Ga grains include 5 Mesoproterozoic, as well as 7 Paleoproterozoic grains. A small group of 4 Silurian – Devonian grains were also present (370 – 404 Ma) (Figure 6.10B) comprising 12% of the sample. The Silurian – Devonian grains comprise 12% of all concordant grains and form a cumulative probability peak at *ca.* 372 Ma (Figure 6.10B), with an average of the  ${}^{206}$ Pb/ ${}^{238}$ U age of all grains in this group of 395 ± 27 Ma. Three outlier grains of  $683 \pm 42$  Ma,  $862 \pm 37$  Ma, and  $938 \pm 52$  Ma were also dated (Figure 6.10B).

Th/U of all dated grains range from 0.02 - 1.61 (Figure 6.10C). The late Neoproterozoic grains possess values ranging from 0.1 - 1.61 with an average of 0.83. The > 1 Ga grains have values ranging from 0.03 - 0.83 with an average of 0.35. The Silurian – Devonian grains have values ranging from 0.2 - 0.65 with an average of 0.44. The outlier grains of 683, 862, and 938 Ma possess Th/U values of 0.02, 0.37, and 0.36 respectively.

The most common grain morphology of all dated grains is subangular, as 50% of the grains possess this shape (Figure 6.10D). The late Neoproterozoic grains are mostly subangular (eight grains), although four angular grains and three subrounded grains are also present. The >1 Ga grains are predominantly subangular as well (six grains), although two subrounded and four rounded grains were also present in this group. The Silurian – Devonian grains are characterized by three subangular grains and one angular grain. The outlier grains of 683 and 938 Ma are both subrounded while the grain of 862 Ma is angular. Evidently, the grains which have faced the most attrition are the >1 Ga grains, although most here are subangular, which is not consistent with >1 Ga grains from most other samples.

Surface areas of all dated grains range from  $803 - 5555 \ \mu\text{m}^2$  (Figure 6.10E). The late Neoproterozoic grains have values that range from  $1082 - 5251 \ \mu\text{m}^2$  with an average surface area of 1978  $\mu\text{m}^2$ . The group of >1 Ga grains possess much smaller surface areas ranging from  $803 - 2034 \ \mu\text{m}^2$  with an average of  $1252 \ \mu\text{m}^2$ . The Silurian – Devonian grains have surface areas ranging from  $857 - 5555 \ \mu\text{m}^2$  with an average of  $2810 \ \mu\text{m}^2$ . The outlier grains of 683, 862, and 938 Ma possess surface areas of 1894, 1093, and 1471  $\mu\text{m}^2$ , respectively.

Aspect ratios of all grains vary from a minimum of 1.0 to a maximum of 2.7 (Figure 6.10F). The late Neoproterozoic grains possess aspect ratios ranging from 1.21 - 2.19 with an average of 1.56. The >1 Ga grains have aspect ratios ranging from 1.10 - 2.5 with an average of 1.45. The Silurian – Devonian grains possess aspect ratios between 1.07 - 2.43 with an average of 1.68. The outlier grains of 683, 862, and 938 Ma possess aspect ratios of 2.7, 1.0, and 1.46 respectively.



Figure 6.10 - Graphs for detrital zircons of the Baccalieu I-78 (4135.29 m) sample. (A) Concordia diagram with detrital zircon ages. (B) Detrital zircon age histogram. (C) Age vs. Th/U. (D) Zircon grain morphology. (E) Age vs. Surface Area. (F) Age vs. Aspect Ratio



Figure 6.11 - SEM images of detrital zircon grains from each identified age group in the Baccalieu I-78 (4135.29 m) sample. 20  $\mu$ m circle represents location grain was ablated.

# 6.8.2 – Interpretations

The most abundant group of grains in this sample is the late Neoproterozoic group. These grains are characterized by variable, but generally high Th/U, subangular grain morphologies, and variable surface areas and aspect ratios. These features indicate, as seen in previous samples, a range of parent rock types for these grains. High Th/U and angular grains indicate plutonic and

volcanic igneous rocks were likely an important source, while the presence of more rounded grains indicates recycled sedimentary rocks may have also been important sediment sources.

The >1 Ga grains are characterized by low Th/U, low surface areas, variable aspect ratios, and a mixture of grain morphologies from subangular to rounded. Likely, these grains have been subject to more attrition than the late Neoproterozoic grains and are derived from recycled sedimentary rocks (rounded morphologies) as well as metamorphic rocks (low Th/U).

The Silurian – Devonian grains possess low Th/U, angular to subangular grains and variable surface areas and aspect ratios. These features indicate a derivation from metamorphic rocks (low Th/U) as well as plutonic and volcanic igneous rocks (angular grains and variable surface areas).

The outlier grains of 683 and 938 Ma are both likely derived from recycled sedimentary rocks (rounded morphologies), and the grain of 862 Ma may be derived from a volcanic igneous rock due to its angular morphology and small surface area.

# 6.9 – Panther P-52 – Upper Tempest Sandstone

#### <u>6.9.1 – Results</u>

A 5 m thick cuttings sample interval from the Upper Tempest Sandstone at 3210 – 3215m contained sufficient detrital zircons for analysis. Observations of the cuttings indicated that the interval was predominantly composed of fine-grained sandstone with some minor interbedded siltstones and mudstones. 66 zircon grains were imaged. Of those, 52 were ablated, and 29 yielded concordant analyses (Figure 6.12A, 6.12B). With 29 dated grains, using the method of Vermeesch (2004), there is a 95% confidence that no fraction >0.15 was missed. The grain populations are significantly different than previous samples from the Rankin Formation and Upper Kimmeridgian Source Rock. Five major groups of zircons are present. The most

abundant group of grains is the late Neoproterozoic group, and 8 grains of this age are present (545 - 649 Ma) (Figure 6.12B) comprising 28% of all concordant grains. A cumulative probability peak is formed at *ca*. 621 Ma (Figure 6.12B) and the average of the  ${}^{206}$ Pb/ ${}^{238}$ U age of all grains in this group is  $603 \pm 30$  Ma. The next most abundant group consists of 7 Permian – Carboniferous grains (275 – 345 Ma) (Figure 6.12B) comprising 24% of the sample. They form a cumulative probability peak at *ca*. 294 Ma (Figure 6.12B), and the average of the  ${}^{206}$ Pb/ ${}^{238}$ U age of all grains in this group is  $299 \pm 23$  Ma. 6 older grains form a cluster of >1 Ga grains which range from 1026 - 2752 Ma (Figure 6.12B) comprising 21% of all dated grains. The group of > 1 Ga grains is composed of 3 Mesoproterozoic grains, 2 Paleoproterozoic grains, and one Neoarchean grain. Another cluster is composed of 3 grains that are Late Jurassic in age (145 - 150 Ma) (Figure 6.12B) and comprise 10% of all grains. These grains form a cumulative probability peak at *ca*. 147 Ma (Figure 6.12B), and the average of the  ${}^{206}$ Pb/ ${}^{238}$ U age of all grains in this group is  $148 \pm 3$  Ma. The final group is composed of two grains that are Ordovician and Devonian, respectively (Figure 6.12B) and comprises 7% of all dated grains. The grains do not form a major peak, but the average of their <sup>206</sup>Pb/<sup>238</sup>U ages is 425 Ma with a standard deviation of 53 Ma. Other outlier grains present include grains of  $691 \pm 19$ ,  $714 \pm 29$ , and  $743 \pm 21$  Ma.

Th/U of all concordant grains range from 0.17 - 1.04 (Figure 6.12C). The late Neoproterozoic grains possess values from 0.33 - 1.03 with an average of 0.63. The Permian – Carboniferous grains have values ranging from 0.23 - 0.55 with an average of 0.38. The > 1 Ga grains have Th/U values ranging from 0.17 - 0.64 with an average of 0.31. The Jurassic grains possess higher Th/U values ranging from 0.64 - 0.91 with an average of 0.75. The final group consists of two grains of Ordovician and Devonian age which possess high Th/U of 0.78 and 0.88 with an average of 0.83. The outlier grains of  $691 \pm 19$ ,  $714 \pm 29$ , and  $743 \pm 21$  Ma possess Th-U ratios of 0.55, 0.37, and 1.04 respectively.

Of all concordant grains, the most common morphology is angular, as 38% of all grains possess this shape (Figure 6.12D). The late Neoproterozoic grains, however are predominantly subangular (4 grains), with 3 subrounded and 1 angular grain. The Permian – Carboniferous grains, which are a new population not detected in previous samples, are predominantly angular (5 grains) with one subangular and one subrounded grain. These grains are a younger population, and the angular shape of the majority of these grains is evidence they have been subject to less attrition that some of the older populations. This can also be said for the Upper Jurassic grains, which are predominantly angular (2 grains), with one subangular grain. The >1 Ga grains are markedly different, as 4 of these grains are rounded, with 1 subrounded grain, and one angular grain. These grains have clearly been subject to more weathering and erosion than the other grains, as is evidenced by their predominantly rounded shapes. The Ordovician grain is subangular, while the Devonian grain is angular in shape. The ungrouped grains of  $691 \pm 19$ , 714  $\pm$  29, and 743  $\pm$  21 Ma possess subangular, subrounded, and angular morphologies, respectively.

Surface areas of all dated grains range from  $781 - 14985 \ \mu\text{m}^2$  (Figure 6.12E). The late Neoproterozoic grains possess values ranging from  $1330 - 14985 \ \mu\text{m}^2$  with an average of 4105  $\mu\text{m}^2$ . The Permian – Carboniferous grains have surface areas ranging from  $1127 - 6406 \ \mu\text{m}^2$ with an average of 2349  $\mu\text{m}^2$ . The > 1 Ga grains possess smaller surface areas ranging from 781  $- 2789 \ \mu\text{m}^2$  with an average of 1860  $\mu\text{m}^2$ . The upper Jurassic grains have variable surface areas of 1197, 3625, and 8759  $\mu\text{m}^2$  with an average of 4527  $\mu\text{m}^2$ . The Ordovician and Devonian grains have surface areas of 913 and 3317  $\mu\text{m}^2$  respectively. Other ungrouped grains of 691  $\pm$  19, 714  $\pm$ 29, and 743  $\pm$  21 Ma possess surface areas of 2025, 1345, and 1211  $\mu\text{m}^2$ , respectively.
Aspect ratios of all concordant grains vary from 1.01 - 2.03 (Figure 6.12F). The group of late Neoproterozoic grains has aspect ratios ranging from 1.18 - 1.82 with an average of 1.37. The group of Permian – Carboniferous grains possess aspect ratios varying from 1.01 - 2.03 with an average of 1.58. The > 1 Ga grains have lower aspect ratios ranging from 1.07 - 1.39 with an average of 1.22. Upper Jurassic grains possess aspect ratios ranging from 1.17 - 1.65 with an average value of 1.36. The final group consisting of just two grains (Ordovician and Devonian) has aspect ratios of 1.33 and 1.29, respectively. The ungrouped grains of  $691 \pm 19$ ,  $714 \pm 29$ , and  $743 \pm 21$  Ma possess aspect ratios of 1.11, 1.3, and 2.02, respectively.



Figure 6.12 - Graphs for detrital zircons of the Panther P-52 (3210 m) sample. (A) Concordia diagram with detrital zircon ages. (B) Detrital zircon age histogram. (C) Age vs. Th/U. (D) Zircon grain morphology. (E) Age vs. Surface Area. (F) Age vs. Aspect Ratio.



Figure 6.13 - SEM images of detrital zircon grains from each identified age group in the Panther P-52 (3210 m) sample. 20  $\mu$ m circle represents location grain was ablated.

## **6.9.2 – Interpretations**

The late Neoproterozoic grains are the most abundant in this sample. They are characterized by variable Th/U, subangular and subrounded grain morphologies, variable surface areas, and low aspect ratios. These features indicate a mixture of parent rock types, which is consistent with findings from previous samples. Igneous rocks were likely an important source (high Th/U). Variable grain surface areas indicate plutonic and volcanic igneous sources were important. Grain morphologies suggest recycled sedimentary rocks are also a potentially important source.

The Permian – Carboniferous grains are characterized by low Th/U values, variable surface areas and aspect ratios, and predominantly angular grain morphologies. These features are somewhat contradictory as they indicate derivation from different types of source terrains. Most of the grains are angular and exhibit euhedral crystal faces. This suggests the grains are first-cycle and derived from igneous rocks, or potentially second cycle sedimentary grains which have not suffered excessive weathering and erosion. However, the Th-U ratios are almost all below 0.5, which is characteristic of metamorphic rocks. This makes an interpretation difficult, but due to the euhedral nature of the grains, the preferred interpretation is that they are derived from igneous rocks (first-cycle) or from sedimentary rocks that have not undergone significant attrition (second-cycle). As seen in previous samples, it is possible for grains from igneous rocks to possess Th-U ratios below 0.5.

The >1 Ga grains possess low Th/U, rounded grain morphologies, low aspect ratios and low surface areas. These features are comparable to those observed in previous samples, and the interpreted grain origins are also similar. These grains are likely derived from recycled, polycyclic sedimentary rocks (rounded grain morphologies, low aspect ratio & surface areas), as well as metamorphic rocks (low Th/U).

The Upper Jurassic grains are characterized by high Th/U, variable aspect ratios, variable surface areas, and angular grain morphologies. The likely source for these grains is from first-cycle plutonic or volcanic igneous rocks. This is shown specifically in the high Th/U

characteristic of igneous zircons as well as the angular grains shapes which often display euhedral crystal faces.

The Ordovician and Devonian grains both possess high Th/U, subangular to angular morphologies, average surface areas and typical aspect ratios. Therefore, these grains appear to be derived from first cycle igneous rocks (angular morphologies and high Th/U).

The other ungrouped grains appear to have different origins. The  $691 \pm 19$  and  $743 \pm 21$  Ma grains likely have an igneous origin due to their angular to subangular morphology and high Th/U. However, the  $714 \pm 29$  Ma grain is subrounded with a low Th/U. It is therefore interpreted as being derived from recycled sedimentary rocks or potentially metamorphic rocks.

# 6.10 – South Tempest G-88 – Lower Tempest Sandstone

#### <u>6.10.1 – Results</u>

A sample was obtained from a conventional core at 4195.8m. The sample is described as a fine-grained sandstone and contains abundant detrital zircons for analysis. Unlike the other conventional core samples which were made into thin sections, this sample was crushed and separated into three different grain size fractions (20-48 $\mu$ m, 48-100 $\mu$ m, & 100-180 $\mu$ m). It was then taken to the hydroseparator for heavy mineral separation, and heavy mineral fractions were mounted in epoxy for analysis by the MLA/SEM. Zircons were imaged from the three grain size fractions. However, the 48-100 $\mu$ m fraction was chosen for further analysis on the LA-ICP-MS as this fraction contained the most zircon grains that were suitable for analysis. From this grain mount, 102 zircons were imaged, 87 were then ablated, and all 87 yielded concordant results (Figure 6.14A, 6.14B). With 87 dated grains, using the method of Vermeesch (2004), there is a 95% confidence that no fraction >0.07 was missed. These grains fall into four major groups. The first is a group of 57 late Neoproterozoic grains (570 – 682 Ma) which comprise 66% of the total sample. The grains form a cumulative probability peak at *ca*. 613 Ma (Figure 6.14B), while the average of all <sup>206</sup>Pb/<sup>238</sup>U ages of this group is 621 Ma with a standard deviation of 27 Ma. The second group is composed of 16 grains >1 Ga (986 – 2838 Ma) which make up 18% of all dated grains. This group consists of 5 Mesoproterozoic, 8 Paleoproterozoic, 1 Neoarchean and 1 Mesoarchean grain, as well as one grain from the early Neoproterozoic (986 ± 34 Ma) that was close in age to a cluster of Mesoproterozoic grains, and was therefore included within this group. 3) A cluster of 6 Carboniferous – Permian grains (286 – 298 Ma) make up 7% of all concordant grains and form a cumulative probability peak at *ca*. 288 Ma (Figure 6.14B). The average of the <sup>206</sup>Pb/<sup>238</sup>U ages of all grains in this group is 294 Ma with a standard deviation of 5 Ma. A group of 5 Cambrian – Devonian grains (416 – 503 Ma) comprises 6% of all concordant grains. The grains do not form a major cumulative probability peak but the average <sup>206</sup>Pb/<sup>238</sup>U age of all grains were present with <sup>206</sup>Pb/<sup>238</sup>U ages of 541 ± 18, 696 ± 33, and 707 ± 34 Ma.

Th-U ratios of all concordant grains range from 0.08 - 2.03 (Figure 6.14C). The late Neoproterozoic grains possess Th/U values between 0.08 - 1.35 with an average of 0.61. The >1 Ga grains possess Th-U ratios ranging from 0.15 - 2.03 with an average of 0.53. The Permian – Carboniferous grains have Th-U ratios between 0.34 - 0.81 with an average of 0.60 and the Cambrian – Devonian grains possess Th-U ratios ranging from 0.09 - 0.61 with an average of 0.40. The ungrouped grains with  $^{206}$ Pb/ $^{238}$ U ages of  $541 \pm 18$ ,  $696 \pm 33$ , and  $707 \pm 34$  Ma have Th-U ratios of 0.40, 0.93, and 0.12 respectively.

The most common grain morphology of all concordant grains is subangular, as 56% of the grains possess this shape (Figure 6.14D). The late Neoproterozoic grains are mostly subangular (34 grains), although 13 angular grains and 10 subrounded grains are also present.

The >1 Ga grains are composed of six subangular, six subrounded and four rounded grains. As observed in previous samples, these grains tend to have more mature morphologies, indicating more attrition than the younger zircon groups. Of the six Permian – Carboniferous grains, four are subangular, while the other two are angular. The Cambrian – Devonian grains are composed of two subangular grains, two subrounded grains, and one angular grain. The ungrouped grains are all subangular in shape.

The surface areas of all concordant grains range from  $2102 - 8447 \ \mu m^2$ , which is generally larger than grains of previous samples (Figure 6.14E). The late Neoproterozoic grains possess surface areas ranging from  $2130 - 8447 \ \mu m^2$  with an average of  $3291 \ \mu m^2$ . The >1 Ga grains are the smallest of all groups and have surface areas that range between  $2102 - 3635 \ \mu m^2$  with an average of 2656  $\ \mu m^2$ . Permian – Carboniferous grains have surface areas ranging from  $2204 - 4285 \ \mu m^2$  with an average of 2924  $\ \mu m^2$ . The final group of Cambrian – Devonian grains possesses surface areas that range from  $2510 - 3744 \ \mu m^2$  with an average of  $3187 \ \mu m^2$ . The ungrouped grains with  $^{206}$ Pb/<sup>238</sup>U ages of  $541 \pm 18$ ,  $696 \pm 33$ , and  $707 \pm 34$  Ma have surface areas of 3392, 2204, and  $3023 \ \mu m^2$  respectively.

Aspect ratios of all concordant grains vary from a minimum of 1.03 to a maximum of 2.52 (Figure 6.14F). The late Neoproterozoic grains possess aspect ratios ranging from 1.04 - 2.52 with an average of 1.46. The >1 Ga grains have aspect ratios ranging from 1.04 - 1.82 with an average of 1.36. Permian – Carboniferous grains have aspect ratios that range between 1.26 - 1.97 with an average of 1.68. The final group of Cambrian – Devonian grains possesses much smaller aspect ratios between 1.03 and 1.45 with an average of 1.29. The ungrouped grains with  $^{206}$ Pb/<sup>238</sup>U ages of  $541 \pm 18$ ,  $696 \pm 33$ , and  $707 \pm 34$  Ma have aspect ratios of 1.40, 1.66 and 1.34 respectively.



Figure 6.14 - Graphs for detrital zircons of the South Tempest G-88 (4195.8 m) sample. (A) Concordia diagram with detrital zircon ages. (B) Detrital zircon age histogram. (C) Age vs. Th/U. (D) Zircon grain morphology. (E) Age vs. Surface Area. (F) Age vs. Aspect Ratio.



Figure 6.15 - SEM images of detrital zircon grains from each identified age group in the South Tempest G-88 (4195.8 m) sample. 20  $\mu$ m circle represents location grain was ablated.

#### <u>6.10.2 – Interpretations</u>

In this sample, the late Neoproterozoic grains are by far the most abundant and are characterized by variable but generally high Th/U, mostly subangular grain morphologies, variable aspect ratios and variable surface areas. These features were also noted in previous samples, and indicate a mixture of different parent rock types. Igneous parent rocks are indicated by the high Th/U and some angular grain shapes. High surface areas of some of these grains suggest an importance of plutonic igneous rocks. Recycled sedimentary rocks are a probable source of the more rounded grains and metamorphic rocks are also a potential source of grains with low Th/U.

The >1 Ga grains possess low Th/U, a mixture of subangular – rounded grains, low surface areas, and low aspect ratios. As interpreted in previous samples, based on the low surface areas, low aspect ratios and more rounded grains, these grains are interpreted to be derived from recycled sedimentary rocks. However, based on the low Th/U of many grains, many of these grains may also be derived from metamorphic parent rocks.

The Permian – Carboniferous grains are characterized by variable but generally high Th/U, angular to subangular grain morphologies, high aspect ratios, and variable surface areas. These features suggest these grains are likely derived from igneous source rocks (high Th/U, angular grains high aspect ratios), or potentially second-cycle sedimentary rocks (subangular grains).

The Cambrian – Devonian grains possess low Th/U, grains that are angular – subrounded, low aspect ratios and low surface areas. It is likely these grains are derived from a variety of different parent rock types. Low Th-U ratios are indicative of a derivation from

metamorphic rocks, however angular grains suggest derivation from igneous sources and subrounded grains indicate derivation from sedimentary rocks.

The ungrouped grains also likely have different origins. The grain dated at  $696 \pm 33$  Ma is likely derived from an igneous source based on its' high Th/U and subangular morphology. The two other ungrouped grains ( $541 \pm 18$ ,  $707 \pm 34$  Ma) are both subangular but have low Th/U, indicating derivation from recycled sedimentary rocks or potentially metamorphic sources.

## **Chapter 7 - Provenance Interpretations**

#### 7.1 - Interpretations of Geochemical Plots – Weathering Diagrams

An important observation from the CIA diagrams (Figure 4.1; Figure 4.2) is that the mudstone and sandstone samples plot in different regions. Although they have similar CIA values, the mudstone samples plot further to the right of the diagrams, due to greater amounts of  $K_2O$ . This is interpreted to result from increased clay mineral content (particularly illite) within the mudstone samples. Illite is a clay mineral that results from diagenetic reactions at depth. It can be derived from the breakdown of smectite and K-feldspar, or alternatively from the breakdown of kaolinite with the addition of  $K^+$  from outside the system (Sutton & Maynard, 1996). Since illite and clay minerals are more abundant in the mudstone beds, it is expected that these samples would plot closer to the  $Al_2O_3 - K_2O$  line. The grouping of sands and muds into distinct populations is also described by McLennan et al. (2003).

Using the CIA diagram to identify major element trends is useful to indicate the degree of weathering within the Upper Jurassic source rocks for the Flemish Pass and Central Ridge. Evidently, these samples possess high weathering indices (average of 77) indicating chemical weathering was most important for these samples. This is consistent with interpretations of Bateman (1995) for the laterally equivalent Egret Member of the Jeanne d'Arc Basin. Bateman (1995) suggested the climate during deposition of the Egret Member was humid, and subtropical based on clay minerals present identified using XRD. A humid, subtropical climate is supported by the high weathering indices seen in these samples.

It is difficult to identify a source rock for either the sandstone or the mudstone samples, as weathering trends are absent. However, trace element data in the next section will provide more details on the source rock.

#### 7.2 – Interpretations of Trace Element Diagrams

#### 7.2.1 - Zr/Sc vs. Th/Sc Plots

Analysis of mudstone samples using a Zr/Sc vs. Th/Sc plot (Figure 4.6A) revealed some noteworthy provenance characteristics. This plot indicates detritus for these Upper Jurassic units was predominantly from an upper crustal or felsic terrane. Interestingly enough, despite deposition on a rifted margin, the mudstone samples do not plot in the field where passive margin sediments typically lie (McLennan et al. 1990). This suggests that sedimentary recycling processes were not too important in these mudstones, and that the majority of the detritus was likely first-cycle in nature. However, examination of the Zr/Sc vs. Th/Sc plot for the Upper Jurassic sandstone samples (Figure 4.7A) revealed some notably different results from the mudstone samples. The sandstones show a distinctly different signature than the mudstones as they plot in the region of the diagram associated with passive margin sediments. Despite plotting in different areas of the diagram than the mudstones, these sandstones are not interpreted to have a different provenance. The sandstone samples are locally interbedded with the mudstone samples and are not separated by any unconformity, or fault. In addition, both sandstones and mudstones possess relatively high Th/Sc as well as Zr/Sc ratios indicating upper crustal signatures. It is therefore probable that their provenance is not significantly different. The reason the sandstones plot in a different region of the diagram is linked to hydraulic sorting of the heavy mineral zircon. As described in Section 4.3.2, Zr is often more abundant in sandstone beds than mudstones, likely due to the enrichment of the heavy mineral zircon in sands. McLennan (2003) describes how Zr is strongly associated with heavy minerals, and is therefore subject to heavy mineral fractionation during sorting and sedimentary recycling processes. Therefore, it is interpreted that sorting and sedimentary recycling processes acted to enrich Zr in the sandstone samples.

Mudstone samples (Figure 4.6A) from different stratigraphic units appear to have a similar provenance based on this plot, however, the Lower Tempest Sandstone samples plot slightly closer to the average composition of the Bulk Continental Crust, indicating a slightly more mafic component and potentially different provenance for the Lower Tempest Sandstone detritus. Within the sandstone samples (Figure 4.7A), there is no major difference in Th/Sc between the different formations but the Zr/Sc does vary somewhat. This can be directly tied to the amount of sedimentary recycling or hydraulic sorting that the detritus has undergone. Knowing this, it appears that three samples from the Upper Kimmeridgian Source Rock of the South Tempest G-88 well have experienced the most sedimentary recycling.

In the previous section, it was mentioned that it did not appear sedimentary recycling processes were important in the mudstone beds and that the detritus was likely first-cycle in nature. The data from the sandstones, however, contradicts this statement. Based on the abundances of Zr in the sandstone beds, it appears that hydraulic sorting and sedimentary recycling processes were very important, and therefore that recycled sedimentary rocks were likely a major source of detritus. It is an interesting question to determine which lithology more accurately estimates the provenance. It is clear that both sands and muds possess an upper crustal signature, but how important are recycled sedimentary rocks to the detritus?

McLennan et al. (1990) analyzed both muds and sands from a wide range of tectonic environments and found that in active tectonic settings, sands and muds possessed no systematic differences. This led them to conclude that in these environments, heavy mineral fractionation is not an important process (McLennan et al. 1990). However, in passive margins, the sands were considerably enriched in Zr compared to the associated mud due to sedimentary recycling and hydraulic sorting of heavy minerals (McLennan et al. 1990). Therefore, it can be concluded that if sedimentary recycling and hydraulic sorting are important, these features will only be noticeable in the sand-sized grain size fraction. These observations from McLennan et al. (1990) are comparable to what is observed in the Upper Jurassic samples from this study. Since the signatures seen in both the sandstones and mudstones from the Central Ridge/Flemish Pass Basin are typical of signatures of passive margin sands and muds from McLennan et al. (1990), it is interpreted that recycled sediments are an important source of detritus for both sandstone and mudstone beds. However, considering the abundance of igneous and metamorphic sources in adjacent terranes, first-cycle sources cannot be considered insignificant.

## 7.2.2 - Sc-Th-Zr Plot

The Sc-Th-Zr ternary plot (Figure 4.6B) gave similar results to the previous plot, as all mudstones samples did not plot within the passive margin field. Most samples plotted within the continental arc field, once again suggesting an upper crustal type of source material. This is expected based on the results of the previous plot, and the fact that passive margin mudstones will not exhibit comparable Zr enrichment that is seen in passive margin sandstones (McLennan et al. 1990). Most formations appear to demonstrate a similar provenance on this plot, although once again, the Lower Tempest Sandstones show higher Sc abundances, indicating slightly more mafic detritus.

Examination of the Sc-Th-Zr ternary plot for the sandstones (Figure 4.7B) once again revealed different results for the sandstones than the mudstones. The sandstones plot much closer to the passive margin field, towards the Zr axis, than the mudstone samples. As was interpreted in the previous diagram, this is likely related to hydraulic sorting of zircon in the sandstone beds. It is therefore interpreted that recycled sediment is an important component to the detritus,

although once again, first cycle sources cannot be ruled out based on the abundance of igneous and metamorphic sources in adjacent terranes.

Three samples from the Upper Kimmeridgian Source Rock plot further towards the Zr end-member than the other samples, indicating sedimentary recycling was more important in those particular samples. Other than these three, the other samples plot in much the same area, suggesting a similar provenance.

#### 7.2.3 – Th-La-Sc Ternary Plot

The final provenance plot for mudstones (Figure 4.6C) is a Th-La-Sc ternary plot. Based on the fields of Cullers (1994), most of these samples appear to be derived from mixed felsic and mafic sources. Although they plot in this field, most samples plot close to the average composition of the upper continental crust, meaning that upper crustal sources are likely most important for these samples which is a similar interpretation to the other trace element geochemical plots. Most formations appear to demonstrate a similar provenance on this plot, although once again, the Lower Tempest Sandstones plot closer to the Sc pole, indicating slightly more mafic sources.

Examination of the Th-La-Sc ternary plot for the sandstone samples (Figure 4.7C) reveals a similar signature to that observed in the mudstone samples. All of the sandstone samples possess an upper crustal affinity, and plot in the same area as the mudstones. Little variability is noted here between the samples from different formations. This diagram does not have the capability of identifying sedimentary recycling, but nonetheless it does reinforce the importance of upper crustal detritus in these Upper Jurassic samples.

# 7.3 – Geochemical Provenance Interpretations

## 7.3.1 - Introduction

Provenance interpretations based on geochemical analysis are presented here. In later sections, the geochemical interpretations are combined with the U-Pb geochronology data to obtain a more complete interpretation of the provenance of the Upper Jurassic units of the Central Ridge and Flemish Pass Basin. This section will address the correlations to potential source terranes based on the geochemical signatures discussed in the previous section.

# 7.3.2 - Rankin Formation, Upper Kimmeridgian Source Rock, Lower Kimmeridgian Source Rock

Samples from the Rankin Formation, Upper Kimmeridgian Source Rock and Lower Kimmeridgian Source Rock all possess similar geochemical signatures. All plots (Figure 4.6; 4.7) suggest that the detritus was derived from felsic rocks as their compositions are similar to that of the average composition of upper continental crust. Sedimentary recycling also appears to be important because the sandstone samples plot in the field associated with passive margin sediments. Based on this information, potential source areas must be predominantly continental in nature, with abundant sedimentary rocks. The terranes in close proximity to the Grand Banks, such as the Avalon Zone, the Central Mobile Belt, and the Meguma Zone definitely fit this description. Other potential sources include the rocks of Iberia, where abundant felsic intrusions are present, and the rocks of Ireland, which are composed of Early to Middle Paleozoic sequences similar to those seen in Central Newfoundland.

A source region that can likely be ruled out based on the presented geochemical data is the Humber Zone of western Newfoundland. Significant ophiolitic sequences are present in the Humber Zone, and if this region was a significant source, it is likely that the resulting detritus would possess a chemistry that reflects the presence of these ophiolitic sequences.

## 7.3.3 - Lower Tempest Sandstone

Samples from the Lower Tempest Sandstone possess slightly different geochemical signatures than those of the Rankin Formation, Upper Kimmeridgian Source Rock, and Lower Kimmeridgian Source Rock. Although interpreted to be derived from predominantly upper crustal material, the Lower Tempest Sandstones possess a more mafic signature than the units discussed in the previous section. The same source rocks are still likely important for the Lower Tempest Sandstone samples, as they possess an overall upper crustal signature, and are surrounded by the same potential source terranes. However, a couple of possibilities exist to explain the more mafic signature noted in these samples. Dearin (2006) studied the provenance of the Ben Nevis Formation sandstones of the Jeanne d'Arc Basin and noted that samples analyzed from earlier in the rifting stage possessed a more mafic component. Dearin (2006) attributed this to more mafic basement rocks being exposed during earlier stages of rifting. However, the basement offshore is thought to be composed of Avalon Zone rocks (Haworth & Lefort, 1978; King et al., 1985, 1986; Williams et al., 1999), which are not known to have a significant mafic component. Therefore, it is not likely this more mafic signature can be associated with the Avalon Zone basement rocks.

Another potential source of the mafic detritus is, as previously discussed, the ophiolites of western Newfoundland. Although the Central Mobile Belt is predominantly felsic in nature, some ophiolites and mafic rocks are present as well. These may represent a potential mafic source. Rift-related Mesozoic rocks discussed in Section 1.6.6 may also represent a mafic source. The majority of known Mesozoic igneous rocks from the island of Newfoundland or offshore Newfoundland have been mafic in composition such as the ultramafic Budgell Harbor Stock in Central Newfoundland, diabase dikes on the Avalon Peninsula, and basalt from the Spoonbill C-30, Cormorant N-83, and Brant P-87 wells from the South Grand Banks (Helwig et al., 1974;

Hodych & Hayatsu, 1980; Amoco et al., 1973; Jansa & Pe-Piper, 1986; Jansa & Pe-Piper, 1988). Mesozoic igneous rocks from the Lusitanian Basin on the Iberian margin are also all mafic in composition (Pinheiro et al., 1996). If these Mesozoic sources were important, their input would likely result in a mafic signature in the detritus. Another potential source of the mafic detritus is from rocks from the Iberian margin. Although the Iberian margin is dominated by Carboniferous – Permian granitoids, mafic rocks are also fairly common. The Ossa Morena Zone, in particular, contains noteworthy mafic igneous rocks, such as gabbroic sequences of the Beja Igneous Complex (Jesus et al., 2006) and the Beja-Acebuches Amphibolite unit (Azor et al., 2008).

Using just whole rock geochemistry, it is difficult to determine which of these options are most likely to explain the slightly different signature of the Lower Tempest Sandstones. However, the next chapter will include an interpretation of the detrital zircon analyses, which will help elucidate the provenance of the Lower Tempest Sandstone samples further.

## 7.4 – Provenance Interpretations of Heavy Mineral Data

#### 7.4.1 - Introduction

Provenance correlations based on heavy mineral analysis are presented here. In later sections, these interpretations are combined with the U-Pb geochronology and whole rock geochemical data to obtain a more complete interpretation of the provenance of the Upper Jurassic units of the Central Ridge and Flemish Pass Basin. This section will address the heavy mineral "fingerprints" of each formation analyzed and determine which formations possess different or similar source terranes.

# <u>7.4.2 – Upper Kimmeridgian Source Rock, Lower Kimmeridgian Source Rock, Rankin</u> <u>Formation</u>

All heavy mineral ratios are interpreted to show a similar provenance for all of the Upper Jurassic units examined. This is particularly true for the Upper Kimmeridgian Source Rock, Lower Kimmeridgian Source Rock and Rankin Formation samples, which all possess similar RZi, MZi, CZi and ZTR values. Each of these units has a similar heavy mineral signature, suggesting the source terranes were similar in nature. However, the Upper and Lower Tempest Sandstone units possess slightly different heavy mineral ratios and are interpreted to have a slightly different provenance.

Overall, ZTR ratios for the Upper Kimmeridgian Source Rock, Lower Kimmeridgian Source Rock, and Rankin Formation are high, with averages of  $79 \pm 11$ ,  $76 \pm 16$ , and  $76 \pm 5$  respectively. Considering that these formations are mudstone units, and that stable heavy minerals are inherently less abundant in mudstones than sandstones (McLennan et al. 1990), a ZTR of ~75 indicates that sedimentary recycling was a potentially important process for deposition of the mudstone beds.

## 7.4.3 – Upper Tempest Sandstone and Lower Tempest Sandstone

The RZi ratios of the Upper Tempest Sandstone possess are unique compared to that of the Upper and Lower Kimmeridgian Source Rock, and Rankin Formation samples previously discussed. Yet, as discussed in Section 5.4.1, this heavy mineral signature (RZi) has been largely affected by a single outlier sample (Figure 5.8), and the other three Upper Tempest samples plot in similar regions to the other formations. From Figures 5.8C and 5.9C, it is evident that the MZi and CZi ratios of the Upper Tempest Sandstone are similar to those of the other formations. If the outlier is disregarded, then it is interpreted that the Upper Tempest Sandstone possesses a similar provenance to the previous formations.

The Upper Tempest Sandstone possesses a higher average ZTR index value than the Upper and Lower Kimmeridgian Source Rock, and the Rankin Formation. This is despite being interpreted to have a similar provenance based on MZi and CZi ratios. The principal reason for the higher ZTR in the Upper Tempest Sandstone is associated with the amount of sedimentary recycling. One potential explanation of this is that sedimentary rocks are more important as a source for this Upper Tempest Sandstone unit. However, the preferred interpretation is that the source terrane is likely similar to that of the previously discussed formations, but that the detritus has simply undergone more sedimentary recycling. This is a more likely explanation given that the Upper Tempest Sandstone samples are more coarse-grained and composed of a greater abundance of sandstone material than the 5 m cuttings intervals from the mudstone units (Kimmeridgian Source Rocks, Rankin Formation). The greater abundance of coarse-grained material would likely be more enriched in stable heavy minerals such as zircon and rutile due to hydraulic sorting. This feature was also discovered in the geochemical plot of Zr/Sc vs. Th/Sc (Figure 4.6A, 4.7A) and discussed in Section 7.2.1. Therefore, it is concluded that the higher ZTR index values of the Upper Tempest Sandstone are related to sedimentary sorting and enrichment of stable heavy minerals within sandstone beds, and not a major shift in provenance.

It is difficult to draw meaningful conclusions for the Lower Tempest Sandstone unit, as only a single sample from this unit was analyzed. However, the CZi for this sample is much higher (46) than other units and plots at a greater value than the error bars for the other samples (Figure 5.9). This potentially indicates a unique provenance for this unit, but this is uncertain due to the absence of other samples.

## 7.4.4 - Summary

Overall, the provenance of all units based on heavy mineral ratios appears broadly similar. This is particularly true for the Upper Kimmeridgian Source Rock, Lower Kimmeridgian Source Rock and Rankin Formation as RZi, MZi, CZi and ZTR values for these formations are all comparable. The Upper Tempest Sandstone is also thought to have a similar provenance, as MZi and CZi ratios are very similar to those of other formations, and when a single outlier is excluded, the RZi is also comparable. The Upper Tempest Sandstone also possesses a higher ZTR index value than the other formations analyzed. This is interpreted to be related to a greater amount of sedimentary recycling in this unit, which is much more coarse-grained than the mudstones of the Kimmeridgian Source Rock or Rankin Formation.

# <u>7.5 - Provenance Interpretations of Geochronological Data – Upper Kimmeridgian Source</u> <u>Rock</u>

#### 7.5.1 - Introduction

Accurate dating of zircons from fine-grained Upper Jurassic sediments has been instrumental in pinpointing their source regions and parental rocks. Geochemical data have also contributed important information for this objective. This section presents interpretations of the provenance and drainage patterns of the Upper Jurassic units based on detrital zircon geochronology.

#### 7.5.2 - Late Neoproterozoic Grains

Analysis of the detrital zircons of the Upper Kimmeridgian Source Rock from both the South Tempest G-88 and Baccalieu I-78 wells revealed similar results. The most abundant grains in these samples are late Neoproterozoic (~600 Ma). Ages of these grains closely match and hence the grains are interpreted to have been derived from Avalon Zone rocks (see Section 1.6.2). The Avalon Zone represents basement to the Grand Banks and is present west, south, and east of the Flemish Pass Basin (Haworth & Lefort, 1979; King et al., 1985, 1986; Krogh et al., 1987) (Figure 1.7). The presence of these grains is therefore expected, but not overly indicative of drainage orientations. As discussed in Section 6.4.2 and 6.5.2, these grains are likely derived from a mixture of recycled sedimentary rocks as well as plutonic and volcanic igneous rocks.

This is consistent with a derivation from the Avalon Zone, as this terrane is characterized by volcanic and intrusive igneous rocks and associated sedimentary successions. Below (Figure 7.1) is a figure demonstrating the similarity in detrital zircon age peaks between grains previously dated from the Avalon Zone (Pollock et al., 2009) and from the late Neoproterozoic detrital zircon ages from this study. It is evident that the main detrital zircon peak seen in the data of Pollock et al. (2009) matches nearly identically with the main late Neoproterozoic peak seen in grains from this study. In addition, data from other offshore Newfoundland samples from Lowe et al. (2011) are plotted. These are also interpreted to be derived from Avalon Zone rocks, and also share the late Neoproterozoic age peak.



Figure 7.1 – Comparison of detrital zircon age peaks from this study, Lowe et al. (2011) and Pollock et al. (2009). For this study, all grains were plotted (n=310). All grains from Lowe et al. (2011) (n=335) and Pollock et al. (2009) (n=278) were also plotted. Data from Lowe et al. (2011) are from Mesozoic sedimentary rocks offshore Newfoundland while samples from Pollock et al. (2009) are from Neoproterozoic to Cambrian sedimentary rocks of the Avalon Zone onshore Newfoundland.

## 7.5.3 - > 1 Ga Grains

It is likely that the Avalon Zone was also an important source for the group of grains of >1 Ga. Grains ranging from the Mesoproterozoic to the Late Archean are thought to be related to the basement of Avalonia. It has been proposed that the Avalon terrane is built upon a dominantly c. 1.0 - 1.2 Ga basement with a smaller component of c. 1.6 Ga crust (Kerr et al. 1995; Murphy et al. 1996). Furthermore, rare c. 2.0 and 2.4 Ga xenocrystic zircons have been detected by Bevier & Barr (1990) in the Mira terrane and Zartman & Hermes (1987) in New

England in Avalonian plutonic rocks. Therefore, it is possible the >1 Ga grains are derived directly from Avalon basement. However, these grains are also common in Avalon Zone cover sequences, especially within the Cambrian – Ordovician cover sequences, as discussed in Section 1.6.2. These Lower Paleozoic cover sequences are thought to occur in the Avalon Uplift and Bonavista Platform areas, in addition to beneath the West Orphan, Northern Jeanne d'Arc and Flemish Pass Basins (King et al., 1986; Bell & Howie, 1990). If the >1 Ga grains are derived from Cambrian - Ordovician cover sequences, a source from the east, south, or north is possible, which is also not overly diagnostic. The characteristics of these grains, such as their low Th/U as well as their predominantly rounded to subrounded nature, were much more helpful in determining the parent rock type. It is probable that they were derived from a mixture of sedimentary and metamorphic sources as discussed in Section 6.4.2 and 6.5.2. This is reasonable because grains of this age would likely have experienced either significant sedimentary recycling or metamorphism. The rounded characteristic of these grains supports derivation from cover sequences of the Avalon Zone. >1 Ga grains from the Early Paleozoic cover sequences would have been subject to numerous sedimentary cycles, and would have many of the same features seen in the >1 Ga grains analyzed in the Upper Kimmeridgian Source Rock sample.

Another potential source of the >1 Ga grains is the Grenville basement of western Newfoundland and Labrador. The Grenville basement of this area has been shown to be composed of gneisses and granites with ages of approximately 1000 Ma and 1500 Ma (Heaman et al. 2002). Although this could explain the presence of some of the > 1 Ga grains in the samples from the Upper Kimmeridgian Source Rock, it cannot account for the grains that are aged > 1.5 Ga. Many of the samples of the Upper Kimmeridgian Source Rock have several grains > 1.5 Ga. If these are compared to those dated by Pollock et al. (2009) from sedimentary rocks of the Avalon Zone of eastern Newfoundland (Figure 7.1), a much better match is observed. There are numerous zircons from these samples dated at >1.5 Ga, and these would represent a good match for the >1.5 Ga grains from the Upper Kimmeridgian Source Rock. Evidently, many of the other grains dated between 1.0 and 1.5 Ga are likely to be derived from the Avalon Zone as well, since grains of this age are important in the study of Pollock et al (2009). It is possible that a small number of the grains aged between 1.0 and 1.5 Ga are sourced from the Grenville basement, but these would represent a small proportion of all the grains in general, meaning that this source region likely represents an insignificant source of detritus at this time. In addition, grain characteristics listed in the previous paragraph suggested Avalon Zone sources for this group are most probable.

## 7.5.4 - Cambrian – Devonian Grains

The youngest significant cluster of grains from the Upper Kimmeridgian Source Rock material is a Cambrian – Devonian group of grains. The ages of these grains closely match those of rocks found in the Gander and Dunnage zones of the Central Mobile Belt. As shown in Figure 7.1, the Cambrian – Devonian age peak from grains of this study closely matches that of Lowe et al. (2011), suggesting the grains have a similar origin. Lowe et al. (2011) also interpreted these grains to be derived from the Central Mobile Belt. This terrane is described in detail in Section 1.6.4 and is located about 400 – 500 km to the west and northwest of the sample locations in Newfoundland, but also to the north and northeast in the offshore extensions of the Porcupine Bank and Basin (Lowe et al. 2011). This implies sediment supply from either a significant distance to the west or from the northeast. To explain the presence of Ordovician – Devonian aged grains in Tithonian sandstones of the Flemish Pass Basin, Lowe et al. (2011) interpreted these grains to be derived from the west. This interpretation would appear feasible for the Upper Kimmeridgian Source Rock as well, although it is also possible that sediment was derived from

the northeast from offshore extensions of the Porcupine Bank and Basin, which possesses a similar geology to that of the Central Mobile Belt. This interpretation is further supported by Cody et al. (2012), who analyzed 2D and 3D seismic data combined with well data and facies interpretations of Upper Jurassic reservoir intervals in the Mizzen area of the northern Flemish Pass. Cody et al. (2012) interpreted major river systems to be entering the basin from the northeast at this time. Since the detrital zircon ages would be similar if derived from the northeast or the west, the interpretation here is that both options are feasible.

An additional consideration for the source of the Cambrian - Devonian grains is that they may have been derived from Carboniferous sedimentary rocks. Abundant Carboniferous sedimentary rocks are present both in the Maritimes basins as well as onshore and offshore Ireland. The St. Anthony Basin as well as the Sydney Basin both extend from northwestern and southwestern Newfoundland towards the east to the Northeast Newfoundland Shelf and the southern Grand Banks, respectively (Figure 1.7). As mentioned in Section 1.6.5, a number of wells on the southern Grand Banks intersected Carboniferous clastic sequences (Howie & Bell, 1990). These Carboniferous sediments would probably be filled with Cambrian - Devonian-aged zircons as they most likely formed from the erosion of the Central Mobile Belt. This is the case for the Carboniferous clastic rocks of the Deer Lake and Bay St. George Basins of western Newfoundland which are dominated by zircons of Ordovician and Silurian age (Sylvester, 2012). This would likely be the same case for Carboniferous clastics deposited both onshore and offshore Ireland, as they would have been eroding rocks analogous to those of the Central Mobile Belt. Carboniferous clastic rocks, therefore, may be a significant source of Cambrian – Devonian grains as well. If Carboniferous sedimentary rocks are an important supply of clastic

material, it similarly does not help distinguish drainage orientations, as input from the west as well as northeast are both possible.

The characteristics of the Cambrian – Devonian grains are reviewed in Section 6.4.1 and 6.5.1 and show a mixture of morphologies as well as variable Th/U and aspect ratios. This indicates a mixture of parent rock types for these grains including both igneous and sedimentary sources. Therefore, it is likely that rocks found within the Central Mobile Belt (Cambrian to Silurian sedimentary rocks, volcanic rocks, and Silurian to Devonian granites) are more important as a source than the Carboniferous clastic rocks. If Carboniferous clastics were the predominant source, there would likely be more rounded grains than what is observed for the Cambrian – Devonian grains, which were often angular to subrounded. Although some of these are probably polycyclic, this can be explained from a derivation from sediments of the Central Mobile Belt. It is therefore concluded that the Cambrian – Devonian grains may be derived from the west from rocks of the Central Mobile Belt of Newfoundland, or alternatively from the northeast from analogous rocks from the Irish conjugate margin.

#### 7.5.5 - Middle Neoproterozoic Grains

Three Middle Neoproterozoic grains were dated in the Upper Kimmeridgian Source Rock of the South Tempest G-88 well. These grains are interesting as although they are likely derived from the Avalon terrane, there are fewer known correlative sources for grains of this age. Some of the oldest rocks of the Avalon Zone such as the Burin Group are dated at *ca*. 763  $\pm$  2 Ma (Krogh et al. 1987) and represent a potential source. A more likely source, however, is the more proximal Flemish Cap granodiorite. With an age in the 750 – 830 Ma range (King et al. 1985), it is located to the east and northeast of the Flemish Pass Basin. This would indicate an easterly or northerly derived provenance. The angular to subangular morphology of these grains indicates

they were likely derived from igneous rocks, which also supports a derivation from the Flemish Cap granodiorite or equivalent rocks.

Other grains present within the Upper Kimmeridgian Source Rock samples that did not fall within a specific group are scarce, and should be considered minor sources. This includes the two Permian – Carboniferous grains in the South Tempest G-88 sample. Although these are interesting grains, they are not abundant and cannot be considered a significant group. The presence of these Carboniferous-Permian aged grains and their origins will be addressed in subsequent samples, where they are more abundant, and are considered a major group.

## 7.6 – Provenance Interpretations of Geochronological Data - Upper Tempest Sandstone

#### 7.6.1 - Introduction

One sample was analyzed from the Upper Tempest Sandstone from a depth of 3210m from the Panther P-52 well. The results from this sample are markedly different than those from the Upper Kimmeridgian Source Rock samples.

## 7.6.2 – Constraints on depositional ages

The first point of interest is the presence of detrital zircon grains that provide constraints on the maximum depositional age of this unit. Lowe (2009) was able to constrain maximum depositional ages for reservoir units within the Flemish Pass Basin and help refine interpretations where biostratigraphic results were conflicting. Dickinson & Gehrels (2009) propose several ways to calculate the maximum depositional age of strata. The more statistically robust method is to calculate the weighted average of the youngest three or more grains that overlap at  $2\sigma$ (Dickinson & Gehrels, 2009). This method is possible in this sample since three Jurassic grains were dated whose ages overlap at an uncertainty of  $2\sigma$ . The weighted average of these three grains is  $147.5 \pm 2.8$  Ma (MSWD = 0.85). However, this method is a conservative method, and can sometimes result in an age that is older than the depositional age (Dickinson & Gehrels, 2009). Another method is to accept the age of the youngest single grain. This technique can be potentially misleading as results from a single grain may not be reproducible. However, in the dataset of Dickinson & Gehrels (2009) it more often results in ages closer to the actual depositional age. In the Upper Tempest Sandstone sample, the youngest grain was dated at 144.9  $\pm$  5.6 Ma. Both of these methods result in a Late Tithonian age for the Upper Tempest Sandstone as the Tithonian Stage ranges from 152.1±0.9 to ~145 Ma (ICS, 2015). An Earliest Cretaceous age is possible, as the youngest grain is dated at the Tithonian/Berriasian boundary, but the uncertainty on the measurement is 5.6 Ma, and as discussed, using the average of the three ages is likely a more statistically robust technique. When compared to biostratigraphic interpretations for this interval, a Late Tithonian age is consistent with findings from Robertson Research (2004), but conflicts with interpretations from the Bujak Davies Group (1987) who interpreted this interval to be Early Kimmeridgian in age (Figure 2.5). Based on the detrital zircon age results, and the Robertson Research (2004) report, the Upper Tempest Sandstone from the Panther P-52 well is considered to have a Late Tithonian age. Because cuttings were used for this sample, there is a possibility that caving occurred (material from previously penetrated beds uphole) and potentially contaminated this sample with younger detrital zircons from above. However, given the abundance of Upper Jurassic grains in this sample and the absence of any Cretaceous or younger grains, it is improbable they originated from cavings.

# 7.6.3 - Identified Grains

Unlike previous samples, the Upper Tempest Sandstone has a distinctly different population of detrital zircons. In addition to previously described zircon groups (Late Neoproterozoic group, >1 Ga group, Cambrian – Devonian Group), two new groups were observed. These include a group of Permian – Carboniferous grains, as well as a group of Upper Jurassic grains discussed in the previous section. The late Neoproterozoic and >1 Ga grains likely represent detritus from Avalonia, and are not overly indicative of drainage orientations. The Cambrian – Devonian grains are uncommon, but likely represent minor detritus from either the Central Mobile Belt from the west or from the northeast. Since they are such a small population, however, the Central Mobile Belt was likely only a minor source of detritus at this time.

## 7.6.4 - Carboniferous – Permian Grains

Seven Permian - Carboniferous grains were dated from the Upper Tempest Sandstone unit of the Panther P-52 well at 3210 m. These grains are noteworthy as there are few known correlative sources from Newfoundland or the Newfoundland offshore. As shown in Figure 7.1, grains of this age were not detected by Lowe et al. (2011) in other rocks from offshore Newfoundland. There are some late Devonian intrusions on the island of Newfoundland such as the St. Lawrence Granite and Francois Granite, dated at  $374 \pm 2$  and  $378 \pm 4$  Ma, respectively (Kerr et al. 1993). In addition, there are a number of shear zones on the island of Newfoundland that are thought to be related to the Hercynian deformation event in the Carboniferous (B. O'Brien, personal communication). Shear zones can be accompanied by magmatism, such as the Dover Fault in eastern Newfoundland (D'Lemos et al. 1997), and it may therefore be possible that Carboniferous igneous rocks once existed in Newfoundland, although none have been observed. If they did exist, they were either eroded, or are just very uncommon. However, even if Carboniferous igneous rocks were present in Newfoundland, it is unlikely that they would make statistically significant detrital zircon populations in offshore sediments, as Avalon, Gander, and Dunnage Zone related grains would be much more abundant. Additionally, if Carboniferous igneous rocks existed in Newfoundland, it is likely that the Carboniferous sedimentary rocks on the island would have a population of Carboniferous zircon grains.

Sylvester et al. (2012) found no Carboniferous detrital zircon grains in the sedimentary rocks of the Deer Lake or Bay St. George Basins. Therefore, the presence of seven Carboniferous – Permian grains, making up 24% of this sample implies a source external to Newfoundland.

A couple scenarios may explain the presence of Carboniferous zircons in this Upper Tempest Sandstone sample. The first option is that these grains are derived directly from Iberia. As explained in Section 1.6.8, Permian-Carboniferous granitic intrusions are abundant on the Iberian Peninsula, and therefore, detritus of this age would be abundant if the Iberian Peninsula represented a significant source. However, the Tithonian represents the initiation of a rifting phase that separated the Grand Banks from Iberia (Sinclair, 1988). Despite the initiation of the rift, as the Tempest Sandstones are interpreted to be deposited by turbidity currents, it is possible that if sediment from Iberia gained access to the rift, it may have been able to reach the Grand Banks region.

The second option is that the Permian-Carboniferous grains are derived from recycled sediments from the Hercynian foreland basin. This option is more complicated, but could still explain the presence of Permian – Carboniferous grains in the Upper Tempest Sandstone sample. Hiscott et al. (2008) preferred this interpretation to explain the presence of Permian – Carboniferous aged detrital micas within post-rift sediments in the Newfoundland Basin, east of the Grand Banks. This model is based on the fact that the Hercynian orogenic belt was in close proximity to the Grand Banks during the Carboniferous/Permian. Therefore, the deformation front for this orogen was near the eventual dividing line between Iberia and the Grand Banks (Hiscott et al. 2008). The associated Hercynian foreland basin would have existed 200-300 km to the west of this orogenic front (Allen & Homewood, 1986; Hiscott et al., 2008). Given this information, it is likely that sediments of this foreland basin would have blanketed at least some

of the Grand Banks, particularly in the region of the Avalon Uplift (Hiscott et al., 2008). These foreland basin sediments would have been deposited in the Late Carboniferous or Permian, and would have likely contained substantial quantities of Permo-Carboniferous zircons from the Iberian granitoids which would have subsequently been available for erosion and deposition into Mesozoic basins.

It is difficult to say which option is more likely based on the detrital zircon ages alone. However, the characteristics of the Permian-Carboniferous grains are noteworthy. As described in Section 6.9.2, the preferred interpretation is that the grains are derived from first-cycle igneous rocks based on the predominantly euhedral to subangular grain shapes. This would appear to support a derivation directly from igneous rocks from Iberia. It is less likely that sediments from the Hercynian foreland basin would possess this morphology, as they would have been through at least two sedimentary cycles by the time of their deposition in the late Jurassic. It is therefore interpreted that these are first-cycle grains from Iberian intrusions.

## 7.6.5 - Jurassic Grains

Three Jurassic grains  $(145 \pm 5 \text{ Ma}, 148 \pm 4 \text{ Ma}, 150 \pm 6 \text{ Ma})$  were dated in the Upper Tempest Sandstone sample (Panther P-52 (3210 m)) and were used in Section 7.6.2 to help refine the depositional age of this unit. The provenance of these grains is difficult to identify as there are few known correlatives to these grains. Some potential Mesozoic sources are outlined in Section 1.6.6. These sources range from areas in the South Grand Banks, to the Orphan Basin, to potential sources on the island of Newfoundland. The ages of the Upper Jurassic grains most closely match that of the granite encountered in the Bonavista C-99 well in the Orphan Basin which was dated at 146  $\pm$  46 Ma (BP Canada, 1975). However, the large uncertainty in this date makes this correlation less reliable. Basalt encountered in the Spoonbill C-30 and Cormorant N- 83 wells from the South Grand Banks has not been dated, and may represent a potential source (Amoco et al. 1973; Jansa & Pe-Piper, 1986). However, as these rocks are basaltic, they are unlikely to contain zircon. Therefore, it is unlikely these rocks are the source of the Mesozoic zircon grains. Other volcanics from the South Grand Banks have ages that do not correspond to the Tithonian ages from this sample. It is therefore possible that these grains are derived from the west from correlative igneous rocks to those intercepted in the Bonavista C-99 well. However, it is also a possibility that they are from a currently unknown source that represents contemporaneous magmatism within the basin. The high Th/U as well as angular shapes of these grains indicate they are likely derived from igneous sources, and are first-cycle in nature. This leaves the Bonavista C-99 granite, as well as other local magmatic rocks as plausible sources.

## 7.7 – Provenance Interpretations of Geochronological Data - Lower Tempest Sandstone

## 7.7.1 - Overview

One sample was analyzed from the Lower Tempest Sandstone unit from the South Tempest G-88 well from 4195.8 m. This sample contains very abundant late Neoproterozoic grains, significant >1 Ga grains, and minor Permian – Carboniferous and Cambrian – Devonian grains. As interpreted in previous samples, the late Neoproterozoic and >1 Ga grains are attributed to detritus from the Avalon Zone, while the Cambrian – Devonian grains are linked to grains derived from the Central Mobile Belt. Permian – Carboniferous grains are likely from Iberia or possibly from recycled Hercynian foreland basin sediments. Based on their angular to subangular morphologies, it is likely these grains are first-cycle and derived from Iberia. An important observation for this sample is the abundance of Avalonian-related grains compared to

other groups. The late Neoproterozoic and >1 Ga groups comprise 84% of all grains dated in this sample.

## 7.8 – Provenance Interpretations of Geochronological Data - Rankin Formation

#### 7.8.1 - Overview

Three samples from the Rankin Formation stratigraphic unit were analyzed. Two of these samples were from the Baccalieu I-78 well at depths of 4142.2m and 4135.29m, respectively. The other sample was the only analyzed from the Lancaster G-70 well, from a depth of 4405m. The two samples from the Baccalieu I-78 well possess detrital zircon signatures similar to those of the Upper Kimmeridgian Source Rock samples where major zircon groups included abundant late Neoproterozoic grains and common > 1 Ga grains (both related to Avalonia), as well as some Cambrian – Devonian aged grains (from the Central Mobile Belt).

#### 7.8.2 – Lancaster G-70 Sample

The Rankin Formation sample from the Lancaster G-70 well (4405 m) possesses a different detrital zircon signature than those analyzed from the Baccalieu I-78 well. They do possess similar zircon groups such as the late Neoproterozoic group, the >1 Ga group, and the Cambrian – Devonian grains. As previously discussed, these grains are likely linked to local Avalonian sources as well as sources related to the Central Mobile Belt. However, in this sample, the >1 Ga group of grains is much more significant than in other Rankin Formation samples. Additionally, the presence of a significant population of Upper Devonian to Permian-aged zircon grains is indicative of a different provenance. This population of grains, with similar ages and characteristics, is also found in the previously discussed Tempest Sandstone samples. In those samples, the Upper Devonian – Permian-aged grains are interpreted as being derived from Iberia or alternatively from Hercynian foreland basin sediments that likely once covered areas on the Southern Grand Banks. Both of these possibilities exist for the Upper Devonian – Permian-aged

grains in the Lancaster G-70 sample as well. However, based on the angular to subangular morphologies of these grains they are likely first-cycle and derived from Iberia.

The single Jurassic-aged grain found in this sample is also fairly interesting. It is not overly indicative of provenance directions since only a single grain was found; however the  $^{206}$ Pb/ $^{238}$ U age of  $175 \pm 9$  Ma may be correlated to a diabase dike dated from the Twillick G-49 well on the Southern Grand Banks at  $177 \pm 5$  Ma (Jansa & Pe-Piper, 1988). This grain may not be directly derived from this intrusion, but is likely related to a contemporaneous event within the basin. It suggests the diabase from the Twillick G-49 well may not be just a localized body, and that magmatism at this time may have been more widespread throughout the basin.

## 7.9 - Late Jurassic Provenance Model

## 7.9.1 - Upper Kimmeridgian Source Rock

The major detrital zircon groups within the Upper Kimmeridgian Source Rock (Figure 6.2; Figure 6.4) suggest a provenance from rocks of the Avalon Zone and Central Mobile Belt from a mixture of first-cycle igneous rocks, recycled sedimentary rocks, and minor metamorphic rocks. It is difficult to conclusively say whether these grains were derived from the west or the east, as rocks from both the Avalon Zone and Central Mobile Belt exist both west and east of the study area. Geochemical analysis also supports sediment derivation from the Avalon Zone or equivalent rocks, with potential input from the Central Mobile Belt. Geochemical plots (Figure 4.6; Figure 4.7) also suggest recycled sedimentary rocks were an important contributor of detritus. Both geochronological and geochemical datasets rule out a source from the Humber Zone of western Newfoundland.

Although determining whether sediment was derived from the west or east is difficult, the presence of detritus interpreted to be from the Flemish Cap granodiorite or correlative
sequences suggests that sediment input was likely from the northeast, although minor input from the west is also possible. It is likely that basin entry points did exist to the north, as was interpreted by Cody et al. (2012) for Upper Jurassic reservoir units of the Flemish Pass Basin. Figure 7.2 shows the interpreted large-scale drainage routes and Figure 7.3 shows the interpreted basin-scale entry points, and areas of either abundant and restricted sediment supply. The provenance interpretation introduced here for the Flemish Pass Basin and Central Ridge appears to concur with previous published data of the Jeanne d'Arc Basin for the Kimmeridgian. Information from the Jeanne d'Arc Basin indicates that during deposition of the equivalent Kimmeridgian Egret Member of the Jeanne d'Arc Basin, the source rock possessed more terrigenous qualities based on the pristine-phytane ratios near the Central Ridge (Fowler & McAlpine, 1994) towards the northeast, as well as increased sedimentation rates towards the same area (Huang et al., 1996). In addition, the southern part of the basin was very restricted, and deposition of limestone and marls was common (Bateman, 1995; Magoon et al., 2005). Finally, Magoon et al. (2005) also noted that the thickness of the Kimmeridgian source rock increased greatly towards the east to over 500 m thick in some wells on the Central Ridge. Magoon et al. (2005) also noted facies change towards the east as the Egret Member source rock becomes split by the Tempest Sandstone into an Upper and Lower Kimmeridgian Source rock (Figure 7.4). This information indicates that during the Kimmeridgian, areas towards the northeast experienced high sedimentation rates and more proximal depositional environments. This indicates that sediment sources were likely in the northeast, which matches the detrital zircon interpretation in this study that indicated derivation from the northeast.

If sediment was derived from the north, this implies sediment supply would have been much more abundant in the northern regions of the basin, with a likely thicker source rock sequence. This is an important consideration for the petroleum potential of the source rock. If the source rock is indeed more proximal to sediment supply in the north, then it is likely that the source rock has a more terrestrial component in this region and would likely generate different types of oil. A terrestrial component to the Flemish Pass source rock was proposed by both Creaney & Alison (1987) as well as Fowler (2007) based on the pristane/phytane ratios of Flemish Pass oils. This information supports the interpretation that the Flemish Pass Basin and Central Ridge were closer to the major sources of detritus at this time in comparison to the Jeanne d'Arc Basin, where the source rock is much more marine in nature (Magoon et al. 2005). Another important consideration is the effect of abundant sediment supply on the preservation of organic matter. Bohacs et al. (2005) outline the importance of clastic input in source rock systems in order to preserve the organic matter. However, for high quality hydrocarbon source rocks, it is also important that the clastic input is not too high, and does not dilute the organic content of the source beds. Evidently, if clastic input into the Flemish Pass Basin and Central Ridge was from the north, it means that the balance between clastic input and accumulation of organic material may be different here than elsewhere on the Grand Banks (such as the Jeanne d'Arc Basin) during this time period.



Figure 7.2 - Interpreted large scale drainage routes during deposition of the Upper & Lower Kimmeridgian Source Rock, and the Rankin Formation. Based on results from detrital zircon geochronology, whole rock geochemistry and heavy mineral ratios. Black lines trace terrane boundaries as well as modern day landmasses (NL- Newfoundland; NS- Nova Scotia; IB- Iberian Peninsula; JDB- Jeanne d'Arc Basin; OB- Orphan Basin; FPB- Flemish Pass Basin). Arrows show interpreted drainage routes. Figure modified from Lowe et al. (2011).



Figure 7.3 - Interpreted basin entry points and areas of abundant and restricted sediment supply during deposition of the Upper & Lower Kimmeridgian Source Rock, and the Rankin Formation. Black lines represent major faults. Figure modified from Cody et al. (2011).



Figure 7.4 - Spatial variation in the Kimmeridgian Source Rock on the Grand Banks. From Magoon et al. (2005).

## 7.9.2 - Rankin Formation and Lower Kimmeridgian Source Rock

The detrital zircon populations of the Rankin Formation samples and their associated characteristics are very similar to those from the Upper Kimmeridgian Source Rock samples (Figure 6.8; Figure 6.10). Detrital zircon analysis was unsuccessful for the Lower Kimmeridgian Source Rock as insufficient zircons were obtained from the samples from these intervals. However, the geochemical signatures and heavy mineral ratios of both the Rankin Formation and Lower Kimmeridgian Source Rock are similar to what was observed in the Upper Kimmeridgian Source Rock samples. Therefore, the provenance interpretation is also similar. A provenance from the northeast supplying detritus from the Avalon Zone as well as from the Central Mobile Belt is considered probable. Therefore, drainage routes in Figures 7.2 and 7.3 are applicable for the Rankin Formation and Lower Kimmeridgian Source Rock as well. The geochemical data and the ZTR heavy mineral index indicate recycled sedimentary rocks are an important source of detritus for both these units. This is confirmed in the Rankin Formation by the morphologies of

zircon grains as many are likely recycled, although some grains from first-cycle igneous and metamorphic sources are noted as well.

## 7.9.3 - Rankin Formation Exception – Lancaster G-70 Sample

The sample analyzed from the Lancaster G-70 well (4405m) displays a slightly different provenance than the other Rankin Formation and Upper Kimmeridgian source rock samples. This was a cuttings sample, and was not analyzed geochemically for reasons discussed in Chapter 4. Heavy mineral ratios do not suggest a major difference in provenance, as ratios for this sample all fall within the range of the error bars of the Upper Kimmeridgian Source Rock, and Lower Kimmeridgian Source Rock as well as other Rankin Formation samples (Figure 5.8; Figure 5.9). However, the detrital zircon analysis has detected a slightly different provenance not suggested by heavy mineral ratios. In this sample, most of the same zircon populations are present; however these populations are in different proportions. In this sample, the most abundant grains are actually the >1 Ga grains. As mentioned previously, these grains are associated with the Avalon Zone, and are common within Ordovician cover sequences (Pollock et al. 2009). The abundance of these grains within the Lancaster G-70 sample indicates that the source for the detritus at this time may have included the aforementioned Ordovician cover sequences. These cover sequences were abundant in late Neoproterozoic grains but also the >1Ga grains. However, another potential option is that these >1 Ga grains are more directly sourced from the Avalonian basement. Since the >1 Ga grains comprise 34% of all those analyzed from the Lancaster G-70 sample, it is possible that they are sourced directly from an uplifted Avalonian basement source, rather than just from Paleozoic cover sequences.

In addition to the abundance of >1 Ga grains, a prominent group of Upper Devonian – Permian grains were detected in this sample which were not common in previous Rankin Formation samples. As described in Section 7.6.4, it is difficult to say definitively where these grains are from, although they are likely derived from Iberia based on their ages and grain morphologies. This information suggests some input from the east for this unit. This can explain the presence of Upper Devonian – Permian grains, and can also account for the late Neoproterozoic, and >1 Ga grains, which are thought to be found in Avalon Zone rocks which surround and underlie the Grand Banks (Haworth & Lefort, 1979; King et al., 1985). However, an eastern provenance does not explain the presence of a major population of Cambrian – Silurian grains. The Cambrian – Silurian grains are found in the majority of samples that are interpreted as being derived from the northeast in other Upper Kimmeridgian Source Rock and Rankin Formation samples. However, the Tempest sandstone samples, which are interpreted as being derived from the east, possess only minor populations of these grains. It is therefore contradictory to see both populations in this sample.

The preferred interpretation to explain the presence of both Upper Devonian – Permian grains as well as Cambrian – Silurian grains is that the grains are predominantly derived from the northeast, similar to other Rankin Formation and Upper Kimmeridgian Source Rock samples. Because of the abundance of >1 Ga grains in this sample, a major portion of this area was likely covered by Ordovician cover sequences or in close proximity to Avalonian basement. However, in addition to input from the northeast, it is likely that some input existed from the south or east at this time as well, and this would have been the source of the Upper Devonian – Permian grains. Figures 7.2 and 7.3 are interpreted to apply to this sample; however an important consideration is that there may have also been periodic input of detritus from more of an easterly direction at this time.

# 7.9.4 - Upper Tempest Sandstone

Samples of the Upper Tempest Sandstone were only available from cuttings, as this interval was not cored in any of the wells studied. For this reason, no geochemical analyses are available for this unit. Major zircon groups present in the Upper Tempest Sandstone sample (Figure 6.12) indicate an easterly provenance. An easterly provenance is suggested by the presence of a significant number of Permian - Carboniferous grains. The grains, as well as their relatively angular morphologies, indicate derivation from intrusions of Iberia. A provenance from the east can also account for the late Neoproterozoic and >1 Ga grains that are linked to the Avalon terrane as Avalonian basement is present to the east of the Grand Banks. Some minor Cambrian – Devonian grains, as well as Jurassic grains may indicate minor input from the west, however. Although an overall easterly provenance is favoured in this study for this unit, observations of Sinclair (1988) and Jansa & Wade (1975) suggest the uplift of the area of the Avalon Uplift began in the late Jurassic. If this is the case, the area to the South would have become a major region of sediment supply and would suggest sediment derivation from the south. This southerly derived provenance was also suggested by DeSilva (1994) for the Tempest sandstones, and also by Enachescu (1994) for the Jeanne d'Arc Formation sandstones in the Terra Nova Field of the Jeanne d'Arc Basin. Since the Jeanne d'Arc Formation is Tithonian in age, it is laterally equivalent to the Upper Tempest Sandstone in question here, whose age was refined to late Tithonian based on ages of detrital zircons present. However, the ages and morphologies of the Permian - Carboniferous zircon grains indicate an easterly provenance for the Upper Tempest Sandstone (Figure 7.5). This is the preferred interpretation based on the detrital zircon data.

The heavy mineral data for this interval are somewhat inconsistent with the detrital zircon results. The detrital zircon data indicates a distinct provenance for this unit, but as discussed in

Section 7.4.3, the heavy mineral ratios of the Upper Tempest Sandstone indicate similar sources as seen in the other analyzed formations.

There are a couple of potential reasons why heavy mineral ratios do not detect the provenance shift indicated by detrital zircon data. One explanation is that since Avalonian detritus is so important in all analyzed samples, including the Upper Tempest Sandstone, that the heavy mineral signature is mostly reflective of this terrane. So, in a sense, it is possible that the Permian – Carboniferous aged grains detected by detrital zircon geochronology are not sufficient to suppress the heavy mineral "fingerprint" of Avalonia. Another possibility is that the heavy mineral "fingerprint" of both Avalonian and other source terranes are very similar. Therefore, if a new provenance region appears, it may not be detected due to the similar nature of both terranes. This interpretation is preferred, because a new source terrane was undoubtedly detected by detrital zircon analysis. An easterly provenance as indicated previously is still the favored interpretation despite the lack of detection from heavy mineral ratios.

As the Tempest Sandstone units are important reservoir intervals on the Grand Banks (flowed 1250 bopd in the South Tempest G-88 well), the drainage orientations and basin entry points have important implications for reservoir quality during this time. Presumably, accumulations of coarse-grained, high quality reservoir rocks are more likely to occur in close proximity to sediment supply and basin entry points whereas finer-grained shales would be deposited basinward. If this is applied to the current interpretation for the Tempest sandstone, it is likely that thicker, higher reservoir quality rocks would be deposited in the east, with decreasing reservoir grade to the west (Figure 7.6). This may be an important consideration for further exploration and drilling in this area.



Figure 7.5 - Interpreted large scale drainage routes during deposition of the Upper & Lower Tempest Sandstone. Based on results from detrital zircon geochronology, whole rock geochemistry and heavy mineral ratios. Black lines trace terrane boundaries as well as modern day landmasses (NL- Newfoundland; NS- Nova Scotia; IB- Iberian Peninsula; JDB- Jeanne d'Arc Basin; OB- Orphan Basin; FPB- Flemish Pass Basin). Arrows show interpreted drainage routes. Figure modified from Lowe et al. (2011).



Figure 7.6 - Interpreted basin entry points and areas of abundant and restricted sediment supply during deposition of the Upper and Lower Tempest Sandstone. Figure modified from Cody et al. (2011).

# 7.9.5 - Lower Tempest Sandstone

Detrital zircon analysis revealed an abundance of late Neoproterozoic and >1 Ga grains (Figure 6.14), suggesting that local, Avalonian detritus is most important in the Lower Tempest Sandstone. Large, westerly- or northeasterly-derived drainage systems are not the preferred interpretation, as they would likely result in more abundant Cambrian – Devonian grains. However, the presence of some of these grains indicates minor input from the west or northeast, or reworking of older Mesozoic rocks with Cambrian – Devonian grains. The Permian-Carboniferous grains composed just 7% of all grains in this sample. A larger proportion of these grains would be expected if major drainage systems were entering the basin from the east (as seen in the Upper Tempest Sandstone sample). However, the presence of a minor population of Permian – Carboniferous grains suggests there was some minor input from the east at this time.

As described in Section 7.3.3, geochemical analysis supports a different provenance for the Lower Tempest Sandstone than the other analyzed units. Although sources from upper crustal rocks such as the Avalon Zone are still likely important, the geochemistry indicated a slightly more mafic source for these samples. Some possibilities for the mafic source include the ophiolites of western Newfoundland and the Central Mobile Belt, Mesozoic igneous rocks as well as mafic rocks of Iberia. When the detrital zircon populations are considered, it is likely that both the ophiolites of western Newfoundland and the Central Mobile Belt can be ruled out. Very few detrital zircons were noted from either the Grenville Zone or the Central Mobile Belt, which would be expected if sources from western or central Newfoundland were important. The potential Mesozoic sources discussed in Section 7.3.3 are almost all basaltic, which contain scarce zircons. It is difficult to say whether these sources were important as they would likely not be easily detected in the detrital zircon analysis. However, a number of Permian – Carboniferous grains in the detrital zircon populations indicate that some detritus was derived from Iberia. This may also explain the mafic source noted in the geochemistry, as the Ossa Morena Zone of Iberia also contains noteworthy mafic igneous rocks. Therefore, it appears both geochronological and geochemical datasets correspond and suggest a provenance of local Avalonian detritus as well as input from Iberia.

Heavy mineral data presented in this study (Figure 5.8; Figure 5.9) are insufficient to draw meaningful provenance conclusions from. But, the one sample from the Lower Tempest Sandstone (Panther P-52 (3600 m)) did possess a fairly unique heavy mineral signature, which, when combined with the geochronological and geochemical datasets helps to support the notion of a different provenance for this unit than the Upper Kimmeridgian Source Rock, Lower Kimmeridgian Source Rock and Rankin Formation units.

Overall, it appears the Lower Tempest Sandstone was sourced from predominantly local sources, making it difficult to define a paleodrainage direction. However a provenance from the east would explain the presence of Permian-Carboniferous, the local Avalonian grains, as well as the geochemical signatures. This option is therefore preferred and the provenance shown in Figure 7.5 is applicable for this unit as well. There may also be some minor drainage from the west or northeast, which would explain the presence of the Cambrian – Devonian grains. However, the small population of these grains indicates they are more likely derived from reworking of older Mesozoic clastic sequences, which would indicate very local detritus, and could have been picked up in westerly flowing paleodrainage systems.

The provenance and basin entry points for the Lower Tempest Sandstone are important considerations for reservoir quality within this unit. As mentioned for the Upper Tempest Sandstone, accumulations of coarse-grained, high quality reservoir rocks are more likely to occur

213

in close proximity to sediment supply and basin entry points. Therefore, for the Lower Tempest Sandstone, it is reasonable to expect higher quality reservoir sandstones to be deposited in the east with decreasing reservoir quality towards the west (Figure 7.6). This may be important for future exploration and development of the Tempest Sandstones.

#### 7.9.6 - Provenance of Interbedded Sandstone and Mudstone

As discussed in Section 6.8.1, it is of interest to study whether the detrital zircon populations and provenance of interbedded mudstones and sandstones is the same. The samples from Baccalieu I-78 from 4142.2m and 4135.29m are locally interbedded mudstone and sandstone samples, respectively. Detrital zircons were analyzed from both of these samples. It is evident that these two units have similar detrital zircon populations with a predominance of late Neoproterozoic and >1 Ga grains. In addition to having similar ages, the zircon grains found in both samples possess similar characteristics in terms of their morphology, Th-U ratio, and aspect ratios. The only difference in grain characteristics is the surface area, as zircons found in the sandstone sample tended to be larger than those found in the mudstone sample. This is expected, however, and does not appear to have affected the relative proportions of the age groups of grains.

Evidently, detrital zircons of interbedded mudstone and sandstone pairs from Kimmeridgian rocks offshore Newfoundland indicate similar provenances. This doesn't necessarily mean that the provenance of both sands and muds are the same, but it is evidence that the zircon populations within these interbedded units are alike. This may impact future provenance studies of fine-grained rocks. Working with mudstones is challenging as the sample preparation, heavy mineral separation, and age-dating process are more time consuming and sometimes less effective than in coarse-grained rocks predominantly due to the fine-grain size of the heavy minerals. Where a mudstone succession is interbedded with siltstones and sandstones, it may be possible to focus the sampling on the interbedded siltstones and sandstones, as their detrital zircon populations will likely be similar. This will eliminate the complications involved in working with the finer-grained rocks and may encourage workers to expand their interpretations beyond the coarse-grained reservoir intervals into less studied fine-grained source rocks, and other important shales.

From a geochemical standpoint, the samples from this study possess different signatures in both the major elements and trace elements in mudstones and their associated sandstone pairs. This is shown in Chapter 4 as many of the samples from this study show contrasting signatures. In this study, the reason for the majority of the geochemical variances appear to be predominantly associated with hydraulic sorting within the sandstone beds that does not affect the interbedded mudstones to the same degree. So, it appears that their provenance is mostly the same, but sorting affects the proportions of different minerals, and hence elements, within different lithologies. The analysis of heavy mineral suites and ratios shows a similar result. The provenance of two units may be the same, but because one unit is a sandstone and the other is a mudstone, they may show different results because of hydraulic sorting.

Although the analysis of mudstones and sandstones for this study show a similar provenance, it is important to consider that samples from different tectonic environments and different geological eras may not provide the same results and it remains an important question whether sands and muds have the same ultimate provenance.

### 7.10 - Conclusions

Detailed analysis from this study of the Upper Jurassic rocks of the Flemish Pass Basin and Central Ridge through a combination of core logging, thin section descriptions, detrital zircon geochronology, whole rock geochemistry, and heavy mineral analysis highlights important provenance characteristics of these units. In addition, this thesis shows that the analysis of fine-grained sedimentary rocks using techniques more common in sandstones, such as detrital zircon geochronology, is feasible and useful for understanding provenance of finegrained sedimentary rocks. Another important finding includes comparing detrital zircon distributions of interbedded sandstone and mudstone pairs. The detrital zircon signatures in both samples are very similar, indicating that the zircons for these samples are derived from the same source.

The depositional environment is defined by core logging, and observing the sedimentary sturctures of the Upper Jurassic rocks. Based on analysis of cores from the Baccalieu I-78, Panther P-52, and South Tempest G-88 wells, the depositional environment can likely be described as a basinal setting with low oxygen levels, where sediment was derived by turbidity currents. This interpretation is supported by a number of features described in Chapter 3. This turbidite interpretation implies a somewhat different depositional environment for the Kimmeridgian Source Rock unit in the Flemish Pass Basin and Central Ridge, than what is noted in the Jeanne d'Arc Basin in the equivalent Upper Jurassic Egret Member. This may explain some differences noted in the type of oil expelled from the source beds in the Flemish Pass Basin (Creaney & Alison, 1987; Fowler et al. 2007). Information from thin section descriptions was helpful in identifying initial provenance characteristics of the sandstone and siltstone beds such as grain angularity and composition. This information indicated a mixture of both first cycle and recycled grains as a sediment source for the sand- and siltstones. Determining this information from the mudstone beds was much more difficult. Nonetheless, the mineralogy of the mudstone beds identified by the MLA-SEM, particularly the presence of illite, chlorite and muscovite, as

well as petrographic observations indicated that a mixture of sources was also likely for these fine-grained rocks.

Whole rock geochemistry was employed on both Upper Jurassic sandstones and mudstones as it is a useful tool for identifying sediment provenance. Both major and trace elements were analyzed; however the trace element diagrams created were most useful in revealing provenance characteristics of the rocks. The samples are interpreted to be derived from a source with an upper crustal signature, commonly seen in passive margins. Sedimentary recycling is interpreted as an important process in these Upper Jurassic samples. Samples from the Upper Kimmeridgian Source Rock, the Lower Kimmeridgian Source Rock as well as the Rankin Formation possess similar characteristics, and thus likely similar source regions. The Lower Tempest Sandstone, however, appears to have a more mafic signature, suggesting a slightly different provenance for this unit.

To supplement interpretations from whole rock geochemistry, heavy mineral ratios were also analyzed in the Upper Jurassic samples from the Flemish Pass Basin and Central Ridge. Heavy mineral ratios are not intended to be used to determine the composition of the source terrane. However, they are useful in identifying a fingerprint for a particular unit or formation. Analyzing heavy mineral ratios from these samples indicates that most of the formations possess a similar provenance fingerprint. This is particularly true for the Upper Kimmeridgian Source Rock, the Lower Kimmeridgian Source Rock, and the Rankin Formation as all heavy mineral ratios within these formations were very comparable. Ratios from the Upper Tempest Sandstone are also similar, with some minor variations likely due to an outlier sample. In addition to the whole rock geochemistry and heavy mineral ratios, detrital zircon geochronology revealed significant provenance information and were the most important for generating a provenance and paleodrainage model. Samples from the Upper Kimmeridgian Source Rock, Lower Kimmeridgian Source Rock, Rankin Formation, Upper Tempest Sandstone, and Lower Tempest Sandstone were analyzed. Zircon populations from within the Upper Kimmeridgian Source Rock, Lower Kimmeridgian Source Rock, and the Rankin Formation were all similar, with grains likely derived from the Avalon Zone, Central Mobile Belt, and underlying basement. Samples from the Upper Tempest Sandstone and Lower Tempest Sandstone had overall similar detrital zircon populations. However, a significant population of Permian – Carboniferous grains are present in these Tempest Sandstone samples. This suggests derivation from intrusive rocks of Iberia. This change in provenance within the Tempest Sandstone samples.

In addition to important provenance information, Upper Jurassic detrital zircons helped to constrain the age of the Upper Tempest Sandstone to within the Tithonian. This is particularly useful as conflicting ages exist in the published biostratigraphic interpretations.

By examining the zircon morphologies, Th-U ratios, sizes and aspect ratios, it appears that both first cycle as well as recycled sediments were important in forming all of these Upper Jurassic samples. This is consistent with the whole rock geochemical data.

After examining all datasets, a provenance model for the Late Jurassic of the Central Ridge and Flemish Pass Basin was developed. The Upper Kimmeridgian Source Rock, Lower Kimmeridgian Source Rock and Rankin Formation are all interpreted as being derived from the northeast. Drainage systems at this time may have reached as far northeast as what is currently Ireland. This type of drainage system implies the thickest package of these units would likely be present in the northeastern regions of the basin.

A considerably different model is proposed for the Tempest Sandstone units. These units are interpreted as being derived from the east. Therefore, the thickest packages of Tempest Sandstones are likely to be found in the eastern regions of the Central Ridge and Flemish Pass Basin.

#### **References Cited**

- Abbey, S. (1983). Studies in "standard samples" of silicate rocks and minerals 1969-1982. Canadian Geological Survey Paper 83-15, 1-114.
- Allen, J.R.L. (1982). Structures and sequences related to gravity-current surges. *In* Sedimentary Structures. Their Character and Physical Basis. Elsevier, Amsterdam. 395-431.
- Allen, P.A. & Homewood, P. (1986). Foreland basins: an introduction. In Foreland Basins. Edited by P.A. Allen & P. Homewood. International Association of Sedimentologists, Special Publication 8, 3-14.
- Alvarez, L.W., Alvarez, W., Asaro, F., Michel, H.V. (1980). Extraterrestrial cause for the Cretaceous-Tertiary Extinction. *Science*, **208**, 1095-1108.
- Amoco Canada Petroleum Company Ltd. (1973). Spoonbill C-30 Well History Report.
- Andersen, T. (2002). Correction in common lead in U-Pb analyses that do not report <sup>204</sup>Pb. *Chemical Geology*, **192**, 59-79.
- Arribas, J. & Tortosa, A. (2003). Detrital modes in sedimenticlastic sands from low-order streams in the Iberian Range, Spain; the potential for sand generation by different sedimentary rocks. *Sedimentary Geology*, **159**, 275-303.
- Azor, A., Rubatto, D., Simancas, J.F., Gonzalez Lodeiro, F., Martinez Poyatos, D., Martin Parra,
  L.M. & Matas, J. (2008). Rheic Ocean ophiolitic remnants in southern Iberia questioned
  by SHRIMP U-Pb zircon ages on the Beja-Acebuches amphibolites. *Tectonics*, 27, 11
  pgs.

- Barrs, M.S., Bujak, J.P. & Williams, G.L. (1979). Palynological zonation and correlation of sixty-seven wells, Eastern Canada. *Geological Survey of Canada, Paper No.* 78-24.
- Bateman, J.A., (1995). Mineralogical and geochemical traits of the Egret Member oil source rockKimmeridgian, Jeanne d'Arc Basin, offshore Newfoundland, Canada. MSc. Thesis.Dalhousie University.
- Bell, J.S. & Howie, R.D. (1990). Paleozoic Geology. In Geology of the Continental Margin of Eastern Canada. Edited by M.J. Keen & G.L. Williams, 141-165.
- Bevier, M.L. & Barr, S.M. (1990). U-Pb age constraints on the stratigraphy and tectonic history of the Avalon terrane, New Brunswick, Canada. *Journal of Geology*, **58**, 53-63.
- Bhatia, M.R. & Crook, K.A.W. (1986). Trace element characteristics of graywackes and tectonic setting discrimination of sedimentary basins. *Contributions to Mineralogy and Petrology*, 92, 181-193.
- Blatt, H. & Christie, J.M. (1963). Undulatory extinction in quartz of igneous and metamorphic rocks and its significance in provenance studies of sedimentary rocks. *Journal of Sedimentary Petrology*, **33**, 559-579.
- Boggs, S. (2006) Principles of Sedimentology and Stratigraphy, 4<sup>th</sup> Edition. 662 pgs.
- Bohacs, K.M., Grabowski, G.J., Carroll, A.R., Mankiewicz, P.J., Miskell-Gerhardt, K., Schwalbach, J.R., Wegner, M.B. & Simo, J.A. (2005). Production, destruction and dilution the many paths to source rock development. *In* The Deposition of Organic-Carbon-Rich sediments: Models, Mechanisms, and Consequences. *Edited by* N. Harris. *SEPM Special Publication*, **82**, 61-101.

BP Exploration Canada Ltd. (1975). Bonavista C-99 Well History Report and Logs.

BP Exploration Canada Ltd. (1979). Hare Bay E-21 Well History Report and Logs.

BP Exploration Canada Ltd. (1991). Biostratigraphic Study of Flemish Pass Wells.

- Brown, D.M., McAlpine, K.D., & Yole, R.W. (1989). Sedimentology and sandstone diagenesis of Hibernia Formation in the Hibernia oil field, Grand Banks of Newfoundland. AAPG Bulletin, 73, 5, 557-575.
- Bujak Davies Group (1987). Palynological biostratigraphy of the interval 395 4203 m, Panther P-52, Grand Banks. GSC Open File Report 1876, 16 pgs.
- Capdevila, R. & Mougenot, D. (1988). Pre-Mesozoic basement of the western Iberian continental margin and its place in the Variscan Belt. *Proceedings of the Ocean Drilling Program, Scientific Results*, 103, 3-12.
- Chorlton, L.B. & Dallmeyer, R.D. (1986). Geochronology of early to middle Paleozoic tectonic development in the Southwest Newfoundland Gander Zone. *Journal of Geology*, 94, 67-89.
- Clarke, D.B., MacDonald, M.A., & Tate, M.C. (1997). Late Devonian mafic-felsic magmatism in the Meguma Zone, Nova Scotia. *Memoir Geological Society of America*, **191**, 107-127.
- C-NLOPB (2011). Schedule of Wells Newfoundland and Labrador offshore area. Baccalieu I-78.
- C-NLOPB (2013). Schedule of Wells Newfoundland and Labrador offshore area. Kyle L-11.

- C-NLOPB (2007). Schedule of Wells Newfoundland and Labrador offshore area. Lancaster G-70, Panther P-52, & South Tempest G-88.
- Cody, J., Hunter, D., Schwartz, S., Marshall, J., Haynes, S., Gruschwitz, K., & McDonough, M. (2012). A Late Jurassic play fairway beyond the Jeanne d'Arc Basin: new insights for a petroleum system in the Northern Flemish Pass Basin. *In* 2012 Proceedings: New understanding of the petroleum systems of continental margins of the world, *Edited by* Norman C. Rosen, Paul Weimer, Sylvia Maria Coutes dos Anjos, Sverre Henrickson, Edmundo Marques, Mike Mayall, Richard Fillon, Tony D'Agostino, Art Saller, Kurt Campion, Tim Huang, Rick Sarg, and Fred Schroeder. 32<sup>nd</sup> Annual Conference, 599-608
- Cohen, K.M., Finney, S.C., Gibbard, P.L., & Fan, J.-X. (2013). The ICS International Chronostratigraphic Chart. Episodes 36, 199-204.
- Cox, R. & Lowe, D.R. (1995a). A conceptual review of regional-scale controls on the composition of clastic sediment and the co-evolution of continental blocks and their sedimentary cover. *Journal of Sedimentary Research, Section A: Sedimentary Petrology* and Processes, 65, 1-12.
- Cox, R., & Lowe, D.R. (1995b). Compositional evolution of coarse clastic sediments in the Southwestern United States from 1.8 to 0.2 Ga and implications for relationships between the development of crustal blocks and their sedimentary cover. *Journal of Sedimentary Research, Section A: Sedimentary Petrology and Processes,* 65, 477-494.
- Creaney, S., & Allison, B.H. (1987). An organic geochemical model of oil generation in the Avalon/Flemish Pass Sub-basins, East Coast Canada. *Bulletin of Canadian Petroleum Geology*, **35**, 12-23.

- Critelli, S., Arribas, J., Le Pera, E., Tortosa, A., Marmaglia, K.M., Marsaglia, K.H. & Latter, K.K. (2003). The recycled orogenic sand provenance from an uplifted thrust belt, Beltic Cordillera, southern Spain. *Journal of Sedimentary Research*, **73**, 72-81.
- Cullers, R.L. (1994). The chemical signature of source rocks in size fractions of Holocene stream sediment derived from metamorphic rocks in the wet mountains region, Colorado, USA. *Chem. Geol.*, **113**, 327-343.
- Currie, K.L. (1995). Plutonic rocks. *In* Geology of the Appalachian-Caledonian Orogen in Canada and Greenland. *Edited by* H. Williams. 629-680.
- Dallmeyer, R.D., Blackwood, R.F. & Odom, A.L. (1981). Age and origin of the Dover Fault; tectonic boundary between the Gander and Avalon zones of the northeastern Newfoundland Appalachians. *Canadian Journal of Earth Sciences*, 18, 1431-1442.
- Daly, J.S., & Flowerdew, M.J. (2005). Grampian and late Grenville events recorded by mineral geochronology near a basement-cover contact in north Mayo, Ireland. *Journal of the Geological Society of London*, 162, 163-174.
- Dearin, A. (2006). Provenance of the Ben Nevis Formation sandstones, White Rose Field, Jeanne d'Arc Basin, Newfoundland, Canada. MSc. Thesis, Memorial University.
- Deptuck, M.E., MacRae, R.A., Schimeld, J.W., Williams, G.L., & Fensome, R.A. (2003). Revised Upper Cretaceous and Lower Palaeogene lithostratigraphy and depositional history of the Jeanne d'Arc Basin, offshore Newfoundland, Canada. AAPG Bulletin, 87, 1459-1483.

- DeSilva, N. (2000). Flemish Pass Basin: hydrocarbon prospectivity and potential deep water development. *Journal of Canadian Petroleum Technology*, **39**, 22-25
- DeSilva, N. (1994). Submarine fans on the northeastern Grand Banks, offshore Newfoundland. GCSSEPM Foundation 15<sup>th</sup> Annual Research Conference – Submarine Fans and Turbidite Systems, Dec. 4-7, 1994. 95-104.
- Dickinson, W.R., Beard, L.S., Brakenridge, G.R., Erjavec, J.L., Ferguson, R.C., Inman, K.F., Knepp, R.A., Lindberg, F.A. & Ryberg, P.T. (1983). Provenance of North American Phanerozoic sandstones in relation to tectonic setting. *GSA Bulletin*, 94, 222-235.
- Dickinson, W.R. & Gehrels, G.E. (2009). Use of U-Pb ages of detrital zircons to infer maximum depositional ages of strata: A test against a Colorado Plateau Mesozoic database. *Earth and Planetary Science Letters*, **288**, 115-125.
- Dickinson, W.R. & Suczek, C.A. (1979). Plate tectonics and sandstone compositions. *AAPG Bulletin*, **63**, 2164-2182.
- Dickinson, W.R. & Valloni, R. (1980). Plate settings and provenance of sands in modern ocean basins. *Geology*, **8**, 82-86.
- Dickson, W.L. (1990). Geology of the North Bay Granite Suite and metasedimentary rocks in southern Newfoundland (NTS 11P/15E, 11P/16 and 12A/2E). Report – Government of Newfoundland and Labrador Dept. of Mines and Energy, Geological Survey.
- D'Lemos, R.S., Schofield, D.I., Holdsworth, R.E., & King, T.R. (1997). Deep crustal and local rheological controls on the siting and reactivation of fault and shear zones, northeastern Newfoundland. *Journal of the Geological Society*, **154**, 117-121.

- Dodson, M.H., Compston, W., Williams, I.S., Wilson, J.F. (1988). A search for ancient detrital zircons in Zimbabwean sediments. J. Geol. Soc. (London), 145, 977-983.
- Driscoll, N.W., & Hogg, J.R. (1995). Stratigraphic response to basin formation: Jeanne d'Arc Basin, offshore Newfoundland. In Hydrocarbon Habitat in Rift Basins. Edited by J.J Lambiase. Geological Society of London Special Publication 80, 145-163.
- Dube, B., Dunning, G.R., Lauziere, K. & Roddick, J.C. (1996). New insights into the Appalachian Orogen from geology and geochronology along the Cape Ray fault zone, southwest Newfoundland. GSA Bulletin, 108, 101-116.
- Enachescu, M.E., Harding, S.C. & Emery, D.J. (1994). Three-dimensional seismic imaging of a Jurassic paleodrainage system. 26<sup>th</sup> Annual Offshore Technology Conference, 179-191.
- Enachescu, M.E. (2012). Call for Bids NL12-02, Parcel 1, Petroleum Exploration Opportunities in the Flemish Pass Basin, Government of Newfoundland and Labrador Department of Natural Resources.
- Enachescu, M.E. (1988). Extended basement beneath the intracratonic rifted basins of the grand banks of Newfoundland. *Canadian Journal of Exploration Geophysics*, **24**, 48-65
- Enachescu, M.E. (2006). Newfoundland and Labrador Call for Bids NL06-01, Jeanne d'Arc Basin.
- Enachescu, M.E. & Hogg, J.R. (2005). Exploring for Atlantic Canada's next giant petroleum discovery, *CSEG Recorder*, **30**, 5, 19-30.

- Enachescu, M.E. (2014). Petroleum exploration opportunities in the Flemish Pass Basin, Newfoundland and Labrador offshore area; Call for Bids NL13-01, Area "C" – Flemish Pass Basin, Parcel 1. Government of Newfoundland Department of Natural Resources.
- Enachescu, M.E., Smee, G.W., Meehan, P.J., Hodder, J., Deutsch, K., Emery, D. (2000). White
  Rose oil field, offshore Newfoundland; from teaser to trophy. *In* American Association of
  Petroleum Geologists 2000 annual meeting. Annual Meeting Expanded Abstracts.
  American Association of Petroleum Geologists 2000. P. 138
- Enachescu, M.E. (1987). Tectonic and structural framework of the northeast Newfoundland continental margin. *In* Sedimentary Basins and Basin Forming Mechanisms. *Edited by* C. Beaumont and A.J. Tankard. *Canadian Society of Petroleum Geologists*, 117-146.
- Esso Resources Canada Ltd. (1986). Esso Parex et al. Baccalieu I-78 well history reports and logs.
- Falvey, D.A. (1974). The Development of continental margins in plate tectonic theory. *Journal* of Australian Petroleum Exploration Association, **14**, 95-106.
- Fedo, C.M., Nesbitt, W.H. & Young, G.M. (1995). Unraveling the effects of potassium metasomatism in sedimentary rocks and paleosols, with implications for paleoweathering conditions and provenance. *Geology*, 23, 10, 921-924.
- Fedo, C.M. Sircombe, K.N. & Rainbird, R.H. (2003). Detrital zircon analysis of the sedimentary record. *In* Zircon: Experiments, Isotopes, and Trace Element Investigations. *Edited by* J.M. Hanchar & P.Hoskin. *Mineralogical Society of America, Reviews in Mineralogy*, 53, 277-303.

- Feely, M., Coleman, D., Baxter, S. & Miller, B. (2004). U-Pb zircon geochronology of the Galway Granite, Connemara, Ireland: implications for the timing of late Caledonian tectonic and magmatic events and for correlations with Acadian plutonism in New England. *Atlantic Geology*, **39**, 175-184.
- Flowerdew, M.J., Daly, J.S. & Whitehouse, M.J. (2005). 470 Ma granitoid magmatism associated with the Grampian Orogeny in the Slishwood Division, NW Ireland. *Journal of the Geological Society of London*, **162**, 563-575.
- Fowler, M.G. & McAlpine, K.D. (1994). The Egret Member, a prolific Kimmeridgian source rock from offshore Eastern Canada. *In* Petroleum Source Rocks. *Edited by* B.J. Katz. 111-130.
- Fowler, M.G., Obermajer, M., Achal, S., Milovic, M. (2007). Results of geochemical analyses of an oil sample from Mizzen L-11 well, Flemish Pass, offshore Eastern Canada. *Geological Survey of Canada*, Open File 5342, 3 p.
- Foster, D.G. & Robinson, A.G. (1993). Geological history of the Flemish Pass Basin, offshore Newfoundland. AAPG Bulletin, 77, 588-609.
- Fralick, P.W. (2003). Geochemistry of clastic sedimentary rocks: ratio techniques. In Geochemistry of Sediments and Sedimentary Rocks: Evolutionary Considerations to Mineral Deposit-Forming Environments. Edited by D.R. Lentz. Geological Association of Canada, GeoText 4, 85-103.

- Gladney, E.S. & Roelandts, I. (1988). 1987 Compilation of elemental concentration data for USGS BHVO-1, MAG-1, QLO-1, RGM-1, SCo-1, SDC-1, SGR-1, and STM-1. *Geostandards Newsletter*, **12**, 253-362.
- Govindaraju, K. (1994). 1994 compilation of working values and descriptions for 383 geostandards. *Geostandards Newsletter*, **18**, 1-158.
- Gradstein, F.M., Jansa, L.F., Srivastava, S.P., Williamson, M.A., Bonham-Carter, G. & Stam, B. (1990). Aspects of North Atlantic paleo-oceanography, Chapter 8. *In* Geology of the Continental Margin of Eastern Canada. *Edited by* M.J. Keen & G.L. Williams. Geological Survey of Canada, Geology of Canada, no. 2, 353-389.
- Hallsworth, C.R., Morton, A.C., Claoue-Long, J. & Fanning, C.M. (2000). Carboniferous sand provenance in the Pennine Basin, UK; constraints from heavy mineral and detrital zircon age data. *Sedimentary Geology*, **137**, 147-185.
- Haworth, R.T. & Lefort, J.P. (1979). Geophysical evidence for the extent of the Avalon zone in Atlantic Canada. *Canadian Journal of Earth Sciences*, **16**, 552-567.
- Heaman, L.M., Erdmer, P. & Owen, J.V. (2002). U-Pb geochronological constraints on the crustal evolution of the Long Range Inlier, Newfoundland. *Canadian Journal of Earth Sciences*, **39**, 845-865.
- Helwig, J., Aronson, J. & Day, D.S. (1974). A late Jurassic mafic pluton in Newfoundland. *Canadian Journal of Earth Sciences*, **11**, 1314-1319.
- Hiscott, R.N., Marsaglia, K.M., Wilson, R.C.L., Robertson, A.H.F., Karner, G.D., Tucholke, B.E., Pletsch, T. & Petschick, R. (2008). Detrital sources and sediment delivery to the

early post-rift (Albian-Cenomanian) Newfoundland Basin east of the Grand Banks: results from ODP Leg 210. *Bulletin of Canadian Petroleum Geology*, **56**, 69-92.

- Hodych, J.P. & Hayatsu, A. (1980). K-Ar isochron age and paleomagnetism of diabase along the trans-Avalon aeromagnetic lineament evidence of late Triassic rifting in Newfoundland. *Canadian Journal of Earth Sciences*, 17, 491-499.
- Hoskin, P.W.O. & Schaltegger, U. (2003). The composition of zircon and igneous and metamorphic petrogenesis. *Reviews in Mineralogy and Geochemistry*, **53**, 27-62.
- Huang, Z., Williamson, M.A., Bateman, J., McAlpine, K.D. & Fowler, M.G. (2007). Cyclicity in the Egret Member (Kimmeridgian) oil source rock, Jeanne d'Arc Basin, offshore eastern Canada. *Marine and Petroleum Geology*, **13**, 91-105.
- Hubbard, R.J. (1988). Age and significance of sequence boundaries on Jurassic and early Cretaceous rifted continental margins. *AAPG Bulletin*, **72**, 49-72.
- Hubert, J.F. (1962). A zircon-tourmaline-rutile maturity index and the interdependence of the composition of heavy mineral assemblages with the gross composition and texture of sandstones. *Journal of Sedimentary Petrology*, **32**, 440-450.
- Hurst, A. & Morton, A.C. (2001). Generic relationships in the mineral-chemical stratigraphy of turbidite sandstones. *Journal of the Geological Society of London*. **158**, 401-404.
- Hurst, A. (1981). Mid Jurassic stratigraphy and facies at Brora, Sutherland. Scot. J. Geol., 17, 169-177.

- Hutchinson, D.R., Klitgord, K.D., Lee, M.W. & Trehu, A.M. (1988). U.S. Geological Survey deep seismic reflection profile across the Gulf of Maine. *Geological Society of America Bulletin*, 100, 172-184.
- Ingall, E.D., Bustin, R.M., Van Cappellen, P. (1993). Influence of water column anoxia on the burial and preservation of carbon and phosphorous in marine shales. *Geochimica et Cosmochimica Acta*, **57**, 2, 303-316.
- Jansa, L.F. & Pe-Piper, G. (1986). Geology and geochemistry of Middle Jurassic and Early Cretaceous igneous rocks on the eastern North American continental shelf. Open File Report 1351 – Geological Survey of Canada.
- Jansa, L.F. & Pe-Piper, G. (1988). Middle Jurassic to Early Cretaceous igneous rocks along eastern North American continental margin. *AAPG Bulletin*, **72**, 347-366.
- Jansa, L.F. & Wade, J.A. (1975). Geology of the continental margin off Nova Scotia and Newfoundland. In Offshore Geology of Eastern Canada. Edited by W.J.M. van der Linden & J.A. Wade. Geological Survey of Canada. Paper 74-30, 51-106.
- Jenkins, W.A.M. (1986). Palynology of the Lancaster F-70 (G-70) well. Flemish Pass, offshore Newfoundland. Associated Biostratigraphic Consultants, Calgary. December, 1986.
- Jenner, G.A., Longerich, H.P., Jackson, S.E. & Freyer, B.J. (1990). ICP-MS a powerful tool for high precision trace element analyses in earth sciences: evidence from analyses of selected U.S.G.S. reference samples. *Chemical Geology*, 83, 105-118.

- Jesus, A.P., Munha, J., Mateus, A., Tassinari, C. & Nutman, A.P. (2007). The Beja Layered Gabbroic Sequence (Ossa-Morena Zone, southern Portugal): geochronology and geodynamic implications. *Geodinamica Acta*, **20**, 139-157.
- Johnson, H., Ritchie, J.D., Gatliff, R.W., Williamson, J.P., Cavill, J. & Bulat, J. (2001). Aspects of the structure of the Porcupine and Porcupine Seabight basins as revealed from gravity modeling of regional seismic transects. *In* Mesozoic successions of the Porcupine and North Porcupine basins, offshore Ireland. The petroleum exploration of Ireland's offshore basins. *Edited by* P.M. Shannon, P.D.W. Haughton & D.V. Corcoran. *Geological Society Special Publications*, **188**, 265-274.
- Jones, D.G., & Plant, J.A. (1989). Geochemistry of shales. *In* Mettalogenic models and exploration criteria for buried carbonate-hosted ore deposits a multidisciplinary study in Eastern England. *Edited by* J.A. Plant & D.G. Jones. British Geological Survey, Keyworth, Nottingham and Institution of Mining and Mettalurgy, London, 65-94.
- Kane, J.S., Arbogast, B. & Leventhal, J. (1990). Characterization of Devonian Ohio Shale SDO-1 as a USGS Geochemical Reference Sample. *Geostandards Newsletter*, 14, 169-196.
- Keen, C.E., Boutilier, R., de Voogd, B., Mudford, B., & Enachescu, M.E. (1987). Crustal geometry and extensional models for the Grand Banks of eastern Canada: constraints from deep seismic reflection data. *In* Sedimentary Basins and Basin Forming Mechanisms. *Edited by* C. Beaumont and A.J. Tankard. *Canadian Society of Petroleum Geologists*, 101-115.

- Keen, C.E., Kay, W.A., Keppie, D., Marillier, F., Pe-Piper, G. & Waldron, J.W.F. (1991). Deep seismic reflection data from the Bay of Fundy and Gulf of Maine: Tectonic implications for the northern Appalachians. *Canadian Journal of Earth Sciences*, 28, 1096-1111.
- Keppie, J.D., & Krogh, T.E. (2000). 440 Ma igneous activity in the Meguma terrane, Nova Scotia, Canada: part of the Appalachian over-step sequence? *American Journal of Science*, 300, 528-538.
- Kerr, A., Dunning, G.R. & Tucker, R.D. (1993). The youngest Paleozoic plutonism in the Newfoundland Appalachians: U-Pb ages from the St. Lawrence and Francois granites. *Canadian Journal of Earth Sciences*, **30**, 2328-2333.
- Kerr, A., Jenner, G.A. & Fryer, B.J. (1995). Sm-Nd isotopic geochemistry of Precambrian to Paleozoic granitoid suites and the deep-crustal structure of the southeast margin of the Newfoundland Appalachians. *Canadian Journal of Earth Sciences*, **32**, 224-245.
- Ketchum, J. W., Jackson, S. E., Culshaw, N. G., & Barr, S. M. (2001). Depositional and tectonic setting of the Paleoproterozoic Lower Aillik Group, Makkovik Province, Canada: evolution of a passive margin-foredeep sequence based on petrochemistry and U–Pb (TIMS and LAM-ICP-MS) geochronology. *Precambrian Research*, **105**(2), 331-356.
- King, A.F. (1990) Geology of the St. John's Area. Newfoundland Department of Mines, Mineral Development Division, Report 90-2, 88pp.
- King, A.F. (1988) Late Precambrian sedimentation and related orogenesis of the Avalon Peninsula, Eastern Avalon Zone. *GAC*, 1988 St. John's, Field Trip Guidebook, A4, 1-84.

- King, L.H., Fader, G.B., Jenkins, W.A.M., & King, E.L. (1986). Occurrence and regional geological setting of Paleozoic rocks on the Grand Banks of Newfoundland. *Canadian Journal of Earth Sciences*, 23, 504-526
- King, L.H., Fader, G.B., Poole, W.H., & Wanless, R.K. (1985). Geological setting and age of the Flemish Cap granodiorite, east of the grand banks of Newfoundland. *Canadian Journal* of Earth Sciences, 22, 1286-1298.
- Kontak, D.J., Ham, L.J., & Dunning, G. (2004). U-Pb dating of the Musquodoboit Batholith, southern Nova Scotia; evidence for a protracted magmatic-hydrothermal event in a Devonian intrusion. *Atlantic Geology*, 40, 207-216.
- Kosler, J. & Sylvester, P.J. (2003). Present trends and the future of zircon in geochronology; laser ablation ICPMS. *In Zircon. Edited by* J.M. Hanchar & P.W.O. Hoskin. *Reviews in Mineralogy and Geochemistry*, 53, 243-275.
- Kreuger Enterprises, Inc. (1972). Amoco-Imperial Jaeger A-49, K-Ar age determination of granite at 3040 feet.
- Krogh, T.E. (1982). Improved accuracy of U-Pb zircon dating by selection of more concordant fractions using a high gradient magnetic separation technique. *Geochemica et Cosmochimica Acta*, **46**, 631-635.
- Krogh, T.E. & Keppie, J.D. (1990). Age of detrital zircon and titanite in the Meguma Group, southern Nova Scotia, Canada; clues to the origin of the Meguma Terrane, *Tectonophysics*, 177, 307-323.

- Krogh, T.E., Strong, D.F., O'Brien, S.J. & Papezik, V.S. (1987). Precise U-Pb zircon dates from the Avalon Terrane in Newfoundland. *Canadian Journal of Earth Sciences*, 25, 442-453.
- Leventhal, J.S. (1983). An interpretation of carbon and sulfur relationships in Black Sea sediments as indicators of environments of deposition. *Geochimica et Cosmochimica Acta*, **47**, 133-137.
- Lilly, H.D. (1966). Submarine surveys on the Great Bank of Newfoundland and in the Gulf of Saint Lawrence. *Maritime Sediments*, **2**, 12-14.
- Lowe, D.G. (2009). Provenance and paleodrainage of Late Jurassic and Early Cretaceous reservoir sandstones in the Flemish Pass and Orphan Basins. MSc. Thesis, Memorial University.
- Lowe, D.G., Sylvester, P.J., Enachescu, M.E. (2011). Provenance and paleodrainage patterns of Upper Jurassic and Lower Cretaceous synrift sandstones in the Flemish Pass Basin, offshore Newfoundland, east coast of Canada. *AAPG Bulletin*, **95**, 1295-1320.
- Ludwig K.R. (2012) User's manual for Isoplot 3.75: A geochronological toolkit for Microsoft Excel. Berkeley Geochronology Center Special Publication No. 5. http://www.bgc.org/isoplot etc/isoplot/Isoplot3 75-4 15manual.pdf.
- MacDonald, L.A., Barr, S.M., White, C.E., & Ketchum, J.W.F. (2002). Petrology, age, and tectonic setting of the White Rock Formation, Meguma terrane, Nova Scotia: Evidence for Silurian continental rifting. *Canadian Journal of Earth Sciences*, **39**, 259-277.
- Maclean, W.H. (1990). Mass change calculations in altered rock series. *Mineralium Deposita*, **25**, 44-49.

- Macquaker, J.H.S. & Adams, A.E. (2003). Maximizing information from fine-grained sedimentary rocks: an inclusive nomenclature for mudstones. *Journal of Sedimentary Research*, 73, 5, 735-744.
- Magoon, L.B., Hudson, T.L., Peters, K.E. (2005). Egret-Hibernia(!), a significant petroleum system, northern Grand Banks area, offshore eastern Canada. *AAPG Bulletin*, **89**, 9, 1203-1237.
- Martel, A.T., McGregor, D.C., & Utting, J. (1993). Stratigraphic significance of Upper Devonian and Lower Carboniferous miospores from the type area of the Horton Group, Nova Scotia. *Canadian Journal of Earth Sciences*, **30**, 1091-1098.
- McAlpine, K.D. (1989). Lithostratigraphy of fifty-nine wells, Jeanne d'Arc Basin. Open File Report – Geological Survey of Canada.
- McAlpine, K.D. (1990). Mesozoic stratigraphy, sedimentary evolution, and petroleum potential of the Jeanne d'Arc basin, Grand Banks of Newfoundland. Geological Survey of Canada Paper 89-17, 50 p.
- McCarthy, K., Rojas, K., Niemann, M., Palmowski, D., Peters, K., Stankiewicz, A. (2011). Basic Petroleum Geochemistry for Source Rock Evaluation. *Oilfield Review*, **23**, 2, 32-43.
- McDonough, M. (2014). Paradigm Shift in East Coast Canada: The Lightening of Flemish Pass Oil. Abstract from Playmaker Forum, Calgary, Alberta, May 2014.
- McCracken, J.N., Haager, A., Saunders, K.I., Veilleux, B.W. (2000). Late Jurassic source rocks in the northern Flemish Pass Basin, Grand Banks of Newfoundland. (2000). Proceedings
of GeoCanada 2000; the millennium geoscience summit. Abstract Volum, Geoscience Association of Canada, Vol. 25.

- McLennan, S.M., Bock, B., Hemming, S.R., Hurowitz, J.A., Lev, S.M. & McDaniel, D.K. (2003). The roles of provenance and sedimentary processes in the geochemistry of sedimentary rocks. *In* Geochemistry of Sediments and Sedimentary Rocks: Evolutionary Considerations to Mineral Deposit-Forming Environments. *Edited by* D.R. Lentz. Geological Association of Canada, GeoText 4, 7-38.
- McLennan, S.M., Taylor, S.R., McCulloch, M.T. & Maynard, J.B. (1990). Geochemical and Nd-Sr isotopic composition of deep-sea turbidites: crustal evolution of and plate tectonic associations. *Geochemica et Cosmochimica Acta*, **59**, 1153-1177.
- Milliken, K.L. (1988). Loss of provenance information through subsurface diagenesis in Plio-Pleistocene sandstones, northern Gulf of Mexico, *Journal of Sedimentary Petrology*, 58, 992-1002.
- Morad, S. (1986). SEM study of authigenic rutile, anatase and brookite in Proterozoic sandstones from Sweden. *Sedimentary Geology*, **46**, 77-89.
- Morton, A.C. (1979). Depth control of intrastratal solution of heavy minerals from the Palaeocene of the North Sea. *Journal of Sedimentary Petrology*, **49**, 281-286.
- Morton, A.C. & Hallsworth, C.R. (1994). Identifying provenance-specific features of detrital heavy mineral assemblages in sandstones. *Sedimentary Geology*, **90**, 241-256.
- Morton, A.C. & Hallsworth, C.R. (1999). Processes controlling the composition of heavy mineral assemblages in sandstones. *Sedimentary Geology*, **124**, 3-29.

- Morton, A.C. & Hurst, A. (1995). Correlation of sandstones using heavy minerals: an example from the Statfjord Formation of the Snorre Field, northern North Sea. *In* Dating and Correlating Biostratigraphically-barren strata. *Edited by* R.E. Dunay & E. Hailwood. *Geological Society of London, Special Publication*, **89**, 3-22.
- Morton, A.C., Knox, W.R. & Hallsworth, C. (2002). Correlation of reservoir sandstones using quantitative heavy mineral analysis. *Petroleum Geoscience*, **8**, 251-262.
- Morton, A.C., Whitham, A.G. & Fanning, C.M. (2005). Provenance of Late Cretaceous to Paleocene submarine fan sandstones in the Norweigan Sea; integration of heavy mineral, mineral chemical and zircon age data. *Sedimentary Geology*, **182**, 3-28.
- Murphy, J.B. & Hamilton, M.A. (2000). Orogenesis and basin development; U-Pb detrital zircon age constraints on evolution of the late Paleozoic St. Mary's Basin, central mainland Nova Scotia. *Journal of Geology*, **108**, 53-71.
- Murphy, J.B., Keppie, J.D., Dostal, J. & Cousins, B.L. (1996). Repeated late Neoproterozoic-Silurian lower crustal melting beneath the Antigonish Highlands, Nova Scotia: Nd isotopic evidence and tectonic interpretations. *In* Avalonian and Related Peri-Gondwanan Terranes of the Circum-North Atlantic. *Edited by* R.D. Nance & M.D. Thompson. *Geological Society of America, Special Papers*, **304**, 109-120.
- Nesbitt, H.W. & Young, G.M. (1982). Early Proterozoic climates and plate motions inferred from major element chemistry of lutites. *Nature*, **299**, 715-717.

- Nesbitt, H.W., Young, G.M., McLennan, S.M. & Keayes, R.R. (1996). Effects of chemical weathering and sorting on the petrogenesis of siliciclastic sediments with implications for provenance studies. *Journal of Geology*, **104**, 525-542.
- Nesbitt, H.W. (2003). Petrogenesis of siliciclastic sediments and sedimentary rocks. *In* Geochemistry of Sediments and Sedimentary Rocks: Evolutionary Considerations to Mineral Deposit-Forming Environments. *Edited by* D.R. Lentz. Geological Association of Canada, GeoText 4, 39-51.
- Newfoundland and Labrador Department of Mines and Energy (2003). C-NOPB request for bids NF-03-01 Parcels 13-14 Flemish Pass Basin.
- Norry, M.J., Dunham, A.C., & Hudson, J.D. (1994). Mineralogy and geochemistry of the Peterborough Member, Oxford Clay Formation, Jurassic, UK: element fractionation during mudrock sedimentation. *Journal of the Geological Society, London*, **151**, 195-207.
- O'Brien, S.J., O'Brien, B.H., Dunning, G.R. & Tucker, R.D. (1996). Late Neoproterozoic Avalonian and related peri-Gondwanan rocks of the Newfoundland Appalachians. *In* Avalonian and Related peri-Gondwanan Terranes of the Circum-North Atlantic. *Edited by* Nance, R.D. & Thompson, M.D. *Geological Society of America, Special Papers*, 304, 9-28.
- O'Brien, S.J., Wardle, R.J., & King, A.F. (1983). The Avalon Zone: A Pan-African terrane in the Appalachian Orogen in Canada. *Geological Journal*, **18**, 195-222.

- O'Neill, P.P. (1991). Geology of Weir's Pond Area, Newfoundland (NTS 2E/1). Report 91-3 Government of Newfoundland and Labrador Dept. of Mines and Energy, Geological Survey.
- Oszczypko, N. & Salata, D. (2005). Provenance analyses of the Late Cretaceous-Paleocene deposits of the Magura Basin (Polish Western Carpathians) evidence from a study of the heavy minerals. *Acta Geologica Polonica*, **55**, 237-267.
- Paton, C., Hellstrom, J., Paul, B., Woodhead, J and Hergt, J (2011) Iolite: Freeware for the visualisation and processing of mass spectrometer data. *Journal of Analytical Atomic Spectrometry*, 26, 2508-2518.
- Pe-Piper, G. & Jansa, L.F. (1999). Pre-mesozoic basement rocks offshore Nova Scotia, Canada: New constraints on the accretion history of the Meguma terrane. *Geological Society of America Bulletin*, **111**, 1773-1791.
- Pe-Piper, G. & Weir-Murphy, S. (2008). Early diagenesis of inner-shelf phosphorite and ironsilicate minerals, Lower Cretaceous of the Orpheus Graben, southeastern Canada; implications for the origin of chlorite rims. *AAPG Bulletin*, **92**, 1153-1168.
- Pe-Piper, G., Karim, A. & Piper, D.J.W. (2011). Authigenesis of titania minerals and the mobility of Ti: new evidence from pro-deltaic sandstones, Cretaceous Scotian Basin, Canada. *Journal of Sedimentary Research*, 81, 762-773.

- Petrus, J.A. & Kamber, B.S. (2012). VizualAge: A novel approach to laser ablation ICP-MS UPb geochronology data reduction. *Geostandards and Geoanalytical Research*, 36, 247270.
- Pettijohn, F.J. (1975). Sedimentary rocks. Harper & Row, Publ., New York, N.Y., United States, 628 p.
- Pinheiro, L., Wilson, R., Reis, R.P., Whitmarsh, R., Ribeiro, A. (1996). The western Iberia margin: a geophysical and geological overview. *Proc.Ocean Drill Program Sci. Res.*, 149, 3-23.
- Piper, D.J.W., Pe-Piper, G., Tubrett, M., Triantafyllidis, S. & Strathdee, G. (2012). Detrital zircon geochronology and polycyclic sediment sources, Upper Jurassic – Lower Cretaceous of the Scotian Basin, southeastern Canada. *Canadian Journal of Earth Sciences*, 49, 1540-1557.
- Pollock, J.C., Wilton, D.H.C., van Staal, C.R. & Morrissey, K.D. (2007). U-Pb detrital zircon geochronological constraints on the Early Silurian collision of Ganderia and Laurentia along the Dog Bay Line; the terminal Iapetan suture in the Newfoundland Appalachians. *American Journal of Science*, **307**, 399-433.
- Pollock, J.C., Hibbard, J.P., Sylvester, P.J. (2009). Early Ordovician rifting of Avalonia and birth of the Rheic Ocean: U-Pb detrital zircon constraints from Newfoundland. *Journal of the Geological Society*, London, **166**, pp. 501-515.
- Potter, P.E., Maynard, J.B. & Depetris, P.J. (2005). Mud and Mudstones: Introduction and Overview. *Springer-Verlag Berlin Heidelberg New York*. 304 pgs.

- Priem, H.N.A. & den Tex, E. (1984). Tracing crustal evolution in the NW Iberian Peninsula through the Rb-Sr and U-Pb systematics of Paleozoic granitoids; a review. *Physics of the Earth and Planetary Interiors*, **35**, 121-130.
- Rast, N., Kennedy, M.J., & Blackwood, R.F. (1976). Comparison of some tectonostratigraphic zones in the Appalachians of Newfoundland and New Brunswick. *Can. J. Earth Sci.*, 13, 868-875.
- Rast, N. (1980). The Avalonian plate in the Northern Appalachians and Caledonides. *In* The Caledonides in the U.S.A. *Edited by* D.R. Wones. International Geologic Correlation Program Project 27 Caledonide Orogen, 1979 Meeting, Blacksburg, Virginia: Virginia Polytechnic Institute and State University Memoir 2, p. 63-66.
- Riediger, C, & Bloch, J. (1995). Depositional and diagenetic controls on source rock characteristics of the Lower Jurassic Nordegg Member, western Canada. *Journal of Sedimentary Research*, 65, 1, 112-126.
- Robertson Research International Ltd. (2004). Palynology (2650-4205 m) and micropaleontology (2635–4210 m), Panther P-52 biostratigraphy report.
- Robertson Research International Ltd. (2002). Stratigraphic correlation of Baccalieu I-78, Gabriel C-60, Lancaster G-70, and South Tempest G-88 wells. Robertson Research International Limited Report Number 6268.
- Romeo, I., Capote, R., Tejero, R., Lunar, R. & Quesada, C. (2006). Magma emplacement in transpression; the Santa Olalla igneous complex (Ossa-Morena Zone, SW Iberia). *Journal of Structural Geology*, 28, 1821-1834.

- Rubey, W.W. (1933). The size distribution of heavy minerals within a water-laid sandstone. Journal of Sedimentary Petrology, **3**, 3-29.
- Schenk, P.E. (1997). Sequence stratigraphy and provenance on Gondwana's margin: The Meguma zone (Cambrian to Devonian) of Nova Scotia, Canada. *Geological Society America Bulletin*, **109**, 395-409.
- Sinclair, I.K. (1988). Evolution of Mesozoic-Cenozoic sedimentary basins in the Grand Banks area of Newfoundland and comparison with Flavy's (1974) rift model. *Bulletin of Canadian Petroleum Geology*, **34**, 3, 255-273.
- Sinclair, I.K. (1993). Tectonism: the dominant factor in mid-Cretaceous deposition in the Jeanne d'Arc Basin, Grand Banks. *Marine and Petroleum Geology*, **10**, 530-549.
- Sláma, J., Košler, J., Condon, D.J., Crowley, J.L., Gerdes, A., Hanchar, J.M., Horstwood, M.S., Morris, G.A., Nasdala, L., Norberg, N. and Schaltegger, U. (2008). Plešovice zircon—a new natural reference material for U–Pb and Hf isotopic microanalysis. *Chemical Geology*, 249(1), 1-35.
- Smale, D. & Morton, A.C. (1987). Heavy mineral suites of core samples from the McKee Formation (Eocene-lower Oligocene), Taranaki; implications for provenance and diagenesis. *New Zealand Journal of Geology and Geophysics*, **30**, 299-306.
- Smith, J. & Higgs, K.T. (2001). Provenance implications of reworked palynomorphs in Mesozoic successions of the Porcupine and North Porcupine basins, offshore Ireland. In Mesozoic successions of the Porcupine and North Porcupine basins, offshore Ireland. The

petroleum exploration of Ireland's offshore basins. *Edited by* P.M. Shannon, P.D.W. Haughton & D.V. Corcoran. *Geological Society Special Publications*, **188**, 291-300.

- Sola, A.R., Pereira, M.F., Williams, I.S., Ribeiro, M.L., Neiva, A.M.R., Montero, P., Bea, F. & Zinger, T. (2008). New insights from U-Pb zircon dating of Early Ordovician magmatism on the northern Gondwana margin; the Urra Formation (SW Iberian Massif, Portugal). *Tectonophysics*, 461, 114-129.
- Stern, R.J. & Bloomer, B.S.H. (1992). Subduction zone infancy: examples from the Eocene Izu-Bonin-Mariana and Jurassic California arcs: *Geological Society of America Bulletin*, 104, 1621-1636.
- Stern, R. A., Bodorkos, S., Kamo, S. L., Hickman, A. H., & Corfu, F. (2009). Measurement of SIMS instrumental mass fractionation of Pb isotopes during zircon dating. *Geostandards* and Geoanalytical Research, 33(2), 145-168.
- Suttner, L.J., Basu, A. & Mack, G.H. (1981). Climate and origin of quartz arenites. *Journal of Sedimentary Petrology*, **51**, 1235-1246.
- Sutton, S.J. & Maynard, J.B. (1996). Basement unconformity control on alteration, St. Francois Mountains, SE Missouri. J. Geol., 104, 55-70.
- Swinden, H.S., & Hunt, P.A. (1991). A U-Pb zircon age from the Connaigre Bay Group, southwestern Avalon Zone, Newfoundland: Implications for regional correlations and metallogenesis. *In: Radiometric Age and Isotopic Studies, Report 4*. Geological Survey of Canada, **90-2**, 3-10.

- Sylvester, P.J. (2012). Mineralogy and provenance of Carboniferous sandstone and shale units in the Deer Lake and Bay St. George Basins, western Newfoundland. Government of Newfoundland and Labrador, PEEP (Petroleum Exploration Enhancement Project) Workshop Presentation 2012.
- Sylvester, P.J. (2012). Use of the Mineral Liberation Analyzer (MLA) for mineralogical studies of sediments and sedimentary rocks. *Mineralogical Association of Canada Short Course* 42, St. John's, NL, May 2012, 1-16.
- Tankard, A.J. & Balkwill, H.R. (1989). Extensional tectonics and stratigraphy of the North Atlantic margins: introduction. *In* Extensional tectonics and stratigraphy of the North Atlantic margins. *Edited by* A.J. Tankard & H.R. Balkwill. *AAPG Memoir 46*, 7-22.
- Tankard, A.J. & Welsink, H.J. (1987). Extensional tectonics and stratigraphy of the Hibernia oil field, Grand Banks, Newfoundland. AAPG Bulletin, 71, 1210-1232
- Tankard, A.J., Welsink, H.J., & Jenkins, W.A.M. (1989). Structural styles and stratigraphy of the Jeanne d'Arc Basin, Grand Banks of Newfoundland. *In* Extensional Tectonics and Stratigraphy of the North Atlantic Margins. *Edited by* Tankard, A.J. and Balkwill, H.R. *AAPG Bulletin*, Memoir 46, 265-282.
- Tate, M.P. & Dobson, M.R. (1988). Syn- and post-rift igneous activity in the Porcupine Seabight Basin and adjacent continental margin W of Ireland. Geological Society Special Publications, 39, 309-334.
- Taylor, S.R. & McLennan, S.M. (1985). The continental crust: its composition and evolution. Blackwell Scientific Publication, Carlton, 312 pgs.

- Totten, M.W. & Hanan, M.A. (2007). Heavy minerals in shales. *In* Heavy Minerals in Use, Developments in Sedimentology. *Edited by* M.A. Mange & D. Wright. **58**, 323-341.
- Totten, M.W. & Hanan, M.A. (1998). The accessory mineral fraction of mudrocks and its significance for whole-rock trace-element geochemistry. *In* Shales and Mudstones.
  Petrography, Petrophysics, Geochemistry and Economic Geology. *Edited by* J. Schieber & W. Zimmerle. Vol. 2, Schweizerbart, Stuttgart, 35-53.
- Tucholke, B.E., Austin, J.A. Jr., & Uchupi, E. (1989). Crustal structure and rift-drift evolution of the Newfoundland basin. *In* Extensional Tectonics and Stratigraphy of the North Atlantic Margins. *Edited by* Tankard, A.J. and Balkwill, H.R. *AAPG Bulletin*, Memoir 46, 265-282.
- Valverde-Vaquero, P. & Dunning, G.R. (2000). New U-Pb ages for Early Ordovician magmatism in Central Spain. *Journal of the Geological Society of London*, **157**, 15-26.
- Valverde-Vaquero, P., van Staal, C.R., van der Velden, A. & Dunning, G.R. (2003). Acadian orogenesis and high grade metamorphism in the Central Mobile Belt of central Newfoundland. *Abstracts with Programs – Geological Society of America*, **35**, 23.
- Valverde-Vaquero, P., van Staal, C.R., McNicoll, V. & Dunning, G.R. (2006). Mid-Late Ordovician magmatism and metamorphism along the Gander margin in central Newfoundland. *Journal of the Geological Society of London*, **163**, 347-362.
- van Staal, C.R. (2007). Pre-Carboniferous Tectonic Evolution and Metallogeny of the Canadian Appalachians. *In* Mineral Deposits of Canada: A Synthesis of Major Deposit-Types, District Metallogeny, the Evolution of Geological Provinces, and Exploration Methods.

*Edited by* W.D. Goodfellow. *Geological Association of Canada, Mineral Deposits Division, Special Publication No.* 5, 793-818.

- van Staal, C.R. (1994). The Brunswick subduction complex in the Canadian Appalachians: record of the Late Ordovician to Late Silurian collision between Laurentia and the Gander margin of Avalon. *Tectonics*, **13**, 946-962.
- Vermeesch, P. (2004). How many grains are needed for a provenance study? *Earth and Planetary Science Letters*, **224**, 441-451.

Weaver, C.E. (1989). Clays, Muds and Shales. Elseiver, New York, 819 p.

- Weaver, C.E. (1960). Possible uses of clay minerals in the search for oil. Bull. Am. Assoc. Pet. Geol., 44, 1505-1518.
- Weltje, G.J. & von Eynatten, H. (2004). Quantitative provenance analysis of sediments; review and outlook. *Sedimentary Geology*, **171**, 1-11.
- White, C.E., Waldron, J.W.F., Barr, S.M., Simonetti, A., & Heamon, L.M. (2008). Provenance of the Meguma Terrane, Nova Scotia. *Abstracts with Programs – Geological Society of America*, 40, 14-15.
- Wiedenbeck, M., Alle, P., Corfu, F., Griffin, W.L., Meier, M., Oberli, F., von Quadt, A., Roddick, J.C. & Spiegel, W. (1995). Three natural zircon standards for U-Th-Pb, Lu-Hf, trace element and REE analyses. *Geostandards Newsletter*, **19**, 1-23.
- Williams, H., Dehler, S.A., Grant, A.C., & Oakley, G.N. (1999). Tectonics of Atlantic Canada. Geoscience Canada, 26, 51-70.

- Williams, H., & Hatcher, R.D. (1983). Appalachian suspect terranes. In Contributions to the tectonics and geophysics of mountain chains. Edited by Hatcher, R.D. Jr., Williams, H.J., and Zietz, I. Geological Society of America, Memoir 159, 33-53.
- Zartman, O. & Hermes, D. (1987). Archean inheritance in zircon from late Paleozoic granites from the Avalon zone of southeastern New England: an African connection. *Earth and Planetary Science Letters*, 82, 305-315.
- Zeiss, A. (1991). Report on the voting about the future usage of the Kimmeridgian and Tithonian stage names. *International Subcommission on Jurassic Stratigraphy Newsletter 20*.
- Zeiss, A. (2003). The Upper Jurassic of Europe: its subdivision and correlation. *Geological* Survey of Denmark and Greenland Bulletin 1, 75-114.

#### Appendix A – Geochemical Data

#### XRF – Major Elements

Lab #	Sample #	Stratigraphic Unit	Na2O	Mgo	Al2O3	SiO2	P2O5	K2O	CaO	TiO2	MnO	Fe2O3	TOTAL
M41868Z	G-88(4185.1m)	LTS	0.71	2.76	16.06	41.74	0.07	3.65	11.27	0.98	0.10	6.37	83.71
M41869Q	G-88(4331.3m)	LKSR	0.88	2.35	15.05	49.85	0.06	2.79	9.18	0.93	0.04	5.91	87.04
M41870B	G-88(4329.6m)	LKSR	0.92	2.72	16.85	64.05	0.07	3.05	2.87	1.12	0.03	3.74	95.42
M41871T	G-88(4327.3m)	LKSR	0.92	2.65	16.28	58.08	0.09	3.04	5.13	1.06	0.04	5.30	92.59
M41872M	G-88(3830.1m)	UKSR	0.53	0.29	3.49	72.43	0.07	0.28	7.02	0.35		0.68	85.14
M41873E	G-88(3832.0m)	UKSR	0.80	0.76	6.51	70.92	0.13	0.66	10.04	0.39	0.03	1.68	91.92
M41874W	G-88(3834.4m)	UKSR	0.95	1.54	9.38	69.96	0.11	1.23	6.66	0.99	0.05	4.64	95.51
M41875P	G-88(3843.4m)	UKSR	1.47	2.63	17.48	52.84	0.11	3.20	5.01	1.03	0.60	5.64	90.01
M41876H	G-88(4183.9m)	LTS	1.17	2.87	14.74	55.36	0.07	2.78	8.52	0.90	0.12	6.23	92.76
M41877Z	G-88(4198.0m)	LTS	0.91	2.44	14.04	50.03	0.09	2.72	10.99	0.93	0.11	5.75	88.01
M41878R	G-88(4327.6m)	LKSR	0.90	2.80	17.00	49.09	0.08	3.36	6.51	1.04	0.05	7.14	87.97
M41879K	I-78(4148.3m)	RF	0.82	1.54	20.07	50.36	0.08	3.44	0.57	1.19	0.39	3.43	81.89
M41880P	I-78(4146.0m)	RF	0.78	1.59	18.87	47.72	0.06	3.66	5.52	1.12	0.12	4.64	84.08
M41881I	I-78(4138.5m)	RF	0.86	1.83	19.26	49.29	0.06	3.68	2.77	1.16	0.13	7.99	87.03
M41882B	I-78(4145.9m)	RF	0.82	1.67	19.72	49.60	0.06	3.80	5.64	1.14	0.08	4.34	86.86
M41883U	I-78(4140.9m)	RF	0.79	1.80	17.81	48.18	0.09	3.44	7.24	1.03	0.23	6.48	87.09
M41884N	I-78(4147.6m)	RF	0.80	1.61	18.77	45.87	0.06	3.53	7.87	1.11	0.14	4.37	84.13
M41885G	I-78(4148.3m)(B)	RF	0.75	1.42	19.51	52.50	0.10	3.71	0.36	1.17	0.07	3.69	83.28
M41886Z	P-52(3757.0m)	LTS	0.88	3.43	18.69	50.63	0.09	4.38	3.82	0.99	0.09	8.95	91.95
M41887R	P-52(3756.7m)	LTS	0.81	2.91	19.11	51.81	0.06	4.52	2.89	1.05	0.07	6.88	90.11
M41888K	P-52(3757.0m)(B)	LTS	0.75	3.38	18.63	46.40	0.09	4.52	3.37	1.01	0.09	10.70	88.94
M41889D	P-52(3754.0m)	LTS	0.86	2.90	20.71	50.77	0.09	5.06	1.69	1.12	0.14	7.92	91.26
M43028	G88(3832.0m)B	UKSR	0.74	0.87	6.66	74.59	0.12	0.62	9.36	0.37	0.02	1.47	94.82
M43029	G88(3838.4m)B	UKSR	0.72	1.27	8.10	58.75	0.09	0.96	12.88	0.76	0.05	3.65	87.23
M43030	G88(4188.1m)	LTS	1.14	1.47	7.19	44.59	0.07	0.77	23.63	0.53	0.23	3.97	83.60
M43031	G88(4188.1m)B	LTS	1.22	1.49	7.88	46.93	0.07	0.90	21.76	0.65	0.21	3.77	84.87
M43032	G88(4330.0m)	LKSR	0.87	2.19	11.99	57.96	0.06	1.88	9.47	0.79	0.09	4.75	90.05
M43033	178(4151.75m)	RF	0.60	1.51	16.21	54.97	0.08	2.99	4.91	0.91	0.10	5.94	88.21
M43034	I78(4135.4m)B	RF	0.53	1.33	14.97	56.03	0.09	2.64	5.94	0.89	0.09	4.67	87.18
M43035	G88(3843.4m)B	UKSR	1.13	2.60	17.84	51.12	0.11	3.47	3.77	1.28	0.06	6.80	88.17
M43036	G88(4325.4m)	LKSR	0.56	2.57	13.04	35.40	0.13	2.70	18.32	0.81	0.08	6.14	79.76
M43037	G88(4183.9m)B	LTS	1.06	2.68	14.44	53.10	0.06	2.78	7.88	0.88	0.11	6.09	89.09
M43038	G88(4185.4m)	LTS	1.04	3.00	16.81	52.81	0.05	3.46	5.40	0.92	0.09	6.90	90.49
			Refer	ence	Standar	ds					-		
	SDO-1		0.33	1.58	14.24	46.54	0.11	3.59	1.06	0.70	0.04	9.30	77.49
	SDO-1		0.36	1.57	14.25	46.81	0.10	3.61	1.05	0.70	0.04	9.36	77.85
	SDO-1		0.35	1.57	14.09	46.96	0.11	3.57	1.05	0.71	0.04	9.29	77.74
	SGR-1		2.70	3.52	6.07	26.39	0.34	2.09	11.49	0.35	0.04	3.98	56.97
	SGR-1		2.64	3.56	5.95	26.24	0.33	2.08	11.48	0.35	0.05	3.95	56.63
	SDO-1		0.29	2.03	13.56	50.15	0.10	3.78	1.35	0.85	0.03	10.88	83.03
	SGR-1		2.42	4.18	7.58	26.28	0.31	2.22	12.61	0.44	0.04	4.22	60.30
		Refere	nce Sta	ndard	s Accep	ted Va	lues						
	SDO-1		0.38	1.54	12.27	49.28	0.11	3.35	1.05	0.71	0.04	9.34	78.07
	SGR-1		2.99	4.44	6.52	28.20	0.33	1.66	8.38	0.25	0.34	3.03	56.15

All values for major elements presented in wt. %. Sample numbers with (B) are duplicate preparations. Stratigraphic units include the Lower Tempest Sandstone (LTS), Lower Kimmeridgian Source Rock (LKSR), Upper Kimmeridgian Source Rock (UKSR), and the Rankin Formation (RF). Reference standards include the SDO-1 (Devonian Ohio Shale) and the SGR-1 (Green River Shale). Accepted values are available from the United States Geological Survey and were established by Kane et al. (1990) for SDO-1 and by Abbey (1983), Gladney and Roelandts (1988) and Govindaraju (1994) for SGR-1.

#### <u>XRF – Trace Elements</u>

Manual         Manuu         Manuu         Manuu <th>, D</th> <th>1.500</th> <th>6.000</th> <th>6.000</th> <th>5.000</th> <th>6.000</th> <th>5.000</th> <th>6.000</th> <th>6.000</th> <th>6.000</th> <th>6.000</th> <th>6.000</th> <th>10.000</th> <th>5.000</th> <th>5.000</th> <th>5.000</th> <th>5.000</th> <th>6.000</th> <th>6.000</th> <th>6.000</th> <th>5.000</th> <th>5.000</th> <th>5.000</th> <th>5.000</th> <th>6.000</th> <th>6.000</th> <th>8.000</th> <th>8.000</th> <th>9.000</th> <th>6.000</th> <th>6.000</th> <th>6.000</th> <th>8.000</th> <th>6.000</th> <th>2.000</th> <th>38.000</th> <th>38.000</th> <th>39.000</th> <th>7.000</th> <th>7.000</th> <th>7.000</th> <th>38.000</th> <th>7.000</th> <th></th> <th>48.800</th> <th>5.400</th> <th></th>	, D	1.500	6.000	6.000	5.000	6.000	5.000	6.000	6.000	6.000	6.000	6.000	10.000	5.000	5.000	5.000	5.000	6.000	6.000	6.000	5.000	5.000	5.000	5.000	6.000	6.000	8.000	8.000	9.000	6.000	6.000	6.000	8.000	6.000	2.000	38.000	38.000	39.000	7.000	7.000	7.000	38.000	7.000		48.800	5.400	
Partial         Partial <t< th=""><th>ŧ</th><th>12.600</th><th>۲D</th><th><ld< th=""><th>14.000</th><th>14.000</th><th>Å</th><th>٩</th><th>đ</th><th>å</th><th>٩</th><th>٩Ņ</th><th>16.000</th><th>18.000</th><th>16.000</th><th>16.000</th><th>17.000</th><th>15.000</th><th>15.000</th><th>18.000</th><th>å</th><th>đ</th><th>15.000</th><th>16.000</th><th>٩D</th><th>۲D</th><th>۲D</th><th>۲D</th><th>12.000</th><th>13.000</th><th>13.000</th><th>15.000</th><th>11.000</th><th>11.000</th><th>17:000</th><th>12.000</th><th>14.000</th><th>14.000</th><th>6.000</th><th>6.000</th><th>7.000</th><th>13.000</th><th>å</th><th></th><th>10.500</th><th>4.800</th><th></th></ld<></th></t<>	ŧ	12.600	۲D	<ld< th=""><th>14.000</th><th>14.000</th><th>Å</th><th>٩</th><th>đ</th><th>å</th><th>٩</th><th>٩Ņ</th><th>16.000</th><th>18.000</th><th>16.000</th><th>16.000</th><th>17.000</th><th>15.000</th><th>15.000</th><th>18.000</th><th>å</th><th>đ</th><th>15.000</th><th>16.000</th><th>٩D</th><th>۲D</th><th>۲D</th><th>۲D</th><th>12.000</th><th>13.000</th><th>13.000</th><th>15.000</th><th>11.000</th><th>11.000</th><th>17:000</th><th>12.000</th><th>14.000</th><th>14.000</th><th>6.000</th><th>6.000</th><th>7.000</th><th>13.000</th><th>å</th><th></th><th>10.500</th><th>4.800</th><th></th></ld<>	14.000	14.000	Å	٩	đ	å	٩	٩Ņ	16.000	18.000	16.000	16.000	17.000	15.000	15.000	18.000	å	đ	15.000	16.000	٩D	۲D	۲D	۲D	12.000	13.000	13.000	15.000	11.000	11.000	17:000	12.000	14.000	14.000	6.000	6.000	7.000	13.000	å		10.500	4.800	
Partializationalizatiolaledizati alequidicationalizationalizationalizationalizationaliza	Pb	1.500	21.000	17.000	14.000	24.000	٩٦	9.000	8.000	18.000	19.000	17.000	29.000	29.000	26.000	29.000	25.000	25.000	25.000	27.000	26.000	31.000	27.000	46.000	6.000	7.000	8.000	8.000	13.000	18.000	15.000	16.000	16.000	18.000	75.000	31.000	31.000	30.000	40.000	40.000	41.000	31.000	42.000		27.900	38.000	
Purple         Purple<	č	4.000	80.000	59.000	94.000	96.000	33.000	42.000	76.000	53.000	57.000	69.000	60.000	97.000	83.000	100.000	79.000	78.000	81.000	100.000	66.000	61.000	73.000	78.000	46.000	60.000	45.000	51.000	55.000	83.000	103.000	96.000	70.000	56.000	21.000	68.000	73.000	70.000	36.000	34.000	31.000	77.000	46.000		79.300	36.000	
Image         Employe         Image         <	P	5.200	44.000	30.000	50.000	51.000	12.000	12.000	29.000	29.000	26.000	35.000	32.000	51.000	47.000	53.000	49.000	46.000	49.000	53.000	29.000	33.000	38.000	37.000	13.000	21.000	21.000	15.000	24.000	36.000	41.000	48.000	36.000	25.000	24.000	33.000	34.000	31.000	26.000	28.000	23.000	33.000	23.000		38.500	20.000	
Image         Standard         Standard <tt>Standard         Standard         <t< th=""><th>Ba</th><th>5.000</th><th>484.000</th><th>398.000</th><th>283.000</th><th>680.000</th><th>182.000</th><th>103.000</th><th>132.000</th><th>494.000</th><th>435.000</th><th>293.000</th><th>590.000</th><th>466.000</th><th>431.000</th><th>374.000</th><th>519.000</th><th>377.000</th><th>409.000</th><th>480.000</th><th>623.000</th><th>618.000</th><th>617.000</th><th>610.000</th><th>121.000</th><th>107.000</th><th>225.000</th><th>126.000</th><th>333.000</th><th>408.000</th><th>465.000</th><th>433.000</th><th>311.000</th><th>441.000</th><th>588.000</th><th>407.000</th><th>403.000</th><th>408.000</th><th>302.000</th><th>305.000</th><th>309.000</th><th>407.000</th><th>310.000</th><th></th><th>397.000</th><th>290.000</th><th></th></t<></tt>	Ba	5.000	484.000	398.000	283.000	680.000	182.000	103.000	132.000	494.000	435.000	293.000	590.000	466.000	431.000	374.000	519.000	377.000	409.000	480.000	623.000	618.000	617.000	610.000	121.000	107.000	225.000	126.000	333.000	408.000	465.000	433.000	311.000	441.000	588.000	407.000	403.000	408.000	302.000	305.000	309.000	407.000	310.000		397.000	290.000	
1         Sample         Description         V       V         V        V </th <th>S</th> <th>4.700</th> <th>24.000</th> <th>16.000</th> <th>17.000</th> <th>17.000</th> <th>٩</th> <th>٩</th> <th>13.000</th> <th>17.000</th> <th>15.000</th> <th>19.000</th> <th>19.000</th> <th>28.000</th> <th>23.000</th> <th>22.000</th> <th>22.000</th> <th>15.000</th> <th>24.000</th> <th>26.000</th> <th>19.000</th> <th>20.000</th> <th>13.000</th> <th>21.000</th> <th>۲D</th> <th>10.000</th> <th>8.000</th> <th>16.000</th> <th>10.000</th> <th>11.000</th> <th>14.000</th> <th>13.000</th> <th>24.000</th> <th>11.000</th> <th>2,000</th> <th>7.000</th> <th>15.000</th> <th>12.000</th> <th>12.000</th> <th>15.000</th> <th>17.000</th> <th>10.000</th> <th>14.000</th> <th></th> <th>6.900</th> <th>5.200</th> <th></th>	S	4.700	24.000	16.000	17.000	17.000	٩	٩	13.000	17.000	15.000	19.000	19.000	28.000	23.000	22.000	22.000	15.000	24.000	26.000	19.000	20.000	13.000	21.000	۲D	10.000	8.000	16.000	10.000	11.000	14.000	13.000	24.000	11.000	2,000	7.000	15.000	12.000	12.000	15.000	17.000	10.000	14.000		6.900	5.200	
Image         Conditionality         C         No	sb	1.700	5.000	3.000	5.000	7.000	5.000	3.000	4.000	4.000	5.000	٩D	3.000	٩	5.000	3.000	3.000	3.000	3.000	3.000	٩D	3.000	3.000	4.000	4.000	4.000	3.000	4.000	4.000	5.000	3.000	6.000	2.000	5.000	3.000	7.000	5.000	6.000	5.000	4.000	4.000	6.000	6.000			3.400	
I         Sample for the formation in the	Sn	3.100	<ld< th=""><th><ld< th=""><th><ld< th=""><th>4.000</th><th>٩ĽD</th><th>٩ĽD</th><th>٩D</th><th>٩D</th><th>٩D</th><th>٩ĽD</th><th>۲D</th><th>٩ĽD</th><th>4.000</th><th><ld< th=""><th>đ</th><th>٩D</th><th>٩D</th><th>4.000</th><th>٩D</th><th>٩D</th><th>٩D</th><th>٩ĽD</th><th><ld< th=""><th>۲D</th><th><ld< th=""><th><ld< th=""><th>٩ĽD</th><th><ld< th=""><th>۲D</th><th>6.000</th><th>۲D</th><th>ŋ,</th><th>Ð</th><th>3.000</th><th>1.000</th><th>3.000</th><th>2.000</th><th>2.000</th><th>3.000</th><th>٩D</th><th>٩</th><th></th><th>3.700</th><th>1.900</th><th></th></ld<></th></ld<></th></ld<></th></ld<></th></ld<></th></ld<></th></ld<></th></ld<>	<ld< th=""><th><ld< th=""><th>4.000</th><th>٩ĽD</th><th>٩ĽD</th><th>٩D</th><th>٩D</th><th>٩D</th><th>٩ĽD</th><th>۲D</th><th>٩ĽD</th><th>4.000</th><th><ld< th=""><th>đ</th><th>٩D</th><th>٩D</th><th>4.000</th><th>٩D</th><th>٩D</th><th>٩D</th><th>٩ĽD</th><th><ld< th=""><th>۲D</th><th><ld< th=""><th><ld< th=""><th>٩ĽD</th><th><ld< th=""><th>۲D</th><th>6.000</th><th>۲D</th><th>ŋ,</th><th>Ð</th><th>3.000</th><th>1.000</th><th>3.000</th><th>2.000</th><th>2.000</th><th>3.000</th><th>٩D</th><th>٩</th><th></th><th>3.700</th><th>1.900</th><th></th></ld<></th></ld<></th></ld<></th></ld<></th></ld<></th></ld<></th></ld<>	<ld< th=""><th>4.000</th><th>٩ĽD</th><th>٩ĽD</th><th>٩D</th><th>٩D</th><th>٩D</th><th>٩ĽD</th><th>۲D</th><th>٩ĽD</th><th>4.000</th><th><ld< th=""><th>đ</th><th>٩D</th><th>٩D</th><th>4.000</th><th>٩D</th><th>٩D</th><th>٩D</th><th>٩ĽD</th><th><ld< th=""><th>۲D</th><th><ld< th=""><th><ld< th=""><th>٩ĽD</th><th><ld< th=""><th>۲D</th><th>6.000</th><th>۲D</th><th>ŋ,</th><th>Ð</th><th>3.000</th><th>1.000</th><th>3.000</th><th>2.000</th><th>2.000</th><th>3.000</th><th>٩D</th><th>٩</th><th></th><th>3.700</th><th>1.900</th><th></th></ld<></th></ld<></th></ld<></th></ld<></th></ld<></th></ld<>	4.000	٩ĽD	٩ĽD	٩D	٩D	٩D	٩ĽD	۲D	٩ĽD	4.000	<ld< th=""><th>đ</th><th>٩D</th><th>٩D</th><th>4.000</th><th>٩D</th><th>٩D</th><th>٩D</th><th>٩ĽD</th><th><ld< th=""><th>۲D</th><th><ld< th=""><th><ld< th=""><th>٩ĽD</th><th><ld< th=""><th>۲D</th><th>6.000</th><th>۲D</th><th>ŋ,</th><th>Ð</th><th>3.000</th><th>1.000</th><th>3.000</th><th>2.000</th><th>2.000</th><th>3.000</th><th>٩D</th><th>٩</th><th></th><th>3.700</th><th>1.900</th><th></th></ld<></th></ld<></th></ld<></th></ld<></th></ld<>	đ	٩D	٩D	4.000	٩D	٩D	٩D	٩ĽD	<ld< th=""><th>۲D</th><th><ld< th=""><th><ld< th=""><th>٩ĽD</th><th><ld< th=""><th>۲D</th><th>6.000</th><th>۲D</th><th>ŋ,</th><th>Ð</th><th>3.000</th><th>1.000</th><th>3.000</th><th>2.000</th><th>2.000</th><th>3.000</th><th>٩D</th><th>٩</th><th></th><th>3.700</th><th>1.900</th><th></th></ld<></th></ld<></th></ld<></th></ld<>	۲D	<ld< th=""><th><ld< th=""><th>٩ĽD</th><th><ld< th=""><th>۲D</th><th>6.000</th><th>۲D</th><th>ŋ,</th><th>Ð</th><th>3.000</th><th>1.000</th><th>3.000</th><th>2.000</th><th>2.000</th><th>3.000</th><th>٩D</th><th>٩</th><th></th><th>3.700</th><th>1.900</th><th></th></ld<></th></ld<></th></ld<>	<ld< th=""><th>٩ĽD</th><th><ld< th=""><th>۲D</th><th>6.000</th><th>۲D</th><th>ŋ,</th><th>Ð</th><th>3.000</th><th>1.000</th><th>3.000</th><th>2.000</th><th>2.000</th><th>3.000</th><th>٩D</th><th>٩</th><th></th><th>3.700</th><th>1.900</th><th></th></ld<></th></ld<>	٩ĽD	<ld< th=""><th>۲D</th><th>6.000</th><th>۲D</th><th>ŋ,</th><th>Ð</th><th>3.000</th><th>1.000</th><th>3.000</th><th>2.000</th><th>2.000</th><th>3.000</th><th>٩D</th><th>٩</th><th></th><th>3.700</th><th>1.900</th><th></th></ld<>	۲D	6.000	۲D	ŋ,	Ð	3.000	1.000	3.000	2.000	2.000	3.000	٩D	٩		3.700	1.900	
I         Sample Supple Vertical         Control Supple Vertical        <	Mo	1.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	e.000	150.000	151.000	152.000	32.000	32.000	33.000	153.000	34.000		134.000	35.000	
I         Sampler         Description         K         Mod         Mod <th>٩N</th> <th>0.600</th> <th>14.000</th> <th>14.000</th> <th>18.000</th> <th>17.000</th> <th>8.000</th> <th>7.000</th> <th>17.000</th> <th>14.000</th> <th>13.000</th> <th>14.000</th> <th>15.000</th> <th>19.000</th> <th>17.000</th> <th>18.000</th> <th>18.000</th> <th>16.000</th> <th>17.000</th> <th>19.000</th> <th>14.000</th> <th>14.000</th> <th>14.000</th> <th>16.000</th> <th>8.000</th> <th>13.000</th> <th>8.000</th> <th>9.000</th> <th>13.000</th> <th>15.000</th> <th>15.000</th> <th>18.000</th> <th>11.000</th> <th>13.000</th> <th>13,000</th> <th>13.000</th> <th>13.000</th> <th>13.000</th> <th>7.000</th> <th>7.000</th> <th>7.000</th> <th>13.000</th> <th>7.000</th> <th></th> <th>11.400</th> <th>5.200</th> <th></th>	٩N	0.600	14.000	14.000	18.000	17.000	8.000	7.000	17.000	14.000	13.000	14.000	15.000	19.000	17.000	18.000	18.000	16.000	17.000	19.000	14.000	14.000	14.000	16.000	8.000	13.000	8.000	9.000	13.000	15.000	15.000	18.000	11.000	13.000	13,000	13.000	13.000	13.000	7.000	7.000	7.000	13.000	7.000		11.400	5.200	
Material	Zr	4.900	128.000	172.000	275.000	253.000	332.000	130.000	575.000	170.000	165.000	178.000	178.000	178.000	164.000	181.000	161.000	165.000	153.000	221.000	158.000	168.000	146.000	186.000	123.000	544.000	157.000	176.000	251.000	214.000	257.000	224.000	118.000	160.000	145.000	156.000	156.000	157.000	34.000	34.000	34.000	160.000	35.000		165.000	53.000	
I         Sendig endity         Example registeries         Evenity endity         K         Total         Y         C         Mod         Co         Y         C         Mod         Y         C         Mod         F         Mod	٨	6.500	27.000	20.000	30.000	30.000	14.000	14.000	30.000	22.000	28.000	27.000	25.000	29.000	25.000	29.000	25.000	25.000	25.000	32.000	28.000	28.000	28.000	30.000	14.000	26.000	21.000	21.000	25.000	29.000	27.000	29.000	25.000	26.000	24.WU	39.000	39.000	39.000	9.000	9.000	9.000	40.000	10.000		40.600	13.000	
Image         Sample         Description         Secription         Secreption         Secreption <th>s</th> <th>0.900</th> <th>324.000</th> <th>303.000</th> <th>191.000</th> <th>269.000</th> <th>99.000</th> <th>147.000</th> <th>182.000</th> <th>243.000</th> <th>224.000</th> <th>288.000</th> <th>661.000</th> <th>191.000</th> <th>233.000</th> <th>180.000</th> <th>236.000</th> <th>259.000</th> <th>260.000</th> <th>263.000</th> <th>194.000</th> <th>183.000</th> <th>189.000</th> <th>179.000</th> <th>150.000</th> <th>245.000</th> <th>394.000</th> <th>391.000</th> <th>516.000</th> <th>204.000</th> <th>216.000</th> <th>255.000</th> <th>439.000</th> <th>214.000</th> <th>188.000</th> <th>72.000</th> <th>71.000</th> <th>72.000</th> <th>337.000</th> <th>339.000</th> <th>340.000</th> <th>73.000</th> <th>346.000</th> <th></th> <th>75.100</th> <th>420.000</th> <th></th>	s	0.900	324.000	303.000	191.000	269.000	99.000	147.000	182.000	243.000	224.000	288.000	661.000	191.000	233.000	180.000	236.000	259.000	260.000	263.000	194.000	183.000	189.000	179.000	150.000	245.000	394.000	391.000	516.000	204.000	216.000	255.000	439.000	214.000	188.000	72.000	71.000	72.000	337.000	339.000	340.000	73.000	346.000		75.100	420.000	
Image         Configment         Configment         Configment         Configment         Con         <	đ	0.900	149.000	122.000	133.000	134.000	12.000	23.000	52.000	118.000	100.000	100.000	141.000	211.000	185.000	193.000	195.000	162.000	191.000	193.000	151.000	162.000	157.000	177.000	22.000	37.000	24.000	29.000	77.000	120.000	98.000	149.000	115.000	101.000	129.000	119.000	120.000	121.000	71.000	71.000	72.000	122.000	73.000	se	126.000		
Image         Sample         Conditional         Sec         Total         Conditional         Sec         Total         Conditional         Sec         Total         Conditional         Sec         Sec         Sec         Sec     <	As	2:900	19.000	8.000	10.000	12.000	8.000	6.000	8.000	5.000	000'6	6.000	12.000	5.000	9.000	14.000	9.000	14.000	7.000	5.000	8.000	12.000	9.000	18.000	7.000	5.000	5.000	6.000	7.000	10.000	13.000	8.000	7.000	000'6	<ul> <li>Control</li> </ul>	58.000	56.000	59.000	51.000	52.000	52.000	58.000	52.000	ptedValu	68.500	67.000	
Image between the sector of the se	Ga	0.700	20.000	16.000	19.000	18.000	4.000	5.000	8.000	21.000	16.000	15.000	20.000	27.000	25.000	24.000	26.000	21.000	25.000	25.000	22.000	24.000	22.000	25.000	6.000	7.000	6.000	6.000	11.000	16.000	14.000	23.000	16.000	16.000	Befere	14.000	15.000	14.000	9.000	8.000	8.000	15.000	9.000	Acce	16.800	12.000	
Image         Sample         Configment         K         Table         Mode	z	3.800	63.000	55.000	52.000	60.000	16.000	21.000	26.000	63.000	66.000	51.000	64.000	75.000	53.000	54.000	51.000	59.000	47.000	84.000	67.000	69.000	64.000	60.000	18.000	25.000	37.000	32.000	50.000	128.000	100.000	59.000	90:00	67.000	000/68	54.000	54.000	54.000	65.000	66.000	66.000	54.000	67.000		64.100	74.000	
Founditient         Evanditient         Evanditient         C         Mod         Mod </th <th>5</th> <th>4.700</th> <th>24.000</th> <th>22.000</th> <th>17.000</th> <th>24.000</th> <th>6.000</th> <th>8.000</th> <th>14.000</th> <th>31.000</th> <th>27.000</th> <th>20.000</th> <th>31.000</th> <th>34.000</th> <th>24.000</th> <th>29.000</th> <th>19.000</th> <th>23.000</th> <th>19.000</th> <th>33.000</th> <th>36.000</th> <th>43.000</th> <th>37.000</th> <th>45.000</th> <th>9.000</th> <th>12.000</th> <th>11.000</th> <th>11.000</th> <th>19.000</th> <th>21.000</th> <th>18.000</th> <th>33.000</th> <th>21.000</th> <th>25.000</th> <th>39.000</th> <th>49.000</th> <th>49.000</th> <th>50.000</th> <th>52.000</th> <th>52.000</th> <th>52.000</th> <th>52.000</th> <th>53.000</th> <th></th> <th>60.200</th> <th>66.000</th> <th></th>	5	4.700	24.000	22.000	17.000	24.000	6.000	8.000	14.000	31.000	27.000	20.000	31.000	34.000	24.000	29.000	19.000	23.000	19.000	33.000	36.000	43.000	37.000	45.000	9.000	12.000	11.000	11.000	19.000	21.000	18.000	33.000	21.000	25.000	39.000	49.000	49.000	50.000	52.000	52.000	52.000	52.000	53.000		60.200	66.000	
Image         Sometyme         Configmenti         Sec         Tot         Y         C         Mod         For         Z           Image         Semety         100         75         100         100         100         100         200           Image         1000         100         100         100         100         100         100         200           Image         1000	ïz	1.500	45.000	36.000	31.000	43.000	9.000	14.000	24.000	40.000	36.000	34.000	43.000	47.000	37.000	51.000	31.000	39.000	43.000	49.000	41.000	46.000	50.000	53.000	14.000	21.000	17.000	21.000	33.000	39.000	31.000	39.000	29.000	33.000	33:000	81.000	80.000	84.000	24.000	26.000	27.000	79.000	27.000		99.500	29.000	
Image         Parameter         P	c	2.200	30.000	26.000	41.000	43.000	173.000	79.000	93.000	33.000	29.000	28.000	19.000	18.000	12.000	19.000	10.000	14.000	16.000	22.000	33.000	24.000	33.000	29.000	117.000	62.000	70.000	65.000	44.000	35.000	45.000	56.000	15.000	33.000	23.000	33.000	31.000	34.000	5.000	5.000	5.000	32.000	6.000		46.800	12.000	
Image and the sector of the secto	Fe203		5.139	4.902	3.206	4.524	0.890	1.482	3.844	4.775	5.196	4.702	5.999	3.169	4.035	6.867	3.687	5.475	3.752	3.188	7.649	6009	9.036	6.915	1.507	3.109	3.285	3.173	4.141	5.135	4.070	5.862	4.903	5.144	168.0	8.559	8.640	8.671	2.686	2.691	2.690	8.790	2.745		9.340	3.030	
Interface         Somelane         Some         Some         Somelane         Some         Som	MnO		0.065	0.038	0.037	0.041	0.018	0.023	0.045	0.060	0.085	0.068	0.049	0.353	0.100	0.114	0.071	0.158	0.104	0.076	0.083	0.066	0.084	0.128	0.023	0.038	0.067	0.070	0.067	0.083	0.073	0.064	0.042	0.082	0.U82	0.042	0.043	0.042	0.031	0.031	0.032	0.042	0.032		0.042	0.034	
Image for a support         Sample for a support         Lunit         K         TO2         V           Image for a support         Unit         St         100         77.9         200         12	ა	3.300	77.000	69.000	89.000	85.000	17.000	22.000	60.000	74.000	60.000	66.000	83.000	104.000	99.000	94.000	95.000	76.000	88.000	95.000	76.000	83.000	84.000	88.000	18.000	46.000	16.000	26.000	64.000	61.000	54.000	97.000	66.000	56.000	68.000	53.000	53.000	51.000	35.000	35.000	34.000	54.000	35.000		66.400	30.000	
Amelie a         Durit (a) but (b) bu	^	1.400	99.000	87.000	94.000	101.000	23.000	30.000	64.000	110.000	87.000	82.000	115.000	137.000	127.000	129.000	131.000	111.000	114.000	130.000	119.000	118.000	124.000	130.000	30.000	48.000	34.000	41.000	64.000	95.000	80.000	130.000	79.000	89.000	10/./UI	140.000	142.000	143.000	127.000	127.000	128.000	142.000	130.000		160.000	130.000	
Image and the set of	Ti02		0.772	0.786	1.046	0.950	0.335	0.319	0.905	0.920	0.786	0.780	0.907	1.100	0.974	1.029	0.990	0.884	0.941	1.085	0.895	0.935	0.921	1.001	0.310	0.644	0.402	0.502	0.685	0.815	0.789	1.183	0.633	0.783	U.834	0.750	0.751	0.760	0.327	0.328	0.330	0.758	0.337		0.710	0.253	
i         Sample r Sample r imit Control         i         i           i         Sample r imit Control         Unit imit Control         Unit imit Control           i         Sample r imit Control         Unit imit Control         Unit imit Control           i         Sample r imit Control         Unit Control         Unit Control           i         Sample r imit Control         Unit Control         Unit Control         Unit Control           i         Sample r imit Control         Unit Control         Unit Control         Unit Control         Unit Control         Unit Control           i         Sample r imit Control         Sample r imit Contro         Unit Control	Sc	1.600	19.000	12.000	12.000	13.000	5.000	6.000	9.000	22.000	16.000	16.000	17.000	18.000	16.000	17.000	17.000	11.000	16.000	19.000	20.000	21.000	23.000	22.000	6.000	8.000	5.000	6.000	9.000	14.000	10.000	22.000	13.000	16.000	70,000	11.000	8.000	10.000	6.000	4.000	3.000	10.000	6.000		13.200	4.600	
Image: State of the second s	tigraphic Unit		LTS	LKSR	LKSR	:KSR	JKSR	JKSR	JKSR	JKSR	LTS	LTS	.KSR	RF	RF	RF	RF	RF	RF	RF	LTS	LTS	LTS	LTS	JKSR	JKSR	LTS	LTS	.KSR	RF	RF	JKSR	.KSR	LTS	12												
Amonte         Amonte           10	₹ Straf	tection	1m)	3m) [	5m) L	3m) L	1m) (	) (mC	tm)	1m)	(me	(mC	Sm) L	(m;	(m)	(m)	(m	(m)	(m	1)(B)	(ju	(m <sup>2</sup>	n) (B	(mC	n)B (	n)B (r	(m)	n)B	Jul)	(m)	n)B	m)B (	1 (m	m)B	Ê	-1	-1	÷	4	Ļ	÷	÷	÷		Ļ	÷.	
Comparison of the second	Sample #	Limit of De	3-88(4185.)	5-88(4331.)	5-88(4329.0	3-88(4327.5	-88(3830.)	7-88(3832.L	7-88(3834.4	7-88(3843.4	3-88(4183.5	7-88(4198.L	3-88(4327.t	-78(4148.3	-78(4146.C	-78(4138.5	-78(4145.5	-78(4140.9	-78(4147.6	78(4148.3m	-52(3757.C	-52(3756.7	52(3757.0n	-52(3754.0	88(3832.0	88(3838.41	388(4188.1	88(4188.1)	388(4330.0	78(4151.75	78(4135.4n	88(3843.41	388(4325.4	88(4183.9	7.CS14)SSC	SDO-	SDO-	SDO-	SGR	SGR-	SGR-	SDO.	SGR-		SDO.	SGR	
	Lab #	ľ	141868Z G	41869Q G	141870B G	141871T G	41872M G	141873E G	41874W G	141875P G	41876H G	141877Z G	141878R G	141879K I-	141880P	1418811 I-	141882B I-	41883U	41884N	418856 -7	141886Z P	141887R P	141888KP-5	41889D P	/M3028 G.	/M3029 G.	M3030 6	/M3031 G.	At3032 6	/#3033 1;	/43034 15	/M3035 G.	A43036 6	M43037 G	v#3U38 (												

All values for trace elements presented in ppm. Sample numbers with (B) are duplicate preparations. Stratigraphic units include the Lower Tempest Sandstone (LTS), Lower Kimmeridgian Source Rock (LKSR), Upper Kimmeridgian Source Rock (UKSR), and the Rankin Formation (RF). Reference standards include the SDO-1 (Devonian Ohio Shale) and the SGR-1 (Green River Shale). Accepted values are available from the United States Geological Survey and were established by Kane et al. (1990) for SDO-1 and by Abbey (1983), Gladney and Roelandts (1988) and Govindaraju (1994) for SGR-1.

## ICP-MS (Trace Elements)

																															۱
		Stratigraphic																													
Lab#	Sample#	Unit	S	F	>	ბ	ą	Ę	8	ž	J	zn z	As Se	æ	Ŷ	Ag	3	Sn S	₽ a	-	г	č	'n	PZ	Ŀ,	Ē	× T	ĥ	Pb	Bi	£
	Limit of Detec:	tion	1747.705.	3 5.7207	1.6048	3.8882	737.3290	1.2783	0.1430	0.8788	0.9718 2.	8634 0.3	859 5.935	17 21.6858	0.1710	0.2148 0	.2282 0.0	1441 0.13	42 0.597	70 21.8412	0.0839	0.1699 \	0.0550 (	0.2429 0.0	0.049	513 0.050	600.0 60	L 0.0510	0.1558	0.0477 C	3331
M41868	G-88(4185.1m)	1 LTS	76321.345	11 4053.5324	4 111.3934	1 87.2014	32672.115	0 664.956.	1 39.7714	1 44.4888 2	7.9987 75	1.8553 19.4	1439 2.597	9 109.9745	3.8976	0.2234 -0	0.0189 6.0	1.34	54 0.421	12 0.5607	36.7706	76.7130	8.8791 3.	3.1417 1.7.	7304 0.20	095 0.19	47 196.36	80 -0.0099	20.4434	0.2721 1:	9790
M41869	G-88(4331.3m)	1 LKSR	64133.362	5 3604.822	5 85.3387	68.9334	30272.783	19 344.244.	1 35.4046	35.1898 3	1.2205 105	5.2596 7.81	195 -0.044	14 107.1868	3 3.1603	0.1305 -0	0.0669 5.5	480 0.75	64 -0.025	30 -0.3445	26.1553	53.1755 (	6.1013 2.	2.0133 1.1	1848 0.1	780 0.14	91 263.05	33 0.0496	16.3627	0.2325 9	3935
M41872	G-88(3830.1m)	N UKSR	41427.285	0 1166.111	0 14.5959	12.2023	3545.4532	2 95.7724	4 218.5515	9 5.4909	8.0841 22	.6444 1.8	778 0.685	13 97.4819	0.8299	0.0853 -0	0.0467 3.6	574 0.24	01 0.445	52 -0.5185	10.7314	23.1114	2.7618 1.	1.0152 0.5.	5152 0.0	682 0.03	75 2137.91	27 0.1122	3.9867	0.0633 2	8166
M41873	G-88(3832.0m)	N UKSR	57787.665	0 1197.700.	1 22.8481	18.9776	7793.9835	5 158.342(	0 110.989	5 12.3606	8.8762 23	1.9752 3.11	196 1.474	12 132.4475	9 0.9384	-0.0176 0	1974 4.2	193 0.26	86 0.462	26 -1.0486	14.8161	31.3914	3.6456 1	4.8026 0.7	787 0.0	818 0.05	32 522.31	36 -0.0020	7.5718	0.1018 3	6383
M41874	G-88(3834.4m)	N UKSR	39489.507	8 3346.242	8 50.9125	46.5390	23274.916.	1 343.052.	1 121.932	1 20.0094 1	7.2300 31	.8730 4.3	773 1.928	122.7793	3 1.3028	0.1876 -0	1.0895 4.6	0.49	40 0.467	77 1.3230	26.2457	52.8180	6.1457 2.	2. 9357 1. 1t	1649 0.1	380 0.11/	49 402.92	38 0.0092	9.9211	0.1735 5	0532
M41875	G-88(3843.4m)	N UKSR	35517.324	10 4736.400t	6 122.5347	90.8839	30962.408	16 490.580	<sup>16</sup> 46.0212	44,4094 3	5.5219 79	0.7531 5.15	957 0.048	117.6629	3 2.1581	0.1694 0.	.0336 5.6	1242 0.57.	58 0.327	76 -0.6803	30.1543 (	61.1097	7.3911 24	8.9653 1.5	808 0.2	140 0.19	64 291.716	51 -0.0208	16.4406	0.3478 1	.2329
M41876	G-88(4183.9m)	1 LTS	63014.625	12 4272.483	4 103.6757	72.9160	36099.396	8 877.951.	2 43.5126	3 40.9441 3	9.0359 10	3.0914 7.7	193 -0.054	11 122.0535	5 0.5274	0.1584 -0	1.1392 5.5	1986 0.62	11 0.731	15 -0.1218	31.2546 (	65.8311	7.7784 3	0.8431 1.9	932 0.3	069 0.21	32 235.78	22 -0.0266	21.1594	0.3007 10	.2124
M41877	, G-88(4198.0m)	1 LTS	70417.862	3 3752.337	8 84.1977	68.5445	29623.846	2 705.493	8 37.3308	36.4677 2	5.0719 71	4453 6.5(	030 -1.060	D5 115.8805	5 0.8106	0.1674 -0	0209 5.5	1024 0.85	65 0.135	55 -0.9728	31.2545 (	65.4995	7.6377 3	0.0577 1.6	337 0.2	396 0.21	19 204.95	31 -0.0443	18.0559	0.2795 10	.0813
M41886	: P-52(3757.0m)	1 LTS	27234.451	0 4076.5378	8 126.1697	89.8372	45250.043	15 650.598.	1 40.1890	1 45.0983 3	8.4180 75	0.4481 9.75	334 0.317	104.4655	5 1.2359	0.2177 -0	0.0189 5.2	1.03	72 0.831	16 -0.4383	32.5621 (	66.2784	7.5506 2	9.6491 1.7	606 0.2	602 0.23	52 244.648	31 0.0291	24.7743	0.3001 1	.2960
M41887	P-52(3756.7m)	1 LTS	23692.036	7 4765.348:	5 141.7306	104.4252	39416.414	12 544.685	4 32.7767	61.1359 5	1.5524 86	343 13.7	7872 4.113	117.0277	7 1.3310	0.1725 0	.1131 6.5	1.37	03 0.515	39 -2.4606	37.5576	77.0172	8.8485 3.	2.9732 1.9	9414 0.2	998 0.27	92 117.246	53 -0.0562	32.4955	0.3697 1	6966.
2	41887 DUP	LTS	22244.035	12 4297.856	0 131.5716	97.7252	36950.433	10 509.474	9 31.2595	55.4497 5	0.0860 84	1.4183 12.4	1019 2.552	98.3072	1.4101	0.2071 0	.0030 5.3	1.14	73 -0.161	11 -2.1184	33.5178 (	68.2143 8	8.1727 2	9.5978 1.7	641 0.4	357 0.21	76 103.48	38 -0.0039	29.5028	0.5078 1	5099
M43028	G88(3832.0m)E	3 UKSR	55970.195	7 1255.348	0 23.2240	20.2815	8317.7532	2 167.996	6 167.697.	7 12.5602	9.3033 22	.4064 3.75	559 1.055	120.3904	1 0.6378	-0.0146 -0	0.1226 4.0	030 0.32	77 0.352	9 0.5274	15.8632	32.9779	4.0656 1.	6.1209 0.8	3776 0.0	981 0.06	67 557.643	19 0.0881	7.9794	0.0757 3	7117
M43029	G88(3838.4m)E	3 UKSR	76577.946	2 2481.400.	1 37.9772	32.8260	21000.437;	3 365.874	3 82.8719	15.0032 1	1.8671 34	1, 1501 3.55	506 5.452	119.7153	3 1.1589	0.0981 -0	1.1008 4.1	312 0.41	41 -0.173	16 0.0290	23.2552	48.1312	5.6108 2.	1.0162 1.1.	1202 0.1	221 0.12	17 329.36	31 0.0029	6.8719	0.1612 7	7228
M43030	G88(4188.1m)	LTS	134660.06	59 1265.516.	1 25.7018	21.0884	20980.230	17 1186.261	19 91.3262	14.0852 1	0.8092 40	0.6641 4.95	556 0.921	0 102.1710	0.6394	0.0133 -0	0.0065 4.0	308 0.49	51 0.993	35 -0.3971	19.7519	40.4737	5.0902 A	0.3891 1.1.	1160 0.1	191 0.08	53 643.592	25 0.0055	9.7813	0.1138 4	8287
M43031	G88(4188.1m)E	3 LTS	135349.99	97 1651.768	5 32.1609	26.5734	21609.720	M 1188.220	75 90.8254	16.2273 1	0.1964 37	7.6923 3.7 <sup>1</sup>	915 2.237	°0 94.4909	0.4221	0.0740 -6	1.1239 3.5	1071 0.55	29 0.168	30 -0.5458	21.9449	43.6053	5.2543 2.	1.1981 1.0	843 0.1	256 0.10	56 638.908	31 0.0057	8.0630	0.1117 5	0398
M43032	. G88(4330.0m)	LKSR	61318.765	18 2774.718	3 57.6836	47.9123	27672.636	4 646.969	17 57.7125	29.9602	8.3306 53	1, 7510 6.6	377 4.993	11 106.0646	5 0.9506	0.1046 -0	0.0130 4.E	026 0.65	04 0.613	38 -1.8329	20.0066	41.0680	4.9044 14	8. 7318 0.9	3992 0.13	255 0.09	89 376.81/	19 0.0151	12.4389	0.1929 7	4639
M43033	178(4151.75m)	RF	34916.366	15 2880.837	6 95.7639	68.9372	35897.364	13 708.558	5 46.5355	41.2225 2	4.7516 15	3.1569 5.85	543 2.995	17 160.3153	3 1.7313	0.2387 0	.0066 5.4	1442 1.02	50 0.000	20 -1.7053	37.6224 8	81.1677	9.4056 3.	6.4234 1.4	1854 0.19	923 0.18	14 337.42	53 -0.0228	17.5180	0.1869 1	5429
M43034	178(4135.4m)B	RF	39077.922	2 2600.507:	3 74.7514	55.5855	28100.155	3 627.981	4 58.4020	36.1564 2	1.8322 12	7.4262 8.28	872 2.786	0 121.9682	2.0855	0.1171 0	.2065 5.2	667 0.95	80 0.465	54 -1.7256	40.1901 1	88.3382 1	0.1832 3.	8.4895 1.2.	2172 0.1	449 0.140	09 334.775	36 -0.0106	13.7424	0.1853 1:	.1998
M43035	G88(3843.4m)E	3 UKSR	26186.755	3 4591.263.	1 123.2114	93.9560	36286.708	434.673	6 63.1037	39.7973 3	0.5829 62	2.1080 5.1(	069 2.395	121.8653	3 2.1920	0.1384 0	.0390 5.7	703 0.46	84 0.014	19 -2.1642	34.7090 (	68.4160	7.5884 2	7.4910 1.2.	223 0.1	518 0.12	51 312.974	17 0.0052	13.8235	0.2954 1:	.1538
M43036	G88(4325.4m)	LKSR	115523.33.	11 2667.093:	3 81.4400	63.6015	32313.881	9 528.980	322.0735	30.0735 1	9.7809 96	1.9788 5.25	525 0.135	4 112.9752	2 1.0484	0.0835 0	.02.74 5.1	05.0 700.50	73 0.423	30 -1.5999	23.1206	49.0754	5.7583 2.	3. 2782 1. 3.	3525 0.1	823 0.12	37 135.460	0.0143	14.7373	0.2192 8	2059
M43037	G88(4183.9m)E	3 LTS	55977.405	18 2903.853.	1 96.1156	69.4550	34011.269	16 789.377	'8 46.3851	38.7771 3	3.9497 87	5237 8.5	392 3.702	0 119.6886	5 0.4520	0.0874 -6	0.0856 4.7	406 0.57	31 -0.035	37 1.8108	22.0724	44.8855	5.4948 2.	1.7855 1.4	1.0 006	483 0.14	98 234.157	70 -0.0203	18.2993	0.2449 7	7271
M43038	G88(4185.4m)	LTS	43867.345	1 3765.011	7 130.7639	90.4819	41532.104	13 761.335.	2 34.0810	48.8958 4	8.0704 118	3.7748 3.25	942 3.700	128.7502	2 0.4777	0.1243 0	.1652 6.5	514 0.50	40 0.116	51 1.9134	24.1924	46.7665	5.5306 2.	1.3646 1.2	2863 0.1	764 0.12	72 194.37	72 -0.0420	25.7546	0.3534 9	4782
2	443038 DUP	LTS	40774.245	13 3397.828.	2 120.3071	83.3905	38301.710	14 702.445 <sup>(</sup>	8 30.9467	45.2663 4	4.8807 11	5.6501 2.8	444 3.776	30 114.9475	5 0.5184	0.0107 0	.0355 5.5	648 0.51	75 0.558	30 1.1185	21.8802	42.2977	5.0715 1:	9.9730 1.3.	3108 0.1	765 0.11	59 184.822	22 -0.0102	24.2051	0.2654 8	5198
													Reference	e Standards	3/Blank																
	BLANK-33		2245.140	1 0.4687	1.5234	0.8954	13.5387	1.6448	1 -0.1332	0.6624	9.0276 2.	2703 0.2	103 1.146	122.3663	3 0.1318	0.0236 -0	0.1556 4.7	00.0 600*	44 0.036	50 4.1384	-0.0163	-0.0380	0.0343 L	0.0738 -0.0	0.0- 7000	075 -0.03	332 -0.494	5 0.0763	0.2143	0.0798 0	6624
	SGR-1B-1		60435.614	V5 1150.031.	1 105.2917	29.6629	16623.866	55 221.857.	3 10.3811	28.2328 6	2.8305 76	3.6568 12.4	1956 5.740	15 137.7595	9 47.9042	0.0385 0	.9964 5.3	3083 2.91	37 0.510	33 1.4111	16.8865	31.6588	3.6202 1.	3.1067 0.8	0.19 0.1	107 0.08	92 5.4575	0.0532	39.0051	0.9108	5605
	6 F O O S		100 00 000	A DEAD OF D	100 LOOD	C0 C3 C3 V	500 CL 00 CL	10V 1 UDC C.	00 30 30 00	1 0 CC 1 V 0	10 10000	C AC TATA	0 V V V V V V V V V V V V V V V V V V V	OCT 005 0.		0 1001 0		010	2000	0000 V.	1000 00		C CAAO F	2 C UDUC 1	C C LLLL	100 000	2000 0 000	10000		1 3265 0	4100

All values for trace elements presented in ppm. Sample numbers with (B) are duplicate preparations. Stratigraphic units include the Lower Tempest Sandstone (LTS), Lower Kimmeridgian Source Rock (LKSR), Upper Kimmeridgian Source Rock (UKSR), and the Rankin Formation (RF). Reference standards include the SDO-1 (Devonian Ohio Shale) and the SGR-1 (Green River Shale). Accepted values are available from the United States Geological Survey and were established by Kane et al. (1990) for SDO-1 and by Abbey (1983), Gladney and Roelandts (1988) and Govindaraju (1994) for SGR-1.

	_	_		_	_		_	-	_	_	_	_	_	_		_	-	_	-	_	_	_	_	_	_	_	_	_	_	_		-
	U	0.0194	1.9522	1.7945	0.6444	0.7905	1.3761	1.7255	1.6233	1.6502	1.8917	2.1893	1.6337	0.6505	1.0368	0.7580	0.6641	1.2849	1.9953	2.0216	1.6293	1.4595	1.3953	1.6533	1.4946		0.0017	5.2508	48.0286		5.4000	48.8 SD 6.5
	£	0.0644	13.8334	11.4800	3.1857	3.9190	9.2184	11.0675	8.9887	9.8131	12.7202	14.1296	11.2111	3.6375	6.7864	4.8716	5.5408	7.5254	11.9371	12.6718	10.8561	8.6650	8.4110	9.3676	8.2673		0.5509	6.5399	14.2153		4.8000	0.5 SD 0.55
	Bi	0.0192	0.3171	0.2818	0.0668	0.1103	0.1845	0.2608	0.2468	0.2296	0.2920	0.3693	0.2850	0.0830	0.1198	0.1300	0.0991	0.2061	0.2545	0.2087	0.3206	0.2596	0.2301	0.3130	0.2874		0.0131	0.8665	0.3391		ы	
	Pb	0.1378	21.6557	17.0595	4.2739	7.8341	10.2237	14.8495	18.6668	16.8679	24.9681	31.1597	26.1454	7.3601	6.3280	10.3453	8.2322	12.0052	16.7222	15.3088	13.5376	16.0526	18.3090	24.8555	22.0384		0.0556	41.9180	30.3528		38.0000	27.9 SD 5.2
	н	0.0375	0.8928	0.7730	0.0287	0.1481	0.3263	0.5868	0.5661	0.5562	0.8929	1.0526	0.8743	0.1089	0.1941	0.1578	0.1544	0.4928	0.7989	0.6362	0.7316	0.6910	0.5710	0.7897	0.7287		-0.0268	0.6187	6.1019		na	
	Ta	0.0113	1.9665	1.9007	8.5502	3.2859	4.1045	1.7525	1.4151	1.4728	1.5988	1.5259	1.2314	5.3612	2.8655	2.9699	2.4192	2.0880	1.5975	2.3541	2.6740	1.1842	1.5782	1.3170	1.1350		0.0074	0.3059	0.9227		na	1.1 SD 0.13
	Ηf	0.0559	3.9881	3.0109	4.1393	1.7534	3.181.5	5.8527	3.0487	2.7927	7.0139	4.8383	3.1049	3.2162	2.4645	1.3890	3.8534	2.2885	2.7906	5.5533	3.1325	2.2878	5.1882	3.1483	2.5970		3.4523	1.6047	8.5568		1.4000	4.7 SD 0.75
	Lu	0.0092	0.2455	0.1975	0.0778	0.0881	0.1389	0.1749	0.2240	0.1847	0.2524	0.3080	0.2294	0.0853	0.1233	0.1300	0.1342	0.1255	0.1746	0.1952	0.1686	0.1721	0.1985	0.1663	0.1419		-0.0041	0.1101	0.4148		na	0.54 SD 0.14
	۲b	0.0399	1.7568	1.3822	0.5278	0.6284	1.0618	1.3700	1.4434	1.4389	1.9865	1.9547	1.4264	0.5652	0.8605	0.7408	1.1769	0.9972	1.2370	1.2883	1.0536	1.1436	1.3032	1.1853	0.9929		0.0170	0.7956	2.7271		0.9400	3.4 Sd 0.46 (
	Tm	0.0081	0.2976	0.2402	0.0963	0.1153	0.1922	0.1982	0.2713	0.2430	0.2667	0.3399	0.2451	0.1011	0.1676	0.1899	0.1379	0.2113	0.2337	0.2112	0.2083	0.2290	0.2076	0.2434	0.2018		-0.0027	0.1603	0.4389		0.1700	.45 SD 0.08
	Er	0.0299	1.8106	1.3734	0.6183	0.8384	1.3480	1.3999	1.6318	1.5646	1.7674	1.9839	1.5154	0.7161	1.1243	1.1460	0.9637	1.2080	1.3097	1.2703	1.1481	1.4263	1.4029	1.3963	1.1652		-0.0340	0.8655	3.1210		1.1000	3,6 SD 0.55 0
	Ю	0.0076	0.6642	0.4756	0.2524	0.3247	0.6662	0.5027	0.6576	0.5665	0.6711	0.6988	0.5349	0.3062	0.4113	0.4084	0.4034	0.3872	0.5304	0.4945	0.4978	0.5754	0.5830	0.5119	0.4439		0.0032	0.3119	1.0995		0.4000	
	Q	0.0201	3.6551	2.3931	1.5115	1.7386	2.4965	2.7760	3.4462	3.1526	3.3870	3.7174	2.8016	1.6855	2.2183	2.4446	2.2497	2.1963	2.8819	3.0984	2.4793	3.3918	3.2535	2.7911	2.2311		0.0248	1.5943	5.4362		1.9000	6.0 SD 0.6
	Tb	0.0080	0.6734	0.4277	0.3100	0.3314	0.4402	0.5114	0.6010	0.5829	0.5726	0.6286	0.4678	0.3218	0.4111	0.4532	0.4230	0.4066	0.5705	0.6118	0.4756	0.6485	0.6021	0.5165	0.4520		0.0023	0.2658	0.9763		na	1.2 SD 0.24
	Gd	0.0407	4.7331	2.9119	2.2185	2.5520	3.3730	3.7126	4.1457	4.5074	4.2965	4.1354	3.5477	2.4498	3.2947	3.7003	3.2855	2.8845	4.7573	4.9772	3.5089	4.9995	4.1855	3.5563	3.0483		0.0149	1.7580	6.8063		2.0000	2 7.4 SD 1.9
	Eu	0.0259	1.3344	0.8145	0.5584	0.6491	0.8712	0.9691	1.0830	1.1568	1.1338	1.1899	0.9423	0.6594	0.8094	0.9939	0.9180	0.7359	1.3595	1.4776	0.9652	1.2821	1.1298	0.9615	0.8047	Irds	-0.0142	0.4232	1.4769	andards	0.5600	1.6 SD 0.2
	Sm	0.0458	6.7496	4.1708	2.5119	3.0813	4.7586	4.6771	5.4102	5.7322	5.6879	6.1779	4.8827	2.8696	3.9278	4.4819	4.2432	3.7992	6.8013	7.8052	5.2493	5.6965	5.0786	4.3907	3.7297	ence Standa	-0.0386	2.2582	7.4854	eference St.	2.7000	7.7 SD 0.8
	Nd	0.1128	35.0315	25.2698	12.8029	15.3996	24.2167	24.6859	26.1774	27.7497	29.2890	32.2915	25.4732	14.7780	19.3170	21.4158	20.7089	17.6723	34.2042	42.7167	27.5463	24.4087	23.5731	20.2451	17.9751	ik and Refer	-0.0473	14.2533	37.3097	d Values - R	16.000	5 36,6 SD 3,3
	Pr	0.0088	9.3511	6.6463	3.1240	3.8415	6.3491	6.3542	6.7568	7.1656	7.3979	8.5388	6.9439	3.6257	5.1619	5.1757	5.1206	5.1120	8.9013	11.1949	7.7765	6.3029	5.8139	5.3451	4.7636	Blar	-0.0037	3.8808	9.2595	Accepte	na	8.9 SD 0.6
	Ce	0.0198	81.2596	59.2426	25.1719	30.8901	53.6777	53.3336	55.2188	60.4289	63.6238	72.4390	57.9294	28.5244	40.1608	40.2179	41.3612	39.6249	74.0593	95.9356	64.8228	52.5523	47.9930	44.2205	37.6356		0.0051	33.8162	76.1373		36.0000	1 79.3 SD 7.8
	гı	0.0120	37.8238	28.7042	11.7400	15.1036	25.5510	25.3775	25.9373	28.8459	30.5816	35.1731	28.3882	14.1983	20.1904	20.1895	21.3517	19.5166	34.0464	43.8582	34.1023	25.2929	22.1930	22.6724	19.5877		0.0018	18.0118	37.3953		20.0000	38.5 SD 4.
	Ba	0.2638	582.4148	464.3940	184.5765	104.5234	138.1922	453.9320	441.0536	288.2229	612.0164	721.6906	531.0332	117.3410	96.4343	235.8918	132.3302	338.0500	380.9687	543.3480	385.4808	355.2393	477.1686	669.3521	558.1393		0.2083	278.6706	454.2658		290.0000	397 SD 38
	Cs	0.0227	10.2189	8.3826	0.5141	1.1939	3.0236	5.8879	5.9989	5.9299	9.7341	11.4789	9.6197	1.1096	1.7689	1.1000	1.2633	4.8056	6.5690	5.2705	8.1102	7.8064	6.3815	8.6548	7.8028		-0.0255	5.1031	6.9378		5.2000	6.9 SD 1.2
	Mo	0.2402	0.8675	1.8264	0.4008	0.5379	0.7133	1.2402	0.3050	0.4027	0.7197	0.8153	0.6944	0.4549	0.4468	0.4049	0.2112	0.4815	1.1506	1.5348	1.4498	0.6931	0.2872	0.2053	0.2248		0.0577	34.0099	170.6324		35.0000	134 SD 21
	Nb	0.0197	13.8872	13.3908	5.2951	3.9617	11.2412	13.3951	11.7442	11.8394	13.1313	14.8643	11.4756	4.3867	7.1463	4.1154	4.8817	9.1406	9.8022	10.6022	15.1945	9.4155	9.7647	11.1025	9.3943		0.0019	5.0945	10.6638		5.2000	11.4 SD 1.2
	Zr	0.0712	74.9470	61.5852	32.1541	21.8503	72.7043	67.6618	63.1241	59.0843	85.5469	96.3702	65.0066	21.6783	50.6003	27.2624	28.2827	43.3567	64.9687	73,8656	56.3706	39.3842	55.2749	51.2295	41.5236		5.1615	24.0725	122.3857		53.0000	165 SD 24
	٢	0.0196	16.2572	11.2834	7.1739	8.0579	10.9427	12.4516	15,5983	14.4484	15.6963	15.8829	12.1993	7.7064	9.8858	11.3308	11.8307	9.3266	11.7180	12.2693	10.2124	14,9015	14.0597	11.7383	10.2691		0.0633	8.3420	31.8560		13.0000	40.6 SD 6.5
	Sr	0.2125	337.0253	342.6913	99.3124	148.4675	183.7520	232.9357	221.5499	289.6110	187.2067	197.3869	162.0034	143.8993	220.0926	390.7704	393.6953	475.6821	196.8504	244.4117	221.7609	460.7754	226.2582	198.9594	170.4974		0.0425	366.1507	77.4066		420.0000	5.1 SD 11.1
	Rb	0.1559	158.8411	139.6306	10.7158	21.9315	53.4674	115.9620	100.5663	101.7581	153.5303	178.1429	147.8157	21.7544	31.9321	22.5524	29.2125	70.7908	119.4125	112.7832	139.1021	123.1906	113.4058	144.7830	125.3666		0.0541	78.5926	134.6900		na	26 SD 3.9 7
	LI I	0.3595	87.0641	66.2608	8.9095	13.9008	33.7237	61.7512	59.2754	61.7224	81.1052	100.7369	82.2127	13.5431	21.0458	19.3184	25.7165	47.2852	58.4606	55.7276	76.7999	73.3136	62.1962	82.0618	73.6518		-0.2856	122.6225	31.8523		147.0000	28.6 sd 5.5 1
tratigraphic	Unit		LIS	LKSR	UKSR	UKSR	UKSR	UKSR	LTS	LTS	LTS	LTS	LTS	UKSR	UKSR	LTS	LTS	LKSR	RF	RF	UKSR	LKSR	LTS	LTS	LTS							
St	nple#	f Detection	(185.1m)	(331.3m)	*830.1m)	832.0m)	\$34.4m)	(843.4m)	:183.9m)	(198.0m)	757.0m)	756.7m)	d.	32.0m)B	38.4m)B	188.1m)	88.1m)B	330.0m)	51.75m)	35.4m)B	343.4m)B	325.4m)	.83.9m)B	185.4m)	b		VNK-33	R-1B-1	0-1-1		-1 USGS	2-1 USGS
	san.	Limit of	68 G-88(4	69 G-88(4	72 G-88(3	73 G-88(3	74 G-88(3.	75 6-88(3.	76 G-88(4.	77 6-88(4.	86 P-52(3.	87 P-52(3.	M41887 DU	28 G88(38	29 G88(38	30 G88(4)	31 G88(41)	32 G88(4:	33 178(41	34 178(41:	35 G88(38	36 G88(4:	37 G88(41.	38 G88(4)	M43038 D U		BLA	SGI	SD		SGR	SDO
	Lab#		M418(	M418t	M4185	M4185	M4185	M4185	M4185	M4185	M418t	M418t		M4302	M4302	M4305	M4305	M4305	M4305	M4305	M4305	M4305	M4305	M4305								

All values for trace elements presented in ppm. Sample numbers with (B) are duplicate preparations. Stratigraphic units include the Lower Tempest Sandstone (LTS), Lower Kimmeridgian Source Rock (LKSR), Upper Kimmeridgian Source Rock (UKSR), and the Rankin Formation (RF). Reference standards include the SDO-1 (Devonian Ohio Shale) and the SGR-1 (Green River Shale). Accepted values are available from the United States Geological Survey and were established by Kane et al. (1990) for SDO-1 and by Abbey (1983), Gladney and Roelandts (1988) and Govindaraju (1994) for SGR-1.

Samplo	Formation				# of grai	ins							Total Heavy Minerals
Sample	Formation	Zircon	Tourmaline	Rutile	Apatite	Monazite	Chromite	Titanite	ZTR ratio	MZi index	RZi index	CZi index	per sample
G-70 (3305)	Upper Kimmeridgian Source Rock	38	397	560	166	17	5	38	-	30.91	93.65	11.63	1221
G-70 (3500)	Upper Kimmeridgian Source Rock	74	121	819	145	11	2	73	81.45	12.94	91.71	2.63	1245
G-70 (3715)	Upper Kimmeridgian Source Rock	31	0	270	303	5	7	58	-	13.89	89.70	18.42	674
P-52 (3400)	Upper Kimmeridgian Source Rock	153	0	868	486	18	26	65	63.18	10.53	85.01	14.53	1616
P-52 (3500)	Upper Kimmeridgian Source Rock	101	0	647	132	8	58	55	74.73	7.34	86.50	36.48	1001
I-78 (4500)	Upper Kimmeridgian Source Rock	162	0	777	70	12	9	14	89.94	6.90	82.75	5.26	1044
I-78 (4705)	Upper Kimmeridgian Source Rock	72	0	290	43	2	2	4	87.65	2.70	80.11	2.70	413
Standard													
Deviation (1 SE)									10.82	9.11	4.89	11.96	
G-70 (4740)	Lower Kimmeridgian Source Rock	45	0	240	16	1	8	5	-	-	-	-	315
G-70 (4820)	Lower Kimmeridgian Source Rock	32	66	426	45	8	3	24	86.75	20.00	93.01	8.57	604
P-52 (3950)	Lower Kimmeridgian Source Rock	41	473	531	597	3	9	103	59.48	6.82	92.83	18.00	1757
G-88 (4495)	Lower Kimmeridgian Source Rock	49	0	354	165	0	5	149	55.82	0.00	87.84	9.26	722
I-78 (5000)	Lower Kimmeridgian Source Rock	154	0	632	76	4	9	22	87.63	2.53	80.41	5.52	897
I-78 (5075)	Lower Kimmeridgian Source Rock	152	0	632	74	1	13	14	88.49	0.65	80.61	7.88	886
Standard													
Deviation (1 SE)									16.48	8.27	6.23	4.77	
G-70 (4200)	Rankin Formation	46	0	306	77	3	5	19	77.19	6.12	86.93	9.80	456
G-70 (4405)	Rankin Formation	75	1	565	131	13	6	58	75.50	14.77	88.28	7.41	849
G-88 (4600)	Rankin Formation	171	1	1363	192	6	195	96	75.84	3.39	88.85	53.28	2024
G-88 (4000)	Rankin Formation	158	0	795	131	10	7	65	81.73	5.95	83.42	4.24	1166
I-78 (4900)	Rankin Formation	57	1	455	107	7	40	80	68.67	10.94	88.87	41.24	747
Standard													
Deviation (1 SE)									4.69	4.56	2.29	22.46	
P-52 (3210)	Upper Tempest Sandstone	489	0	272	23	11	11	2	94.18	2.20	35.74	2.20	808
G-88 (3600)	Upper Tempest Sandstone	50	0	400	55	6	14	17	83.03	10.71	88.89	21.88	542
G-88 (3700)	Upper Tempest Sandstone	49	0	298	69	2	19	19	76.10	3.92	85.88	27.94	456
G-88 (3500)	Upper Tempest Sandstone	193	0	1197	135	5	14	59	86.71	2.53	86.12	6.76	1603
Standard													
Deviation (1 SE)									7.54	3.99	25.65	12.19	
P-52 (3600)	Lower Tempest Sandstone	36	230	479	345	5	31	54	63.14	12.20	93.01	46.27	1180

Appendix B – Heavy Mineral Data & Grain Size Distributions



Grain size distribution of heavy minerals in samples from the Lancaster G-70 well calculated by the MLA/SEM. X-axis shows sieve size ( $\mu$ m) and y-axis shows cumulative passing wt.%. As sieve size increases, a greater percentage of mineral grains will pass through a particular sieve size.



Grain size distribution of heavy minerals in samples from the South Tempest G-88 well calculated by the MLA/SEM. X-axis shows sieve size (µm) and y-axis shows cumulative passing wt.%. As sieve size increases, a greater percentage of mineral grains will pass through a particular sieve size.



Grain size distribution of heavy minerals in samples from the Baccalieu I-78 well calculated by the MLA/SEM. X-axis shows sieve size ( $\mu$ m) and y-axis shows cumulative passing wt.%. As sieve size increases, a greater percentage of mineral grains will pass through a particular sieve size.



Grain size distribution of heavy minerals in samples from the Panther P-52 well calculated by the MLA/SEM. X-axis shows sieve size ( $\mu$ m) and y-axis shows cumulative passing wt.%. As sieve size increases, a greater percentage of mineral grains will pass through a particular sieve size.

## Appendix C – Detrital Zircon U-Pb Data

Baccalieu I-78	(4500 m	) Sampl	le
----------------	---------	---------	----

| 3511 300)*100                           | 3.3                 | 6.4        |            | 1.0        | 1.0                    | 1.0<br>7.7<br>4.9    | 1.0<br>7.7<br>4.9<br>5.2     | 1.0<br>7.7<br>4.9<br>5.2<br>3.7      | 1.0<br>7.7<br>5.2<br>8.8<br>8.8   | 1.0<br>7.7<br>4.9<br>5.2<br>3.3<br>8.8<br>8.8<br>8.0<br>8.0  | 1.0<br>7.7<br>4.9<br>5.2<br>3.3.7<br>8.8<br>8.8<br>8.0<br>8.0<br>8.0   | 1.0<br>7.7<br>5.5.2<br>5.5.2<br>8.8<br>8.8<br>8.8<br>8.8<br>8.8<br>8.8<br>8.8<br>8.5<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7   | 1.0<br>7.7<br>4.9<br>5.5<br>2.5<br>2.5<br>2.5<br>2.5<br>2.5<br>2.5<br>2.5<br>2.5<br>2.5  | 110<br>7.77<br>5.52<br>5.52<br>5.52<br>8.82<br>8.82<br>8.80<br>8.85<br>7.8<br>7.8<br>7.8   | 1.0<br>7.7<br>5.5<br>5.4<br>9.3<br>8.8<br>8.8<br>8.8<br>9.0<br>9.0<br>0.2<br>8.8<br>5.0<br>0.2<br>8.8<br>0.2<br>8.8<br>0.2<br>8.8<br>0.2<br>8.8<br>0.2<br>8.8<br>0.2<br>8.8<br>0.2<br>8.0<br>0.2<br>8.9<br>0.2<br>8.9<br>0.2<br>8.9<br>0.0<br>1.0<br>1.0<br>1.0<br>1.0<br>1.0<br>1.0<br>1.0<br>1.0<br>1.0   | 1.0<br>7.7.7<br>7.4.9<br>8.8.8<br>8.8.8<br>8.8.0<br>9.0<br>2.0<br>2.0<br>8.8<br>8.8<br>8.8<br>8.8<br>8.8<br>7.7<br>8<br>8.8<br>9.0<br>2.2<br>7<br>7<br>8.8<br>8.0<br>9.0<br>2.7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7  | 10<br>7.7.7<br>7.7.7<br>5.5.2<br>3.3.7<br>3.3.7<br>8.8.8<br>8.8.8<br>8.8.8<br>8.8.8<br>8.8.8<br>8.8.5<br>7.7.8<br>0.002<br>7.8<br>7.8<br>7.8<br>7.8<br>7.8<br>7.8<br>7.8<br>7.8<br>7.8<br>7.8  | 10<br>777<br>552<br>552<br>552<br>552<br>552<br>880<br>880<br>880<br>880<br>502<br>880<br>778<br>893<br>773<br>817<br>773<br>817<br>7178  |
10<br>7.7.7<br>7.7.7<br>8.8.8<br>8.8.8<br>8.8.0<br>9.8.5<br>9.9.0<br>9.0.2<br>9.0.2<br>9.0.2<br>7.7.8<br>9.0.2<br>9.0.2<br>7.7.8<br>9.0.2<br>7.7.8<br>9.0.2<br>7.7.8<br>9.0.2<br>7.7.8<br>9.0.2<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7 | 10<br>7.77<br>8.82<br>8.80<br>8.80<br>8.80<br>9.93<br>9.93<br>7.93<br>7.93<br>7.93<br>7.93<br>7.93<br>7.93   | 10<br>777<br>777<br>888<br>880<br>880<br>880<br>880<br>880<br>712<br>880<br>717<br>847<br>71<br>71<br>71<br>71   |
10<br>7.7.7<br>7.7.7<br>7.7.8<br>8.8.8<br>8.8.8<br>8.8.8<br>8.8.0<br>9.9<br>9.9<br>1.1.5<br>5.6.2<br>7.1.8<br>1.1.5<br>5.6.2<br>7.1.8<br>5.6.2<br>7.1.8<br>5.6.2<br>7.7.8<br>5.6.2<br>7.7.8<br>5.6.2<br>7.7.8<br>5.6.2<br>7.7.8<br>5.6.2<br>7.7.8<br>5.6.2<br>7.7.7<br>7.7.8<br>5.6.2<br>7.7.8<br>5.6.2<br>7.7.8<br>5.6.2<br>7.7.8<br>5.6.2<br>7.7.8<br>5.6.2<br>7.7.8<br>5.6.2<br>7.7.8<br>5.6.2<br>7.7.8<br>5.6.2<br>7.7.8<br>5.6.2<br>7.7.8<br>5.6.2<br>7.7.8<br>5.6.2<br>7.7.8<br>5.6.2<br>7.7.8<br>5.6.2<br>7.7.8<br>5.6.2<br>7.7.8<br>5.6.2<br>7.7.8<br>5.7.8<br>5.7.8<br>5.7.8<br>5.7.8<br>5.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>5.7.7<br>7.7.8<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.8<br>7.7.8<br>7.7.8<br>7.7.8<br>7.7.8<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.8<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7.7<br>7.7 | 10<br>777<br>8.52<br>8.80<br>8.80<br>8.80<br>7.80<br>7.80<br>7.81<br>7.11<br>7.12<br>7.11<br>7.12<br>7.11<br>7.12<br>7.12<br>7.1  | 10<br>777<br>777<br>852<br>888<br>880<br>880<br>880<br>880<br>7128<br>993<br>7128<br>7128<br>7128<br>7128<br>714<br>71<br>718<br>850<br>71<br>718<br>850<br>71   | 10<br>7.7.7<br>7.7.7<br>7.7.8<br>8.8.8<br>8.8.8<br>9.002<br>9.002<br>9.9.9<br>1.1.5<br>8.8<br>1.1.5<br>8.8<br>1.1.5<br>8.8<br>1.1.5<br>8.8<br>1.1.5<br>8.8<br>1.1.5<br>8.8<br>1.1.5<br>8.8<br>1.1.5<br>8.8<br>1.1.5<br>8.8<br>1.1.5<br>8.8<br>1.1.5<br>8.8<br>1.1.5<br>8.8<br>1.1.5<br>8.8<br>1.1.5<br>8.8<br>8.8<br>8.8<br>1.1.5<br>8.8<br>8.8<br>8.8<br>8.8<br>8.8<br>8.8<br>8.8<br>8.8<br>8.8<br>8   
  | 10<br>777<br>552<br>553<br>553<br>553<br>888<br>880<br>880<br>115<br>880<br>71<br>71<br>71<br>71<br>71<br>71<br>888<br>737<br>71<br>71<br>888<br>737<br>70<br>10<br>73<br>10<br>70<br>888<br>70<br>70<br>70<br>70<br>70<br>70<br>70<br>70<br>70<br>70<br>70<br>70<br>70  
  | 10<br>7.77<br>7.77<br>8.88<br>8.80<br>8.80<br>8.80<br>7.78<br>8.80<br>7.17<br>8.80<br>7.17<br>8.80<br>7.12<br>8.80<br>7.12<br>8.80<br>7.12<br>8.80<br>7.12<br>7.12<br>7.12<br>7.12<br>7.12<br>7.12<br>7.12<br>7.12   
   | 10<br>17.7<br>17.7<br>17.7<br>17.7<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17.5<br>17   | 10<br>777<br>777<br>777<br>777<br>771<br>771<br>771<br>7   
   | 10<br>7.77<br>7.77<br>8.88<br>8.88<br>8.80<br>7.78<br>8.80<br>7.12<br>8.81<br>7.12<br>8.81<br>7.12<br>8.81<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.82<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>8.83<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>7.12<br>8.83<br>8.83<br>8.83<br>8.83<br>8.83<br>8.83<br>8.83<br>8.8  | 10<br>777<br>777<br>777<br>755<br>888<br>886<br>886<br>886<br>755<br>751<br>753<br>755<br>755<br>755<br>755<br>755<br>755<br>755<br>755<br>755   
   | 10<br>777<br>777<br>777<br>888<br>880<br>990<br>900<br>880<br>712<br>712<br>880<br>712<br>712<br>880<br>880<br>880<br>880<br>880<br>880<br>880<br>880<br>880<br>88  | 10<br>7.7.7<br>7.7.7<br>8.8.8<br>8.8.8<br>8.8.8<br>8.8.8<br>7.1.8<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>7.1.2<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.8.1<br>8.5 |
|---|---------------------|------------|------------|------------|------------------------|----------------------|------------------------------|--------------------------------------|---|--|--|---|--|--|---|--|--|---
--	--	--
--
--|---
--
--|--
--
--
---|---|
| 100 age /207Ph-2                        | 6                   | 96         | Ś          | 6          | 196                    | 6668                 | 6 6 8 8                      | 999                                  | 2 6 6 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8   |  |  |   |  |  |   |  |  | (9) (2) (2) (2) (2) (2) (2) (2) (2) (2) (2  | (2) (2) (2) (2) (2) (2) (2) (2) (2) (2)       
  |  | (9 9 9 8 8 8 8 8 8 8 9 9 9 9 8 2 9 9 8 8 8 8   | (2) (2) (2) (2) (2) (2) (2) (2) (2) (2)  
  | (9,9,9,9,9,9,9,9,9,9,9,9,9,9,9,9,9,9,9,   | (2) 20 30 30 30 30 30 30 40 30 40 30 40 30 40 40 40 40 40 40 40 40 40 40 40 40 40  | (2) (2) (2) (2) (2) (2) (2) (2) (2) (2)   
  | 0  
  | (2) 20 30 30 30 30 30 30 40 40 40 40 40 40 40 40 40 40 40 40 40  
   | (2) (2) (2) (2) (2) (2) (2) (2) (2) (2)  | (2) (2) (2) (2) (2) (2) (2) (2) (2) (2)  
   | (2) 20 30 30 30 30 30 30 30 40 40 40 40 40 40 40 40 40 40 40 40 40   | (9,9,9,9,9,9,9,9,9,9,9,9,9,9,9,9,9,9,9,  
   | (2) (2) (2) (2) (2) (2) (2) (2) (2) (2)   |   |
| e/zurr=zuru uye/ zuu                    | /3.9                | 91.0       |            | /4.3       | 90.0                   | /4.3<br>90.0<br>84.1 | 74.3<br>90.0<br>84.1<br>79.1 | 79.1<br>90.0<br>84.1<br>79.1<br>20.1 | 74.3<br>90.0<br>84.1<br>79.1<br>20.1<br>90.7  | 9.4.3<br>9.00<br>8.4.1<br>7.9.1<br>20.1<br>90.7<br>94.6  | 9.4.3<br>9.4.1<br>79.1<br>20.1<br>94.6<br>91.8<br>91.8   |   | 90.0<br>90.0<br>84.1<br>20.1<br>20.1<br>94.6<br>94.6<br>94.8<br>93.2<br>93.2   | 90.0<br>90.1<br>79.1<br>20.1<br>20.1<br>94.6<br>94.6<br>91.8<br>91.8<br>91.3<br>95.2   | 9.0.0<br>8.4.1<br>7.9.1<br>20.1<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.8<br>9.4.8<br>9.3.2<br>9.5.4<br>9.5.4<br>103.9  | 9.0.0<br>8.4.1<br>78.4.1<br>79.1<br>20.1<br>20.1<br>94.6<br>94.6<br>94.6<br>94.6<br>94.8<br>93.2<br>93.2<br>93.2<br>55.4<br>1033.9<br>55.4<br>1033.9<br>55.4   | 90.0<br>84.1<br>79.1<br>20.1<br>20.1<br>20.1<br>20.1<br>94.6<br>94.6<br>95.8<br>95.4<br>103.9<br>95.4<br>103.9<br>85.8<br>83.8<br>83.8   | 9.0.0<br>9.0.1<br>8.4.1<br>7.9.1<br>2.0.1<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.8<br>9.4.8<br>9.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8 |
9.0.0<br>8.4.1<br>7.9.1<br>7.9.1<br>2.0.1<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.8<br>9.2.2<br>9.3.2<br>9.3.3<br>9.3.3<br>9.3.3<br>9.3.3<br>9.3.3<br>9.3.3<br>9.3.3<br>9.3.3<br>9.3.3<br>9.3.3<br>9.3.3<br>9.3.3<br>9.3.3<br>9.3.3<br>9.3.3<br>9.3.3<br>9.3.4<br>9.3.4<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6.6<br>9.4.6.6<br>9.4.6.6<br>9.4.6.6.6<br>9.4.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6.  | 9.0.0<br>9.0.1<br>9.1.1<br>2.0.1<br>2.0.1<br>9.1.6<br>9.1.8<br>9.2.2<br>95.4<br>95.4<br>103.9<br>5.8<br>103.8<br>83.8<br>83.8<br>83.8<br>83.8<br>83.8<br>90.6<br>90.6  | 9.0.0<br>9.0.1<br>8.1.1<br>2.0.1<br>9.1.8<br>9.1.8<br>9.1.8<br>9.2.4<br>9.2.8<br>9.2.4<br>9.2.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.8<br>8.5.4<br>9.0.6<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.4<br>8.0.40 |
9.0.0<br>8.4.1<br>7.9.1<br>7.9.1<br>7.9.1<br>7.9.1<br>9.0.7<br>9.2.8<br>9.2.2<br>9.3.2<br>9.3.2<br>9.3.3<br>9.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.8<br>15.3.9<br>15.5.8<br>15.5.8<br>15.5.8<br>15.5.8<br>15.5.8<br>15.5.8<br>15.5.8<br>15.5.8<br>1  | 90.0<br>84.1<br>79.1<br>20.1<br>20.1<br>20.1<br>20.1<br>20.2<br>20.2<br>20.2<br>20  | 9.0.0<br>9.0.1<br>8.1.1<br>2.0.1<br>2.0.1<br>2.0.1<br>2.0.1<br>2.0.1<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.8<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.2.9<br>3.0.000000000000000000000000000000000  | 90.0<br>84.1<br>78.41<br>78.41<br>70.1<br>20.1<br>20.1<br>94.6<br>94.8<br>95.8<br>95.4<br>95.8<br>95.8<br>95.8<br>95.8<br>95.8<br>95.8<br>95.8<br>95.8  
  | 90.0<br>8.1<br>7.9<br>20.1<br>20.1<br>20.1<br>20.1<br>20.2<br>20.2<br>20.2<br>20.6<br>20.6<br>20.6<br>20.6<br>20.6   
  | 9.0.0<br>8.4.1<br>7.9.1<br>7.9.1<br>7.9.1<br>9.4.6<br>9.4.6<br>9.4.6<br>9.3.2<br>9.3.2<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8011.0.5.8011.0.5.8011.0.5.8011.0.5.8011.0.5   
   | 9.0.0<br>8.4.1<br>7.9.1<br>2.0.1<br>9.0.7<br>9.0.7<br>9.1.8<br>9.2.2<br>9.3.2<br>9.3.2<br>9.3.8<br>8.3.8<br>8.3.8<br>8.3.8<br>8.3.8<br>8.3.8<br>8.3.8<br>8.3.8<br>8.3.8<br>8.3.6<br>9.0.6<br>9.0.6<br>9.0.6<br>9.3.3<br>1.105.6<br>1.105.6<br>9.3.3<br>9.3.3<br>9.4.0<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6<br>9.4.6.6<br>9.4.6.6<br>9.4.6.6<br>9.4.6.6.6<br>9.4.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6.6.  | 90.0<br>90.1<br>90.1<br>20.1<br>20.1<br>20.1<br>20.1<br>20.2<br>20.2<br>20.2<br>2  
   | 9.0.0<br>8.4.1<br>7.9.1<br>7.9.1<br>7.9.1<br>9.4.6<br>9.4.6<br>9.4.6<br>9.8.2<br>9.8.2<br>9.8.2<br>9.8.2<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8<br>1.0.5.8011.0.5.8011.0.5.8010000000000000  | 9.0.0<br>8.4.1<br>7.9.1<br>7.0.1<br>7.0.1<br>7.0.1<br>7.0.1<br>9.4.6<br>9.4.6<br>9.4.6<br>9.5.8<br>8.0.5<br>8.0.5<br>8.0.6<br>9.0.6<br>9.0.6<br>9.4.0<br>1.0.6<br>9.4.0<br>1.0.6<br>8.2<br>1.0.6<br>9.3.3<br>9.4.0<br>1.0.6<br>9.4.0<br>1.0.6<br>9.4.0<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.0.7<br>1.  
   | 9.0.0<br>9.0.1<br>9.1.1<br>9.1.7<br>9.1.6<br>9.1.8<br>9.1.8<br>9.1.8<br>9.2.8<br>9.2.8<br>9.0.6<br>9.0.6<br>9.0.6<br>9.0.6<br>9.0.6<br>9.0.6<br>1105.8<br>9.0.6<br>1105.8<br>9.0.6<br>1105.8<br>9.0.6<br>1105.8<br>9.0.6<br>1105.8<br>9.0.6<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>1105.8<br>10 | 9.0.0<br>8.4.1<br>7.9.1<br>7.9.1<br>7.9.1<br>9.4.6<br>9.4.6<br>9.4.6<br>9.3.8<br>9.3.8<br>9.3.8<br>1.0.3.8<br>1.0.3.8<br>1.0.3.8<br>1.0.4<br>9.4.0<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4<br>1.0.4        |
| 34 49                                   |                     | 71         | 1400       |            | 37                     | 37<br>43             | 37<br>43<br>28               | 37<br>43<br>28<br>36                 | 37<br>43<br>28<br>36<br>27<br>27  | 37<br>43<br>28<br>36<br>27<br>56   | 37<br>43<br>28<br>36<br>27<br>56<br>36   | 37<br>43<br>28<br>36<br>27<br>56<br>36<br>40  | 37<br>43<br>28<br>36<br>56<br>56<br>40<br>26<br>26   | 37<br>37<br>28<br>36<br>36<br>56<br>56<br>36<br>36<br>36<br>26<br>26<br>26<br>36<br>20   | 37<br>37<br>43<br>28<br>36<br>56<br>36<br>40<br>26<br>100<br>70   | 37<br>37<br>28<br>36<br>27<br>56<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>70<br>70<br>70   | 37<br>28<br>38<br>38<br>36<br>36<br>40<br>40<br>36<br>36<br>36<br>36<br>36<br>30<br>37<br>37<br>37<br>37<br>37<br>37<br>37<br>37<br>37<br>37<br>37<br>37<br>37   | 37<br>28<br>28<br>36<br>36<br>40<br>40<br>36<br>36<br>36<br>36<br>30<br>37<br>30<br>30<br>30<br>30<br>30<br>30<br>30<br>30<br>30<br>30<br>30<br>30<br>30  |
37<br>38<br>38<br>38<br>38<br>38<br>38<br>38<br>38<br>38<br>38<br>38<br>38<br>38   | 37<br>37<br>28<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>100<br>26<br>26<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36  | 37<br>37<br>23<br>38<br>38<br>38<br>36<br>40<br>26<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>37<br>38<br>36<br>36<br>37<br>36<br>36<br>36<br>36<br>37<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36   | 37<br>38<br>28<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36  
   | 37<br>37<br>28<br>28<br>28<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>28<br>28<br>28<br>28<br>27<br>28<br>28<br>27<br>28<br>28<br>210<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20<br>20   | 37<br>36<br>23<br>23<br>23<br>23<br>23<br>23<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>27<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26   | 37<br>38<br>28<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36   
   | 37<br>38<br>28<br>28<br>28<br>29<br>29<br>26<br>38<br>26<br>38<br>26<br>38<br>26<br>41<br>41<br>38<br>41<br>31<br>30<br>38<br>31<br>38<br>31<br>38<br>31<br>38<br>38<br>38<br>38<br>38<br>38<br>38<br>38<br>38<br>38<br>38<br>38<br>38  
   | 37<br>36<br>236<br>237<br>236<br>236<br>236<br>40<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>27<br>28<br>26<br>27<br>28<br>24<br>27<br>28<br>24<br>27<br>28<br>24<br>27<br>28<br>26<br>28<br>27<br>28<br>28<br>28<br>27<br>28<br>28<br>28<br>28<br>28<br>28<br>28<br>28<br>28<br>28<br>28<br>28<br>28   
  | 37<br>38<br>38<br>38<br>38<br>38<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36<br>36   | 37<br>38<br>23<br>23<br>23<br>25<br>43<br>40<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26  
  | 37<br>38<br>236<br>237<br>236<br>36<br>40<br>236<br>40<br>236<br>240<br>238<br>41<br>238<br>41<br>110<br>110<br>110<br>238<br>41<br>41<br>41<br>33<br>54<br>41<br>33<br>54<br>41<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>41<br>38<br>411<br>10<br>41<br>110<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>1  | 37<br>38<br>236<br>236<br>236<br>36<br>40<br>100<br>41<br>258<br>41<br>254<br>41<br>254<br>41<br>1100<br>41<br>1100<br>41<br>1150<br>1150<br>1150<br>115  
  | 37<br>36<br>236<br>237<br>236<br>236<br>236<br>40<br>236<br>738<br>738<br>738<br>738<br>738<br>738<br>738<br>738<br>738<br>738  | 37<br>36<br>236<br>237<br>236<br>237<br>236<br>40<br>236<br>240<br>238<br>41<br>238<br>41<br>238<br>41<br>110<br>241<br>241<br>24<br>24<br>24<br>24<br>24<br>24<br>24<br>24<br>24<br>24<br>24<br>24<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26<br>26   |
| 17 535                                  |                     | 24 1173    | 180 7600   | 16 602     |                        | 19 679               | 19 679<br>10 464             | 19 679<br>10 464<br>29 433           | 19         679           10         464           29         433           11         365 | 19         679           10         464           29         433           11         365           19         957 | 19         679           10         464           29         433           29         433           11         365           19         957           16         596 | 19         679           10         464           29         433           29         433           11         365           19         957           16         957           18         630   | 19         679           10         464           229         433           111         365           129         957           13         957           14         429           14         429 | 19         679           10         464           229         433           11         365           12         957           13         957           14         429           14         429           14         429           17         1720                          | 19         679           10         464           29         433           29         433           11         365           13         365           14         396           15         596           16         596           18         630           19         423           20         14           21         420           22         1720           24         1035 | 19         679           110         464           123         365           139         957           19         957           19         957           19         957           19         957           16         596           18         630           14         429           130         221           1304         1304           21         1304  | 19         679           10         464           11         365           11         365           11         365           12         957           13         630           14         429           14         429           14         429           14         429           14         429           12         1035           21         1035           21         1035           13         400   | 19         679           10         464           11         365           11         365           11         365           12         957           13         679           14         429           14         429           27         1720           27         1720           23         1035           24         1035           21         1304           21         1304           21         1304           17         821           17         821  | 19         679           20         464       
   20         464           21         365           11         365           19         957           19         957           19         957           19         956           19         957           19         956           20         966           21         120           22         1036           21         1304           21         1304           21         1304           21         1304           21         1304           21         1304           21         1304           21         600  | 19         679           10         679           11         365           12         35           13         365           14         365           15         396           16         396           16         396           16         396           1720         147           124         129           224         1035           21         13035           21         13035           21         13035           21         13035           21         13035           21         13035           21         13046           21         400           21         600           21         610   | 19         679           20         464           20         463           11         365           11         365           11         365           11         365           12         597           13         597           14         423           14         423           13         1720           24         1035           24         1036           21         1704           22         1304           1304         661           14         661           15         820           25         823   | 19         679           20         464           20         464           21         365           11         365           19         957           19         957           19         957           19         956           19         957           19         957           24         1035           27         10304           27         10304           27         10304           10         10304           10         10           21         13034           10         801           10         801           10         801           10         801           11         801           12         14           661         812           23         1910   
  | 19         673           10         464           10         464           11         355           11         355           12         355           16         357           16         367           16         367           16         367           21         1720           22         1720           23         1720           24         1035           21         1204           103         211           120         400           21         1304           21         1304           22         1304           23         1305           24         661           25         812           25         821           25         1292           29         1292           29         1292  | 19         679           20         464           20         463           11         365           11         365           11         365           11         365           12         597           13         565           14         365           15         567           16         596           24         1035           24         1035           24         1035           24         1035           27         1720           17         821           1304         661           25         812           25         812           25         812           255         812           255         812           255         666   | 19         673           29         464           29         463           29         464           21         11           26         464           21         955           21         956           21         957           22         1720           23         1720           24         1035           21         1035           21         1035           21         1035           21         1035           21         1035           22         1036           23         1304           24         1304           25         821           26         93           27         1304           28         1304           29         1304           21         646           23         1910           23         1910           24         686  
  | 19         673           20         673           21         20         464           21         21         355           11         355         353           16         356         363           16         356         365           16         356         367           16         366         366           21         1720         361           22         1720         303           23         1720         304           103         211         1304           21         1304         821           23         1304         821           24         661         312           25         812         812           25         312         666           25         1292         666           25         1291         666           25         657         656           555         655         656  
  | 13         673           29         464           29         464           29         464           21         11           365         56           11         957           16         956           16         966           16         966           16         966           21         1170           22         11304           23         11304           21         11304           22         11304           23         12103           24         403           251         1304           261         1003           271         1304           283         13910           293         1910           293         1910           293         1910           293         1910           294         660           295         6160           296         636           2910         638           2911         377  
   | 13         673           29         673           29         464           29         463           11         955           13         955           14         956           16         956           18         630           18         630           18         630           22         11720           21         11720           22         1035           21         1035           21         1035           21         1035           22         1035           23         1010           24         1035           25         812           26         120           27         1035           28         1210           29         121           29         121           29         121           29         137           29         137           29         137           29         137           29         137           29         137           29         646   | 19         679           20         679           21         20           21         355           21         355           21         355           21         355           22         34           23         355           24         355           25         351           365         366           37         1705           36         300           37         1304           37         1304           37         1304           37         1304           37         1304           37         1304           37         666           37         666           37         667           37         668           37         658           37         458           37         458   
   | 13         673           29         4673           29         464           29         464           20         464           21         11           26         56           26         56           26         56           26         56           27         11720           28         11304           29         404           20         400           21         1304           22         1304           23         1304           24         661           25         12910           263         13040           27         1304           283         13010           294         661           295         1297           295         12910           296         13010           296         13010           296         13010           296         13010           297         663           298         111           307         663           203         131           304   | 10         673           29         673           29         464           29         463           21         11           26         464           26         464           26         464           26         464           27         11           27         11720           27         11720           27         1035           21         1035           21         1036           21         1035           21         1036           21         1035           21         1035           21         1036           21         610           22         11           23         121           24         685           13         646           635         1310           23         131           243         645           253         131           263         1232           21         635           23         133           458         1365  
   | 19         673           20         673           21         724           11         355           12         355           13         355           14         357           15         356           21         1305           22         1420           23         1420           24         1035           21         1720           22         1420           23         1304           24         661           255         812           255         812           255         812           255         812           255         812           255         812           255         812           255         812           255         656           255         657           256         658           257         812           256         658           253         1292           254         137           255         658           256         658      256         53   | 13         673           29         4673           29         4674           29         463           11         355           14         596           21         355           21         356           21         356           21         356           22         31           23         11720           24         403           27         11720           21         1304           22         1304           23         1304           24         600           253         1304           263         1304           271         1304           283         1310           293         1312           293         1312           293         1312           293         1312           293         1312           293         1312           293         1312           293         131           293         131           293         1325           293         503           293   |
| 567 17<br>1187 24                       | 1187 24             | 1000       | 1880 1.84  | 596 16     | 669 19                 |                      | 415 10                       | 415 10 739 29                        | 415 10<br>739 29<br>372 11  | 415         10           739         29           372         11           968         19                          | 415         10           739         29           372         11           968         19           602         16   | 415         10           739         29           372         11           968         19           602         16           620         18           620         18  | 415         10           739         29           372         11           968         19           602         16           620         18           633         14           6432         14   | 415         10           739         29           737         11           968         19           602         16           632         18           632         18           632         18           632         18           632         18           633         1706 | 415         10           739         29           372         11           968         19           968         19           602         16           602         16           620         18           620         18           1706         27           1022         24  | 415         10           739         29           372         11           968         19           602         16           620         18           620         18           1070         23           10705         24           10705         27           11020         27           1163         21  | 415         10           739         29           739         29           372         11           968         19           602         16           632         14           432         14           1706         27           1022         24           1169         27           1169         21           1371         10  | 415         10           739         20           372         11           968         19           962         16           602         16           620         18           620         18           1706         27           1102         24           1103         27           371         10           371         10           371         10           371         170           810         17   | 415         10           739         20       
   372         11           968         19           968         19           602         18           602         18           620         18           10706         27           11202         24           11202         27           371         10           810         11           810         11           810         17           810         17           831         14   | 415         10           739         20           737         11           968         19           968         19           602         14           602         14           1706         27           1706         27           11022         21           371         11022           371         11022           371         10           371         10           371         10           830         17           831         17           833         14           533         14   | 415         10           739         11           372         11           968         16           978         13           978         14           978         14           978         14           978         14           978         14           978         14           979         23           1106         21           11169         21           11169         21           331         11           831         14           563         14           831         14           831         14           831         14           831         14           831         14           831         14           831         14  | 415         10           739         20           739         21           958         19           968         19           660         18           660         18           660         18           673         18           1012         21           1169         21           1169         21           1169         21           831         10           833         14           833         14           833         14           833         14           833         14           833         14           833         14           834         21           832         14           833         14           834         21           830         53           830         53           831         54           820         53   
  | 415         10           739         11           372         11           968         13           972         13           972         13           602         16           620         18           620         18           1102         24           1102         24           1102         24           31         10           31         10           31         11           31         10           31         10           810         17           810         17           811         25           924         21           931         1820           1820         25           1385         25   | 415         20           739         73           372         111           968         13           972         141           968         143           972         143           910         1070           1100         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           831         14           931         14           1180         21           1180         53           1382         13           94         54           54         54  | 415         10           730         730           372         11           966         13           602         16           620         18           620         18           620         18           1022         24           11022         24           11022         24           11022         24           11023         23           311         102           810         17           830         17           840         23           811         24           830         17           94         23           351         33           364         21           1135         23           1335         29           1335         29           647         13           653         14   
  | 415         10           739         739           372         11           968         13           978         13           978         14           978         143           1102         24           1102         24           1102         24           1102         24           1102         24           1103         21           311         102           311         102           311         1102           311         1102           311         1102           311         1102           311         120           312         11           313         11           311         23           311         24           311         23           311         24           311         25           311         26           311         26           32         23           313         24           314         25           315         55           316         55 </td <td>445         20           739         73           372         11           968         13           972         14           968         14           968         14           972         14           972         14           1107         21           1102         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           263         14           281         24           1380         28           1380         53           1380         53           1380         53           1380         53           1383         13</td> <td>415         10           730         730           773         11           772         11           968         10           602         10           603         13           604         13           605         14           605         14           102         24           1102         24           1102         24           1102         24           1102         24           1102         24           1102         24           310         11           310         11           310         11           310         21           311         21           311         21           311         21           311         21           311         21           312         23           1385         29           1385         29           313         45           325         15           385         14      
    385         14           365         14     &lt;</td> <td>415         10           730         730           372         11           908         13           912         13           912         13           912         143           913         1102           91         1760           92         11           93         11           93         11           93         11           93         11           93         11           91         1160           91         1160           91         1160           91         1160           91         1160           91         1160           91         1160           91         1160           91         1160           91         1160           91         1160           92         13           93         13           935         14           935         14           945         13           445         13</td> <td>415         20           730         73           372         11           908         13           912         11           908         13           908         143           912         143           1102         21           1102         21           1102         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           263         14           281         14           281         24           1382         26           643         15           658         14           265         13           445         13           655         13</td> <td>415         10           739         11           773         11           968         19           602         19           603         13           604         13           605         14           605         14           1002         24           1102         24           1116         27           1116         21           3810         17           3810         17           3810         17           3810         13           3810         13           3810         13           3810         13           381         13           381         13           381         13           382         38           1385         23           1385         23           1385         24           1385         25           138         45           445         13           667         13           675         13           675         20           415         50</td> <td>415         10           739         739           372         11           908         1372           912         1372           912         1372           913         1102           1102         24           11169         21           11022         24           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11180         21           11180         21           11180         21           11820         21           213         31           214         21           215         13</td> <td>445         10           739         10           773         11           968         10           620         18           620         18           620         18           620         18           473         11           620         18           431         1706           1102         24           1102         24           311         101           311         102           311         11           311         11           311         23           311         24           311         20           311         21           311         23           311         23           311         24           254         23           435         13           435         14           435         13           435         13           435         13           435         13           435         13           436         13           430         13     </td> | 445         20           739         73           372         11           968         13           972         14           968         14           968         14           972         14           972         14           1107         21           1102         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           263         14           281         24           1380         28           1380         53           1380         53           1380         53           1380         53           1383         13   
   | 415         10           730         730           773         11           772         11           968         10           602         10           603         13           604         13           605         14           605         14           102         24           1102         24           1102         24           1102         24           1102         24           1102         24           1102         24           310         11           310         11           310         11           310         21           311         21           311         21           311         21           311         21           311         21           312         23           1385         29           1385         29           313         45           325         15           385         14           385         14           365         14     <   | 415         10           730         730           372         11           908         13           912         13           912         13           912         143           913         1102           91         1760           92         11           93         11           93         11           93         11           93         11           93         11           91         1160           91         1160           91         1160           91         1160           91         1160           91         1160           91         1160           91         1160           91         1160           91         1160           91         1160           92         13           93         13           935         14           935         14           945         13           445         13  
   | 415         20           730         73           372         11           908         13           912         11           908         13           908         143           912         143           1102         21           1102         21           1102         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           263         14           281         14           281         24           1382         26           643         15           658         14           265         13           445         13           655         13  | 415         10           739         11           773         11           968         19           602         19           603         13           604         13           605         14           605         14           1002         24           1102         24           1116         27           1116         21           3810         17           3810         17           3810         17           3810         13           3810         13           3810         13           3810         13           381         13           381         13           381         13           382         38           1385         23           1385         23           1385         24           1385         25           138         45           445         13           667         13           675         13           675         20           415         50   
   | 415         10           739         739           372         11           908         1372           912         1372           912         1372           913         1102           1102         24           11169         21           11022         24           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11169         21           11180         21           11180         21           11180         21           11820         21           213         31           214         21           215         13  | 445         10           739         10           773         11           968         10           620         18           620         18           620         18           620         18           473         11           620         18           431         1706           1102         24           1102         24           311         101           311         102           311         11           311         11           311         23           311         24           311         20           311         21           311         23           311         23           311         24           254         23           435         13           435         14           435         13           435         13           435         13           435         13           435         13           436         13           430         13   |
| 529 17<br>529 17<br>1144 30<br>1710 230 | 1144 30<br>1710 230 | 1710 230   |            | 582 17     | 635 17                 | 395 10               |                              | 397 18                               | 397 18<br>367 9   | 397 18<br>367 9<br>949 21  | 397         18           367         9           949         21           590         17   | 397         18           367         9           949         21           590         17           611         15   | 397         18           367         9           949         21           590         17           611         15           428         11   | 397         18           367         9           949         21           590         17           611         15           428         11           1669         41   | 397         18           367         9           369         21           949         21           949         21           949         17           611         15           1669         41           1653         41           1024         25   | 337         18           367         9           949         21           590         17           611         15           156         41           166         41           1024         25           927         22   | 337         18           357         18           367         9           349         21           590         17           611         15           613         11           1669         41           1024         25           1023         25           363         8  | 337         18           357         18           357         9           349         17           590         17           611         15           614         15           614         25           1024         25           357         363           827         20   | 337         18           357         18       
   367         18           949         1           590         17           590         17           591         17           592         11           1664         41           10269         41           10264         25           927         22           363         8           363         8           352         24           552         14  | 337         18           337         18           347         21           949         21           949         21           550         17           1669         41           1669         41           1024         25           363         8           363         8           363         8           362         20           362         20           362         21           362         20           362         20           362         20           362         20           362         20           362         20   | 397         18           387         19           949         21           949         21           950         17           611         15           611         15           1166         41           1668         41           1668         41           1668         41           1668         41           1668         41           1668         41           1668         41           1668         16           552         14           552         14           551         15  | 397         18           367         9           949         21           950         17           15         15           161         15           1024         25           933         36           94         11           15669         41           1024         25           933         8           363         8           363         8           363         8           552         14           662         15  
  | 397         18           367         9           949         21           950         17           15         115           16         11           16         11           16         11           16         11           16         11           16         11           16         11           16         12           102         23           363         8           382         20           82         20           82         20           82         21           105         15           117         16           125         24  | 397         18           397         18           397         19           910         17           5100         17           511         11           428         11           428         21           428         21           428         21           428         21           222         20           233         28           2522         14           5522         14           552         14           552         14           562         15           5133         26           562         26           592         26           592         26           593         39           507         39  | 397         18           367         9           949         21           950         17           15         15           161         15           1566         41           1568         41           1568         41           1568         41           1568         41           157         25           9102         25           911         25           912         26           913         36           913         36           925         14           692         24           692         39           697         13           677         14   
  | 337         38           337         38           347         94           949         21           949         21           650         17           610         17           610         17           610         17           611         17           612         11           1066         11           11         11           1066         11           11         12           11         12           11         12           11         12           11         12           12         23           23         24           552         14           552         14           553         14           554         17           662         34           663         34           666         16  
  | 397         18           397         18           397         19           919         17           1500         17           1610         17           1618         11           428         41           1669         41           155         11           233         28           333         8           352         14           173         17           181         17           252         14           252         14           552         14           552         14           262         14           27         14           262         14           27         14           263         36           367         14  
   | 397         18           367         9           949         17           950         17           11         15           12         15           13         15           14         15           15         15           16         15           17         15           18         15           19         16           10         15           11         15           12         15           12         15           13         15           13         13           13         13           13         13           13         14           13         14           13         14           13         14           13         14           13         14           13         14           14         14           15         14           15         14           15         14           16         15           17         14           18  | 397         38           397         38           949         21           949         21           550         17           550         17           550         17           550         17           550         17           550         11           223         24           552         14           552         14           552         14           552         14           552         14           552         14           551         15           552         14           553         14           551         14           551         13           551         14           551         14           561         14           561         14  
   | 397         18           397         18           397         19           590         17           590         17           590         17           611         15           1566         41           1669         41           1569         41           1510         22           252         24           552         24           552         24           552         24           551         14           662         24           611         15           618         39           618         39           641         18   | 397         18           397         18           949         17           1590         17           161         15           428         11           428         11           15669         41           151         156           1024         25           253         26           552         14           665         16           677         13           677         14           12         26           261         15           27         13           661         16           688         19           661         38  
   | 397         38           397         38           949         21           550         17           550         17           550         17           551         11           123         21           124         21           252         24           552         24           552         24           552         24           551         17           551         17           551         14           602         24           603         24           611         13           886         38           886         38  | 397         18           397         18           949         21           550         17           510         17           511         15           156         11           428         11           428         11           428         11           552         23           552         24           552         24           552         24           552         24           662         24           613         15           613         15           614         12           615         24           616         13           618         13           618         13           618         13           618         13           618         38           836         38           836         38           616         13           617         13           618         13           619         38   |
| 99                                      |                     | 42 11      | 160 17     | 49 56      | 54 65                  | 39 35                | 00                           | 63 35                                | 83<br>28<br>38<br>38<br>38  | 6 3<br>20 3<br>39 3<br>39 3<br>30 3<br>30 3<br>30 3<br>30 3<br>30 3<br>3   | 59 35<br>59 35<br>52 94<br>52 52   | 8 22 3 9 34 77<br>2 2 3 9 36 34<br>9 2 2 3 9 34 77<br>9 3 2 3 3<br>9 3 4 77<br>9 4 7 77<br>9 4 7 77<br>9 4 7 77<br>9 7 7 77<br>9 7 7 7<br>9 7 7 7<br>9 7 7<br>9 7 7<br>9 7 7<br>9 7 7 7 7 | 83<br>59<br>36<br>68<br>69<br>4;<br>52<br>52<br>52<br>54<br>54<br>55<br>54<br>55<br>55<br>55<br>55<br>55<br>55<br>55<br>55<br>55   | 83<br>59<br>36<br>59<br>36<br>68<br>63<br>63<br>44<br>44<br>16<br>16   | 83 35<br>59 36<br>52 59 92<br>68 6:<br>68 6:<br>69 4;<br>70 16<br>61 10   | 33         35         35           55         3         55         36           53         5         5         5         5           53         5  | 53         35           55         36           53         36           52         52           53         55           68         63           69         63           30         16           61         10           61         10           61         10           61         31  | 33         35           36         36           36         36           36         36           36         36           36         43           30         16           40         30           41         10           35         38           35         88   | 83         35         35           66         9         6           73         5         5           73         5         5           74         10         10           83         3         15           84         4         16           83         3         16           84         4         10           85         3         3   
  | 83         35         35           86         92         92           86         92         92           86         92         92           86         93         94           86         91         10           87         10         10           87         36         94           87         10         10           87         36         93           87         36         94           87         36         94           87         36         94           87         36         94           87         36         94   | 36         37         38<   | 36         35         36         37         36         37         36         37         36         37         36         37         36         37         36         37         36         37         36<   
  | 58         58         58         58         58         58         56         58         56<  | 58         58         58         58         58         56<   | 58         58         58         58         58         58         56<  
  | 36         36         36         38         36<   
  | 58         58         58         58         58         58         58         58         56         58         56<   
   | 58         58         58         58         58         58         58         58         58         58         58         58         58         58         58         58         58         58         56<   | 36         36<   | 58         58   
     58         58         58         58         58         58         58         58         58         58         56         58         56<   | 3         3         3         4         3         5         3         4         3         5         3         4         3         5         1  
   | 8         9   | 36         36         38<  |
| 716                                     | •                   | 1257       | 2300       | 647        | 755                    | 499                  |                              | 1980                                 | 1980<br>405   | 1980<br>405<br>1003  | 1980<br>405<br>643   | 1980<br>405<br>1003<br>643<br>622   | 1980<br>405<br>1003<br>643<br>622<br>622   | 1980<br>405<br>643<br>643<br>622<br>459<br>1749  | 1980<br>405<br>643<br>643<br>622<br>459<br>1749<br>986  | 1980<br>405<br>643<br>643<br>643<br>622<br>622<br>1749<br>986<br>986   | 1980<br>405<br>643<br>643<br>622<br>622<br>459<br>1749<br>986<br>986<br>986<br>433   | 1980<br>405<br>405<br>643<br>643<br>622<br>459<br>1749<br>986<br>986<br>1661<br>1661<br>1661<br>777   |
1980<br>405<br>403<br>643<br>643<br>643<br>643<br>643<br>643<br>653<br>685<br>459<br>177<br>777<br>685   | 1980<br>405<br>403<br>643<br>643<br>623<br>623<br>986<br>1749<br>986<br>1661<br>433<br>177<br>777<br>777<br>777<br>665<br>665  | 1980<br>405<br>405<br>403<br>643<br>643<br>643<br>459<br>1749<br>966<br>1661<br>1661<br>1661<br>1661<br>1661<br>1661<br>166  | 1980<br>105<br>103<br>643<br>643<br>643<br>643<br>643<br>149<br>1749<br>1661<br>1661<br>1661<br>1661<br>1651<br>1652<br>1622<br>3572  
   | 1980<br>405<br>405<br>643<br>643<br>643<br>643<br>459<br>1661<br>1661<br>1661<br>1661<br>1661<br>1661<br>1661<br>16   | 1980<br>105<br>1005<br>643<br>643<br>643<br>622<br>433<br>177<br>439<br>433<br>433<br>777<br>777<br>777<br>777<br>6825<br>6825<br>6825<br>6825<br>1622<br>1622<br>1622   | 1980<br>1003<br>645<br>643<br>643<br>643<br>652<br>458<br>1749<br>966<br>1749<br>965<br>453<br>1661<br>1461<br>1461<br>1464<br>1162<br>1622<br>1622<br>1622  
   | 1990<br>1035<br>1037<br>643<br>643<br>643<br>459<br>459<br>1149<br>1661<br>1661<br>1661<br>433<br>685<br>625<br>625<br>625<br>625<br>625<br>1167<br>1167<br>857<br>857<br>857<br>857<br>857<br>857<br>857<br>857<br>857<br>85   
   | 1980<br>1033<br>643<br>643<br>643<br>643<br>643<br>458<br>1749<br>8166<br>1149<br>177<br>777<br>777<br>777<br>777<br>777<br>777<br>777<br>777<br>815<br>815<br>815<br>815<br>815<br>815<br>815<br>815<br>815<br>815   
  | 1990<br>1043<br>643<br>1043<br>643<br>643<br>458<br>1749<br>866<br>1661<br>1749<br>1661<br>1749<br>662<br>652<br>1662<br>1454<br>1464<br>1157<br>1464<br>1167<br>1464<br>1167<br>253<br>263<br>263<br>563<br>563<br>563<br>563<br>563<br>563<br>563<br>563<br>563<br>5   | 1980<br>1980<br>643<br>643<br>643<br>643<br>643<br>458<br>1661<br>1749<br>966<br>855<br>652<br>1661<br>177<br>177<br>852<br>1661<br>1167<br>177<br>852<br>853<br>857<br>853<br>853<br>853<br>853<br>853<br>853<br>853<br>853<br>853<br>853  
  | 1980<br>1033<br>623<br>623<br>623<br>623<br>623<br>1749<br>966<br>1749<br>1749<br>1749<br>1749<br>1757<br>665<br>3572<br>1657<br>1651<br>1157<br>665<br>363<br>663<br>672<br>663<br>663<br>663<br>663<br>663<br>663<br>663<br>663<br>663<br>66   | 1990<br>1043<br>643<br>1043<br>643<br>643<br>458<br>1749<br>866<br>1661<br>1749<br>662<br>1661<br>1464<br>1454<br>1464<br>1464<br>1464<br>1464<br>1464  
  | 1980<br>1980<br>643<br>643<br>643<br>643<br>643<br>459<br>1744<br>966<br>1774<br>177<br>777<br>777<br>655<br>1657<br>177<br>777<br>777<br>777<br>857<br>1661<br>177<br>777<br>857<br>857<br>857<br>857<br>857<br>857<br>857<br>857<br>8   | 1980<br>1035<br>643<br>1035<br>653<br>653<br>1749<br>966<br>1749<br>1749<br>1749<br>1749<br>1749<br>1749<br>1749<br>1747<br>1777<br>665<br>353<br>2537<br>2538<br>2539<br>2539<br>2539<br>2538<br>2539<br>2530  |
| 0.0017                                  |                     | 0.0037     | 0.2500     | 0.0019     | 0.0022                 | 0.0014               |                              | 0.0018                               | 0.0018  | 0.0018<br>0.0014<br>0.0029   | 0.0018<br>0.0014<br>0.0029<br>0.0018   | 0.0018<br>0.0014<br>0.0029<br>0.0018<br>0.0018  | 0.0018<br>0.0014<br>0.0029<br>0.0018<br>0.0013   | 0.0018<br>0.0014<br>0.0029<br>0.0028<br>0.0018<br>0.0021<br>0.0013<br>0.0013   | 0.0018<br>0.0014<br>0.0029<br>0.0018<br>0.0018<br>0.0013<br>0.0013<br>0.0057  | 0.0018<br>0.0014<br>0.0029<br>0.0021<br>0.0013<br>0.0013<br>0.0013<br>0.0057<br>0.0037   | 0.0018           0.0014           0.0029           0.0021           0.0021           0.0021           0.0021           0.0037           0.0037           0.0037           0.0037           0.0037  | 0.0014<br>0.0014<br>0.0029<br>0.0021<br>0.0021<br>0.0021<br>0.0021<br>0.0057<br>0.0003<br>0.0003  |
0.0014<br>0.0014<br>0.0029<br>0.0021<br>0.0021<br>0.0021<br>0.0037<br>0.00037<br>0.00035<br>0.0025   | 0.0014           0.0014           0.0018           0.0018           0.0018           0.0021           0.0018           0.0018           0.0018           0.0018           0.0018           0.0018           0.0019           0.0017           0.0018           0.0013           0.0013           0.0013           0.0013           0.0013           0.0013           0.0013           0.0013           0.0013           0.0013           0.0013  | 0.0018<br>0.0014<br>0.0012<br>0.0013<br>0.0013<br>0.0013<br>0.0013<br>0.0013<br>0.0013<br>0.0013<br>0.0013<br>0.0025<br>0.0021<br>0.0025   | 0.0018           0.0014           0.0018           0.0018           0.0013           0.0013           0.0013           0.0013           0.0013           0.0027           0.0013           0.0027           0.0027           0.0027           0.0027           0.0027           0.0027           0.0027           0.0027           0.0027           0.0027           0.0027           0.0027           0.0027           0.0027           0.0027           0.0027           0.0027           0.0027           0.0028           0.0028  
   | 0.0018           0.0023           0.0024           0.0023           0.0021           0.0021           0.0021           0.0021           0.0021           0.0021           0.0021           0.0021           0.0021           0.0021           0.0021           0.0021           0.0021           0.0021           0.0021           0.0021           0.0021           0.0021           0.0022           0.0023           0.0023           0.0024           0.0023           0.0024           0.0023           0.0024           0.0023           0.0024           0.0023           0.0024           0.0023           0.0024           0.0023           0.0024           0.0025  | 0.0018<br>0.0024<br>0.0029<br>0.0029<br>0.0037<br>0.0037<br>0.0037<br>0.0037<br>0.0037<br>0.0037<br>0.0003<br>0.0002<br>0.00028<br>0.00028<br>0.00028<br>0.00028<br>0.00028  | 0.0018<br>0.0024<br>0.0029<br>0.0029<br>0.0037<br>0.0037<br>0.0037<br>0.0041<br>0.0037<br>0.0041<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00022<br>0.00022<br>0.00022<br>0.00022<br>0.00022<br>0.00022<br>0.00022<br>0.00022<br>0.00022<br>0.00021<br>0.00021<br>0.00021<br>0.00022<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.00021<br>0.000210000000000  
   | 0.0018 0.0014 0.0014 0.0018 0.001 0.0018 0.0021 0.0027 0.0037 0.0037 0.0037 0.0037 0.0037 0.0003 0.0  
   | 0.0018 0.0014 0.0018 0.0018 0.0001 0.0001 0.0002 0.0003 00  
  | 0.0018 0.00014 0.00014 0.00018 0.00019 0.00029 0.0003 0.00   | 0.0018 0.0014 0.0014 0.0018 0.001 0.001 0.001 0.0027 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0037 0.0004 0.0004 0.0002
0.000   | 0.0018 0.0014 0.0018 0.0018 0.0018 0.0018 0.0029 0.0029 0.0039 0.0039 0.0031 0.003 0.0031 0.003  | 0.0018 0.00248 0.00248 0.00218 0.00218 0.0021 0.0021 0.0021 0.0021 0.0021 0.0021 0.0021 0.0021 0.0021 0.0021 0.0022 0.002 0.0022 0.002 0.0022 0.00  
  | 0.0018 0.0014 0.0014 0.0018 0.0018 0.0018 0.0019 0.0021 0.0021 0.001 0.001 0.001 0.0021 0.0021 0.0022 0.002 0.0  | 0.0018 0.00014 0.00018 0.00018 0.00018 0.00021 0.00057 0.00057 0.00031 0.0003 0.0003 0.0003 0.0003 0.0003 0.0003 0.0002 0  |
| 4 0.0268                                |                     | 7 0.0598   | 6 1.1900   | 6 0.0302   | 9 0.0342               | 5 0.0232             |                              | 4 0.0217                             | 4 0.0217<br>8 0.0182  | 4 0.0217<br>8 0.0182<br>5 0.0485   | 4         0.0217           8         0.0182           5         0.0485           9         0.0299  | 4         0.0217           8         0.0182           5         0.0485           9         0.0299           1         0.0317  | 4         0.0217           8         0.0182           5         0.0485           9         0.0239           11         0.02317           16         0.0214                                       | 4         0.0217           8         0.0182           5         0.0485           9         0.0299           11         0.0317           16         0.0214           4         0.0214   | 4         0.0217           8         0.0182           5         0.0485           9         0.0299           11         0.0214           6         0.0214           6         0.0214           6         0.0214           6         0.0214           6         0.0214           7         0.0300           9         0.0526  | 4         0.0217           8         0.0182           5         0.0485           9         0.0239           1         0.0214           6         0.0214           6         0.0214           6         0.0214           7         0.0317           6         0.0214           7         0.0317           8         0.0226           9         0.0526           2         0.0667  | 4         0.0217           8         0.0182           5         0.0485           9         0.0299           1         0.0317           6         0.0214           6         0.0214           7         0.0317           9         0.0229           9         0.0229           6         0.0214           9         0.0226           9         0.0226           9         0.0226           9         0.0226           9         0.0526           9         0.0526           2         0.0667           4         0.0200   | 4         0.0217           8         0.0182           9         0.0182           9         0.0299           1         0.0317           6         0.0214           6         0.0216           7         0.0317           8         0.0124           9         0.0214           9         0.0214           9         0.0214           10         0.0317           11         0.0317           12         0.0314           13         0.00216           14         0.00206           14         0.00506           15         0.00506           16         0.00506           17         0.00415   | 4         0.0217           8         0.0182   
       9         0.0182           9         0.0239           1         0.0317           6         0.0214           6         0.0214           9         0.0239           9         0.0214           1         0.0317           1         0.0314           1         0.0314           1         0.0314           1         0.0314           1         0.0314           1         0.0314           1         0.0324           1         0.0324           1         0.03333           5         0.03333  | 4         0.0217           8         0.0182           9         0.0182           1         0.0345           1         0.0347           6         0.0214           9         0.0214           9         0.0216           9         0.0526           9         0.0526           9         0.0526           10         0.0415           5         0.03307           7         0.0307  | 4         0.0217           8         0.0182           9         0.0182           1         0.0317           6         0.0214           6         0.0214           9         0.0216           9         0.0226           9         0.0526           1         0.0100           2         0.00415           0         0.01033           1         0.0333           1         0.0333           1         0.0333   | 4         0.0217           8         0.0182           9         0.0182           9         0.02345           9         0.02345           9         0.02345           6         0.0214           1         0.0317           6         0.0214           9         0.0226           2         0.06526           2         0.06526           3         0.0333           5         0.0333           7         0.0333           7         0.0337           8         0.0397  
  | 4         0.0217           8         0.02137           9         0.0289           9         0.0214           1         0.0317           6         0.0214           9         0.0214           9         0.0224           9         0.0214           9         0.0214           9         0.0214           9         0.0226           9         0.0526           1         0.0307           1         0.0307           1         0.0307           1         0.0307           1         0.0667  | 4         0.0217           8         0.0182           9         0.0182           9         0.0249           1         0.0317           6         0.0256           9         0.0556           9         0.0556           9         0.0556           9         0.0556           9         0.0556           9         0.0556           0         0.0410           1         0.0410           1         0.0410           1         0.0410           1         0.0410           1         0.0430           1         0.0430           1         0.0430           1         0.0430           1         0.0430           1         0.0430           1         0.0430           1         0.0330           2         0.0330           2         0.0330           2         0.0330           3         0.03335  | 4         0.0217           8         0.0182           9         0.0182           9         0.0299           1         0.0214           6         0.0234           2         0.0657           2         0.0675           5         0.06415           6         0.0246           7         0.06415           7         0.0430           8         0.0309           8         0.0309           1         0.0430           7         0.0430           7         0.0430           7         0.0430           8         0.0509           1         0.0430           7         0.0430           7         0.0430           7         0.0430           8         0.0333           7         0.0430           7         0.0430           7         0.0430  
  | 4         0.0217           8         0.0182           8         0.0182           9         0.0295           9         0.0295           9         0.0295           9         0.0295           9         0.0265           9         0.0266           9         0.0267           9         0.0266           9         0.0266           9         0.0266           9         0.0266           9         0.0266           9         0.0266           9         0.0266           9         0.0266           9         0.0266           9         0.0410           1         0.0400           1         0.0697           1         0.0697           1         0.0697           1         0.06937           1         0.06937           1         0.06937           1         0.06937           1         0.06937           1         0.06937           1         0.06937           1         0.06937           1         0.0347   
  | 4         0.0217           8         0.01827           9         0.01837           9         0.01837           1         0.00397           1         0.00375           1         0.00457           1         0.00456           1         0.00456           1         0.00456           1         0.00456           1         0.00456           1         0.00415           1         0.00415           1         0.00415           1         0.00415           1         0.00415           1         0.00415           1         0.00415           1         0.00415           1         0.00415           1         0.00415           1         0.00415           1         0.00417           1         0.00417           1         0.00417           1         0.00317           1         0.00317           1         0.00317           1         0.00317           1         0.00317   
   | 4         0.0217           8         0.0182           9         0.0182           9         0.0234           1         0.0201           1         0.0024           2         0.0025           2         0.0057           1         0.0057           2         0.0057           3         0.0045           4         0.0057           1         0.0057           1         0.0057           1         0.0047           1         0.0047           1         0.0047           1         0.0047           1         0.0041           1         0.0041           1         0.0041           1         0.0041           1         0.0041           1         0.00431           1         0.00431           1         0.00431           1         0.00431           1         0.00431           1         0.00431           1         0.00431           1         0.00431           1         0.00431           1         0.00431 <td>4         0.0217           5         0.0485           5         0.0485           9         0.0294           9         0.0294           6         0.0214           6         0.0214           7         0.0667           7         0.01080           8         0.01026           9         0.0224           9         0.0236           9         0.0336           6         0.0410           7         0.0410           17         0.0410           17         0.0410           17         0.0337           17         0.0410           17         0.0410           17         0.0410           17         0.0337           17         0.0337           17         0.0337           17         0.0337           17         0.0337           17         0.0337           17         0.0337           18         0.0347           19         0.0334           10         0.0347</td> <td>4         0.0217           8         0.0182           9         0.0182           9         0.0274           1         0.0124           1         0.0124           2         0.0182           2         0.0667           2         0.01020           3         0.01244           4         0.0120           5         0.0120           1         0.0120           1         0.0120           1         0.0120           1         0.0120           1         0.0131           1         0.0133           1         0.0131           1         0.0131           1         0.0131           1         0.0131           1         0.0131           1         0.0131           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133     <!--</td--><td>4         0.0217           8         0.0182           9         0.0182           1         0.0021           1         0.0021           1         0.0031           2         0.0037           1         0.0027           1         0.0031           2         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           2         0.0337           2         0.0337           2         0.0337           2         0.0332           2         0.0332           2         0.0332           2         0.0332           2         0.0332           2         0.0332           2         0.0332           2         0.0332           2         0.0332           2         0.0332     <td>4         0.0217           5         0.0485           6         0.0248           9         0.0299           9         0.0214           6         0.0214           7         0.00580           9         0.01280           9         0.0214           1         0.00580           1         0.00580           1         0.01280           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.01235           1         0.01235           2         0.01335           3         0.01383           3         0.01383           3         0.01383</td><td>4         0.0217           8         0.0182           9         0.0128           9         0.0224           1         0.0124           1         0.0124           1         0.0124           1         0.0124           1         0.0124           1         0.0167           2         0.0667           3         0.0123           1         0.0120           1         0.0120           1         0.0120           1         0.0120           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           2         0.0133           3         0.02138           3         0.02138           3         0.02138</td></td></td> | 4         0.0217           5         0.0485           5         0.0485           9         0.0294           9         0.0294           6         0.0214           6         0.0214           7         0.0667           7         0.01080           8         0.01026           9         0.0224           9         0.0236           9         0.0336           6         0.0410           7         0.0410           17         0.0410           17         0.0410           17         0.0337           17         0.0410           17         0.0410           17         0.0410           17         0.0337           17         0.0337           17         0.0337           17         0.0337           17         0.0337           17         0.0337           17         0.0337           18         0.0347           19         0.0334           10         0.0347   
   | 4         0.0217           8         0.0182           9         0.0182           9         0.0274           1         0.0124           1         0.0124           2         0.0182           2         0.0667           2         0.01020           3         0.01244           4         0.0120           5         0.0120           1         0.0120           1         0.0120           1         0.0120           1         0.0120           1         0.0131           1         0.0133           1         0.0131           1         0.0131           1         0.0131           1         0.0131           1         0.0131           1         0.0131           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133 </td <td>4         0.0217           8         0.0182           9         0.0182           1         0.0021           1         0.0021           1         0.0031           2         0.0037           1         0.0027           1         0.0031           2         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           2         0.0337           2         0.0337           2         0.0337           2         0.0332           2         0.0332           2         0.0332           2         0.0332           2         0.0332           2         0.0332           2         0.0332           2         0.0332           2         0.0332           2         0.0332     <td>4         0.0217           5         0.0485           6         0.0248           9         0.0299           9         0.0214           6         0.0214           7         0.00580           9         0.01280           9         0.0214           1         0.00580           1         0.00580           1         0.01280           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.01235           1         0.01235           2         0.01335           3         0.01383           3         0.01383           3         0.01383</td><td>4         0.0217           8         0.0182           9         0.0128           9         0.0224           1         0.0124           1         0.0124           1         0.0124           1         0.0124           1         0.0124           1         0.0167           2         0.0667           3         0.0123           1         0.0120           1         0.0120           1         0.0120           1         0.0120           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           2         0.0133           3         0.02138           3         0.02138           3         0.02138</td></td> | 4         0.0217           8         0.0182           9         0.0182           1         0.0021           1         0.0021           1         0.0031           2         0.0037           1         0.0027           1         0.0031           2         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           1         0.0037           2         0.0337           2         0.0337           2         0.0337           2         0.0332           2         0.0332           2         0.0332           2         0.0332           2         0.0332           2         0.0332           2         0.0332           2         0.0332           2         0.0332           2         0.0332 <td>4         0.0217           5         0.0485           6         0.0248           9         0.0299           9         0.0214           6         0.0214           7         0.00580           9         0.01280           9         0.0214           1         0.00580           1         0.00580           1         0.01280           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.01235           1         0.01235           2         0.01335           3         0.01383           3         0.01383           3         0.01383</td> <td>4         0.0217           8         0.0182           9         0.0128           9         0.0224           1         0.0124           1         0.0124           1         0.0124           1         0.0124           1         0.0124           1         0.0167           2         0.0667           3         0.0123           1         0.0120           1         0.0120           1         0.0120           1         0.0120           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           2         0.0133           3         0.02138           3         0.02138           3         0.02138</td>   
   | 4         0.0217           5         0.0485           6         0.0248           9         0.0299           9         0.0214           6         0.0214           7         0.00580           9         0.01280           9         0.0214           1         0.00580           1         0.00580           1         0.01280           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.04100           1         0.01235           1         0.01235           2         0.01335           3         0.01383           3         0.01383           3         0.01383  | 4         0.0217           8         0.0182           9         0.0128           9         0.0224           1         0.0124           1         0.0124           1         0.0124           1         0.0124           1         0.0124           1         0.0167           2         0.0667           3         0.0123           1         0.0120           1         0.0120           1         0.0120           1         0.0120           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           1         0.0133           2         0.0133           3         0.02138           3         0.02138           3         0.02138  |
| 025 0.522                               |                     | 346 0.625. | 310 0.979t | 0.564t     | 324 0.513 <sup>t</sup> | 211 0.571            | 100 0 000                    | 120 0.402                            | 011 0.306   | 220 0.7022<br>211 0.3060<br>028 0.565  | 220 U-102<br>011 0.306<br>028 0.565<br>024 0.517   | 2006(<br>2010) 0.306(<br>2280) 0.565(<br>0240) 0.517(<br>0200) 0.330  | 2006<br>2006<br>228 0.565<br>024 0.517<br>020 0.330<br>015 0.368   | 220 0.3065<br>228 0.5655<br>224 0.517<br>220 0.330<br>015 0.368<br>015 0.368   | 220 0.3065<br>711 0.3065<br>728 0.5655<br>724 0.517<br>020 0.330<br>015 0.368<br>015 0.368<br>036 0.754<br>036 0.336  | 220 0.3062<br>111 0.3065<br>128 0.555<br>128 0.517<br>120 0.330<br>115 0.336<br>115 0.356<br>115 0.566<br>115 0.566 | 220         0.0005           111         0.3006           128         0.5517           129         0.5117           120         0.330           120         0.3368           015         0.3368           056         0.754           056         0.754           056         0.754           056         0.754           056         0.754           075         0.3368           0366         0.413           029         0.413           029         0.515  | 220         0.5055           221         0.5655           222         0.5655           222         0.5655           222         0.5655           222         0.5655           222         0.5175           220         0.3380           220         0.3380           220         0.3386           220         0.3386           220         0.3386           220         0.3386           220         0.3386           220         0.3386           220         0.5154           220         0.3386           220         0.5154           220         0.5154           220         0.515           220         0.515  | 220         0.5005           111         0.3006           222         0.5557           220         0.3302           220         0.3302           220         0.3305           220         0.3306           220         0.3302           220         0.3302           220         0.3302           220         0.3302           220         0.3302           220         0.3302           220         0.3302           220         0.3302           220         0.3302           220         0.5154           220         0.5154           220         0.5154           220         0.5154           220         0.5154           220         0.5154           2215         0.5055  
   | 220         0.7005           231         0.3006           231         0.3066           232         0.5175           232         0.5175           232         0.3302           232         0.3305           236         0.3368           2366         0.3368           2026         0.3368           2026         0.6155           2026         0.6155           2026         0.6155           2026         0.6155           2026         0.6155           2026         0.6155           2020         0.6051           2020         0.201   | 220         0.0005           228         0.517           228         0.517           229         0.517           220         0.330           215         0.517           220         0.330           215         0.333           220         0.333           215         0.336           226         0.343           236         0.333           200         0.336           201         0.336           202         0.343           203         0.343           203         0.343           203         0.343           203         0.343           203         0.343           203         0.3515           203         0.3515           203         0.3515           203         0.3515           203         0.3515           203         0.3515   | 220         0.0005           211         0.3066           221         0.3066           222         0.517           220         0.330           220         0.330           220         0.330           226         0.336           236         0.336           236         0.336           236         0.343           236         0.343           236         0.343           236         0.343           236         0.343           236         0.343           236         0.343           236         0.343           236         0.343           236         0.515           2020         0.515           2021         0.505           2026         0.5015           2026         0.3201           236         0.3201           236         0.3201           236         0.3201           236         0.3201           236         0.3201           236         0.3301  | 220         0.0005           223         0.565           228         0.565           229         0.517           220         0.330           220         0.3336           255         0.7336           266         0.744           266         0.743           270         0.3336           266         0.743           266         0.743           266         0.743           266         0.743           266         0.743           270         0.515           2020         0.6515           2020         0.6515           2020         0.6515           2021         0.515           2022         0.5052           2026         0.6502           2026         0.6021           2026         0.301           2026         0.301           2026         0.6654           2037         0.697   
   | 200 0.0000<br>2011 0.0000<br>2011 0.0000<br>2011 0.0000<br>2010 0.0000<br>2010 0.0000<br>2010 0.001<br>2010 0.001<br>2010 0.001<br>2010 0.000<br>2010 0.0000<br>2010 0.0000<br>2010 0.0000<br>2010 0.0000<br>2010 0.0000<br>2010 0.0   | 200 0.000<br>2011 0.0000<br>2017 0.0505<br>2010 0.0507<br>2010 0.0310<br>2015 0.0310<br>2016 0.0316<br>2016 0.0316<br>2016 0.051<br>2010 0.001<br>2010 0.001   
   | 200 0.0000<br>200 0.0000<br>201 0.00000<br>201 0.00000<br>201 0.0000<br>201 0.0000<br>201 0.0000<br>201   | 200 0.0000<br>200 0.0505<br>201 0.0505<br>201 0.0317<br>201 0.0317<br>201 0.0317<br>202 0.0316<br>202 0.0316<br>202 0.0316<br>203 0.0316<br>203 0.0316<br>203 0.031<br>203 0.031  
  | 2006.0000000000000000000000000000000000  | 200 0.0652 201 0.0000 2010 2010 2010 2010 2010 20  | 200 0.0562<br>201 0.5652<br>202 0.3317<br>203 0.   
   | 200 0.0002<br>200 0.0005<br>200 0.0005<br>200 0.0005<br>200 0.0001<br>200 0.0001<br>200 0.001<br>200 0.0010  | 200 0.0652 201 0.0000 201 0.0000 201 0.0000 201 0.0000 201 201 0.0000 201 201 201 201 201 201 201 201 201   | 200 0.0562<br>201 0.0562<br>201 0.0562<br>201 0.0562<br>201 0.0562<br>201 0.0561<br>201 0.051<br>201 0.051<br>201 0.051<br>201 0.051<br>201 0.051<br>201 0.051<br>201 0.051<br>201 0.055<br>201 0.055  |
| .0854 0.00                              |                     | .1944 0.00 | .4720 0.08 | .0945 0.00 | .1037 0.00             | .0632 0.00           | .0636 0.00                   |                                      | .0586 0.00  | .0586 0.00<br>.1586 0.00   | .0586 0.00<br>.1586 0.00<br>.0960 0.00   | .0586 0.00<br>1586 0.00<br>.0960 0.00<br>.0994 0.00   | 0586 0.00<br>1586 0.00<br>0960 0.00<br>0994 0.00<br>0686 0.00  | 0586         0.00           .1586         0.00           .0960         0.00           .0934         0.00           .0686         0.00           .2965         0.00   | 0.586         0.00           1586         0.00           0960         0.00           0994         0.00           0994         0.00           1726         0.00  | 0.586         0.00           1.586         0.00           0.960         0.00           0.994         0.00           0.955         0.00           0.956         0.00           1.726         0.00           1.728         0.00           1.728         0.00           1.728         0.00  | 0586         0.00           .1586         0.00           .0960         0.00           .0994         0.00           .0986         0.00           .0986         0.00           .0986         0.00           .0986         0.00           .1726         0.00           .1548         0.00           .1726         0.00           .0578         0.00   | 0586         0.00           .1586         0.00           .0960         0.00           .0954         0.00           .0956         0.00           .0956         0.00           .0956         0.00           .0956         0.00           .0956         0.00           .0956         0.00           .0956         0.00           .0956         0.00           .0956         0.00           .0565         0.00           .1726         0.00           .1356         0.00           .1356         0.00   | 0586         0.00           1586         0.00 
         0960         0.00           0954         0.00           0058         0.00           0058         0.00           0058         0.00           0156         0.00           0156         0.00           0157         0.00           0157         0.00           01369         0.00           0137         0.00           01369         0.00  | 0586         0.00           1586         0.00           0960         0.00           0954         0.00           0954         0.00           0586         0.00           0586         0.00           0587         0.00           0588         0.00           0593         0.00           0593         0.00           0593         0.00           0593         0.00           0593         0.00           0393         0.00           0393         0.00           0393         0.00  | 0.00         0.00           1586         0.00           0.946         0.00           0.956         0.00           0.956         0.00           0.956         0.00           0.956         0.00           0.956         0.00           0.956         0.00           0.956         0.00           0.957         0.00           0.9578         0.00           0.9578         0.00           0.9578         0.00           0.9393         0.00           0.9393         0.00           0.931         0.00  | 0.00         0.00           1586         0.00           0.960         0.00           0.994         0.00           0.995         0.00           0.996         0.00           0.997         0.00           0.997         0.00           0.997         0.00           0.976         0.00           0.9778         0.00           0.9128         0.00           0.912         0.00           0.912         0.00           0.912         0.00           0.912         0.00           0.912         0.00           0.912         0.00           0.912         0.00           0.912         0.00           0.913         0.00           0.913         0.00           0.913         0.00   
  | 0.00         0.00           11586         0.00           0.0960         0.00           0.0966         0.00           0.0966         0.00           0.0966         0.00           0.0566         0.00           0.0566         0.00           0.05786         0.00           0.05780         0.00           0.0127         0.00           0.02730         0.00           0.03912         0.00           0.0912         0.00           0.0912         0.00           0.0912         0.00           0.0912         0.00           0.0912         0.00           0.09912         0.00           0.09912         0.00           0.09912         0.00           0.09912         0.00           0.09912         0.00           0.0391         0.00           0.0391         0.00           0.0391         0.00           0.0391         0.00           0.0391         0.00           0.0391         0.00   | 0.00         0.00           1.1586         0.000           0.9960         0.000           0.9966         0.000           0.9966         0.000           0.9965         0.000           0.9965         0.000           0.9686         0.000           0.9686         0.000           0.9686         0.000           0.9686         0.000           0.9687         0.000           0.9778         0.000           0.9833         0.000           0.9833         0.000           0.9833         0.000           0.9833         0.000           0.9833         0.000           0.9933         0.000           0.9933         0.000           0.9933         0.000           0.9933         0.000           0.9933         0.000           0.8934         0.000   | C556         0.00           1558         0.00           1594         0.00           1594         0.00           1595         0.00           1595         0.00           1595         0.00           1595         0.00           1546         0.00           1547         0.00           1548         0.00           1549         0.00           1350         0.00           0391         0.00           1135         0.00           2131         0.00           1350         0.00           1351         0.00           1354         0.00           1354         0.00           1354         0.00           1354         0.00           1354         0.00           1354         0.00           1354         0.00           1354         0.00           1354         0.00           1354         0.00           1355         0.00           1354         0.00   
  | C556         0.00           1558         0.00           1546         0.00           100         100  
  | 55%         0.00           158%         0.00           158%         0.00           294         0.00           294         0.00           295         0.00           295         0.00           295         0.00           295         0.00           295         0.00           295         0.00           254         0.00           254         0.00           254         0.00           254         0.00           254         0.00           255         0.00           2693         0.00           2893         0.00           2893         0.00           2893         0.00           2893         0.00           2893         0.00           2893         0.00           2893         0.00           2893         0.00           2893         0.00           2893         0.00           2893         0.00           2803         0.00           2804         0.00           2805         0.00           2805  
   | 55%         0.00           158         0.00           158         0.00           2994         0.00           2994         0.00           2994         0.00           2994         0.00           2994         0.00           2994         0.00           2994         0.00           2994         0.00           2994         0.00           2994         0.00           2994         0.00           2994         0.00           2991         0.00           2091         0.00           2091         0.00           2091         0.00           2091         0.00           2091         0.00           2091         0.00           2091         0.00           2091         0.00           2012         0.01           2013         0.01           2014         0.01           2015         0.00           2019         0.00           2019         0.00           2019         0.00           2019         0.00           2019  | 558         0.00           1586         0.00           1586         0.00           094         0.00           095         0.00           094         0.00           111         0.00           111         0.00           111         0.00           111         0.00           111         0.00           111         0.00           111         0.00           111         0.00           111         0.00           111         0.00           111         0.00           111         0.00           111         0.00           111         0.00           111         0.00           111         0.00           111         0.00           111         0.00           11019         0.00           11012         0.00           11012         0.00           11012         0.00           1000         0.00           1000         0.00           1000         0.00           1000         0.00           1000         0.0   
   | 558         0.00           1586         0.00           1586         0.00           094         0.00           095         0.00           094         0.00           015         0.00           016         0.00           017         0.00           018         0.00           018         0.00           018         0.00           018         0.00           018         0.00           013         0.00           0291         0.00           02019         0.00           0132         0.00           0132         0.00           0132         0.00           0132         0.00           0133         0.00           0143         0.00           0153         0.00           0154         0.00           0159         0.00           0159         0.00           0159         0.00           0159         0.00           0159         0.00           0159         0.00           0159         0.00           0159         <   | G586         0.00           1586         0.00           1586         0.00           1586         0.00           1586         0.00           1586         0.00           1586         0.00           1586         0.00           1586         0.00           1586         0.00           1517         0.00           1518         0.00           1519         0.00           1519         0.00           13150         0.00           1319         0.00           1319         0.00           1319         0.00           1313         0.00           1313         0.00           1313         0.00           1313         0.00           1313         0.00           1313         0.00           1313         0.00           1313         0.00           1313         0.00           1313         0.00           1313         0.00           1313         0.00   
   | 5586         0.00           1596         0.00           1596         0.00           1594         0.00           1594         0.00           1595         0.00           1596         0.00           1597         0.00           1596         0.00           1597         0.00           1598         0.00           1596         0.00           1596         0.00           1598         0.00           1593         0.00           1135         0.00           1135         0.00           1138         0.00           1139         0.00           1131         0.00           1022         0.00           1022         0.00           1022         0.00           1023         0.00           1024         0.00           1028         0.00           1029         0.00           10319         0.00           1032         0.00           1033         0.00           1034         0.00           1035         0.00           1036 </td <td>558         0.00           1596         0.00           1596         0.00           0594         0.00           0595         0.00           0596         0.00           0597         0.00           0596         0.00           0597         0.00           0596         0.00           0517         0.00           11726         0.00           0517         0.00           0513         0.00           0511         0.00           0512         0.00           0513         0.00           0513         0.00           0514         0.00           0512         0.00           0513         0.00           0513         0.00           0514         0.00           0513         0.00           0513         0.00           0513         0.00           0513         0.00           0513         0.00           0513         0.00           0513         0.00           0513         0.00           0513         0.00           0513</td>  | 558         0.00           1596         0.00           1596         0.00           0594         0.00           0595         0.00           0596         0.00           0597         0.00           0596         0.00           0597         0.00           0596         0.00           0517         0.00           11726         0.00           0517         0.00           0513         0.00           0511         0.00           0512         0.00           0513         0.00           0513         0.00           0514         0.00           0512         0.00           0513         0.00           0513         0.00           0514         0.00           0513         0.00           0513         0.00           0513         0.00           0513         0.00           0513         0.00           0513         0.00           0513         0.00           0513         0.00           0513         0.00           0513  |
| 0.0260 0.                               |                     | 0.0590 0.  | 8.5000 0.  | 0.0220 0.  | 0.0290 0.              | 0.0100 0.            | 0.0530 0.                    |                                      | 0.0120 0.   | 0.0120 0.  | 0.0120 0. <sup>1</sup><br>0.0300 0.<br>0.0210 0.   | 0.0120 0.<br>0.0300 0.<br>0.0210 0.   | 0.0120 0.0<br>0.0300 0.0<br>0.0210 0.0<br>0.0270 0.0   | 0.0120 0.0<br>0.0300 0.0<br>0.0210 0.0<br>0.0180 0.0   | 0.0120         0.0           0.0300         0.0           0.0210         0.0           0.0270         0.0           0.0180         0.0           0.0970         0.0           0.0490         0.0  | 0.0120         0.0           0.0300         0.0           0.0210         0.0           0.0270         0.0           0.0180         0.0           0.0180         0.0           0.0180         0.0           0.0180         0.0           0.0180         0.0           0.0180         0.0           0.0180         0.0   | 0.0120         0.0           0.0300         0           0.0210         0           0.0210         0           0.0210         0           0.0210         0           0.0210         0           0.0210         0           0.0210         0           0.0210         0           0.0210         0           0.0210         0           0.0210         0           0.0210         0           0.0490         0           0.0091         0  | 0.0120         0.0           0.0300         0.0           0.0210         0.0           0.0270         0.0           0.0180         0.0           0.0270         0.0           0.0490         0.0           0.0490         0.0           0.0250         0.0  | 2.0120         0.1           2.0230        
0.1           2.0210         0.1           0.0211         0.1           0.0277         0.1           0.0279         0.1           0.0279         0.1           0.0279         0.1           0.0279         0.1           0.0279         0.1           0.0279         0.1           0.0279         0.1           0.0279         0.1           0.0279         0.1           0.0279         0.1           0.0259         0.1           0.0250         0.1   | 0.0120         0.0           0.0120         0.0           0.0210         0.0           0.0210         0.0           0.0270         0.0           0.0077         0.0           0.01400         0.0           0.0270         0.0           0.0270         0.0           0.0270         0.0           0.0270         0.0           0.0270         0.0           0.0270         0.0           0.0270         0.0           0.0270         0.0           0.0290         0.0           0.0290         0.0  | 0.0120         0.0           0.0120         0.0           0.0210         0.0           0.0210         0.0           0.0210         0.0           0.0210         0.0           0.0210         0.0           0.0210         0.0           0.0180         0.0           0.0180         0.0           0.0180         0.0           0.00140         0.0           0.00250         0.0           0.02200         0.0           0.02200         0.0           0.02200         0.0   | 20120         0           2020         0           20300         0           20210         0           20210         0           20210         0           20210         0           20210         0           20210         0           20210         0           20210         0           20210         0           20210         0           20210         0           20210         0           20210         0           20210         0           20220         0           202200         0           20200         0           20200         0   
   | 0.0120         0.0120         0.0120           0.0300         0.0120         0.0120           0.0210         0.0120         0.0120           0.0210         0.0120         0.0120           0.0210         0.0120         0.0120           0.0210         0.01200         0.0120           0.0201         0.01200         0.0120           0.0201         0.01200         0.01200           0.02000         0.01200         0.01200           0.02000         0.01200         0.01200           0.02000         0.01200         0.01200           0.02000         0.01200         0.0100           0.02000         0.0100         0.0100  | 20120 0<br>100000 0<br>000000 0<br>0000000 0<br>000000 0<br>0000000 0<br>000000 0<br>0000000 0<br>000000 0<br>000000 0<br>000000 0<br>0000000 0<br>00000000   | 10120         0           10120         0           10120         0           10121         0           10121         0           10121         0           10121         0           10121         0           10121         0           10121         0           10121         0           10121         0           10121         0           10121         0           101220         0           101220         0           101220         0           101220         0           1012200         0           1012200         0           1012200         0           1012200         0           1012200         0           1012200         0           1012200         0           1012200         0           1012200         0           1012200         0           1012200         0           1012200         0           1012200         0           1012200         0           1012200         0 <td>1,0120 0,0120 0,0120 0,0120 0,0120 0,0120 0,0120 0,0120 0,0120 0,0120 0,01020 0,01020 0,01020 0,0100000 0,0100000 0,0100000 0,0100000 0,0100000 0,0100000 0,0100000 0,0100000 0,01000000 0,01000000 0,01000000 0,01000000 0,01000000 0,01000000 0,010000000 0,010000000 0,010000000 0,010000000 0,0100000000</td> <td>1,0120         0           1,0120         0           1,02120         0           1,02120         0           1,02120         0           1,02120         0           1,02120         0           1,02120         0           1,02120         0           1,02120         0           1,02020         0           1,02020         0           0,02020         0           0,02020         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000<!--</td--><td>10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           101200         0           101200         0           1012000         0           1012000         0           1012000         0           1012000         0           1012000         0           1012000         0           1012000         0           1012000         0           101200         0           101200         0</td><td>20120000<br/>20120000<br/>201200000000<br/>20120000000000</td><td>20120 0<br/>20120 0<br/>200</td><td>20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 0
20120 0 0 20120 0 0 20120 0 0 20120 0 0 20120 0 0 20120 0 0 20120 0 0 20120 0 0 20120 0 0 20120 0 0 2012</td><td>10120         10120         10120           10120         101         101         101           10120         101         101         101         101           10120         101         101         101         101         101           10120         101         1</td><td>10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0</td></td>  | 1,0120 0,0120 0,0120 0,0120 0,0120 0,0120 0,0120 0,0120 0,0120 0,0120 0,01020 0,01020 0,01020 0,0100000 0,0100000 0,0100000 0,0100000 0,0100000 0,0100000 0,0100000 0,0100000 0,01000000 0,01000000 0,01000000 0,01000000 0,01000000 0,01000000 0,010000000 0,010000000 0,010000000 0,010000000 0,0100000000  
   | 1,0120         0           1,0120         0           1,02120         0           1,02120         0           1,02120         0           1,02120         0           1,02120         0           1,02120         0           1,02120         0           1,02120         0           1,02020         0           1,02020         0           0,02020         0           0,02020         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000         0           0,02000 </td <td>10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           101200         0           101200         0           1012000         0           1012000         0           1012000         0           1012000         0           1012000         0           1012000         0           1012000         0           1012000         0           101200         0           101200         0</td> <td>20120000<br/>20120000<br/>201200000000<br/>20120000000000</td> <td>20120 0<br/>20120 0<br/>200</td> <td>20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 0 20120 0 2012</td> <td>10120         10120         10120           10120         101         101         101           10120         101         101         101         101           10120         101         101         101         101         101           10120         101         1</td> <td>10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0</td> | 10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           101200         0           101200         0           1012000         0           1012000         0           1012000         0           1012000         0           1012000         0           1012000         0           1012000         0           1012000         0           101200         0           101200         0  
   | 20120000<br>20120000<br>201200000000<br>20120000000000   | 20120 0<br>20120 0<br>200   | 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 01 20120 0 0 20120 0 2012   
   | 10120         10120         10120           10120         101         101         101           10120         101         101         101         101           10120         101         101         101         101         101           10120         101         1   | 10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           10120         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0           101200         0  |
| 0.7460                                  |                     | 2.2190     | 41.1000    | 0.8030     | 0.9400                 | 0.5050               | 1.0650                       |                                      | 0.4450  | 0.4450<br>1.5940   | 0.4450 0.4450 0.8130 0.8130  | 0.4450<br>1.5940<br>0.8130<br>0.8460  | 0.4450<br>1.5940<br>0.8130<br>0.8460<br>0.5300   | 0.4450<br>1.5940<br>0.8130<br>0.8460<br>0.5300<br>4.3940   | 0.4450<br>1.5940<br>0.8130<br>0.8460<br>0.5300<br>4.3940<br>1.7410  | 0.4450<br>1.5940<br>0.8130<br>0.8460<br>0.5300<br>0.5300<br>1.7410<br>2.1680   | 0.4450 0<br>1.5940 7<br>0.8130 0<br>0.8460 1<br>0.5300 0.5300 0.5300 0.5300 0.5300 0.4300 0.4420 0.03000 0.03000 0.0300 0.0300 0.0300 0.0300 0.0300 0.0300 0.0300 | 0.4450 0<br>1.5940 1<br>0.8130 0<br>0.8460 1<br>0.5300 1<br>1.7410 1<br>1.7410 0<br>0.4420 0<br>0.4420 0<br>1.2270 0  |
0.4450<br>1.5940<br>0.8130<br>0.8460<br>1.3300<br>1.7410<br>1.7410<br>0.4420<br>0.4420<br>0.4420<br>0.7760<br>0.7760   | 0.1740<br>0.1750<br>0.8130<br>0.8130<br>0.8130<br>0.8460<br>0.8460<br>0.3300<br>0.1740<br>0.1740<br>0.7740<br>0.7740<br>0.7740   | 0.4450<br>1.5940<br>0.8130<br>0.8130<br>0.8460<br>0.8460<br>0.5300<br>0.5300<br>0.5300<br>0.5300<br>0.5300<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760   | 0.4450 0.4450 0.4450 0.8130 0.8130 0.8130 0.83130 0.8460 1.5300 1.5300 1.5300 1.5300 1.5300 1.2300 0.4420 0.5420 0.5420 0.7440 0.7420 0.7760 0.7760 0.7760 0.7760 5.2000 5.2000 5.2000 0.7500 0.7700
0.7700 0  | 0.4450<br>1.5940<br>0.84130<br>0.84130<br>0.84130<br>0.84330<br>0.5340<br>1.7410<br>1.7410<br>1.7410<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>2.21680<br>2.21680<br>0.2720<br>0.7760<br>0.7760<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.2720<br>0.27200<br>0.27200<br>0.27200<br>0.27200<br>0.27200<br>0.27200<br>0.27200<br>0.27200  | 0.04450<br>1.5940<br>0.88130<br>0.88130<br>0.88130<br>0.88130<br>0.5300<br>0.5300<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.7760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.077760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.077600<br>0.07760<br>0.07760<br>0.07760<br>0.077600<br>0.0776000000000000000000   | 0.4450         1.5940         1.5940         1.5940         1.5940         1.5940         1.5940         1.5140         1.2140         1.2170         1.2170         1.2170         1.2270         1.12270         1.12270         1.12270         1.12270         1.12260         1.12260         1.12610 <td>0 04450 1<br/>1.5940 0<br/>0.8460 1<br/>0.8460 1<br/>0.8460 1<br/>0.8460 1<br/>0.8460 1<br/>0.8460 1<br/>0.12200 0<br/>0.7400 0<br/>0.7400 0<br/>0.7400 0<br/>0.7400 0<br/>0.7200 0<br/>0.7200 0<br/>0.8940 0<br/>0.9750 0<br/>0.0750 0<br/>0.07500 0<br/>0.07500 0<br/>0.07500 0<br/>0.07500 0<br/>0.07500 0<br/>0.07500 0</td> <td>0.4450         1.4590         1.5940         1.5940         1.5940         1.5940         1.51630         1.2171         1.2171         1.2121         1.2270         1.2270         1.2270         1.2270         1.22500         0.017340         0.017340         0.017340         1.22500         0.017340         0.017320         0.018350         0.018350         0.018350         0.018350         0.018350         0.018350         0.018350         0.018350         0.018350         0.018350         0.018350         0.018350         0.018350         0.018250         0.018250         0.018250         0.018250         0.018250         0.018250        
<!--</td--><td>0.04450<br/>1.5940<br/>1.5940<br/>0.05300<br/>0.05300<br/>0.05300<br/>0.05300<br/>0.05300<br/>0.05300<br/>0.05300<br/>0.05300<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.077600<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.077600<br/>0.077600<br/>0.0776000000000000000000000000000000000</td><td>04450<br/>01450<br/>01590<br/>018460<br/>018460<br/>011111111111111111111111111111111111</td><td>0.04450         1.1590         1.1590           1.1590         0.08460         1.1590           0.08460         1.1710         0.1450           0.111         1.17410         1.17410           0.1760         0.7760         1.12270           0.12610         0.12610         0.12610           0.12610         0.12610         0.12610           0.8750         0.08940         0.8940           0.8750         0.08940         0.08540           0.8940         0.08540         0.04530           0.8940         0.04530         0.04530           0.9110         0.9110         0.9110</td><td>0 04450 101590 01459 101590 01459 101590 011590 0101590 01059460 01039460 01039460 01039460 0103940 0101740 011112700 011112700 011112700 011112700 011112700 011112700 011112700 0111112700 0111112700 01111111111</td><td>0 04450 0<br/>11590 0<br/>08460 0<br/>08460 0<br/>03460 1<br/>117410 1<br/>117410 1<br/>117410 1<br/>117410 1<br/>11270 0<br/>07760 0<br/>07760 0<br/>07760 0<br/>07760 0<br/>07760 0<br/>0<br/>07760 0<br/>0<br/>07760 0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0</td><td>0 04450 1015940 01450 1015940 0115940 0115940 01015940 01015940 01015940 01015940 010151410 011111111111111111111111111</td></td>   | 0 04450 1<br>1.5940 0<br>0.8460 1<br>0.8460 1<br>0.8460 1<br>0.8460 1<br>0.8460 1<br>0.8460 1<br>0.12200 0<br>0.7400 0<br>0.7400 0<br>0.7400 0<br>0.7400 0<br>0.7200 0<br>0.7200 0<br>0.8940 0<br>0.9750 0<br>0.0750 0<br>0.07500 0<br>0.07500 0<br>0.07500 0<br>0.07500 0<br>0.07500 0<br>0.07500 0  
   | 0.4450         1.4590         1.5940         1.5940         1.5940         1.5940         1.51630         1.2171         1.2171         1.2121         1.2270         1.2270         1.2270         1.2270         1.22500         0.017340         0.017340         0.017340         1.22500         0.017340         0.017320         0.018350         0.018350         0.018350         0.018350         0.018350         0.018350         0.018350         0.018350         0.018350         0.018350         0.018350         0.018350         0.018350         0.018250         0.018250         0.018250         0.018250         0.018250         0.018250 </td <td>0.04450<br/>1.5940<br/>1.5940<br/>0.05300<br/>0.05300<br/>0.05300<br/>0.05300<br/>0.05300<br/>0.05300<br/>0.05300<br/>0.05300<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.077600<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.07760<br/>0.077600<br/>0.077600<br/>0.0776000000000000000000000000000000000</td> <td>04450<br/>01450<br/>01590<br/>018460<br/>018460<br/>011111111111111111111111111111111111</td> <td>0.04450         1.1590         1.1590           1.1590         0.08460         1.1590           0.08460         1.1710         0.1450           0.111         1.17410         1.17410           0.1760         0.7760         1.12270           0.12610         0.12610         0.12610           0.12610         0.12610         0.12610           0.8750         0.08940         0.8940           0.8750         0.08940         0.08540           0.8940         0.08540         0.04530           0.8940         0.04530         0.04530           0.9110         0.9110         0.9110</td> <td>0 04450 101590 01459 101590 01459 101590 011590 0101590 01059460 01039460 01039460 01039460 0103940 0101740 011112700 011112700 011112700 011112700 011112700 011112700 011112700 0111112700 0111112700 01111111111</td> <td>0 04450 0<br/>11590 0<br/>08460 0<br/>08460 0<br/>03460 1<br/>117410 1<br/>117410 1<br/>117410 1<br/>117410 1<br/>11270 0<br/>07760 0<br/>07760 0<br/>07760 0<br/>07760 0<br/>07760 0<br/>0<br/>07760 0<br/>0<br/>07760 0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0<br/>0</td> <td>0 04450 1015940 01450 1015940 0115940 0115940 01015940 01015940 01015940 01015940 010151410 011111111111111111111111111</td>   |
0.04450<br>1.5940<br>1.5940<br>0.05300<br>0.05300<br>0.05300<br>0.05300<br>0.05300<br>0.05300<br>0.05300<br>0.05300<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.077600<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.07760<br>0.077600<br>0.077600<br>0.0776000000000000000000000000000000000   | 04450<br>01450<br>01590<br>018460<br>018460<br>011111111111111111111111111111111111  | 0.04450         1.1590         1.1590           1.1590         0.08460         1.1590           0.08460         1.1710         0.1450           0.111         1.17410         1.17410           0.1760         0.7760         1.12270           0.12610         0.12610         0.12610           0.12610         0.12610         0.12610           0.8750         0.08940         0.8940           0.8750         0.08940         0.08540           0.8940         0.08540         0.04530           0.8940         0.04530         0.04530           0.9110         0.9110         0.9110  
   | 0 04450 101590 01459 101590 01459 101590 011590 0101590 01059460 01039460 01039460 01039460 0103940 0101740 011112700 011112700 011112700 011112700 011112700 011112700 011112700 0111112700 0111112700 01111111111  | 0 04450 0<br>11590 0<br>08460 0<br>08460 0<br>03460 1<br>117410 1<br>117410 1<br>117410 1<br>117410 1<br>11270 0<br>07760 0<br>07760 0<br>07760 0<br>07760 0<br>07760 0<br>0<br>07760 0<br>0<br>07760 0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0  
  | 0 04450 1015940 01450 1015940 0115940 0115940 01015940 01015940 01015940 01015940 010151410 011111111111111111111111111   |
|   | 0.0022              | 0.0022     | 0.0260     | 0.0016     | 0.0020                 | 0.0013               | 0.0058                       |                                      | 0.0017  | 0.0017   | 0.0017<br>0.0016<br>0.0017   | 0.0017<br>0.0016<br>0.0017<br>0.0022  | 0.0017<br>0.0016<br>0.0017<br>0.0022<br>0.0022   | 0.0017<br>0.0016<br>0.0017<br>0.0022<br>0.0021<br>0.0023   | 0.0017<br>0.0016<br>0.0017<br>0.0022<br>0.0023<br>0.0023  | 0.0017<br>0.0016<br>0.0017<br>0.0022<br>0.0023<br>0.0023<br>0.0023   | 0.0017<br>0.0016<br>0.0017<br>0.0022<br>0.0023<br>0.0024<br>0.0026   | 0.0017<br>0.0016<br>0.0017<br>0.0021<br>0.0021<br>0.0023<br>0.0024<br>0.0026<br>0.0013<br>0.0013  |
0.0017<br>0.0016<br>0.0017<br>0.0021<br>0.0021<br>0.0023<br>0.0026<br>0.0026<br>0.0013<br>0.0013   | 0.0017<br>0.0016<br>0.0017<br>0.0012<br>0.0021<br>0.0023<br>0.0026<br>0.0013<br>0.0013<br>0.0013<br>0.0013<br>0.0013<br>0.0016<br>0.0016   | 0.0017<br>0.0016<br>0.0017<br>0.0021<br>0.0021<br>0.0026<br>0.0014<br>0.0016<br>0.0014<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016   | 0.0017<br>0.0016<br>0.0017<br>0.0021<br>0.0023<br>0.0024<br>0.0013<br>0.0014<br>0.0014<br>0.0016<br>0.0014<br>0.0016<br>0.00180<br>0.00180  
   | 0.0017<br>0.0016<br>0.0016<br>0.0023<br>0.0024<br>0.0026<br>0.0014<br>0.0014<br>0.0016<br>0.0014<br>0.0016<br>0.0004<br>0.0004<br>0.0004<br>0.0004<br>0.0006  | 0.0017<br>0.0016<br>0.0017<br>0.0027<br>0.0023<br>0.0024<br>0.0026<br>0.0013<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0018<br>0.0018<br>0.0018<br>0.0017<br>0.0026<br>0.0025<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0027<br>0.0026<br>0.0026<br>0.0026<br>0.0027<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0000000000 | 0.0017<br>0.0016<br>0.0016<br>0.0023<br>0.0023<br>0.0024<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025   
   |
0.0017<br>0.0016<br>0.0016<br>0.0023<br>0.0024<br>0.0024<br>0.0016<br>0.0016<br>0.0016<br>0.0018<br>0.0018<br>0.0018<br>0.0018<br>0.0025<br>0.0025<br>0.0020<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0.0025<br>0000000000  | 0.0017<br>0.0016<br>0.0016<br>0.0023<br>0.0023<br>0.0024<br>0.0014<br>0.0014<br>0.0018<br>0.0018<br>0.0018<br>0.0018<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0017<br>0.0017<br>0.0017<br>0.0017<br>0.0023<br>0.0023<br>0.0023<br>0.0024<br>0.0023<br>0.0024<br>0.0023<br>0.0024<br>0.0023<br>0.0024<br>0.0024<br>0.0023<br>0.0024<br>0.0024<br>0.0024<br>0.0023<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0024<br>0.0026<br>0.0024<br>0.0026<br>0.0024<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0026<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.00000000   
   | 0.0017<br>0.0016<br>0.0016<br>0.0023<br>0.0023<br>0.0023<br>0.0024<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00016<br>0.00016<br>0.00017<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00015<br>0.00016<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.0000000000   
  | 0.0015<br>0.0016<br>0.0016<br>0.0023<br>0.0023<br>0.0023<br>0.0023<br>0.0026<br>0.0026<br>0.0026<br>0.0003<br>0.00016<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>0.0005<br>00005<br>000005<br>00000000 | 0.0017<br>0.0016<br>0.0016<br>0.0013<br>0.00013<br>0.00014<br>0.00014<br>0.00014<br>0.00014<br>0.00014<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00016<br>0.00016<br>0.00016<br>0.00017<br>0.00016<br>0.00016<br>0.00016<br>0.00017<br>0.00016<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00016<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>0.00005<br>00   | 0.0017<br>0.0016<br>0.0016<br>0.00012<br>0.00012<br>0.00014<br>0.00014<br>0.00014<br>0.00014<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00015<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00017<br>0.00016<br>0.00016<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00016<br>0.00017<br>0.00016<br>0.00016<br>0.00017<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.0000000000   
   | 0.0017<br>0.0016<br>0.0016<br>0.0023<br>0.0024<br>0.0026<br>0.0016<br>0.0018<br>0.0018<br>0.0018<br>0.0018<br>0.0018<br>0.0018<br>0.0018<br>0.0018<br>0.0018<br>0.0018<br>0.0018<br>0.0018<br>0.0018<br>0.0018<br>0.0018<br>0.0018<br>0.0018<br>0.0018<br>0.0018<br>0.0016<br>0.0016<br>0.0016<br>0.0016<br>0.0017<br>0.0016<br>0.0017<br>0.0017<br>0.0017<br>0.0017<br>0.0017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00017<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00017<br>0.00017<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.00016<br>0.0000000000   | 0.0017<br>0.0016<br>0.0017<br>0.0022<br>0.0023<br>0.0024<br>0.0014<br>0.0016<br>0.0029<br>0.0020<br>0.0020<br>0.0020<br>0.0020<br>0.0020<br>0.0020<br>0.0020<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0015<br>0.0025<br>0.00015<br>0.0002<br>0.0002<br>0.00015<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.0002<br>0.00000000  |
| 2 2000                                  | 0.005 /             | 0.0827     | 0.2520     | 0.0615     | 0.0646                 | 0.0574               | 0.1220                       | 0110 0                               | 0.ccu.0   | 0.0728   | 0.0728<br>0.0613   | 0.0728<br>0.0728<br>0.0613<br>0.0617  | 0.0ccU0<br>0.0728<br>0.0613<br>0.0617<br>0.0569  | 0.0200<br>0.0728<br>0.0613<br>0.0617<br>0.0569<br>0.1072   | 0.0220<br>0.0728<br>0.0613<br>0.0617<br>0.0569<br>0.1072<br>0.0734  | 0.0220<br>0.0728<br>0.0613<br>0.0617<br>0.0569<br>0.1072<br>0.0734<br>0.1018   | 0.0728<br>0.0728<br>0.0613<br>0.0617<br>0.0569<br>0.1072<br>0.0734<br>0.0734<br>0.0733   | 0.0200<br>0.0728<br>0.0613<br>0.0617<br>0.0569<br>0.1072<br>0.0734<br>0.0018<br>0.0053<br>0.0553  |
0.0028<br>0.0728<br>0.0617<br>0.0617<br>0.0569<br>0.1072<br>0.0734<br>0.01018<br>0.0553<br>0.0553<br>0.0652<br>0.0652  | 0.0550<br>0.0728<br>0.0617<br>0.0617<br>0.0569<br>0.1073<br>0.0734<br>0.0734<br>0.0733<br>0.0733<br>0.053<br>0.053<br>0.0652<br>0.0652<br>0.0655   | 0.0053<br>0.0017<br>0.0017<br>0.0059<br>0.0059<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0052<br>0.0052<br>0.0052<br>0.0052<br>0.0052   | 0.0059<br>0.00513<br>0.0613<br>0.0613<br>0.0613<br>0.0613<br>0.0613<br>0.0734<br>0.0053<br>0.0553<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0053<br>0.0652<br>0.0053<br>0.0653<br>0.0653   
   | 0.0028<br>0.00728<br>0.0617<br>0.0659<br>0.0734<br>0.0734<br>0.0733<br>0.0733<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0555<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.00550<br>0.00550<br>0.00550<br>0.00550<br>0.00550<br>0.005500000000                    | 0.0728<br>0.0778<br>0.0617<br>0.0617<br>0.0569<br>0.0734<br>0.0734<br>0.0752<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.05530<br>0.05530<br>0.05530<br>0.05530<br>0.05530000000000   | 0.0550         0.0550           0.0617         0.0613           0.0617         0.0614           0.0553         0.0724           0.0734         0.0734           0.0553         0.0553           0.0552         0.0553           0.0552         0.0553           0.0552         0.0553           0.0552         0.0553           0.0553         0.0553           0.0552         0.0552           0.0552         0.0552           0.0552         0.0552           0.0552         0.0552           0.0552         0.0552           0.0552         0.0552           0.0552         0.0552           0.0552         0.0552           0.0552         0.0552  
   |
0.00500<br>0.0613<br>0.0613<br>0.0613<br>0.0613<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.0053<br>0.00530<br>0.00530<br>0.00530000000000   | 0.0550<br>0.0613<br>0.0613<br>0.0517<br>0.0517<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0552<br>0.0552<br>0.0553<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.05520<br>0.05520<br>0.05520<br>0.05520<br>0.05520<br>0.05520000000000  
   | 0.0050<br>0.00613<br>0.05617<br>0.05617<br>0.05627<br>0.0734<br>0.0734<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0552<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.0553<br>0.05530<br>0.05530<br>0.05530<br>0.05530<br>0.05530000000000  
  | 0.0550<br>0.0613<br>0.0613<br>0.06617<br>0.05637<br>0.0234<br>0.02034<br>0.0553<br>0.0652<br>0.0652<br>0.0652<br>0.0652<br>0.0653<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.0563<br>0.05630000000000000000000000000000000000  | 0.00550<br>0.00613<br>0.00617<br>0.006017<br>0.00603<br>0.00503<br>0.0078<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00523<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.005553<br>0.005530<br>0.005550000000000  | 0.00590<br>0.00561<br>0.00561<br>0.00561<br>0.00563<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00552<br>0.00525<br>0.00525<br>0.00526<br>0.00532<br>0.00543<br>0.00543<br>0.00543<br>0.00543<br>0.00543<br>0.00543<br>0.00543<br>0.00543<br>0.00543<br>0.00543<br>0.00543<br>0.00543<br>0.00543<br>0.00543<br>0.00543<br>0.00543<br>0.00543<br>0.00543<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.0055<br>0.005   
   | 0.00590<br>0.00613<br>0.00613<br>0.006617<br>0.00663<br>0.00734<br>0.00734<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00615<br>0.00813<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00803<br>0.00853<br>0.00853<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.00553<br>0.005530<br>0.005530<br>0.0   | 0.00590<br>0.00613<br>0.0613<br>0.0569<br>0.02563<br>0.02734<br>0.0734<br>0.0525<br>0.0525<br>0.0525<br>0.0525<br>0.0525<br>0.0525<br>0.05616<br>0.05616<br>0.05616<br>0.05616<br>0.05616<br>0.05616<br>0.05616<br>0.05616<br>0.05616<br>0.05616<br>0.05616<br>0.05616<br>0.05616<br>0.05616<br>0.05616<br>0.05616<br>0.05616<br>0.05616<br>0.05616<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05625<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.05655<br>0.056555<br>0.056555<br>0.056555<br>0.056555<br>0.056555<br>0.0565555555<br>0.056555555555555555  |
|   | 0.3976              | 0.1482     | 0.3636     | 0.3247     | 0.2697                 | 0.4006               | 0.7417                       | 0.4368                               | 0000-0  | 0.1550   | 0.1550   | 0.1550<br>0.3147<br>0.2631  | 0.1550<br>0.1550<br>0.3147<br>0.2631<br>0.4037   | 0.1550<br>0.3147<br>0.2631<br>0.4037<br>0.0933   | 0.1550<br>0.3147<br>0.3147<br>0.2631<br>0.4037<br>0.0933<br>0.1544  | 0.1550<br>0.1550<br>0.3147<br>0.2631<br>0.2631<br>0.0933<br>0.0933<br>0.1544   | 0.1550<br>0.1550<br>0.3147<br>0.2631<br>0.4037<br>0.4033<br>0.0933<br>0.1528<br>0.1628<br>0.1628   | 0.1550<br>0.1550<br>0.3147<br>0.2631<br>0.2631<br>0.0933<br>0.0933<br>0.1628<br>0.1628<br>0.1892<br>0.1892  |
0.11550<br>0.11550<br>0.213147<br>0.23147<br>0.20337<br>0.20337<br>0.20337<br>0.1544<br>0.1528<br>0.11852<br>0.11892<br>0.11892  | 0.1550<br>0.1550<br>0.3147<br>0.2631<br>0.2631<br>0.2631<br>0.2631<br>0.2633<br>0.1628<br>0.1528<br>0.1528<br>0.1892<br>0.1892<br>0.3010<br>0.3006   | 0.1500<br>0.1157<br>0.3147<br>0.3147<br>0.2631<br>0.4037<br>0.4037<br>0.1544<br>0.1128<br>0.1128<br>0.1128<br>0.3100<br>0.3006<br>0.3006<br>0.3779   | 0.1500<br>0.1550<br>0.3147<br>0.3147<br>0.2631<br>0.4037<br>0.2631<br>0.4037<br>0.4037<br>0.1628<br>0.1185<br>0.1185<br>0.1185<br>0.3006<br>0.3779<br>0.3779<br>0.3183  
   | 0.1500<br>0.13147<br>0.2631<br>0.2631<br>0.0033<br>0.1648<br>0.1624<br>0.1892<br>0.3010<br>0.3010<br>0.3079<br>0.3779<br>0.3779<br>0.3779<br>0.1429   | 0.1450<br>0.1455<br>0.1463<br>0.2631<br>0.4037<br>0.2633<br>0.2633<br>0.1544<br>0.1585<br>0.1585<br>0.1582<br>0.3100<br>0.3133<br>0.3133<br>0.3131<br>0.3131   | 0.1570<br>0.3147<br>0.2631<br>0.2631<br>0.4037<br>0.4037<br>0.1628<br>0.1628<br>0.1628<br>0.1628<br>0.3006<br>0.3005<br>0.3005<br>0.3179<br>0.3183<br>0.3179<br>0.3005<br>0.3129<br>0.3238<br>0.2313<br>0.2313   
   | 0.15700<br>0.3147<br>0.2631<br>0.2631<br>0.2631<br>0.1544<br>0.1544<br>0.1828<br>0.1828<br>0.3010<br>0.3183<br>0.3183<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.3377<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33779<br>0.33770<br>0.33770<br>0.33770<br>0.33770<br>0.33770<br>0.33770<br>0.33770<br>0.33770<br>0.33770<br>0.33770<br>0.33770<br>0.33770<br>0.33770<br>0.33770<br>0.337700<br>0.337700<br>0.337700<br>0.337700<br>0.337700<br>0.33770000000000  
   | 0.15700<br>0.3147<br>0.3147<br>0.033147<br>0.033147<br>0.1354<br>0.1354<br>0.1362<br>0.1362<br>0.1362<br>0.31802<br>0.31802<br>0.31802<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3179<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.3170<br>0.31700<br>0.31700<br>0.31700<br>0.31700<br>0.31700000000000000000000000000000000000  
  | 0.1370<br>0.3147<br>0.2831<br>0.0283<br>0.0337<br>0.1584<br>0.1588<br>0.1588<br>0.3109<br>0.3179<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3149<br>0.3290<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.3379<br>0.33790<br>0.33790<br>0.33790000000000000000000000000000000000   |
0.14500<br>0.3147<br>0.23147<br>0.02631<br>0.02633<br>0.02933<br>0.1544<br>0.1544<br>0.1544<br>0.1544<br>0.1544<br>0.1544<br>0.3133<br>0.11429<br>0.3109<br>0.3149<br>0.3149<br>0.3208<br>0.3314<br>0.3208<br>0.3314<br>0.3208<br>0.3314<br>0.3208<br>0.3314<br>0.3208<br>0.3314<br>0.3208<br>0.3314<br>0.3208<br>0.3314<br>0.3208<br>0.3314<br>0.3313<br>0.3208<br>0.3314<br>0.3313<br>0.3313<br>0.3315<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.3313<br>0.33130000000000                 | 0.15500<br>0.15117<br>0.40231<br>0.40233<br>0.40233<br>0.40233<br>0.40233<br>0.1544<br>0.1568<br>0.1568<br>0.1568<br>0.1568<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3298<br>0.3183<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3298<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.3388<br>0.33888<br>0.33888<br>0.33888<br>0.33888<br>0.33888<br>0.33888<br>0.33888<br>0.33888<br>0.33888<br>0.33888<br>0.33888<br>0.33888<br>0.33888<br>0.33888<br>0.33888<br>0.33888<br>0.33888<br>0.338888<br>0.33888<br>0.33888<br>0.338888<br>0.338888<br>0.338888<br>0.338888<br>0.338888<br>0.3388888<br>0.338888888888  | 0.14500<br>0.3147<br>0.3147<br>0.0373<br>0.0333<br>0.1544<br>0.1544<br>0.1544<br>0.1392<br>0.3105<br>0.3105<br>0.3131<br>0.1429<br>0.3131<br>0.1429<br>0.3131<br>0.2504<br>0.3149<br>0.3315<br>0.3469<br>0.3469<br>0.3469<br>0.3469<br>0.2663<br>0.3663<br>0.2663  
   | 0.1320<br>0.3147<br>0.3147<br>0.4037<br>0.4033<br>0.0333<br>0.1584<br>0.1485<br>0.1485<br>0.3006<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3183<br>0.3283<br>0.333<br>0.333<br>0.333<br>0.333<br>0.333<br>0.333<br>0.333<br>0.333<br>0.333<br>0.333<br>0.333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.3333<br>0.33333<br>0.33333<br>0.33333<br>0.33333<br>0.33333<br>0.33333<br>0.33333<br>0.33330<br>0.33330<br>0.333330<br>0.          | 0.1550<br>0.3147<br>0.3147<br>0.3147<br>0.0333<br>0.1544<br>0.1544<br>0.1544<br>0.1544<br>0.1544<br>0.1544<br>0.1544<br>0.3105<br>0.3056<br>0.3105<br>0.3112<br>0.3129<br>0.3129<br>0.3149<br>0.3298<br>0.3149<br>0.3298<br>0.3149<br>0.3298<br>0.3149<br>0.3298<br>0.3310<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.349<br>0.340<br>0.349<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.340<br>0.330<br>0.330<br>0.330<br>0.330<br>0.330<br>0.330<br>0.330<br>0.330<br>0.330<br>0.330<br>0.330<br>0.330<br>0.330<br>0.330<br>0.330<br>0.330<br>0.330<br>0.330<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.3300<br>0.33000<br>0.33000<br>0.33000<br>0.3300000000  |
| 2                                       | 11.7096             | 5.1440     | 2.1186     | 10.5820    | 9.6432                 | 15.8228              | 15.7233                      | 17.0649                              |   | 6.3052   | 6.3052<br>10.4167  | 6.3052<br>10.4167<br>10.0604  | 6.3052<br>10.4167<br>10.0604<br>14.5773  | 6.3052<br>10.4167<br>10.0604<br>14.5773<br>3.3727  | 6.3052<br>10.4167<br>10.0604<br>14.5773<br>3.3727<br>5.7937   | 6.3052<br>10.4167<br>10.0604<br>14.5773<br>3.3727<br>5.7937<br>5.7937<br>6.4599  | 6.3052<br>10.4167<br>10.4604<br>14.5773<br>3.3727<br>5.7937<br>6.4599<br>6.4599  | 6.3052<br>10.4167<br>10.4167<br>14.573<br>3.3727<br>5.7937<br>5.7937<br>6.4599<br>1.7.2891<br>7.3529  |
6.3052<br>10.4167<br>10.0604<br>14.5773<br>3.3727<br>5.7937<br>6.4599<br>17.2891<br>7.3529<br>11.1982  | 6.3052<br>10.4167<br>10.0604<br>14.5773<br>3.3727<br>5.7937<br>6.4599<br>17.2891<br>7.3529<br>11.1982<br>11.1982<br>10.9649  | 6.3052<br>6.3052<br>10.4167<br>10.0604<br>14.5773<br>3.3227<br>5.7937<br>6.4599<br>17.3891<br>7.3529<br>11.1382<br>11.1382<br>10.9649<br>11.2233   | 6.3052<br>10.4167<br>10.4167<br>14.5773<br>3.3227<br>5.7337<br>6.4599<br>17.3529<br>17.13529<br>11.13529<br>11.13529<br>11.13529<br>11.13529<br>11.2333<br>8.8106   
   | 6.3052<br>10.4167<br>10.0604<br>14.5773<br>3.3727<br>5.3737<br>6.4599<br>17.2891<br>7.3529<br>11.1982<br>11.1982<br>11.1982<br>11.2333<br>8.81056<br>4.3649<br>4.3649   | 6.3052<br>10.4167<br>10.4167<br>10.0604<br>14.5073<br>3.3727<br>5.7937<br>6.4599<br>6.4599<br>17.3829<br>17.3829<br>17.3829<br>11.2833<br>11.2333<br>11.2333<br>8.8106<br>4.88106<br>4.88106<br>12.2100  | 6.3052           10.4167           10.04167           10.0504           10.0504           3.3727           5.7937           5.7937           6.4599           17.2801           17.2801           17.2801           17.2801           17.2801           17.2803           17.2804           17.2805           17.2804           17.2805           9.2806           8.806           8.806           9.2807           9.7807           9.7807  
   | 6.3052           10.4167           1.0.4167           1.1.01604           1.1.1025           5.7337           5.7337           5.7337           1.1.1022           1.1.1322           1.1.1322           1.1.1322           1.1.1322           8.8106           4.3649           9.8135           9.8135  
   | 6.3052           10.4167           10.4167           11.010604           11.101624           5.7937           5.7937           5.7937           5.7937           5.7937           10.1233           11.1382           11.1383           11.1383           11.1383           11.1382           11.1383           11.1383           11.1383           11.1383           11.1383           11.1383           11.1383           12.2100           12.2100           9.7847           9.7847           9.7847           9.7847           9.7847  
  | 6.3052         10.4167           10.4167         14.5773           3.3727         3.3727           3.3727         3.3727           1.4.5773         3.3727           1.1.1.482         11.1.482           1.1.1.382         11.1.382           1.1.1.233         8.8106           9.8105         9.8135           9.8135         9.8135  |
6.3052<br>10.165<br>10.165<br>3.3727<br>3.3727<br>3.3727<br>3.3727<br>3.3727<br>3.3727<br>3.3727<br>1.1.925<br>1.1.925<br>1.1.925<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.926<br>1.1.9266<br>1.1.9266<br>1.1.9266<br>1.1.9   | 6.3052           10.4167           10.4167           10.4567           14.5773           3.3727           3.3727           3.3727           3.3727           3.3727           3.3727           3.3727           3.3727           3.3727           3.3727           3.3727           3.3727           3.3727           3.3727           3.3727           3.3727           3.3727           3.3727           3.3727           3.3777           3.3778           3.3729           1.17.2891           1.17.2891           1.12.233           8.8106           4.3649           9.818           9.318           9.318           9.316           9.3266           1.12.219%           9.920%           1.12.219%  | 6.3052         6.3052           10.0605         10.0466           3.3727         3.3727           5.3727         5.381           1.1.523         1.1.233           1.1.323         1.1.233           1.1.1.322         1.1.233           1.1.1.322         1.1.1.233           1.1.1.323         1.1.1.233           1.1.1.323         1.1.1.233           1.1.1.323         1.1.1.233           1.1.1.323         1.1.1.233           1.1.1.323         1.1.1.233           1.1.1.323         1.1.1.233           1.1.1.323         1.1.1.323           1.1.1.323         1.1.1.323           1.1.1.333         8.8.106           1.1.1.333         1.1.1.333           1.1.1.333         1.1.1.333           1.1.1.333         1.1.1.333           1.1.1.333         1.1.1.333           1.1.1.333         1.1.1.333           1.1.1.333         1.1.1.333           1.1.1.333         1.1.1.333           1.1.1.333         1.1.1.333           1.1.1.333         1.1.1.333           1.1.1.311         1.1.1.313           1.1.1.311         1.1.1.3133           1.1.1.1.311 </td
<td>6.3052<br/>100.667<br/>10.0666<br/>145773<br/>3.3277<br/>3.3277<br/>3.3277<br/>3.3277<br/>3.3277<br/>3.3277<br/>5.3289<br/>1.12891<br/>7.32891<br/>7.32891<br/>1.12892<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12891<br/>1.12991<br/>1.12991<br/>1.12991<br/>1.12991<br/>1.12991<br/>1.12991<br/>1.12991<br/>1.12991</td> <td>6.3052<br/>100.664<br/>100.664<br/>5.3727<br/>5.3727<br/>5.3727<br/>5.3727<br/>5.3727<br/>5.3725<br/>5.3727<br/>5.3725<br/>5.3727<br/>5.3725<br/>5.3727<br/>5.3725<br/>1.32280<br/>1.1.2821<br/>1.1.282<br/>1.1.2821<br/>1.1.282<br/>1.1.2320<br/>9.2648<br/>1.1.233610<br/>1.2.2006<br/>1.2.21076<br/>9.2678<br/>1.6.1571<br/>1.6.1571<br/>1.6.1571<br/>1.6.1571<br/>1.6.1571<br/>1.7.2046<br/>1.6.1572<br/>1.6.1572<br/>1.6.1572<br/>1.6.1572<br/>1.6.1572<br/>1.7.2046<br/>1.6.1572<br/>1.6.2546<br/>1.6.1572<br/>1.6.2546<br/>1.6.1572<br/>1.6.2546<br/>1.6.1572<br/>1.6.2546<br/>1.6.1572<br/>1.6.2546<br/>1.6.1572<br/>1.6.2546<br/>1.6.1572<br/>1.6.2546<br/>1.6.1572<br/>1.6.2546<br/>1.6.1572<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546<br/>1.6.2546</td> | 6.3052<br>100.667<br>10.0666<br>145773<br>3.3277<br>3.3277<br>3.3277<br>3.3277<br>3.3277<br>3.3277<br>5.3289<br>1.12891<br>7.32891<br>7.32891<br>1.12892<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12891<br>1.12991<br>1.12991<br>1.12991<br>1.12991<br>1.12991<br>1.12991<br>1.12991<br>1.12991  |
6.3052<br>100.664<br>100.664<br>5.3727<br>5.3727<br>5.3727<br>5.3727<br>5.3727<br>5.3725<br>5.3727<br>5.3725<br>5.3727<br>5.3725<br>5.3727<br>5.3725<br>1.32280<br>1.1.2821<br>1.1.282<br>1.1.2821<br>1.1.282<br>1.1.2320<br>9.2648<br>1.1.233610<br>1.2.2006<br>1.2.21076<br>9.2678<br>1.6.1571<br>1.6.1571<br>1.6.1571<br>1.6.1571<br>1.6.1571<br>1.7.2046<br>1.6.1572<br>1.6.1572<br>1.6.1572<br>1.6.1572<br>1.6.1572<br>1.7.2046<br>1.6.1572<br>1.6.2546<br>1.6.1572<br>1.6.2546<br>1.6.1572<br>1.6.2546<br>1.6.1572<br>1.6.2546<br>1.6.1572<br>1.6.2546<br>1.6.1572<br>1.6.2546<br>1.6.1572<br>1.6.2546<br>1.6.1572<br>1.6.2546<br>1.6.1572<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546<br>1.6.2546  |
|   | 1 0.78              | 2 0.26     | 3 0.72     | 4 0.61     | 5 0.68                 | 5 1.05               | 7 1.11                       | 3 0.35                               |   | θ 0.71   | 3 0.71<br>0 0.46   | ) 0.71<br>0 0.46  | 9 0.71<br>0 0.46<br>1 0.60<br>2 0.75   | 9 0.71<br>0 0.46<br>1 0.60<br>12 0.75<br>3 0.50  | 9         0.71           0         0.46           1         0.60           12         0.75           13         0.50           14         0.33  | 9         0.71           0         0.46           1         0.60           2         0.75           3         0.50           1         0.60           13         0.50           15         0.42  | 9         0.71           0         0.46           1         0.60           2         0.75           3         0.50           4         0.33           5         0.42           6         0.18  | 3         0.71           0         0.46           1         0.60           2         0.75           3         0.50           3         0.50           4         0.33           5         0.42           6         0.18           17         1.05  | 3         0.71           0         0.46       
   1         0.60           2         0.75           3         0.50           3         0.50           6         0.48           1         0.60           1         0.60           2         0.75           3         0.50           1         0.33           1         0.33           1         1.05           1         1.05           10         0.42           10         0.42           10         0.47   | )         0.71           0         0.46           1         0.60           2         0.75           3         0.50           4         0.33           6         0.48           6         0.48           7         1.05           8         0.40           8         0.47           10         0.60   | 9         0.71           0         0.46           0         0.46           1         0.50           2         0.50           3         0.50           3         0.50           1         0.10           1         1.05           1         0.10           1         1.05           1         1.05           1         1.05           1         1.05           1         0.50           1         0.50           1         0.55           1         0.55           1         0.55           1         0.55           1         0.55           1         0.55  | 9         0.71           0         0.46           1         1         0.60           2         2         0.75           3         0.50         0.42           6         0.18         0.13           7         1.05         0.42           8         0.47         0.50           9         0.57         0.50           17         1.05         0.42           19         0.95         0.47           10         0.95         0.47           11         1.06         0.95  
  | )         0.71           0         0.46           1         0.046           2         0.75           3         0.50           5         0.42           6         0.18           6         0.18           7         1.05           8         0.47           9         0.47           10         0.47           11         1.05           11         1.05           11         1.06   | 3         0.71           1         0.46           1         0.46           2         0.75           2         0.75           3         0.50           1         1.01           1         1.03           1         1.03           1         1.05           1         1.05           1         1.05           1         1.05           1         1.05           1         1.06           1         1.06           1         1.06           1         1.06           1         1.06           1         1.06  | 9         0.71           0         0.46           0         0.56           1         1           0         0.57           0         0.56           0         0.44           0         0.33           0         0.42           0         0.42           0         0.42           0         0.42           0         0.42           0         0.42           0         0.42           0         0.56           0         0.70           0         0.70           0         0.70           0         0.70           0         0.70           0         0.70  
  | 9         0.071           0.466         0.046           0.050         0.33           0.050         0.33           0.041         0.048           0.050         0.048           0.041         0.048           0.050         0.095           0.095         0.095           0.095         0.095           0.005         0.095           0.005         0.005           0.005         0.005           0.005         0.005           0.005         0.005           0.005         0.005           0.005         0.005           0.005         0.005  
  | 9         0.71           0.46         0.46           0.05         0.73           0.05         0.73           0.05         0.47           0.11         0.03           0.11         0.116           0.11         0.05           0.11         0.05           0.11         0.05           0.11         0.05           0.11         0.02           0.11         0.02           0.11         0.02           0.110         0.03           0.110         0.02           0.110         0.02           0.02         0.03   
   | 9         0.71           0.46         0.46           0.05         0.75           0.05         0.75           0.105         0.75           0.107         0.105           1.106         0.118           1.106         0.118           1.106         0.110           1.106         0.110           1.106         0.110           1.106         0.110           1.106         0.110           1.106         0.110           1.106         0.110           1.106         0.110           1.106         0.110           1.106         0.110           1.106         0.110           1.106         0.110           1.106         0.110           1.106         0.110           1.106         0.110           1.106         0.110           1.107         0.110           1.108         0.110           1.108         0.110           1.108         0.110           1.108         0.110           1.108         0.110           1.108         0.110  | 9         0.71           0.46         0.046           0.5         0.5           0.5         0.5           0.5         0.33           0.6         0.13           0.7         0.6           0.8         0.42           0.13         0.03           0.13         0.13           0.14         1.05           0.13         0.13           0.14         0.10           0.13         0.13           0.14         0.10           0.15         0.10           0.10         0.25           0.10         0.22           0.22         0.210           0.23         0.22           0.10         0.28           0.06         0.28           0.06         0.28           0.06         0.28           0.06         0.28           0.06         0.28           0.06         0.28  
   | 9         0.71           0.466         0.466           0.50         0.57           0.50         0.57           0.50         0.57           0.50         0.33           0.51         0.105           0.51         0.138           0.51         0.138           0.51         0.138           0.51         0.138           0.51         0.138           0.52         0.138           0.51         0.105           0.51         0.105           0.52         0.105           0.52         0.106           0.52         0.106           0.52         0.106           0.52         0.106           0.53         0.52           0.53         0.52           0.53         0.52           0.53         0.53           0.53         0.54           0.53         0.54           0.53         0.54           0.54         0.54           0.55         0.54           0.54         0.54           0.55         0.54   | 9         0.71           0.46         0.71           0.64         0.71           0.71         0.60           0.71         0.60           0.71         0.71           0.71         0.71           0.71         0.71           0.72         0.05           0.73         0.05           0.74         0.13           0.75         0.42           0.71         1.05           0.71         0.05           0.71         0.05           0.71         0.05           0.72         0.10           0.73         0.10           0.74         0.72           0.72         0.10           0.74         0.74           0.75         0.10           0.74         0.74           0.75         0.74           0.75         0.74           0.74         0.74           0.75         0.74           0.74         0.74           0.75         0.74           0.74         0.74           0.75         0.74           0.74         0.74           0.75  
   | 9         0.71           0.46         0.46           0.51         0.53           0.50         0.53           0.51         0.42           0.51         0.53           0.51         0.42           0.51         0.42           0.51         0.53           0.51         0.42           0.51         0.57           0.51         0.57           0.51         0.57           0.51         0.57           0.51         0.57           0.51         0.57           0.51         0.57           0.51         0.51           0.53         0.52           0.53         0.52           0.53         0.52           0.53         0.52           0.53         0.53           0.53         0.53           0.53         0.53           0.53         0.53           0.54         0.53           0.53         0.54           0.54         0.54           0.54         0.54           0.54         0.54           0.54         0.54           0.54   | 7         0.71           0.46         0.71           0.46         0.73           0.50         0.75           0.50         0.74           0.50         0.74           0.71         0.60           0.71         0.60           0.71         0.60           0.71         0.61           0.72         0.03           0.73         0.03           0.74         0.33           0.74         0.33           0.74         0.70           0.74         0.70           0.70         0.71           0.71         0.71           0.71         0.71           0.71         0.71           0.71         0.71           0.71         0.71           0.71         0.71           0.71         0.71           0.71         0.71           0.71         0.71           0.71         0.71           0.71         0.71           0.71         0.71           0.71         0.71           0.71         0.71           0.71         0.71           0.74   |
|   | 178_4500_1          | 178_4500_2 | 178_4500_5 | 178_4500_4 | 178_4500_5             | 178_4500_6           | 178_4500_7                   | 178_4500_5                           | 0 010 011   | 1/8_45UU   | 1/8_4500_1   | 1/8_4500_1<br>178_4500_1<br>178_4500_1  | 2 005 4500 1<br>178 4500 1<br>178 4500 1<br>178 4500 1   | 2 00c9 4500 1<br>178 4500 1<br>178 4500 1<br>178 4500 1<br>178 4500 1  | 2 0024 500 1/<br>178 4500 1<br>178 4500 1<br>178 4500 1<br>178 4500 1<br>178 4500 1   | v 1/8 4500 1/<br>78 4500 1<br>78 4500 1<br>78 4500 1<br>78 4500 1<br>78 4500 1<br>78 4500 1  | 7/8 4500 1/<br>78 4500 1/<br>78 4500 1<br>78 4500 1<br>78 4500 1<br>78 4500 1<br>78 4500 1<br>78 4500 1  | VILVE 4500 11<br>78 4500 11<br>78 4500 1<br>78 4500 1   | //2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2
4500 11/2 45   | //2 4500 11/2 45 | //2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 12/2 4500 11/2 4500 12/2 45   | //2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 11/2 4500 21/2
4500 21/2 4500 21/2 4500 21/2 4500 21/2 4500 21/2 4500 21/2 4500 21/2 4500 21/2 4500 21/2 4500 21/2 4500 21/2 45  | 1/2 4500 10<br>78 4500 11<br>78 4500 11<br>78 4500 1<br>78 4500 2<br>78 45000 2<br>78 45000 2<br>78 45000 2<br>78 45000000000000000000000000 | 1/18         4300         11           78         4500         11           78         4500         11           78         4501         11           78         4501         11           78         4501         11           78         4501         11           78         4501         11           78         4501         11           78         4501         11           78         4501         17           78         4501         17           78         4501         17           78         4501         17           78         4501         17           78         4501         17           78         4501         17           78         4501         17           78         4501         2           77         4502         2           77         4502         2           78         4502         2           78         4502         2           78         4502         2           78         4502         2           78<  | I/18         4.200         5         4.200         5         4.200         1         78         4.500         1         78         4.500         1         78         4.500         1         78         4.500         1         78         4.500         1         78         4.500         1         78         4.500         1         178         4.500         1         178         4.500         1         178         4.500         1         178         4.500         1         178         4.500         1         178         4.500         1         178         4.500         1         178         4.500         1         178         4.500         1         178         4.500         1         178         4.500         2         1         178         4.500         2         1         18         4.500         2         1         18         4.500         2         1         18         4.500         2         1         18         4.500         2         1         18         4.500         2         1         18         4.500         2         1         18         4.500         2         1         18         4.500         2         13 <t< td=""><td>I/18         4.500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1</td><td>I/18         4500         15           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778&lt;</td><td>1/18, 4500 5, 124 4500 1, 178, 4500 1, 178, 4500 1, 178, 4500 1, 178, 4500 1, 178, 4500 1, 178, 4500 1, 178, 4500 1, 178, 4500 1, 178, 4500 2, 178,</td><td>I/18         4500         1           78         4500         1         78         4500         1           78         4500         1         178         4500         1         1         18         4500         1         178         4500         1         178         4500         1         178         4500         1         178         4500         1         178         4500         1         178         4500         1         178         4500         2         1         18         4500         1         178         4500         2         1         18         4500         1         178         4500         2         1         18         4500         2         1         18         4500         2         1         18         4500         2         1         18         4500         2         1         18         4500         2         1         18         4500         2         1         18         4500         2         1         18         18         18         1         13        
4500         2         1         18         4500         2         1         18         4500         2</td><td>I/18         4500         1           73         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           78</td><td>178, 4500, 21 178, 4500, 21 178, 4500, 11 178, 4500, 11 178, 4500, 11 178, 4500, 11 178, 4500, 12 178, 4500, 21 178, 4500, 21 178, 4500, 22 178, 4500, 42 17</td><td>I/18         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           78         4500         2           78         4500         2           78         4500         2           78         4500         2           78</td><td>I/18         45001           78         45001           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           778         4500           778         4500           778         4500           778         4500           778         4500           778         4500           778         4500           778         4500           778         4500           778         4500           778         4500           778         4500           778         4500           778         4500           778         4500</td></t<> | I/18         4.500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1   
  | I/18         4500         15           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         11           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778<  
   | 1/18, 4500 5, 124 4500 1, 178, 4500 1, 178, 4500 1, 178, 4500 1, 178, 4500 1, 178, 4500 1, 178, 4500 1, 178, 4500 1, 178, 4500 1, 178, 4500 2, 178,  | I/18         4500         1           78         4500         1         78         4500         1           78         4500         1         178         4500         1         1         18         4500         1         178         4500         1         178         4500         1         178         4500         1         178         4500         1         178         4500         1         178         4500         1         178         4500         2         1         18         4500         1         178         4500         2         1         18         4500         1         178         4500         2         1         18         4500         2         1         18         4500         2         1         18         4500         2         1         18         4500         2         1         18         4500         2         1         18         4500         2         1         18         4500         2         1         18         18         18         1         13         4500         2         1         18         4500         2         1         18         4500         2   | I/18         4500         1           73         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           78   
  | 178, 4500, 21 178, 4500, 21 178, 4500, 11 178, 4500, 11 178, 4500, 11 178, 4500, 11 178, 4500, 12 178, 4500, 21 178, 4500, 21 178, 4500, 22 178, 4500, 42 17   | I/18         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         1           78         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           778         4500         2           78         4500         2           78         4500         2           78         4500         2           78         4500         2           78  
   | I/18         45001           78         45001           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           78         4500           778         4500           778         4500           778         4500           778         4500           778         4500           778         4500           778         4500           778         4500           778         4500           778         4500           778         4500           778         4500           778         4500           778         4500           778         4500  |

	Data	for Tera-W	asserburg p	lot		Data for	Wetherill	olot	SUC						Dates				% Concordancy (	206Pb-238U	Concordancy (206Pb-238)	-
	<sup>238</sup> U/ <sup>206</sup> Pb	2SE	<sup>207</sup> Pb/ <sup>206</sup> Pb	2SE	<sup>207</sup> Pb/ <sup>235</sup> U	2SE 2	<sup>06</sup> Pb/ <sup>238</sup> U	2SE	Rho	ni /a4	207	Pb/ <sup>206</sup> Pb	2SE <sup>206</sup> F	ob/ <sup>238</sup> U 2	SE <sup>207</sup> PI	o/ <sup>235</sup> U 2	SE <sup>208</sup> P	b/ <sup>232</sup> Th 2	SE age/207Pb-206	b age)*100	age/207Pb-235U age)*100	-
337A_1 0.11	12.4224	0.5092	0.0586	0.0027	0.6470	0.0270	0.0805	0.0029	0.7120	0.0198 0.	0020	533	71	501	19	04	19	396	39 94.0		99.4 2	_
337A 2 0.20	12.5/86	0.3164	0.059/	0.0022	0.6610	0.0140	0.0795	0.0014	0.4693	0.0255 0.0	0018	5/6 633	43	493 Ano	12	15	24	508	55 85.6 16 06.2		95.7 08.7	-
337A 4 0.98	10.5485	0.2782	0.0612	0.0028	0.7940	0.0260	0.0948	0.0017	0.264.3	0.0300	0000	602	67	584	15	94	10	100	0.79		98.3 28.3	
37A 5 0.48	5.0505	0.1837	0.1573	0.0058	4.3200	0.1500	0.1980	0.0062	0.8832	0.0571 0.	0039	2415	35	1153	37 1	574	35	121 7	4 47.7		68.9	-
37A 6 0.39	9.4518	0.3752	0.0625	0.0034	0.8880	0.0410	0.1058	0.0037	0.4877	0.0330 0.	0024	659	96	648	24	47	26	655 4	17 98.3		100.2	-
37A_7 0.41	12.1065	0.4983	0.0694	0.0036	0.7930	0.0370	0.0826	0.0031	0.5099	0.0277 0.	0021	920	87	511	20	97	53	552 4	11 55.5		85.6	-
37A_8 0.34	15.4321	0.4287	0.0586	0.0028	0.5070	0.0170	0.0648	0.0013 (	0.1724	0.0208 0.	0016	473	71	405	11 4	-15	14	415 3	85.5		97.5	_
337A_9 0.30	5.2274	0.1585	0.1019	0.0047	2.6290	0.0930	0.1913	0.0046	0.4617	0.0627 0.	0044	1638	64	1127	31 1:	306	33	229 8	33 68.8		86.3	_
37A_10 0.52	5.2854	0.1397	0.0782	0.0029	2.0560	0.0500	0.1892	0.0036 (	0.5741	0.0569 0.	0037	1139	38	1116	27 1	132	25	118 7	1 98.0		98.6	,
337A_11 1.24	11.0011	0.3510	0.0654	0.0029	0.8240	0.0280	0.0909	0.0024 (	0.3788	0.0289 0.	0019	739	99	560	17	07	19	575 3	38 75.8		92.3	- 1
337A_12 1.20	10.1523	0.3298	0.0606	0.0027	0.8250	0.0280	0.0985	0.0026	0.5004	0.0296 0.	0020	608	67	606	18	10	81	289	266 687		99.3 20.7	- 1
337A_13 0.47	17.3913	0.5747	0.0624	0.0033	0.4960	0.0220	0.0575	0.0016	0.1626	0.0192 0.	0014	597	85	360	11	06	17	386	27 60.3		88.7	-
837A 14 0.47	5.5157	0.2251	0.1270	0.0054	3.1300	0.1100	0.1813	0.0066	0.7160	0.0221 0.	0021	2065	51	1076	41	148	8	442	11 52.1		74.3	-
337A 15 0.27	34.0136	3.0080	0.1410	0.0220	0.4910	0.0640	0.0294	0.0025	0.3094	0.0080	0036	1800	290	186	16	01	43	157	2 10.3		46.4	-
337A_16 0.23	3.2258	0.1020	0.1099	0.0048	4.6100	0.1500	0.3100	0.0080	0.4850	0.0875 0.	9900	1779	57	1743	48	749	36	691 1.	20 98.0		99.7	- 1
337A_17 0.59	10.6157	0.3268	0.0603	0.0026	0.7750	0.0290	0.0942	0.0023	0.4956	0.0302 0.	0020	582	66	580	17	62	50	601	10 01		100.2	- 1
8837B_1 0.50	3.9904	0.1131	0.1043	0.0034	3.6410	0.0630	0.2506	0.0047	0.6242	0.0729 0.	0025	1701	27	1441	36	558	27	422 4	18 84.7		92.5	_
3837B_2 0.63	10.0705	0.2434	0.0597	0.0020	0.8250	0.0130	0.0993	0.0011 0	0.4028	0.0320 0.	0011	587	35	611	14 6	10	16	637 2	21 104.7		100.2	_
3837B_3 0.69	3.1250	0.0938	0.2198	0.0068	9.7300	0.2000	0.3200	0.0069 (	0.8806	0.0625 0.	0025	2980	17	1791	47 2.	406	33	227 4	18 60.1		74.4	
3837B_4 0.27	13.1406	0.3454	0.0573	0.0021	0.6090	0.0120	0.0761	0.0012	0.4044	0.0240 0.	0010	492	45	473	12 4	84	14	482 1	96.1		97.8	-
3837B_5 0.35	18.4298	0.4416	0.0542	0.0018	0.4076	0.0067	0.0543	0.0006 (	0.3068	0.0170 0.	9000	377	38	341	8	47	10	340 1	2 90.3		98.3	
3837B_6 0.91	10.5153	0.2764	0.0635	0.0023	0.8370	0.0190	0.0951	0.0014 0	0.4246	0.0301 0.	0010	701	46	586	14 6	18	17	600 2	20 83.5		94.7	
3837B_7 0.61	12.8041	0.3771	0.0633	0.0025	0.6880	0.0180	0.0781	0.0016 (	0.3544	0.0182 0.	0008	694	55	486	14 5	29	17	364 1	6 70.0		91.8	
8837B_8 0.71	14.8611	0.3754	0.0560	0.0020	0.5230	0.0100	0.0673	0.0009	0.4719	0.0215 0.	0007	453	45	420	10 4	26	13	431 1	5 92.6		98.5	_
8837B_9 0.50	1.9516	0.0457	0.1840	0.0055	13.0700	0.1000	0.5124	0.0042	0.6566	0.1404 0.	0045	2688	1	2667	49 2	385	31	9055 E	80 99.2		99.3	1
337B_10 0.45	3.4083	0.0778	0.1071	0.0032	4.3310	0.0350	0.2934	0.0025 (	0.6151	0.0876 0.	0028	1750	14	1658	33	399	26	697 5	52 94.7		97.6	,
837B_11 0.53	14.4509	0.4177	0.0610	0.0021	0.5810	0.0100	0.0692	0.0014	0.5288	0.0234 0.	8000	632	39	431	12	65	13	468	7 68.3		92.8	1
837B 12 0.21	3.0303	0.0735	0.1119	0.0036	5.0700	0.0630	0.3300	0.0039	0.4848	0.1012 0.	0041	1826	22	1838	39	329	1	944	4 100.		100.5	
37B 13 1.24	10.7527	0.3122	0.0610	0.0024	0.7880	0.0200	0.0930	0.0018	0.2920	0.0253 0.	0012	623	59	5/4	9	89	11	505	23 92.1		97.5	-
3/B_14 0.4/	9.8039	0.2307	0.0609	0.0020	0.8530	0.0120	0.1020	0.0011	1/291	0.0324 0.	1100	633	87	626	4 9	12	10	100	22 98.8		99.8	- 1
3/B_15 U.5U	0.7070	0.1885	0.0705	G200.0	1.2040	07.70	0.1303	10010	0. 1649	0.0445 0.	9100	930	40	189	2 2	32	2	199	22 84:3		94.94 0	1
0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4 6761	0.000	0.0040	2000.0	0.000	0.00.0	0.000	00000	0.020.0	0.01010	0016	1200	E0 4	242		186	0.40	211	2017 0E 2		90.0 0 1	1
837 3 0.40	10.4403	0.2402	0.0501	0.0010	2.434U	0.0100	0.0057	0.0016	0.4423	0 0300 0	01.00	1309 546	50	500	13	20/	19	211 816	7 108.0		30.4	
837 4 0.79	8.2169	0.2026	0.0745	0.0026	1.2560	0.0290	0.1217	0.0023	2201	0.0241 0.	2000	1045	54	741	17	25	2 0	482	3 70.9		8.68	1
837 5 0.64	11.3507	0.2834	0.0643	0.0019	0.7800	0.0160	0.0881	0.0017	0.5823	0.0198 0.	0000	751	40	544	13	85	15	396	2 72.4		92.9	1
837 6 0.54	11.7647	0.2768	0.0581	0.0023	0.6850	0.0240	0.0850	0.0015	0.3086	0.0247 0.	6000	516	73	527	12	28	2 6	493	8 102.1		99.7	1
837 7 0.69	10.7991	0.2682	0.0572	0.0026	0.7410	0.0280	0.0926	0.0019 (	0.1629	0.0299 0.	0010	457	80	571	14	63	50	595 1	9 124.9		101.4	1
837_8 0.94	3.3322	0.0688	0.1042	0.0028	4.3250	0.0630	0.3001	0.0041	0.4739	0.0859 0.	0015	1697	27	1690	30 1	396	25	664 2	83.69		9.66	
837_9 0.23	3.5676	0.0738	0.1006	0.0026	3.8920	0.0560	0.2803	0.0039 (	0.5447	0.0864 0.	0023	1639	26	1593	29 1	312	25 1	672 4	13 97.2		98.8	
337_10 0.32	1.5480	0.0383	0.1344	0.0041	12.0700	0.2700	0.6460	0.0130	0.5268	0.1437 0.	0066	2139	37	3206	63 2	306	33	2720 1	20 149.9	_	123.0	- 1
337_11 0.52	11.0865	0.2458	0.0589	0.0018	0.7350	0.0150	0.0902	0.0014	0.3737	0.0268 0.	9000	542	46	556	12	58	15	535	102.1		99.7 	1
<u>537_12_0.99</u>	11.6822	0.2593	0.0646	0.0021	0.7640	0.0200	0.0856	0.0014	0.4281	0.0279 0.	9000	744	52	529	11	8/	11	556	2 71.1		91.5	
337 13 0.40	5.6948	0.1362	0.0724	0.0027	1.7470	0.0470	0.1756	0.0032	0.2756	0.0511 0.	0019	976	09	1042	23	028	52	005	36 106.8		101.4	
337_14 0.53	5.5157	0.1278	0.0755	0.0021	1.8890	0.0380	0.1813	0.0031	0.4660	0.0538 0.	0011	1071	36	1073	23	981	53	058	22 100.2		99.3 55 t	
00/ 10 0.00	10.4603	0.1580	0.0606	0.0000	0.7760	0.0200	0.0056	0.0017	1.4027	0.0305 0.	00.10	643 674	34 81	100	0 0	10	0 0	1/1	8 83.0		90.4 101 D	
70 0 120	11 57 41	0.6162	0.0642	0.0045	0.7660	0.0200	0.0000	1000	1404	0 0231	0010	1/0	140	202	2 2	00	<u>o</u> 8		100.1		0.101	
227 18 0.20	11.3741	0.0102	0.0581	0.0018	00000	0.0390	0.0800	0.0014	0.1494	0 08000	81.00	527	140	200	14	23	12 12	575	105.0		34.2 100.0	_
837 19 0.43	6.1576	0.1441	0.0736	0.0026	1.6270	0.0380	0.1624	0.0028	0.2351	0.0506 0.	0015	10.06	54	026	10	80	2 62	995	96.4		0.99	
337 20 0.35	10.6724	0.2392	0.0587	0.0019	0.7610	0.0210	0.0937	0.0016	0.4197	0.0283 0.	6000	523	54	577	13	72	17	564	110.3		100.9	
337 21 0.54	10.6724	0.2392	0.0580	0.0019	0.7420	0.0190	0.0937	0.0015	0.2963	0.0296 0.	0008	526	53	578	12	62	16	591	109.8		102.8	
337_22 0.73	18.2815	0.6684	0.1235	0.0100	0.9480	0.0770	0.0547	0.0018 0	0.1266	0.0237 0.	0015	1870	130	343	12	55	30	473 2	29 18.3		52.4	1
837_23 0.36	6.3573	0.1859	0.0752	0.0024	1.6110	0.0480	0.1573	0.0039 (	0.6082	0.0436 0.	0018	1063	50	941	26 5	73	25	862 3	85 88.5		96.7	
837_24 0.24	7.1685	0.1696	0.0761	0.0025	1.4720	0.0310	0.1395	0.0026	0.3709	0.0354 0.	0013	1092	48	841	19 5	16	21	703	26 77.0		91.8	
837_25 0.43	2.4576	0.0501	0.1410	0.0035	7.8900	0.1000	0.4069	0.0054 (	0.6282	0.1279 0.	0025	2239	20	2199	38	217	27 27	2429 4	14 98.2		99.2	- 1
837_26 1.05	22.5225	0.6594	0.0525	0.0018	0.3210	0.0100	0.0444	0.0011	0.6041	0.0146 0.	0003	312	58	281	80	82	6	292	20.0		99.5	- 1
33/ 2/ 0.5/	11/8/9	0.1949	7690.0	0.0016	0.8310	0.0130	0.1013	2100.0	0.4596	0.0320 0.	0000	208	33	779	2	13	<u>د</u>	030	1001 L		101.4	1
02.7 20 10.50	5.2241 2.2124	0.0577	0.1227	0200.0	6 0830	0.0010	0.2556	0700.0	1.5244	0.1062 0.0	2100	COLL	21	1131	25	140	17 10	871	12 87.1 27 07 07 07 0		99.3 08.7	- 1
337 30 0.51	10.0705	0.3347	0.0667	0.0032	0.8950	0.0400	0.0993	0.0029	0.3717	0.0386 0.	0021	766	06	612	19	51	28	765 4	6.67 01		94.0	
37_31 0.78	1.9231	0.0481	0.1907	0.0053	13.6500	0.2700	0.5200	0.0100	0.6452	0.1581 0.	0034	2740	27 ::	2711	56 2	727	31 2	362 E	6.96 98.9		99.4	
37_32 0.65	3.5236	0.0931	0.1078	0.0030	4.2530	0.0910	0.2838	0.0062	0.6543	0.0817 0.	0020	1762	32	1608	38 1	383	28	587 3	37 91.3		95.5	
337_33 0.64	9.3197	0.2345	0.0634	0.0028	0.9490	0.0340	0.1073	0.0021	0.1996	0.0336 0.	0013	661	77	658	16 6	19	52	668	25 99.5		96.9	
337_34 0.75	4.7059	0.1041	0.0912	0.0027	2.6840	0.0530	0.2125	0.0034 (	0.4351	0.0724 0.	0015	1450	38	1242	25 1:	323	25	412 2	9 85.7		93.9	_
337_35 0.56	15.4560	0.3344	0.0558	0.0020	0.4970	0.0130	0.0647	0.0010	0.3019	0.0203 0.	9000	419	58	405	6	60	12	406	1 96.6		0.06	1
337_36 0.48	11.8483	0.2948	0.0595	0.0017	0.6880	0.0140	0.0844	0.0017	0.5824	0.0238 0.	9000	578	37	522	12 5	33	14	475 1	11 90.3		98.0	

## South Tempest G-88 (3837.3 m) Sample

	$\left  \right $	Data for Tere	a-Wasserburg	plot		Data fo	r Wetherill	plot		-	╞				Dates				% Con	rordancy (206Ph-23811	%Concordancy (206Pb-238U
Identifier	n/u 238U/	<sup>4206</sup> Pb 2SE	<sup>207</sup> Pb/ <sup>206</sup> Pl	0 2SE	<sup>207</sup> Pb/ <sup>235</sup> U	2SE	<sup>206</sup> Pb/ <sup>238</sup> U	2SE	Rho	Pb/***Th	25E 207	Pb/ <sup>206</sup> Pb	2SE 206	Pb/ <sup>238</sup> U	2SE 207	ob/ <sup>235</sup> U	2SE 208	Pb/ <sup>232</sup> Th	2SE age/2	207Pb-206Pb age)*100	age/207Pb-235U age)*100
G70 4405 1	0.79 9.3	985 0.415 440 0.41 <i>E</i>	0.0689	0.4083	1.0300	0.0340	0.1064	0.0028	0.4130	0.0377 0	0023	882	28 S	655 7.70e	28	718	26	748	44	74.3	91.2
G70 4405 2	130 45	419 0.115 537 0.100	2 0.039/8	0.2770	23.4300	0.0500	0.2106	0.0140	0.7018	0.3/60 0	0720	3909	8 %	1 276	9/ 40	3235 1388	33	646U 1153	320 65	56.8 81.1	010
G70 4405 4 (	1.64 4.7	619 0.294	0.5230	0.5358	14.8400	0.5600	0.2100	0.0110	0.8699	0.3810 0	0230	4304	9 6	1226	68	2812	57	6510	340	28.5	43.6
G70 4405 5 \	7.43 2.4	752 0.104.	2 0.1366	0.4852	7.5400	0.1600	0.4040	0.0091	0.6653	0.1308 C	.0071	2178	31	2188	78	2175	39	2487	130	100.5	100.6
G70 4405 6	0.15 2.4	528 0.102	0.2008	0.2044	11.2800	0.3700	0.4077	0.0091	0.5251	0.4470 0	0410	2831	46 Pe	2201	79	2540	47	7390	570	77.7	86.7
G70 4405 8 (	1.24 10.1	1729 0.507	0.1783	0.3684	2.4300	0.1100	0.0983	0.0034	0.3151	0.1334 0	0110	2629	22	604	29 29	1251	43	2550	190	23.0	48.3
G70 4405 9 1	1.57 2.5	510 0.110	5 0.1394	0.4536	7.4400	0.1900	0.3920	0.0100	0.6607	0.1118 0	.0063	2218	36	2139	82	2163	41	2140	110	96.4	98.9
G70_4405_10	1.60 2.8	547 0.114	1 0.1147	0.3294	5.5700	0960.0	0.3503	0.0054	0.6048	0.1014 0	.0054	1876	26	1939	99	1915	36	1950	98	103.4	101.3
G70 4405 11	0.46 11.:	1483 0.447.	1 0.0622	0.3849	0.7640	0.0240	0.0897	0.0017	0.1634	0.0304 0	0018	622	72	554	21	572	22	604	35	89.1	96.8
G70 4405 12	1.21 17.	3010 0.868	0.2860	-0.0146	2.3200	0.1500	0.0578	0.0021	0.4924	0.0335 0	0023	3353	82	362	18	1209	53	999	44	10.8	29.9
G70 4405 13	1.03 12.1	V734 0.050	0.1810	10/0/0	2 3400	0.2200	0.0064	0.0024	0.1900	0 0679 0	2200	2412	140	487	25	1207	33 74	0/3 1320	43	20.2	46.0
G70 4405 15 (	1.31 10.7	796 0.437	0.1810	0.1399	1 4720	0.0570	0.0932	0.0018	0.4248	0.060.5	100.34	1791	61	575	3 8	916	33	1189	69	32.1	49.1 62.8
G70 4405 16	1.28 10.5	3170 0.4410	0.0820	0.3203	1.0500	0.0230	0.0916	0.0016	0.4891	0.0435 0	.0026	1250	37	565	ន	728	23	859	51	45.2	7.77
G70 4405 17 N	0.33 6.8	493 0.304	9 0.1179	0.0905	2.3580	0.0780	0.1460	0.0037	0.2072	0.0945 0	.0064	1907	52	878	36	1225	37	1822	120	46.0	71.7
G70_4405_18	3.6.	576 0.147.	2 0.0931	0.5250	3.4850	0.0570	0.2734	0.0050	0.5944	0.0781 C	.0044	1496	30	1558	56	1523	34	1522	83	104.1	102.3
G70_4405_19	3.8	820 0.180.	3 0.1107	0.4738	3.9100	0.1300	0.2576	0.0079	0.7188	0.0578 0	.0047	1818	45	1476	62	1617	41	1135	89	81.2	91.3
G70 4405 20 C70 4405 21	1.10 2.2	727 0.103 872 0.086	3 0.1732 1 0.1777	0.3960	10.7600	0.2600	0.4400	0.0120	0.5495	0.1223 0	0065	2586	86 6	2355	87	2502	42 38	2332	120	91.1 07.5	94.1 06.6
G70 4405 22	12 7.1	378 0.331	0.0709	0.4806	1.3620	0.0360	0.1401	0.0042	0.3901	0.0420 0	0024	936	2 2	844	37	871	28	832	47	90.2	96.9
G70 4405 23 1	).56 12.5	3032 0.682	5 0.0883	0.3415	0.9670	0.0430	0.0775	0.0030	0.5768	0.0302 0	0020	1403	72	481	24	687	29	602	39	34.3	70.0
G70_4405_24	0.54 5.3	562 0.263.	9 0.1493	0.5480	3.8100	0.1200	0.1867	0.0063	0.6218	0.0491 0	.0035	2342	51	1107	49	1591	40	968	67	47.3	69.6
G70 4405 25	0.66 3.9	761 0.158	0.1052	0.5875	3.6240	0.0560	0.2515	0.0048	0.7670	0.0669 0	0038	1720	ន	1445	22	1557	34	1310	71	84.0 400 F	92.8
G70 4405 20	1.02 3.0	142 0.120	0.1131	0.3780	0.1900	0.1200	0.1847	0.000	0.0050	0.1004 U	RCN0	1840	90 40	1001	85	1355	40	128.4	83	50 3	100.Z B0.F
G70 4405 28 (	167 2.8	409 0.1130	0.1177	0.4034	5.6730	0.0880	0.3520	0.0063	0.8113	0.1066	0057	1923	17	1942	3 89	1931	36	2045	100	101.0	100.6
G70 4405 29 (	1.47 9.1	324 0.400	0.1061	0.2604	1.5800	0.0780	0.1095	0.0026	0.2841	0.0533 0	0036	1730	33	670	88	962	41	1055	71	38.7	69.6
G70 4405 30	1.37 52.1	1921 2.124	7 0.1069	-0.0054	0.2860	0.0110	0.0192	0.0004	0.5037	0.0128 0	0008	1723	58	122	5	254	12	258	16	7.1	48.1
G70 4405 31	0.29 6.9	541 0.333	7 0.0910	0.4057	1.8120	0.0600	0.1438	0.0045	0.5225	0.0733 0	.0047	1454	55	865	39	1049	32	1429	88	59.5	82.5
G70 4405 32	0.78 4.2	808 0.177	8 0.1402	0.3998	4.4450	0660.0	0.2336	0.0048	0.6007	0.0681 0	0037	2226	33	1352	51 Sr	1724	36	1335	72	60.7	78.4
G/U 4405 33	1.84 9.3	985 0.388 2767 1 0700	0.0627	0.4897	0.9260	0.0190	0.1064	0.0021	0.5645	0.0329 0	1001	686	RF 00	653	12	499	22	654 44F	55, 55	95.2	98.2
G70 4405 35 (	1.66 9.82	232 0.4342	0.0683	0.5241	0.9570	0.0270	0.1018	0.0026	0.3899	0.0293 0	0016	863	80	627	27	083 683	23	583 583	8 8	72.7	91.8
G70 4405 36	1.17 3.3.	212 0.154	4 0.2540	0.6426	10.2400	0.2300	0.3011	0.0095	0.2135	0.1152 0	.0066	3187	55	1695	71	2452	40	2200	120	53.2	69.1
G70_4405_37_\	0.06 13.5	5685 0.644	4 0.0629	0.4059	0.6310	0.0200	0.0737	0.0023	0.6177	0.0201 0	.0016	710	55	460	21	495	20	402	32	64.8	92.9
G70 4405 38	0.30 9.1	996 0.431	3 0.1475	0.8168	2.1830	0.0410	0.1087	0.0033	0.1610	0.0790 0	9900	2290	59	664	30	1178	30	1528	120	29.0	56.4
G70 4405 39 G70 4405 40 1	1.01 13.4	1010 0.849	0.08/4	0.6429	0.8770	0.0340	0.0744	0.0038	0.3944 0.2808	0.0231 0	0015	1320	100	462 608	82 82	639	25	462 620	67.	35.0 02.6	72.3 98.6
G70 4405 41 (	1.53 8.6	356 0.350	0.1818	0.3162	2.9140	0.0650	0.1158	0.0021	0.5178	0.0950 0	.0053	2661	33	706	27	1388	34	1829	96	26.5	50.9
G70 4405 42 \	7.83 12.4	4070 0.615	7 0.1300	-0.0678	1.4290	0.0870	0.0806	0.0027	0.6323	0.0373 0	.0025	2069	25	500	24	896	42	739	49	24.2	55.8
G70 4405 43	0.74 9.7	752 0.544	7 0.1517	0.0683	2.1800	0.1400	0.1023	0.0044	0.6133	0.0517 0	0035	2352	75	628	83	1167	52	1019	67	26.7	53.8
G70 4405 45 1	1.38 9.9	108 0.034	0.0658	0.2046	0.9090	0.0280	0.4090	0 0000	0.7074	0 0372 0	10022	780	21	621 621	24 04	2000 653	42	2000	42	79.6	95.1 95.1
G70 4405 46	.64 16.1	1290 0.754	4 0.1214	0.3013	1.0270	0.0310	0.0620	0.0019	0.7934	0.0254 0	.0015	1978	32	387	18	713	25	506	30	19.6	54.3
G70 4405 47	7.59 11.5	9190 0.483	0.0612	0.4996	0.7120	0.0120	0.0839	0.0014	0.5332	0.0263 0	0014	648	¥ ۲	519	20	546	18	525	28	80.1	95.1
G70 4405 40 1	1.75 4.1	102 0.211	0.1113	0.30/0	3.2490	0.1700	0.2750	0.0100	0.0077	0.0137	7000	1010	6	1301	2 8	1541	55 55	870	120	68.1 68.1	04:0
G70 4405 50 (	10.6	1529 0.5390	0.1056	0.4797	1.3310	0.0470	0.0913	0.0031	0.4579	0.0366 0	0025	1713	88	563	27	857	34	726	48	32.9	65.7
G70 4405 51	1.19 8.5-	470 0.452	9 0.1156	0.2627	1.8840	0.0780	0.1170	0.0047	0.7131	0.0740 0	0320	1879	44	713	36	1077	40	1040	310	37.9	66.2
G70_4405_52	1.31 16.1	1031 0.700	1 0.1092	0.3239	0.9420	0.0270	0.0621	0.0017	0.5637	0.0173 0	.0010	1773	49	388	17	672	27	347	21	21.9	57.7
G70 4405 53	0.91 8.5	324 0.480	0.3360	0.5235	5.5200	0.2700	0.1172	0.0051	0.3260	0.1018 0	0072	3621	21	713	88 9	1918	64	1957	130	19.7	37.2
G70 4405 55 1	1.2/ 2/.(	2/10 1.168 1919 0.713	3 0.1574	0.2040	1.2030	0.0470	0.0592	0.0014	0.6430	0.0172 U	2100.	30/9	8 8	372	15	/96 845	34	344	68	15.3	29.3
G70 4405 56 (	1.67 3.3	670 0.136	0.1374	0.5130	5.6800	0.1200	0.2970	0.0068	0.5501	0.1048 0	0062	2178	3 88	1675	62	1927	45	2013	110	76.9	86.9
G70 4405 57	0.6 9.0	662 0.632	9 0.1271	0.7928	1.9300	0.0710	0.1103	0.0067	0.6155	0.0238 0	.0018	1995	88	677	46	1085	40	474	35	33.9	62.4
G70 4405 58	1.40 7.2	046 0.487.	9 0.3470	0.5539	6.7800	0.3600	0.1396	0.0082	0.3116	0.0744 0	.0058	3730	110	836	53	2074	61	1460	110	22.4	40.3
G70 4405 59	1.15 11.	1235 0.445	1 0.1282	0.6070	1.5420	0.0480	0.0899	0.0018	0.0388	0.0413	0026	2014	02	555	21	945	35	818	50	27.6	58.7
G70 4405 60	3.1	949 0.673	0.3780	0.6070	1 2170	3.5000	0.3130	0.0650	0.6123	0.4100	1200	3780	180	1710	290	2800	180	6500 ene	1500	45.2 13 E	61.1 41.6
G70 4405 62 (	1.53 9.50	057 0.4150	0.2180	0.1177	3.2700	0.2700	0.1052	0.0027	0.2984	0.1170 0	0130	2810	30 160	532 646	27	1402	82	2200	or 240	23.0	46.1

#### Lancaster G-70 (4405 m) Sample - Uncorrected Data

- 1914 - P-1	Data for Ter	ra-Wasserburg	3 plot - Anderse	en corrected		Data f	or Wether	ill plot - A	nderse n co	rrected				Date	- Anderse	n corrected			% C	oncordancy (206Pb-238U	% Concordancy (206Pb-238U
Identifier -	<sup>238</sup> U/ <sup>206</sup> Pb	2SE	<sup>207</sup> Pb/ <sup>206</sup> Pb	2SE	<sup>207</sup> Pb/ <sup>235</sup> U	2SE	<sup>206</sup> Pb/ <sup>238</sup> U	2SE	Rho	<sup>208</sup> Pb/ <sup>232</sup> Th	2SE	<sup>207</sup> Pb/ <sup>206</sup> Pb	2SE <sup>2</sup>	<sup>06</sup> Pb/ <sup>238</sup> U	2SE 20	<sup>7</sup> Pb/ <sup>235</sup> U	2SE 20	<sup>8</sup> Pb/ <sup>232</sup> Th	2SE ag	e/207Pb-206Pb age)*100	age/207Pb-235U age)*100
G70 4405 1 G70 4405 2	9.3985 2.3410	0.2400	0.0570	0.0013	0.8270	0.0580	0.1050	0.0052	0.8581	0.0377	0.0012	469 2166	52 87	648 165.1	30	608 1884	32	3010	37	138.2 76.2	106.6 87.6
G70 4405 3	4.5537	0.0950	0.0872	0.0014	2.6680	0.2300	0.2173	0.0099	0.9193	0.0588	0.0016	1351	31	1265	53	1299	99	1000	110	93.6	97.4
G70_4405_4	4.7619	0.2500	0.1610	0.0210	2.6800	0.6000	0.1218	0.0085	0.5779	0.3810	0.0130	2340	280	740	49	1310	180	2980	450	31.6	56.5
G70 4405 5	2.4752	0.0560	0.1315	0.0017	7.1700	0.4900	0.4020	0.0180	0.8392	0.1308	0.0026	2114	23	2183	85	2129	61	2289	190	103.3	102.5
G70 4405 6	2.4528	0.0530	0.1406	0.0034	0.2500	0.4300	0.3799	0.0180	0.8199	0.0214	0.0350	2231	42	20/8	8/	2134	2 K	2087	£ %	93.1 773.5	97.4 110.5
G70 4405 8	10.1729	0.3500	0.0593	0.0011	0.6620	0.0500	0.0840	0.0054	0.9257	0.1334	0.0088	573	40	520	32	513	8	831	120	90.8	101.4
G70 4405 9	2.5510	0.0690	0.1338	0.0027	7.1100	0.4800	0.3910	0.0190	0.7929	0.1118	0.0028	2137	35	2124	88	2121	61	1992	100	99.4	100.1
G70 4405 10	2.8547	0.0440	0.1106	0.0014	5.3600	0.3300	0.3489	0.0150	0.7989	0.1014	0.0015	1800	24	1930	71	1871	55	1887	100	107.2	103.2
G70_4405_11	11.1483	0.2000	0.0547	0.0006	0.6630	0.0290	0.0887	0.0038	0.6810	0.0304	0.0009	390	24	548	23	514	18	544	40	140.5	106.6
G70 4405 12	17.3010	0.5800	0.0495	0.0010	0.2760	0.0210	0.0393	0.0027	0.8279	0.0335	0.0015	158	43	248	17	245	16 0r	235	26	157.0	101.2
G/U 44U5 13	12.1221	0.5200	0.0524	0.0012	0.5040	0.0550	0.0000	0.0048	0.9050	0.0670	0.0063	309	25 70	431	67	404	65 af	392 604	40	1.09.5	104.6
G70 4405 15	10.7296	0.2400	0.0554	0.0008	0.6600	0.020.0	0.0861	0.0037	0.8746	0.0605	0.0014	400	35 40	430	22	513 513	9	904 1904	5 2	1.20.1	100.4
G70 4405 16	10.9170	0.1900	0.0565	0.0007	0.6880	0.0370	0.0884	0.0037	0.9118	0.0435	0.0015	465	30	545	22	529	22	535	t 4	117.3	103.7
G70 4405 17	6.8493	0.1800	0.0613	0.0018	1.1310	0.0710	0.1352	0.0066	0.7339	0.0945	0.0042	684	57	817	37	767	8	996	. 98	119.4	106.5
G70 4405 18	3.6576	0.0660	0.0922	0.0010	3.4610	0.1800	0.2737	0.0110	0.7177	0.0781	0.0019	1469	20	1557	57	1514	41	1482	80	106.0	102.8
G70 4405 19	3.8820	0.1200	0.1065	0.0039	3.8700	0.3600	0.2580	0.0130	0.8990	0.0578	0.0036	1734	69	1486	71	1593	80	1120	260	85.7	93.3
G70_4405_20	2.2727	0.0620	0.1668	0.0036	10.2200	0.7500	0.4390	0.0220	0.7709	0.1223	0.0019	2518	36	2343	97	2443	71	2221	140	93.1	95.9
G70 4405 21	2.1872	0.0330	0.1696	0.0018	10.6200	0.8000	0.4540	0.0210	0.8463	0.1310	0.0016	2549	19	2410	91	2488	74	2344	140	94.5	96.9
G70 4405 22	7.1378	0.2000	0.0635	0.0021	1.2050	0.1100	0.1387	0.0070	0.7606	0.0420	0.0011	770	60	837	39	804	48	794	42	108.7	104.1
G70 4405 23	12.9032	0.4900	0.0541	0.0015	0.5520	0.0460	0.0734	0.0039	0.9608	0.0302	0.0013	359	99	456	24	443	8	410	41	127.0	102.9
G/U 44U5 24	2002 0	0.1700	0.0045	0.0013	0.0900 c	0.3000	2011.0	0.0092	0.995/	0.0491	0.0016	110/	33	101/	25	1046	28	124.4	40 40 40	91.9 04 E	97.2
G70 4405 25	3.9/01	0.0640	0.1000	0.000	3.2000	0.3000	1842.0	0.0150	0.0920	0.1064	0.00.0	1610	10	1825	20	1720	<u>د</u> ه	1214	130	110.7	97.3 106.1
G70 4405 27	5 4142	0.2900	0.036	0.0036	2 1300	0.2900	0.1790	0.0130	0.9781	0.0656	0.0020	1264	8	1059	02	1138	86	096	120	R3.8	93.1
G70 4405 28	2.8409	0.0500	0.1142	0.0010	5.4900	0.3300	0.3505	0.0150	0.8730	0.1066	0.0017	1866	16	1933	71	1897	8 23	1959	120	103.6	101.9
G70 4405 29	9.1324	0.2400	0.0578	0.0018	0.8240	0.0540	0.1028	0.0049	0.8402	0.0533	0.0024	491	74	630	29	606	90	674	46	128.3	104.0
G70 4405 30	52.1921	0.9500	0.0461	0.0000	0.1115	0.0030	0.0175	0.0007	0.9968	0.0128	0.0005	3	+	112	5	107	3	140	11	4215.1	104.2
G70 4405 31	6.9541	0.2100	0.0625	0.0020	1.1850	0.0940	0.1385	0.0071	0.8286	0.0733	0.0028	700	65	835	40	791	44	606	93	119.3	105.6
G70 4405 32	4.2808	0:0930	0.0871	0.0015	2.6900	0.2500	0.2204	0.0110	0.9434	0.0681	0.0014	1360	31	1283	58	1326	99	764	83	94.3	96.8
G70 4405 33	9.3985	0.1900	0.0596	0.0008	0.8540	0.0590	0.1060	0.0046	0.8486	0.0329	0.0005	580	31	649	27	624	32	634	36	111.9	104.0
G70 4405 34 C70 4405 35	22.6757	0.7600	0.0474	0.0006	0.2780	0.0170	0.0426	0.0022	0.9508	0.0223	0.0007	64 6 64	27	269	14	248	13	282	32	419.8 0E 4	108.3
G70 4405 35	3 2212	010010	0.1100	0.0008	3 0000	0.6400	0.2480	0.0048	0.0670	0.1152	0.000/	1770	61 61	1425	23	157.4	130	1124	43	80.1 80.1	99.Z QN F
G70 4405 37	0.02 IZ 13 5685	0.4200	0.0564	0.0005	0.5620	0.0330	0.0735	0.00.36	0.9262	0.0201	0.0013	470	22	457	21	455	30	211	100	97.2	100.4
G70 4405 38	9.1996	0.2800	0.0620	0.0008	0.8330	0.0940	0.0971	0.0056	0.9806	0620.0	0.0053	674	26	596	33	608	25	410	20	88.4	0.86
G70 4405 39	13.4409	0.7600	0.0527	0.0013	0.5190	0.0540	0.0717	0.0050	0.9701	0.0231	0.0009	299	58	446	30	426	88	373	37	149.2	104.7
G70 4405 40	10.1010	0.1700	0.0559	0.0006	0.7570	0.0380	0.0982	0.0041	0.6876	0.0312	0.0010	436	26	605	24	571	22	561	41	138.8	106.0
G70_4405_41	8.6356	0.1500	0.0592	0.0009	0.7920	0.0430	0.0977	0.0044	0.8370	0.0950	0.0022	555	37	601	26	591	24	879	83	108.3	101.7
G70 4405 42	12.4070	0.4100	0.0511	0.0014	0.5090	0.0320	0.0729	0.0039	0.8764	0.0373	0.0017	226	62	453	23	415	21	468	58	200.4	109.2
G70 4405 44	9.1786 2.1786	0.0480	0.1783	0.0020	11 4300	0.5700	0.4640	0.0040	0.20030	0.1080	0.0033	2636	35	2454	84	004 2666	8 8	223.2	100	03.1	-00-3 06 ()
G70 4405 45	9.9108	0.2000	0.0567	0.0010	0.7640	0.0390	0.0995	0.0044	0.8233	0.0372	0.0011	464	41	611	26	575	23	656	43	131.7	106.3
G70 4405 46	16.1290	0.5000	0.0503	0.0008	0.3930	0.0290	0.0564	0.0028	0.9580	0.0254	0.0008	192	36	353	17	334	21	255	26	183.9	105.7
G70 4405 47	11.9190	0.2100	0.0550	0.0007	0.6330	0.0420	0.0832	0.0035	0.8841	0.0263	0.0004	400	29	516	21	498	56	497	32	128.9	103.5
G/U 44U5 48	4./103	0.050.0	0.0664	1200.0	2.4500	0.2000	00100	0.0110	0.0350	0.0435	0.0027	1301	4/ 75	GLZL	00	1242	400	933	120	93.4	97.0
G/U 44403 42	4.44444 10.0520	0.3900	0.0587	0.0007	0.6770	0.0540	0.0858	0.0047	0.8657	0.0366	0.0014	1001	28	1200	28	1 261	33	380	140 67	80.0 Q5 2	100.8
G70 4405 51	8.5470	0.3400	0.0591	0.0021	0.8900	0.0970	0.1086	0.0064	0.9406	0.0740	0.0320	538	82	664	37	642	3 23	800	360	123.4	103.4
G70 4405 52	16.1031	0.4400	0.0496	0.0010	0.3930	0.0370	0.0576	0.0028	0.9633	0.0173	0.0004	163	44	361	17	334	26	243	18	221.5	108.1
G70 4405 53	8.5324	0.3600	0.0622	0.0020	0.6620	0.0640	0.0755	0.0065	0.8205	0.1018	0.0044	659	74	468	39	516	40	713	120	71.0	20.7
G70 4405 54	27.0270	0.7200	0.0464	0.0002	0.1757	0.0090	0.0275	0.0014	0.9844	0.0172	0.0007	5	4	175	6	164		133	16	3294.3	106.5
G/0 4405 55	16.8919 3 3670	0.4000	0.0504	0.0006	0.3482	0.0180	0.0510	0.0024	0.909/	0.0558	0.0016	20/	30	321	15	302	14	489	48	155.2	106.3 05.6
G70 4405 57	0.0662	0.0790	0.1100	0.0012	0.8050	0.4300	0.1027	0.0140	0.83210	0.0238	0.0010	600	40	100/	50	640	31	1049 252	31	90.0 00.4	0.05 8 80
G70 4405 58	7.1633	0.4200	0.0669	0.0023	0.9280	0.1300	0.0946	0.0100	0.8358	0.0751	0.0038	813	81	580	29	667	67	483	91	71.3	87.0
G70 4405 59	11.1235	0.2300	0.0531	0.0009	0.5840	0.0360	0.0807	0.0040	0.9191	0.0413	0.0011	311	37	502	24	466	23	572	30	161.4	107.7
G70 4405 60	3.1949	0.5100	0.1330	0.0340	6.1000	3.8000	0.2460	0.0700	0.9937	0.4100	0.1200	1830	330	1360	320	1540	320	1830	780	74.3	88.3
G/0 4405 62	9.5057	0.2600	0.0595	0.0012	0.6950	0.0410	0.0857	0.0056	0.9357	0.1170	0.0110	1/2	30	285	33	538	24	239 849	38 23	80.0	104.0
15 SOF 200	2.0001	N14 VUV	0.000	2100.0	0.0000	250	2000	2.0000	0.000	V.111V	0.0110	1 100	~~~	010	5	000	7-1	010	2	w.w	00.0

## Lancaster G-70 (4405 m) Sample - Andersen (2002) Corrected Data

Baccalieu I-78 (	(4142.2 m)	Sample
	· · · · · · · · · · · · · · · · · · ·	

ncordancy (206Pb-238U	/207Pb-235U age)*100	100.4434251	97.12230216	96.5095986	98.60828242	97.4789916	93.3333333	100.4923599	100.1581028	100.0963855	96.7555556	100.9031611	90.94466182	89.02980342	100.2412351	99.0863341	99.70674487	99.55595027	97.96610169	99.45091514	99.90284049	
% Concordancy (206Pb-238U % Co	age/207Pb-206Pb age) *100 age	105.4414125	90.48257373	85.20801233	91.35220126	93.62389023	80.51502146	104.3915344	101.4411529	109.3157895	84.5984456	101.8743668	73.75339982	77.78393352	102.6853377	98.44660194	99.23195084	102.4680073	86.01190476	100.2852349	99.48776323	
	2SE	45	50	35	35	69	35	38	82	59	48	130	51	91	45	120	8	37	39	37	100	
	<sup>208</sup> Pb/ <sup>232</sup> Th	673	729	500	517	1050	514	599	1308	417	691	2133	826	1357	717	2018	1161	569	584	576	1720	
	2SE	20	27	18	16	25	18	18	27	15	21	30	20	33	16	30	29	19	18	18	29	-
se.	<sup>207</sup> Pb/ <sup>235</sup> U	654	695	573	589	1190	603	589	1265	415	675	1993	895	1577	622	2047	1944	563	590	601	1750	
Dat	2SE	25	27	23	23	42	22	22	45	17	24	67	30	58	23	99	64	22	23	22	58	
	<sup>206</sup> pb/ <sup>238</sup> U	657	675	553	581	1160	563	592	1267	415	653	2011	814	1404	623	2028	1938	561	578	598	1748	
	2SE	55	06	31	25	15	59	53	33	77	57	18	21	19	34	17	14	65	40	49	21	1
	<sup>207</sup> Pb/ <sup>206</sup> Pb	623	746	649	636	1239	669	567	1249	380	772	1974	1103	1805	607	2060	1953	547	672	596	1757	
36 E	ă	0.0023	0.0025	0.0018	0.0018	0.0036	0.0018	0.0019	0.0043	0.0015	0.0025	0.0070	0.0027	0.0048	0.0023	0.0066	0.0042	0.0019	0.0020	0.0019	0.0056	
08n L /232-	ni /a4	0.0339	0.0368	0.0251	0.0259	0.0534	0.0258	0.0301	0.0669	0.0208	0.0348	0.1113	0.0417	0.0693	0.0361	0.1050	0.0591	0.0286	0.0293	0.0289	0.0888	1010
2	Rho	0.2660	0.1461	0.7924	0.8260	0.8141	0.3146	0.1851	0.4050	0.1426	0.1945	0.6466	0.6592	0.8903	0.2840	0.5269	0.6812	0.2071	0.6491	0.3033	0.4150	
plot	2SE	0.0017	0.0022	0.0020	0.0019	0.0026	0.0016	0.0012	0.0026	0.0012	0.0014	0.0039	0.0017	0.0065	0.0012	0.0037	0.0038	0.0013	0.0019	0.0011	0.0029	
Wetherill	06 Pb/ <sup>238</sup> U	0.1073	0.1103	0.0896	0.0943	0.1973	0.0913	0.0962	0.2173	0.0666	0.1067	0.3663	0.1346	0.2440	0.1015	0.3699	0.3510	0.0908	0.0940	0.0972	0.3117	10010
Data for	ZSE 2	0.0250	0.0420	0.0190	0.0160	0.0310	0.0210	0.0180	0.0440	0.0160	0.0270	0.0740	0.0180	0.0990	0.0120	0.0630	0.0510	0.0210	0.0170	0.0190	0.0520	0.000
	<sup>07</sup> Pb/ <sup>235</sup> U	0.9070	1.0010	0.7580	0.7850	2.2340	0.8030	0.7870	2.4650	0.5070	0.9480	6.1300	1.4140	3.7260	0.8430	6.4990	5.7750	0.7440	0.7900	0.8080	4.6040	00010
ot	ZSE 2	0.0020	0.0031	0.0015	0.0014	0.0017	0.0021	0.0019	0.0021	0.0022	0.0022	0.0027	0.0017	0.0025	0.0015	0.0028	0.0026	0.0021	0.0017	0.0018	0.0024	0,000
isserburg pl	<sup>7</sup> Pb/ <sup>206</sup> Pb	0.0605	0.0662	0.0614	0.0609	0.0816	0.0626	0.0595	0.0824	0.0549	0.0651	0.1213	0.0765	0.1105	0.0602	0.1272	0.1200	0.0593	0.0621	0.0600	0.1073	1000
yr Tera-Wa	2SE 20	0.3735	9.3781	9.4858	9.4498	9.1978	9.4439	0.3998	0.1779	0.6087	0.3689	9.1043	0.2925	9.1848	0.3786	0.1023	9.1136	9.4366	9.4527	9.4022	0.1235	00000
Data fc	<sup>38</sup> U/ <sup>206</sup> Pb	9.3197	9.0662	11.1607	10.6045	5.0684	10.9529	10.3950	4.6019	15.0150	9.3721	2.7300	7.4294	4.0984	9.8522	2.7034	2.8490	11.0132	10.6383	10.2881	3.2082	1,001
ть/п	2	0.50	0.86	0.41	0.47	0.24	0.50	0.99	0.31	0.43	0.34	0.47	0.58	0.82	1.24	0.64	0.14	0.84	0.32	0.85	0.66	
ontifior	nennier	78_4142_1	178 4142 2	178 4142 3	178_4142_4	178_4142_5	178_4142_6	178_4142_7	178_4142_8	178 4142 9	78_4142_10	78_4142_11	78_4142_12	78_4142_13	78_4142_14	78_4142_15	78 4142 16	78_4142_17	78_4142_18	78_4142_19	78_4142_20	10 01 1 01

#### Baccalieu I-78 (4135.29 m) Sample

lancy (206Pb-238U %) 2b-206Pb age)*100 a	1 38 105.8	110.5	113.3	73.2					_																											
%Concorc age/207	1 38				37.2	86.7	106.1	98.7	98.0	99.1	100.4	96.8	114.8	97.8	99.1	94.6	74.6	88.5	20.0	72.1	66.3	87.5	96.5	103.5	94.7	100.5	97.2	117.4	97.9	84.2	88.6	80.5	113.4	102.5	128.9	84.7
2SE		35	110	28	6	55	120	28	50	19	29	120	28	86	30	55	29	90	17	39	20	68	110	33	100	60	26	32	82	06	28	130	65	63	3700	56
<sup>208</sup> Рb/ <sup>232</sup> Тh	26 5	423 654	490	586	156	947	2290	607	1117	387	657	1886	602	2100	611	1215	598	1971	271	884	409	1420	1988	713	917	1416	559	508	719	1984	618	1261	700	683	3300	605
2SE	58	33	35	27	14	26	46	25	33	16	24	47	24	42	27	35	28	43	8	30	18	41	54	23	55	37	8	17	35	44	24	63	31	32	85	31
es <sup>207</sup> pb/ <sup>235</sup> U	838	432 662	610	586	272	651	2178	613	1095	372	653	2071	578	2057	616	1217	627	1994	327	916	398	1461	1988	615	981	1478	570	394	1186	1876	619	1555	625	650	655	629
Dat 2SE	37	32	31	26	13	29	93	27	47	16	28	89	26	79	28	50	27	75	13	36	19	60	95	27	52	61	25	18	50	71	28	67	19	19	42	19
<sup>206</sup> Pb/ <sup>238</sup> U	862	674	623	546	237	638	2260	609	1084	370	649	2029	591	2025	606	1183	573	1857	219	820	370	1378	1974	612	938	1480	565	404	1171	1723	600	1409	628	649	683	596
2SE	30	001	110	87	67	40	33	49	31	38	25	18	52	9	77	20	84	11	98	26	52	20	45	40	160	14	40	54	14	22	27	36	53	46	270	46
<sup>:07</sup> Pb/ <sup>206</sup> Pb	815	59/ 610	550	746	630	736	2130	617	1106	373	647	2095	515	2071	612	1251	768	2099	1093	1137	558	1574	2046	591	990	1473	581	344	1196	2046	677	1751	554	633	530	704
ZSE	0.0020	0.0018	0.0054	0.0014	0.0005	0.0029	0.0065	0.0014	0.0026	0.0010	0.0015	0.0062	0.0014	0.0048	0.0015	0.0029	0.0015	0.0049	0.0008	0.0020	0.0010	0.0036	0.0061	0.0017	0.0054	0.0032	0.0013	0.0016	0.0042	0.0049	0.0014	0.0070	0.0033	0.0032	2.3000	0.0029
ht <sup>222</sup> тh	0.0425	0.0329	0.0252	0.0294	0.0077	0.0480	0.1197	0.0305	0.0568	0.0193	0.0330	0.0981	0.0302	0.1094	0.0307	0.0620	0.0300	0.1024	0.0135	0.0447	0.0205	0.0729	0.1035	0.0359	0.0468	0.0726	0.0281	0.0255	0.0366	0.1033	0.0311	0.0647	0.0352	0.0344	2.5000	0.0304
Rho	0.3524	0.0939	0.2049	0.1057	0.5898	0.5729	0.4936	0.0698	0.4178	0.0709	0.4312	0.8963	0.2148	0.6134	0.1626	0.6674	0.0439	0.8687	0.4693	0.5754	0.5728	0.8685	0.6422	0.1759	0.0098	0.6465	0.1920	0.1240	0.7013	0.6255	0.7063	0.8953	0.3824	0.4636	0.0551	0.4931
lot 2SE	0.0015	0.0025	0.0027	0.0019	0.0012	0.0018	0.0077	0.0010	0.0023	0.0005	0.0009	0.0084	0.0011	0.0023	0.0017	0.0020	0.0017	0.0041	0.0014	0.0021	0.0016	0.0041	0.0120	0.0010	0.0061	0.0021	0.0010	0.0008	0.0018	0.0041	0.0018	0.0120	0.0021	0.0022	0.0068	0.0024
Wetherill p <sup>56</sup> Pb/ <sup>238</sup> U	0.1430	0.1104	0.1014	0.0884	0.0375	0.1038	0.4205	0.0991	0.1832	0.0590	0.1060	0.3706	0.0960	0.3687	0.0987	0.2015	0.0930	0.3342	0.0346	0.1354	0.0591	0.2387	0.3580	0.0996	0.1571	0.2581	0.0915	0.0646	0.1992	0.3068	0.0976	0.2450	0.1023	0.1056	0.1127	0.0967
Data for 2SE <sup>2</sup>	0.0180	0.0430	0.0490	0.0300	0.0110	0.0220	0.1300	0.0170	0.0290	0.0071	0.0110	0.1600	0.0180	0.0360	0.0290	0.0270	0.0320	0.0910	0.0190	0.0240	0.0120	0.0710	0.2300	0.0140	0.1100	0.0320	0.0130	0.0120	0.0220	0.0800	0.0150	0.1700	0.0190	0.0160	0.1600	0.0150
<sup>7</sup> Pb/ <sup>235</sup> U	1.2820	0.9260	0.8170	0.7820	0.3050	0.9010	7.5200	0.8270	1.9400	0.4428	0.9030	6.7100	0.7660	6.5810	0.8390	2.3200	0.8560	6.1370	0.3780	1.4700	0.4800	3.2380	6.1200	0.8320	1.6200	3.2910	0.7520	0.4760	2.2150	5.3410	0.8420	3.6500	0.8530	0.8950	1.0400	0.8540
t 2SE <sup>20</sup>	0.0012	0.0032	0.0037	0.0028	0.0019	D.0014	0.0027	0.0015	0.0014	D.0011	0.0009	0.0019	0.0015	0.0014	0.0022	0.0011	0.0026	0.0015	0.0040	0.0013	0.0015	0.0014	0.0035	0.0012	0.0059	0.0011	0.0012	0.0015	0.0010	0.0020	0.0010	0.0037	0.0022	0.0022	0.0120	0.0023
sserburg plo Pb/ <sup>206</sup> Pb	0.0664	0290.0	0.0606	0.0659	0.0612	0.0638	0.1316	0.0605	0.0763	0.0542	0.0612	0.1300	0.0581	0.1281	0.0610	0.0822	0.0652	0.1301	0.0784	0.0780	0.0592	0.0975	0.1267	0.0600	0.0748	0.0923	0.0592	0.0540	0.0801	0.1262	0.0623	0.1071	0.0593	0.0612	0.0710	0.0634
r Tera-Wa: 2SE <sup>207</sup>	3228	4595	5155	5631	4933	4641	1131	4684	2562	7746	4362	1383	4883	1251	4927	2291	5203	1433	7542	3545	8875	2106	1561	4637	3809	1801	5013	7180	2319	1487	5039	2166	3058	2959	5747	3422
Data for J/ <sup>206</sup> Pb	3930 0.	0580 0.	.8619 0.	1.3122 0.	3.6667 1.	.6339 0.	.3781 0.	J.0908 0.	.4585 0.	3.9377 0.	.4349 0.	.6983 0.	0.4167 0.	.7122 0.	0.1317 0.	.9628 0.	<ol> <li>7.7527</li> <li>0.</li> </ol>	.9922 0.	3.9017 1.	.3855 0.	3.9205 0.	.1894 0.	.7933 0.	<ol> <li>0.0402</li> <li>0.</li> </ol>	3654 0.	.8745 0.	<ol> <li>9254</li> <li>0.</li> </ol>	5.4703 0.	.0201 0.	.2595 0.	<ol> <li>2459</li> <li>0.</li> </ol>	.0816 0.	0.7752 0.	.4697 0.	.8731 0.	9.3413 0.
1/n 38	.37 6	37 9	10	.06 1	.79 26	.10 9	.07 2	.53 1(	.66 5	.20 16	00.	.37 2	.80 1(	.39 2	10	.21 4	.11 1(	40 2	.11 28	.33 7	.65 16	.24 4	.34 2	.52 1(	.36 6	.33 3	74 10	.44 15	.03 5	.28 3	.61 1(	.83 4	.77 9	.95 9	.02	.92 1(
entifier Ti	4135 1 0	4135 3 1	4135 4 0	4135 5 1	4135_6 C	4135 7 C	4135_8 C	_4135_9 C	4135_10 C	4135_11 C	4135_12 1	4135_13 C	4135_14 C	4135_15 C	4135_16 C	4135_17 C	4135_18 1	4135_19 C	4135_20 1	4135_21 1	4135_22 C	4135_23 C	4135_24 C	4135_25 C	4135_26 C	4135_27 C	4135_28 C	4135_29 C	4135_30 C	4135_31 G	4135_32 1	4135_33 C	4135_34 C	4135_35 C	4135_36 C	4135_37 C

## Panther P-52 (3210 m) Sample

		Data for	Tera-Wasser	burg plot	L	ľ	Data for W	'etherill plo	, t	208 123	35				Dates				% Concordancy (206Pb-238U	%Concordancy (206Pb-238U
	23 73	8.0/ <sup>206</sup> Pb 2	SE <sup>207</sup> Pb/	<sup>206</sup> Pb 2	SE <sup>207</sup> PŁ	y/ <sup>235</sup> U 2.	SE <sup>206</sup> F	·b/ <sup>238</sup> U	2SE Rhc	/07	10 11	<sup>207</sup> Pb/ <sup>206</sup> Pb	2SE <sup>2X</sup>	<sup>16</sup> Pb/ <sup>238</sup> U	2SE <sup>207</sup>	Pb/ <sup>235</sup> U	2SE <sup>208</sup> Pb/	<sup>32</sup> Th 2SE	age/ 207P b-206Pb age)*100	age/207Pb-235U age)*100
P52_3210_1	0.88	43.0108 1.1	8499 0.05	572 0.0	0.1	770 0.0	1170 0.	0233 0.	0010 -0.03	74 0.008	0.0005	499	219	148	9	166	14 16	11	29.7	89.2
P52_3210_2	0.91	43.9754 1	7211 0.05	509 0.0	0.1	590 0.0	100 0.	0227 0.	0009 0.32	0.007	3 0.0004	236	159	145	9	149	9 14	7 7	61.3	97.1
P52_3210_3	0.92	12.3153 0.	4702 0.05	382 0.(	0.5	0.0 066	300 0.	0812 0.	0031 0.99.	4 0.026	0.0011	1387	29	503	18	669	15 51	21	36.3	72.0
P52_3210_4	0.74	12.2399 0. a 615 A 0 3	3596 0.08	325 0.(	0.5	0.0	0 00 00 00 00 00 00 00 00 00 00 00 00 0	1040 0.	0024 0.47	0.028	0.0011	1257	88	506	14	753	14 57	8 8	40.2	75.6
P52 3210 6	0.36	5.7971 0.5	1479 0.05	314 0.0	0023 1.9	570 0.0	450 0.	1725 0.	0044 0.49(	0.057	1 0.0020	1231	2 23	1026	24	1098	15 11	7 41	83.3	93.4
P52 3210 7	0.49	10.9649 0.5	3006 0.05	322 0.0	040 1.1	0.0 069	370 0.	0912 0.	0025 0.142	2 0.042	0.0019	1472	82	563	15	780	17 83	36	38.3	72.2
P52 3210 8	0.54	41.3223 1.8	3783 0.07	762 0.0	0.2	590 0.0	1200 0.	0242 0.	0011 0.230	0.011	7 0.0008	1100	171	154	7	236	16 23	5 17	14.0	65.4
P52_3210_9	0.27	4.3706 0.:	1261 0.15	325 0.(	040 4.1	370 0.0	920 0.	2288 0.	0066 0.49	0.075	1 0.0034	2131	53	1326	34	1662	18 146	1 64	62.2	79.8
P52_3210_10	0.52	10.2881 0.1	2434 0.06	518 0.0	0.8	370 0.0	160 0.	0972 0.	0023 0.53	32 0.030	5 0.0010	667	55	598	14	616	60 6	9 20	89.6	0.79
P52_3210_11	0.17	3.6140 0.:	1176 0.10	0.0	032 4.0	1400 0.1	000	2767 0.	0090 0.70	37 0.086	5 0.0036	1746	55	1571	46	1643	21 167	7 66	90.0	95.6
P52_3210_12	0.19	8.6281 0.3	3871 0.25	301 0.0	0110 3.6	400 0.1	800 0.	1159 0.	0052 0.50	94 0.226	0.0150	3053	77	705	30	1543	37 407	0 250	23.1	45.7
P52_3210_13	0.33	9.8717 0.2	2534 0.06	521 0.0	0.8	880 0.0	1200 0.	1013 0.	0026 0.35	32 0.031	2 0.0012	678	65	622	15	644	11 62	l 24	91.8	96.6
P52_3210_14	0.68	11.3379 0.	3085 0.06	567 0.0	0.8	070 0.0	12.40 0.	0882 0.	0024 0.27	6 0.028	5 0.0011	828	78	545	14	596	13 57	0 21	65.8	91.4
P52_3210_15	0.31	21.5564 0.	5111 0.05	558 0.0	0.3	1006 0.0	064 0.	0464 0.	0011 0.45	6 0.014	8 0.0005	442	99	292	7	313	5 29	3 11	66.0	93.4
P52_3210_16	0.67	9.4340 0.1	2314 0.06	510 0.0	0.8	920 0.0	160 0.	1060 0.	0026 0.52.	6 0.034	4 0.0011	639	56	649	15	648	9 68	3 22	101.5	100.2
P52_3210_17	0.55	8.8417 0	2502 0.0£	532 0.(	0.5	0.0 0960	1280 0.	1131 0.	0032 0.39.	6 0.035	7 0.0014	715	74	691	19	700	14 70	3 26	96.6	98.7
P52_3210_18	0.71	43.1779 1.	1932 0.05	204 0.(	0.1	639 0.0	0.067	0232 0.	0006 0.15	96 0.007	0.0003	213	106	148	4	153	6 14	9	69.1	96.6
P52_3210_19	0.29	28.4657 0.4	8913 0.06	585 0.(	0.3	M03 0.0	077 0.	.0351 0.	0011 0.59	30 0.014	0.0005	884	99	223	7	297	6 29	11	25.2	75.0
P52_3210_20	0.10	23.4742 0.1	8817 0.05	599 0.0	0.3	\$620 0.0	1110 0.	0426 0.	0016 0.56	55 0.021	0.0012	600	8	269	6	314	8 42	24	44.8	85.7
P52_3210_21	0.88	16.1812 0	3927 0.05	577 0.(	0.5	010 0.0	1120 0.	.0618 0.	0015 0.32.	24 0.020	1 0.0007	518	88	387	6	411	8 40	14	74.7	94.2
P52_3210_22	1.32	11.0865 0.	3319 0.07	700 0.(	0.8	830 0.0	1250 0.	0902 0.	0027 0.28.	10.028	3 0.0010	928	20	556	16	643	14 56	3 20	59.9	86.5
P52_3210_23	0.17	25.8198 0.	7333 0.05	267 0.(	0.3	8122 0.0	0.74 0.	.0387 0.	0011 0.51	0.012	9 0.0005	480	99	245	2	275	6 25	11	51.0	88.9
P52_3210_24	0.41	21.3630 0.:	5020 0.05	532 0.(	0.3	3482 0.0	071 0.	.0468 0.	0011 0.42	69 0.014	0.0005	337	8	295	7	303	5 29	10	87.5	97.5
P52_3210_25	0.64	1.8762 0.4	0598 0.15	911 0.(	0057 13.i	8700 0.3	3400 0.	5330 0.	0170 0.63	4 0.143	0.0055	2752	49	2758	72	2737	23 271	4 96	100.2	100.8
P52_3210_26	0.24	4.8031 0.	1430 0.05	334 0.(	0024 2.3	870 0.0	0. 0.	2082 0.	0062 0.65	4 0.064	2 0.0025	1279	26	1217	ŝ	1239	17 125	6 47	95.2	98.2
P52_3210_27	0.45	10.4493 0.	3057 0.0£	531 0.(	0.8	330 0.0	12.10 0.	0957 0.	0028 0.54	55 0.032	0.0012	712	5	589	16	614	12 63	3 23	82.8	95.9
P52_3210_28	0.50	17.7305 0.4	8488 0.12	220 0.(	0.5	3280 0.0	0. 0.	.0564 0.	0027 0.25	80 0.032	3 0.0021	1986	124	355	16	661	29 64	42	17.9	53.7
P52_3210_29	0.78	13.4409 0.4	4336 0.0t	536 0.(	0027 0.6	570 0.0	0.00	0744 0.	0024 0.27	0.024	3 0.0012	728	6	462	15	507	18 48	1 24	63.4	91.1
P52 3210 30	0.30	2.6954 0.	0944 0.14	106	7.1	700 0.2	300	3710 0.	0130 0.51	78 0.138	0.0078	2235	88	2031	8 5	2130	31 261	2 140	9.09 7.02	95.4
P52_3210_31	0.46	.0 /080/ U.	294/ 0.0	10 10	3.0 2.20	2230 0.0	1200	0 7660.	0029 0.34	94 0.030	0.0016	593	20 S	609	1,	60/	16 60	DF :	102./	100.3
P52_3210_32	0.0	43.4594 I.	5243 0.0,	/49 0.	2.0 5c00	1360 0.C	1160	0730 0.	30.0 6000	200.0 Z	0.000	1066	142 or	14/ 17F	υ \$	505	13 18		13.8	70.1
P.52_3210_33	1.04	22.8833 I	2044 0.02	10 600	2010 1010	J.U UCE3	0 0/1	1111	0075 0.84	00 0.014	DTOD'O	488	8 5	C/7	14	167	57 71 71	8 8	50.4 104 A	94.5 101 0
P 32 3210 34	1 03	0 2003 0.	1301 0.06	10 100	1.1 ELUC			018 0	0037 0.45.	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	/TOD/12	71/	ŧ ¤	745 745	77	00/9	10 10	* ×	204:4	0.TOT
P52 3210 36	1.03	10.4822 0.5	3516 0.06	592 0.C	1025 0.9	250 0.0	380	0954 0	0032 0.674	15 0.032	0.0015	905	24	587	19	666	20 63	0 6 0 6	649	88.1
P52 3210 37	0.86	9.8814 0.5	3027 0.06	508 0.0	0.8	520 0.0	320 0.	1012 0.	0031 0.25	86 0.032	0.0017	632	: 28	620	18	626	17 65	8	98.1	9.0
P52_3210_38	0.17	5.7045 0.:	1627 0.07	739 0.(	020 1.7	810 0.0	1480 0.	1753 0.	0050 0.56	0.059	1 0.0028	1039	55	1042	28	1039	18 115	9 54	100.3	100.3
P52_3210_39	0.48	9.6061 0.	3045 0.05	959 0.(	0035 1.3	910 0.0	1510 0.	1041 0.	0033 0.47	52 0.051	4 0.0030	1546	69	637	19	881	22 101	0 57	41.2	72.3
P52_3210_40	7.02	0.5128 0.0	0657 0.07	735 0.(	0028 20.2	2000 2.7	000 1.	9500 0.	2500 0.95	11 0.048	9 0.0029	1028	11	6790	540	3100	130 96	26	660.7	219.0
P52_3210_41	0.82	43.0663 2.1	0402 0.06	525 0.(	0.1	920 0.0	1150 0.	0232 0.	0011 0.40	52 0.008	3 0.0006	691	160	148	7	180	12 16	5 12	21.4	82.2
P52_3210_42	0.37	8.5324 0	3713 0.06	536 0.(	0026 1.C	9410 0.0	00 0	.1172 0.	0051 0.45	32 0.034	0.0019	728	81	714	59	722	20 67	32	98.0	98.9
P52_3210_43	0.47	42.1941 2.4	4925 0.07	754 0.(	0.2	360 0.0	260 0.	0237 0.	0014 0.21	0.011	0.0011	1079	216	151	6	217	22 23	53	14.0	69.5
P52_3210_44	0.28	8.3682 0	2941 0.05	0.0	0033 1.5	9400	0.00	.1195 0.	0042 0.58	15 0.071	0.0038	1488	67	728	24	942	24 135	2	48.9	77.3
P52_3210_45	0.38		8/41 0.02	0/8 1/1	200 0.20	0.0	0 071	0441 0.	-0.10 /TUU	210.0 V.013	/ 0.000	275	۹ ۲	2/2	3	300	17 50	4	23.2	92.6
P.52_3210_46	55.U	.0 8181.81		10.1	5.0 6TOC	1.0 0.2	0 051	.0 Uccu.	0.133	9.010 P	6000.0	478	ę :	<del>9</del>	1	805	11 12	8	80.4	90.2
P52_3210_47	0.38	4.1946 0.	1531 0.14	125 0.(	1040	1.0 0.1	800	2384 0.	008/ 0.83	.5 0.068	0.0033	8577	<del>8</del> 4	13/8	<del>4</del>	1//2	31 134	67	61.0	//.8
P52_3210_48	0.26	12.2850 0.	5433 0.0	10 0.0	J049 I.(	0.0 0.0 200 0.0	500	0814 0.	0036 0.37.	1 0.034	0.002/	1419	104	504	77	/39	25 68	ж «	35.5	68.2 01 0
P52_3210_49	0.04	42.3908 1.	10.0 2689 24 20 0.02	1.0 520	1.0 2200	1.0 0.0	0.19	0. 023b		20 0.00 0.000	0.004	667	£ [	150	٩	158 158	- ID	ۍ ۲	50.3	95.0
P52_3210_50	0.02	3.9210 U.	Z153 U.L.	70 777	1039 4.2	200 0.2	200 1 00 1 00		0140 0.03	19 U.UDY	0.0040	1989	7 6	1408	77	1695 245	4/ 13	8 4	/3.8	80./ or 1
P52_3210_51	0.40	21.0084 U.	70.0 1.0.0	203 U.I	2020 U.S	564U U.L	113U U	04/b0	201/ 100	CTU.U 20	1 0.000	404 275	<i>ک</i> 8	667 80c	;; c	310	01 0	2 C	C.140 9 No	1.66
707 2010 53	CC:0	20.4034 V.	10.15 0.06	10 VU:	TO SLUC	VO 001		10400 v	2010 LCVV	CTO 0 24	0,0016	008	20 20	300	ν ç	ULC CU3	10 11	3 6	24:0	23.4
C.C. ULAC 201	0.72	100CTT	4343 0.0	1 nsc	1070 Nr.	1.0 NOTO	> 	- C000-	VCDD	0.040	~~~~ I 0	660	0/	- 000	77	00z	/T /T	7c +	c.cc	C:00

%Concordancy (206Pb-238U	age/207Pb-235U age)*100	104.7	104.2	102.7	102.0 98.8	99.8	102.1 05.1	98.7	99.2 99.5	103.0	102.3	99.0 103.4	97.6	101.2	102.5	101.8	99.1	99.1 101.0	101.0	101.4	103.2	101.4	96.0 101 0	100.0	100.1	104.3	97.7	100.2	93 06. 4	102.2	98.0	101.3	94.6	99.1	102.1	0.45 8.09	100.0	100.3	101.1	101.9	100.0	97.6	100.3	101.2	97.8	96.1 100.9	101.4	101.7	99.0	97,2	99.7	100.1	99.7	101.5	98.9	99.9 104.8	100.8	95.9	97.6	2.001	91.1	98.3	99.7 100.1	102.8	98.0	100.3	104.8	102.5	103.4	101.5
% Concordancy (206Pb-238U	age/207Pb-206Pb age) *100	125.7	124.3 108.4	108.5	115.5 98.0	98.4	114.6 01 F	105.3	94.7 106.8	127.5	105.9	99.3 118.9	92.8	107.7	109.9 165.0	111.6	100.1	101.1	104.6	107.2	125.4	107.3	81.3	98.5	106.7	121.3	100.3	01.3	91.3	114.4	104.1	107.6	79.3	95.6	126.6	20.05	110.3	104.7	103.6	119.8	112.2	95.6	113.8	116.3	92.2	96.3 102.1	107.6	113.2	96.9	90.0 89.7	100.7	101.2	107.6	101.5	97.2	131.2	112.8	7.67	93.2	113.0	60.4	93.5	100.7	105.4	90.2	99.0 108.4	116.0	116.2	122.6	102.6
	2SE	22	62 58	120	55	8	59 140	88	88	8	160	88	32	22	88	88	88	ខ	2 23	8	98	88 :	4 2	58	66	65	83	170	0.70	64	8	8	55	8	6/	0	8	50	8	4	B¥	8	82	59	ន	8 120	8	8	8	37	35	100	5	16	100 5	88 6	8	17	45	ਲ ਲ	4	37	য ম	110	88	99 99	38	84	37	36
	Pb/ <sup>232</sup> Th	614	756	1346	615 1965	629	600 1555	622	580	619	1880	698 649	274	598	1052	0/C	1000	688	540 617	673	423	656	458	020 619	661	634	599	1961	1001 2746	687	634	1108	611	655	615 1060	304	660	565	626	432	601 601	630	684	625	581	632 2582	625	582	612	711	591	2085 610	254	288	2040	712	454	309	603	562	312	712	200	2221	522	634	512 1312	617	638	682
	2SE 206	14	17	14	16	10	22 25	18	12	12	13	1	9	14	15	16	11	4	17	1	12	1	2	10	6	15	16	30	30	10	17	13	10	10	32	2 6	14	11	8	10	1 10	÷	24	17	11	2/	28	26	26	28	26	50	18	15	49	37	20	17	35	25	17	29	07 VC	51	26	30	40	31	28	29
	b/ <sup>235</sup> U	579	642 961	1284	605 1963	622	606 1647	628	593	594	1770	669	293	591	9/9	624	1023	665	535 610	658	419	623	443	64	621	607	611	040	000	631	200	1079	609	636	029	677	643	593	621	408	000	619	674	605	589	632 2557	639	589	605	900	608	2177	297	284	2052	651 651	439	311	621	502	324	708	510	2166	589	619	1239	645	609	652
Dates	2SE 207	21	24	41	20	20	23	21	20	20	53	22	10	20	5 5	23	32	22	23	22	15	21	GL 0	21	22	23	22	73	24	200	22	36	21	21	28	96	22	19	20	14	77	20	26	21	21	30	31	28	29	32	29	91	19	14	25 5	98	21	15	32	26	15	33	87	6	28	31	58	38	31	32
	b/ <sup>238</sup> U	306	986	319	517 940	320	519 566	\$20	588	512	811	362	286	598	003	335	014	559	517	367	133	332	974	17	321	333	597	78.7	684	345	287	093	576	330	533	210 215	53	595	528	116	50	50	376	512	576	580	348	599	665	229	306	180	96	288	030	808	142	598	306	503	295	396	201	226	217	321	299	361	330	362
	SE <sup>206</sup> p	9 69	73	39	28	43	10	83	25 22	62	24	54 44	51	74	/0	76 6	35 1	67	5 5 6 7	44	73 4	48	200	20	44	78 6		20/	22	51 5	82	42 1	54	43	240	47 47	88	51 5	36	60	2 82	8 8	97 6	79 (	69	5 5	61	58	222	22	56 6	33	8 8	62	30	20	46 2	74 2	10	54 54	00	22	202	38	51	87	49 1	92	74 6	66 6
	/ <sup>206</sup> ph 2	32	10 38	16	20	0	10	68	21	00	10	12	8	22	2 2	- 60	13	22	8.0	22	12	8	3 5	10	32	22	8,		28	3 2	t st	16	56	60	0 5	2 6	. 8	38	90	47	200		1	50	25	28	222	60	8	2 22	02	2 2	75	2	189	200	32	74	001	55	66	4	00 82	110	40	22	20	3 68	4	15
L	207Pb	29 44	37 49 9	62 12	328	29 65	30 5-	30	27 6.	29 44	88 17	32 69	13 30	29 51	200	37 0	46 10	32	23 62	31 6	20 3-	30	20 20	300	30 51	30 55	28	10 00	30 28	31 20	32	51 10	28 73	30	38	20 00	31 22	26 54	28 60	23	000	29	38	30 52	27 6	70 25	17 60	16 52	17 6	19 00	16 60	58 21	22	08 21	20 20	30 22	13	3.	22	18 18 29	90 44	19 7	10	64 21	14	20 60	37 11	51	19 5	18 6-
	<sup>2</sup> Th 25	9 0.00	0.00	8 0.00	0.00	6 0.00	0.00	3 0.00	0.00	1 0.00	0.00	2 0.00	7 0.00	1 0.00	0.00	0.00	8 0.00	5 0.00	0.00	00.0	2 0.00	0.00	0.0	2 0.00	3 0.00	9 0.00	0.00		8.0		00.0	3 0.00	7 0.00	0.00	0.00	800	2 0.00	3 0.00	5 0.00	0.00		7 0.00	4 0.00	4 0.00	0.00	3 0.00	4 0.00	2 0.00	8 0.00	200	7 0.00	0.00	0.00	3 0.00	0.00	0000	0.00	4 0.00	0.00	0.0	6 0.00	0.00	4 0	0.00	2 0.00	0.00	0.00	0.00	1 0.00	3 0.00
	<sup>208</sup> Pb/ <sup>23</sup>	0.030	0.038	0.068	0.030	0.031	0.030	0.031	0.029	0.031	0.097	0.035	0.013	0.030	0.053	0.035	0.050	0.034	0.031	0.033	0.021	0.033	0.022	0.031	0.033	0.031	0.030	0.006	0.030	0.034	0.031	0.056	0.030	0.032	0.031	0.016	0.033	0.028	0.031	0.021	0.032	0.031	0.034	0.031	0.029	0.031	0.031	0.029	0.030	0.035	0.029	0.108	0.012	0.014	0.106	0.036	0.022	0.015	0.030	0.028	0.015	0.035	020.0	0.115	0.026	0.031	0.067	0.031	0.032	0.034
	Rho	0.3085	0.3143	0.4275	0.2970	0.4713	0.1270	0.1935	0.3957	0.2192	0.6257	0.4178	0.4273	0.1935	0.2842	0.2231	0.4748	-0.0086	0.1280	0.5276	0.3012	0.4301	1012.0	0.3892	0.4700	0.2968	0.3868	0.2883	0.6136	0.01.00	0.3529	0.4569	0.3824	0.4250	0.1141	0.1378	0.1543	0.3823	0.4898	0.2453	0.4300	0.4413	0.2457	0.2760	0.1749	0.5136	0.3064	0.3082	0.3677	0.4847	0.4215	0.5036	0.9746	0.2224	0.5352	0.1836	0.4475	0.2188	0.1726	0.2868	0.4665	0.4027	1004 0	0.5535	0.5175	0.2059	0.4683	0.0781	0.3111	0.3572
rill plot	U 2SE	0.0037	0.0042	0.0077	0.0034	0.0035	0.0040	0.0037	0.0034	0.0035	0.0110	0.0037	0.0016	0.0034	0.0061	0.0040	0.0058	0.0038	0.0039	0.0038	0.0025	0.0035	0.0025	0.0036	0.0037	0.0040	0.0037	0.0030	0.0180	0.01.00	0.0038	0.0065	0.0035	0.0035	0.0047	0.0144	0.0038	0.0033	0.0035	0.0023	0.0035	0.0034	0.0046	0.0037	0.0035	0.0050	0.0053	0.0048	0.0049	0.0054	0.0049	0.0200	0.0031	0.0023	0.0180	0.0063	0.0035	0.0024	0.0055	0.0046	0.0024	0.0057	0.0049	0.0210	0.0048	0.0052	0.0110	0.0056	0.0053	0.0054
for Wethe	<sup>206</sup> pb/ <sup>238</sup>	0.0987	0.1656	0.2274	0.1005	0.1010	0.1009	0.1010	0.0954	0.0997	0.3244	0.1056	0.0453	0.0973	0.1686	0.1036	0.1703	0.1078	0.1004	0.1092	0.0695	0.1030	0.0662	0.1047	0.1012	0.1033	0.0969	0.2140	0.5140	0.1053	0.0955	0.1849	0.0936	0.1027	0.1034	0.1003	0.1048	0.0967	0.1021	0.0666	0.1005	0.0984	0.1107	0.0996	0.0936	0.1010	0.1057	0.0973	0.0975	0.1078	0.0985	0.4038	0.0471	0.0457	0.3707	0.1119	0.0710	0.0473	0.0986	0.0926	0.0469	0.1141	2080.0	0.4150	0.0938	0.1010	0.2235	0.1083	0.1028	0.1083
Data	2SE	0.0240	0.0310	0.0490	0.0180	0.0180	0.0380	0.0330	0.0220	0.0220	0.0770	0.0200	0.0074	0.0250	0.0390	0.0280	0.0290	0.0280	0.0310	0.0200	0.0180	0.0200	0.0160	0.0190	0.0160	0.0280	0.0300	0.1000	0.1500	0.0190	0.0310	0.0370	0.0190	0.0180	0.0580	0.0300	0.0270	0.0190	0.0140	0.0160		0.0200	0.0460	0.0310	0.0200	0.6300	0.0520	0.0460	0.0460	0.0550	0.0470	0.4200	0.0240	0.0190	0.3600	0.0780	0.0300	0.0220	0.0620	0.0460	0.0220	0.0580	0.0460	0.4200	0.0450	0.0560	0.1400	0.0580	0.0510	0.0540
	<sup>207</sup> pb/ <sup>235</sup> L	0.7660	0.8840	2.5490	0.8160	0.8470	0.8240	0.8550	0.7960	0.8000	4.7270	0.9330	0.3332	0.7930	0.7010	0.8530	1.7400	0.9370	0.8210	0.9140	0.5130	0.8490	0.5480	0.8840	0.8460	0.8190	0.8190	0.8800	3.1000	0.8650	0.8050	1.8940	0.8240	0.8750	0.8620	0.0000	0.8850	0.7960	0.8460	0.4950	0.8250	0.8410	0.9310	0.8210	0.7840	0.8610	0.8780	0.7920	0.8130	0.9510	0.8210	7.5800	0.3410	0.3242	6.5800	0.9450	0.5410	0.3610	0.8440	0.7570	0.3760	1.0060	0.8760	7.4900	0.7880	0.8410	2.3950	0.8920	0.8230	0.9100
lot	2SE	0.0021	0.0023	0.0020	0.0017	0.0015	0.0030	0.0026	0.0019	0.0019	0.0021	0.0016	0.0015	0.0023	0.0022	0.0024	0.0017	0.0023	0.0027	0.0015	0.0021	0.0016	0.0021	0.0017	0.0015	0.0024	0.0024	0.0031	0.0044	0.0017	0.0025	0.0019	0.0019	0.0016	0.0047	0.0026	0.0022	0.0017	0.0013	0.0019	0.0018	0.0016	0.0030	0.0024	0.0022	0.0036	0.0018	0.0016	0.0015	0.0016	0.0016	0.0027	0.0022	0.0016	0.0024	0.0039	0.0012	0.0020	0.0036	0.0019	0.0016	0.0018	0.0013	0.0031	0.0015	0.0028	0.0019	0.0027	0.0021	0.0020
isserburg i	<sup>7</sup> Pb/ <sup>206</sup> Pb	0.0578	0.0588	0.0815	0.0586	0.0611	0.0589	0.0605	0.0591	0.0576	0.1047	0.0590	0.0531	0.0598	0.0542	0.0606	0.0734	0.0635	0.0598	0.0606	0.0539	0.0600	0.0592	0.0619	0.0599	0.0589	0.0615	0.1100	0.2015	0.0595	0.0599	0.0734	0.0636	0.0619	0.0624	0.0683	0.0609	0.0594	0.0599	0.0536	0.0580	0.0614	0.0607	0.0585	0.0614	0.1686	0.0598	0.0590	0.0607	0.0635	0.0609	0.1345	0.0523	0.0525	0.1295	0.0611	0.0550	0.0549	0.0635	0.0591	0.0576	0.0641	0.0508	0.1323	0.0615	0.0623	0.0777	0.0600	0.0588	0.0620
or Tera-Wa	2SE 20	0.3798	0.3503	0.1489	0.3366	0.3431	0.3929	0.3627	0.3736	0.3521	0.1045	0.3166	0.7787	0.3591	0.2146	0.3727	0.2000	0.3270	0.3869	0.3187	0.5176	0.3299	0.53/5	0.3284	0.3613	0.3749	0.3941	0.1524/	0.0670	0.3337	0.4167	0.1901	0.3995	0.3318	0.4396	0.4374	0.3460	0.3529	0.3358	0.5185	0.3465	0.3511	0.3754	0.3730	0.3995	0.4901	0.4744	0.5070	0.5155	0.4647	0.5050	0.1227	1.3974	1.1008	0.1310	0.5031	0.6943	1.0727	0.5657	0.6657	1.0911	0.4378	0.4040	0.1219	0.5456	0.5098	0.2202	0.4775	0.5015	0.4604
Datafu	1/ <sup>206</sup> Pb	0.1317	9.1324	4.3975	9.9502	9.9010	9.9108 3.6208	9.9010	0.2987	0.0301	3.0826	9.2507	2.0605	0.2775	5.9312 0.6270	9.6525	5.8720	9.2764	9.9602	9.1575	4.3885	9.7087	4.0028	9.5511	9.8814	9.6805	0.3199	3 1847	3. 1047 1 0475	9 4967	0.4712	5.4083	0.6838	9.7371	9.6/12	2.002	9.5420	0.3413	9.7943	5.0150	3 05/12	0.1626	9.0334	0.0402	0.6838	2.0284	9.4607	0.2775	10.2564	9.2764	0.1523	2.4765	1.2314	21.8771	2.6976	3.9366	4.0845	21.1417	0.1420	7991	1.3220	8.7642	0.0603	2.4096	0.6610	9.9010	4.4743	9.2336	9.7276	9.2336
1	Th/U 23	1.02	1.01	0.75	0.55	0.47	0.55	0.64	1.12	0.66	0.33	0.79	0.34	0.36	0.40	0.68	0.15	0.45	0.40	0.40	0.61	1.18	0.29	0.08	0.29	0.59	0.89	0.10	0.10	0.44	0.39	0.57	0.40	0.71	0.38	0.28	0.30	0.70	0.78	0.42	0.46	0.65	0.36	0.48	0.84	0.59	0.74	0.27	0.45	0.88	0.62	0.35	0.68	0.49 2	0.36	0.53	0.09	0.56 2	0.55	0.56	0.69 2	0.93	1.30	0.37	0.53	0.53	0.37	0.42	0.77	0.69
	ldentifier	G88_4195_1	G88 4195 2 G88 4195 3	G88 4195 4	G88 4195 5 G88 4195 6	G88 4195 7	G88 4195 8 G88 4105 0	G88 4195 10	G88 4195 11 G88 4195 12	G88 4195 13	G88_4195_14	G88 4195 15 G88 4195 16	G88 4195 17	G88 4195 18	G88 4195 19 G88 4105 20	G88 4195 21 G88 4195 21	G88 4195 22	G88 4195 23	G88 4195 25 G88 4195 25	G88 4195 26	G88 4195 27	G88 4195 28	G88 4195 29	G88 4195 31	G88_4195_32	G88_4195_33	G88_4195_34	CB8 4195 35	C00 4130 30	G88 4195 38	G88 4195 39	G88 4195 40	G88_4195_41	G88_4195_42	G88 4195 43 Cee 4105 44	GR8 4105 45	G88 4195 46	G88_4195_47	G88 4195 48	G88 4195 49	C88 4195 50	G88 4195 52	G88 4195 53	G88_4195_54	G88 4195 55	G88 4195 57 G88 4195 57	G88_4195_58	G88_4195_59	G88 4195 60	G88 4195 62	G88 4195 63	G88 4195 64 Can 4105 65	G88 4195 66	G88_4195_67	G88_4195_68	G88 4195 70 G88 4195 70	G88_4195_71	G88_4195_72	Con 4105 73	G88 4195 /4 G88 4195 75	G88_4195_76	G88 4195 77	C88 4195 /8	G88 4195 80	G88 4195 81	Cos 4195 82	G88 4195 84	G88 4195 85	G88_4195_86	G88_4195_87

## South Tempest G-88 (4195.8 m) Sample

# U/Pb data for Reference Standards

#### <u>91500 zircon</u>

%Con cord an cv (206P b-238U	age/207Pb-235U age)*100	100.95	100.86	90'66	100.75	99.45	99.53 99.53	100.95	100.57	100.09	100.00	102.65 a8 a7	102.10	102.10	100.38	103.36	99.71	100.10	102.58	99.25	102.37	100.38	100.09	97.94	101.101	103.14	100.68	76-101	100.47	98.77	90.66	100.57	102.05	97.28	98.69	100.00	100.38	100.19	100.37	98.68 100.47	99.91	101.61	97.57 100 57	99.91	99.34	100.38	100.75	101.24	101.34	99.44	98.42 og oc	99.25	100.28	100.28	100.96	100.00	98.70	100.00	99.81	101.79	100.65	98.79	100.75	99.25	101.80	100.48	98.23	101.04	98.59	100.28	101.92	99.81 100.86
% Concord an cv/ 206Pb-238U	age/207Pb-206Pb age) *100	100.63	105.20	55.34 101.01	101.94 99.28	100.20	96.75 94.05	100.73	95'96	103.25 99.09	95.16	109.32 e4 14	102.04	101.32	91/16	105.74	98.57 52	25 25 25 25 25 25	101.02	101.32	104.25	8,8,8	12.38	16:16	38.44 100.51	111.33	38.76	20.001	98.22	38.01	21.12	100.27	104.81	91.32	02'36	100.02	50'H0T	72.66	100.67	96.42 101 66	101.47	106.80	95.75 100.78	101.30	96.34 	97.24 94.75	100.83	102.43	107.51 109.57	88	98.42 11	100.09	103.32 100.67	101.61	103.53	100.58	92:08	100.65	100.19	107.58	105.48	103.11	107.90	100.09	112.47 105.66	100.76	16:31 	107.78 99.43	94.43	104.83	106.97	02.66
	ZSE	63	60	62	61	63	69	65	88	66 66	62	63	68	67	69	67	62	99	63	65	65	96	71	74	80	99	70	88 97	89	67	51	S :	202	49	52	51	51	50	53	10	52	54	23	54	52	52 52	51	54	75	70	22 EZ	74	75	72	73	78	79	75	82	82	62	80	62	78	818	11	82	6Z	82	78	79	97 29
	<sup>d3</sup> Pb/ <sup>2 II</sup> Th	1054	1046	1051	1081	1074	1057	1090	1017	1040	1025	975	1064	1042	1083	1100	1017	1047	1040	1063	1055	1048	1080	1080	007	1087	1061	1001	1048	1087	1051	1081	1061	1032	1080	1026	1057	1070	1059	5601	1048	1098	1039	1039	1058	10/1	1063	1046	1074	994	1059	1044	1104	1034	1085	1080	1040	1082	1114	1068	1095	1080	1016	1042	1044	1052	1061	1048	1063	1067	1085	1071 1097
	2SE 2	23	22	24	24 26	22	24	22	52	23	24	23	25	24	25	27	23	26	25	24	24	25	25	27	25	22	27	17	26	27	17	8	1/	16	18	19	18	18	19	17	16	17	19	18	18	18	17	19	53 53	22	22	24	23	24	23	24	25	26	25	25	24	26	27	25	26	25	27	25	26	26	26	25 25
	N <sub>stz</sub> /qd	1049	1043	1059	1062	1082	1057	1050	1059	1065	1057	1056	1049	1047	1053	1043	1043	1037	1047	1066	1055	1045	1059	1069	1054	1052	1035	1072	1055	1055	1069	1060	1057	1067	1067	1058	1064	1064	1069	1063	1055	1054	1072	1067	1062	1059	1064	1051	1045	1064	1079	1068	1056	1072	1045	1041	1078	1081	1073	1059	1070	1073	1071	1063	1054	1052	1073	1056	1067	1060	1039	1054 1045
Dates	2SE 20	28	2	ୟ ୫	ୟ ଜ	8 8	ୟ ନ	8	1 8	8 16	5 22	88	8	31	818	31	8	88	8	32	8	77 77	31	31	\$ F	8	31	8 6	8	31	25	2	4 x	2	25	<b>7</b> 8	7 92	25	26	Q X	92	25	K1 K1	27	26	72	8	26	R1 R3	54	8 8	រង	24	25	24	26	27	22 ×	25	8	n K	27	9 12	25	92 72	52	12	8 %	26	22	a ki	23
	D <sub>862</sub> /qd <sub>5</sub>	1059	1052	1049	1070	1076	1062	1060	1065	1064	1057	1064	1071	1069 107E	1057	1078	1040	1038	1074	1058	1080	1086	1060	1047	1065	1085	1042	1076	1060	1042	1059	1066	1071	1038	1053	1058	1068	1066	1073	1067	1054	1071	1046	1066	1055	10/0	1072	1064	1059	1058	1062	1060	1059	1075	1055	1041	1064	1081	1071	1078	1077	1060	1079	1055	1054	1057	1054	1067	1052	1063	1059	1052 1054
	2SE 20	76	76	74	73	72	71	73	81	71	81	76	79	78	85	86	76	62	78	76	77	28	80	82	5	8	84	8 5	83	81	99	۳ i	71	69	71	6 F	69	70	67	10	99	70	69	70	71	71 76	2 2	74	5 5	53	2 23	59	58	58	57	63	62	62	61	65	65	71	5 12	64	22	68	68	69	64	70	77	88
	b/ <sup>205</sup> Pb	1052	1000	1100	1060	1074	1119	1052	1103	1081	1111	992	1050	1055	1084	1019	1055	1052	1063	1044	1036	1090	1074	1139	1050	975	1055	1066	1079	1063	1090	1063	1044	1137	1100	1058	1074	1069	1066	1050	1089	1003	1092	1052	1095	1100	1063	1089	382 383	1070	1079	1059	1052	1058	1019	1085	1119	1074	1069	1002	1021	1028	1000	1054	954	1049	1099	1057	1114	1014	666	1079
	SS SS	0033	0031	0032	0032 M34	0033	038	0036	0031	0035 0035	0032	0033 M37	0036	0035	0037	0037	0032	0034 M49	033	0034	0034	1400	0038	0041	0036 0037	0035	8600	100	0035	0035	0027	0028	0028 0028	0026	0027	0027	0027	0027	0028	500.	0027	0028	0028 7027	0028	0027	0029	0027	0028	0037	0036	0038 0038	80038	0039	0038	80038	0041	0041	0039	0043	0043	0042	0042	0041	0041	0041 0042	004	0043	0041	0043	0041	0042	0041 0042
	ff all	538 0.	0.0229	0. 533 0.	0.00 0.00 0.00	0.0	054 0.	0. 0.	0.0	544 0.	522 0.	0 0.01	0.0	0.228 0.	0.000	057 0.	0.01	0.0 0.0 0.0	533 0.	0.0	0.0	0.0 0583	0.0	0.0	0 700	053 0.	0.545 0.	0 700	533 0.	0.554 0.	0.534 0.	0.0	0.000 0.000 0.000 0.0000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000	525 0.	1552 0.	0.0	536 0.	0.542 0.	054 0.	0 0 0	0.0	1561 0.	053 0.	0.053	0.538 0.	0.0545 0.0536 0.0536 0.0536 0.0536 0.0536 0.0536 0.0536 0.0536 0.0536 0.0536 0.0536 0.0536 0.0536 0.0536 0.053	0.0	0.534 0.	0.0541 0.000	1505 0.	0.0 1545 0.0	531 0.	1552 0.	0.0226	0.0 0.0	0.0	0.529	0526 0.	0.0	0. 254.4 0.	555 0.	065 0.	0.0 0518 0.	053 0.	533 0. 537 0.	537 0	054 0.	0.0541 0.0	0.0	0.0	0.0554 0.	056 0.
1	10 200 PF	031 0.0	531 0.0	273 0.0	169 0.0 529 0.0	376 0.0	00 00 201 00	254 0.0	592 0.0	837 0.0	815 0.0	516 0.0	330 0.0	139 0.0	784 0.0	325 0.	917 0.0	450 0.0	575 0.0	395 0.0	761 0.0	134 00	301 0.0	297 0.0	881 O.C	0.0	887 0.0	-0 - 0	607 0.0	054 0.0	267 0.0	667 0.0	20 26	892 0.0	743 0.0	689	774 0.0	972 0.0	522 0.	260 01	873 0.0	243 0.0	962 0.	119 0.	244 0.0	442 0.0	032 0.0	251 0.0	769 0.0	582 0.0	951 0.0	00 660	368 0.0	965 0.0	241 0.0	376 0.0	138 0.0	20 00	028 0.0	334 0.0	906 00	633 0.	720 0.0	313 0.	362 0.0	719 0.0	465 0.	255 0.0	105 0.0	701 0.0	142 0.0	418 0.0 566 0.
	SE RI	052 0.3	0.2 0.2	053 0.2	054 0.3	055 0.3	054 0.3	055 0.2	03	055 0.2	057 0.2	056 0.2	0.3	056 0.3	026 0.2	058 0.1	054 0.3	0.2	0.3	059 0.3	059 0.2	056 0.4	057 0.3	057 0.3	05.4 0.3	0.4	057 0.3	0.0	059 0.2	057 0.4	046 0.3	049 0.2	047 0.2	046 0.2	047 0.2	048 0.3	047 0.3	046 0.1	048 0.3	016 0.3	046 0.3	046 0.3	045 0.2	049 0.3	048 0.2	049 0.2	047 0.2	049 0.3	045 0.1	043 0.2	043 0.2	047 0.3	043 0.2	045 0.2	045 0.3	047 0.2	050 0.3	047 0.3	046 0.3	047 0.3	045 0.2	048 0.2	049 0.2	045 0.2	049 0.2	046 0.1	049 0.3	048 0.3	048 0.3	045 0.2	046 0.3	043 0.2
the rill plo	Z 082/	786 0.0	774 0.0	772 0.0	809 0.0 816 0.0	822 0.0	771 0.0	790 0.0	200 000	799 0.0	779 0.0	838 0.0	811 0.0	807 0.0	786 0.0	822 0.0	751 0.0	751 0.0	816 0.0	785 0.0	830 0.0	744 0.0	788 0.0	762 0.0	00 823	832 0.0	748 0.0	010 010 010	792 0.0	761 0.0	786 0.0	801 0.0	830 0.0	747 0.0	777 0.0	787 0.0	807 0.0	795 0.0	810 0.0		768 0.0	810 0.0	754 0.0	804 0.0	783 0.0	805 0.0	812 0.0	798 0.0	819 0.0	788 0.0	791 0.0	790 0.0	784 0.0	814 0.0	780 0.0	758 0.0	799 0.0	831 0.0	810 0.0	818 0.0	819 0.0	789 0.0	819 0.0	781 0.0	814 0.0 798 0.0	782 0.0	782 0.0	768 0.0	776 0.0	796 0.0	785 0.0	774 0.0
ataforWe	SE <sup>206</sup> Pb	540 0.1	630 0.1	650 0.1	660 0.11 680 0.11	640 0.12	570 0.1	660 0.1	700 0.1	240 0.1	570 0.1	210 0.12	700 0.12	570 0.12 TEO 0.12	730 0.1	730 0.12	660 0.1	570 0.1. 520 0.1	700 0.11	690 0.1	890 0.12	730 0.1	740 0.1	760 0.1	10 012	700 0.11	740 0.1	1.0 01/	710 0.1	760 0.1	490 0.1	490 0.12	510 0.12 510 0.13	460 0.1	520 0.1	510 0.1	520 0.12	500 0.1	530 0.12	210 0.1 400 0.1	460 0.1	490 0.11	530 0.1	500 0.11	500 0.1	520 0.12	480 0.11	520 0.1	570 0.1 540 0.1	520 0.1	540 0.1	680 0.1	540 0.1 540 0.1	690 0.12	710 0.1	660 0.1	710 0.1	740 0.12 580 0.12	690 0.11	720 0.12	690 0.12	750 0.1	760 0.12	710 0.1	710 0.1	10 0.1 0.1	760 0.1	720 0.1	750 0.1	720 0.1	720 0.1	710 0.1 690 0.1
ľ	/ <sup>25</sup> U 25	230 0.0	350 0.0	0.0 000	740 0.0	920 0.0	0.0 001	110 0.0	220 0.0	130 0.0	320 0.0	130 0.0	380 0.0	260 0.0	0.0	230 0.0	110 0.0	0.0 0.0	0.0	700 0.0	160 0.0	40 00	710 0.0	780 0.0	130 0.0	310 0.0	380 0.0	550 0.0	180 0.0	0.0	720 0.0	350 0.0	0.0 0.24	580 0.0	770 0.0	280 0.0	0.0	550 0.0	700 0.0	10 0.0	0.0	200 0.0	550 0.0	510 0.0	520 0.0	530 0.0	000	220 0.0	360 0.0 130 0.0	0.0	360	310 0.0	0.0	530 0.0	0.0	960 0.0	0.0 086	0.0	910 0.0	0.0	0.0	190 0.0	0.0	150 0.0	280 0.0	120 0.0	300 0.0	0.0 0.0	740 0.0	160 0.0	000	170 0.0 L40 0.0
╞	5E <sup>207</sup> Pb	028 1.8	027 1.7	028 1.8	027 1.8	027 1.8	027 1.8	027 1.8	031 1.8	026 1.8	031 1.8	027 1.8	029 1.8	029 1.8	032 1.8	031 1.8	028 1.8	7.1 020	029 1.8	028 1.8	028 1.8	0.24 L.8	030 1.8	032 1.8	1 1 8 1 8 1 8	028 1.8	031 1.7	1 100	031 1.8	030 1.8	025 1.8	027 1.8	02/ 1.8	027 1.8	027 1.8	026 1.8	026 1.8	026 1.8	025 1.8	27 T 27	024 1.8	025 1.8	026 1.8	026 1.8	027 1.8	027 1.8	026 1.8	027 1.8	024 18	022 1.8	022 1.8	024 1.8	023 1.8	024 1.8	023 1.8	026 1.7	026 1.8	025 1.9	025 1.8	026 1.8	026 1.8	028 1.8	028 1.8	026 1.8	028 1.8	027 1.8	027 1.8	026 1.8	027 1.8	028 1.8	026 1.8	031 1.8
ourg plot	<sup>36</sup> Pb 25	44 0.0	25 0.0	62 0.0	43 0.0	52 0.0	69 0.0	44 0.0	60 60	36 0.0	66 0.0	22 0.0	43 0.0	45 0.0	56 0.0	32 0.0	45 0.0	44 0.0	48 0.0	41 0.0	38 0.0	71 0.0	52 0.0	77 0.0	43 00	16 0.0	45 0.0	0.0 40	54 0.0	48 0.0	58 0.0	48	41 0.0	76 0.0	62 0.0	46 0.0	52 0.0	50 0.0	49 0.0	49 0.0	39 0.0	26 0.0	76 0.0	44 0.0	60 0.0	62 0.0	48 0.0	39 0.0	47 28 0.0	61 0.0	51 0.0 48 0.0	57 0.0	42 0.0	49 0.0	37 0.0	46 0.0	76 0.0	36 0.0	58 0.0	41 0.0	45 0.0	57 0.0	4/ 0.0	49 0.0	28 0.0	48 0.0	62 0.0	34 0.0	65 0.0	00 00	38 0.0	47 0.0 54 0.0
a-Wassert	207Pb/	0.07	2 0.07	8 0.07	0.07 8	7 0.07	4 0.07	7 0.07	9 0.0	9 0.07 8 0.07	1 0.07	8 0.07	0.07	5 0.07	6 0.07	7 0.07	1 0.07	0.07	9 0.07	2 0.07	2 0.07	1 0.07	3 0.07	6 0.07	8 0.0/	8 0.07	5 0.07	0.0	0.07	8 0.07	2 0.07	1 0.07	1 0.0/	0.07	8 0.07	8 0.07	0.0	8 0.07	5 0.07	20 0 0	2 0.07	4 0.07	0.07	6 0.07	0.07	9 0.07	1 0.07	6 0.07	0.07	5 0.07	1 0.07	7 0.07	1 0.07	8 0.07	0.07	1 0.07	5 0.07	0.07	4 0.07	2 0.07	0.07	0.07	0.0	9 0.07	9 0.07	9 0.07	3 0.07	0.07	2 0.07	6 0.07	4 0.07	6 0.07 7 0.07
ata for Ter	Pb 2SE	0.163	0.165	3 0.168	9 0.165 6 0.166	5 0.165	5 0.175	0.171	6 0.169	6 0.169 8 0.176	1 0.180	7 0.165 6 0.174	8 0.170	0 0.171	0.175	5 0.174	0 0.176	0.176	6 0.175	2 0.185	0.176	0.184	8 0.178	4 0.183	20120	5 0.175	8 0.186	//1.0 7	4 0.183	6 0.183	1 0.144	5 0.151	0.143	1 0.150	5 0.148	0.150	0.143	0.142	9 0.146	7 0.146	1 0.147	9 0.140	5 0.146	2 0.150	5 0.151	2 0.150	8 0.143	7 0.151	5 0.136 5 0.136	8 0.134	0.134	6 0.146	7 0.143	7 0.136	0.142	3 0.152	6 0.154	5 0.140	9 0.140	6 0.142 0.142	5 0.136	7 0.150	0.148	8 0.141	7 0.146	7 0.144	7 0.154	0.148	6 0.152	0.139	2 0.148	0 0.136 8 0.135
Ľ	238U/20	5.599	5.637	5.643	5.527	5.488	5.561	5.586	5.558	5.558	5.621	5.440	5.521	5.534	5,599	5.488	5.711	5.711	5.506	5.602	5.464	5.733	5.592	5.675	108-5	5.458	5.720	5.485 C 51 C	5.580	5.678	5.599	5.552	5.454	5.724	5.627	5.596	5.534	5.571	5.524	5.649	5.656	5.524	5.701	5.543	5.608	5.540	5.518	5.561	5.592	5.592	5.583	5.586	5.605	5.512	5.618	5.688	5.558	5.461 5.646	5.524	5.500	5.497	5.589	5.497	5.614	5.512	5.611	5.611	5.558	5.630	5.567	5.602	5.637
ŀ	⊇/#	1 0.26	3 0.26	4 0.26	5 0.25 6 0.26	7 0.26	8 0.25 9 0.26	1 0.26	2 0.26	4 0.25	5 0.26	7 0.26	8 0.25	0.26	1 0.26	2 0.26	0.26	5 0.26	6 0.26	1 0.26	8 0.25	0.26	1 0.26	12 0.25	12.0 12.0	5 0.25	16 0.26	070 0	9 0.26	0.26	1 0.25	2 0.25	4 0.25	5 0.25	6 0.25	7 0.25	9 0.25	0.25	1 0.25	270 27	4 0.25	5 0.25	7 0.26	8 0.26	9 0.25	1 0.25	2 0.25	3 0.25	2 0.25	3 0.26	5 0.27	6 0.26	7 0.25 R 0.26	9 0.27	1 0.26	12 0.26	13 0.26	14 0.27 5 0.27	16 0.25	0.26	9 0.27	20 0.27	2 0.27	23 0.26	24 0.26 15 0.26	0.26	27 0.26	39 0.26	0.26	31 0.26	33 0.26	1 0.26 ? 0.25
	Identifier	jn26 91500	jn26_91500_	jn26_91500	jn26 91500	jn26_91500_	jn26_91500 jn26_91500	jn26_91500_1	jn26_91500_1	jn26 91500 1 in26 91500 1	jn26_91500_1	jn26_91500_1 in26_91500_1	jn26 91500 1	jn26_91500_1	in26 91500 2	jn26_91500_2	jn26_91500_2	jn26_91500_2 in26_91500_2	jn26 91500 2	jn26_91500_2	jn26_91500_2	in26 91500 3	jn26_91500_3	jn26_91500_3	in26 91500 3	n26 91500 3	jn26_91500_3	1026 91500 2	in26 91500 3	jn26_91500_4	jn13_91500_	jn13_91500	in13 91500 2	jn13_91500	jn13_91500_	jn13_91500_	in13 91500 5	jn13 91500 1	jn13_91500_1	1 00519 5100 1	jn13 91500 1	Jn13_91500_1	in13_91500_1	jn13_91500_1	jn13_91500_1	in13 91500 2	jn13 91500 2	jn13_91500_2	oc14 91500 oc14 91500	oc14 91500	oc14 91500	oc14 91500	oc14 91500	oc14 91500	oc14 91500 ;	oc14 91500 1	oc14_91500_1	oc14 91500 ;	oc14 91500 1	oc14 91500 1	oc14 91500 1	oc14 91500 2	oc14 91500 2	oc14 91500 2	oc14 91500 2	oc14 91500 2	oc14 91500 2	oc14 91500 2	oc14 91500 3	oc14 91500 2	oc14 91500 5	oc6 91500

99.07	102.18	100.00	100.86	99.91	101.92	100.47	98.05	98.60	102.18 96.31	100.46	103.63	102.87	100.48	100.76	100.48	90:90 1001	100.66	98.79	101.05	99.62	100.85	98.24 103.08	101.05	98.52	101.04	98.68 100 E0	100.56	99.62	102.02	100.95	36.42	00 53	100.57	57.97	101.89	101.34	98.52	100.47	98.59	100.46	101.32	100.28	100.38	00.00	97.86	100.95	100.66	100.28	101.61	37.40	98.70	99.34	100.19	102.49	99.91	99.72	100.00	99.05	101.51	30,00	101.04	100.00	59.05	98,89	100.28	98.43 20.31	06:66	99.71	100.28	99.63 	100.19	100.37	100.00	99.05	100.67	97.82	99.26 00.71	101.12	101.40	99.81
96.65	105.98	99.86 96 93	105.50	95.74	105.03	100.05	93.66	98.92	106.12 88.73	100.42	107.20	102.95	97.54	104.15	98.09	90.30	104.02	98.97	103.51	102.32	105.54	90.03 1/08 AE	104.12	96.55	104.00	96.05 103 35	104.08	102.03	106.21	104.02	30.37	10.5UL	105.54	96,63	108.45	104.12	96.55	104.00 or or	90.0b 103.35	104.03	105.93	102.18	97.91	90.00 07.65	92.80	102.53	100.78	100.23	104.78	101.59	96.75	95.74	104.84	106.21	96.59	98.24	ar:407	97.37	104.51	104.05	104.40	100.63	96.12 99.05	96.73	98.71	98.44 27.05	97.90	100.00	100.37	101.08	106.23	0.011	103.94	97.93	100.97	97.54	94,69 101 17	101.50	102.46	101.80
77	83	8	78	81	81	77	81	83	86	82	84	82	68	5	88	83	95	55	53	52	55	2/	58	58	57	5 3	55	51	56	22 r	នេះ	2 2	55	57	2	56	28	2	¥ 3	55	49	43	42	\$	47	48	47	48	<del>8</del>	÷	53	45	46	50	52	56	8	53	2, 2	22	5	R	22 53	59	59	38	1/	68	74	73	2 #	C F	73	69	70	69	8 6	79	£ 1	75
1069	1077	1046	991	1054	1036	1031	1031	1027	1083	1112	1066	1033	1135	1000	1111	1055	1095	1056	1053	1091	1031	1043	1052	1031	1036	10/0	1077	1057	1094	1095	OCOT	1001	1031	1043	1054	1052	1034	1036	10/0	1077	1123	992	1063	1050	1039	1060	1071	1071	1063	1086	1044	1028	1054	1080	1049	1076	1039	1055	1059	1058	1026	1014	1124	1034	1080	1078	1034	1017	1121	1047	1088	1041	1033	1022	1047	1026	1012	1101	1096	1075
25	26	26	28	28	29	28	50	30	30	31	29	28	28	ю.	72	50	26	25	26	25	25	Q 2	26	26	26	2	25	26	28	27	/7	77	28	27	27	26	28	77	97	27	24	25	24	0 2	24	24	25	25	25	52	26	25	26	25	27	26	52	25	27	26	26	28	<sup>26</sup>	28	28	27	36	35	35	37	98	35	35	36	35	35	36	36	37	36
1076	1054	1048	1046	1062	1042	1064	1076	1072	1053	1076	1046	1045	1045	1048	1051	1043	1053	1070	1051	1061	1057	1056	1051	1079	1056	1062	1079	1060	1040	1050	#014	1052	1060	1082	1058	1048	1079	1062	1063	1080	1063	1064	1050	000T	1073	1055	1059	1076	1057 +07E	1049	1076	1063	1053	1045	1079	1058	1068	1053	1061	1035	1062	1059	1058	1084	1057	1082	1046	1043	1088	1084	1073	1073	1054	1052	1038	1053	1077	1070	1068	1076
24	26	<sup>26</sup>	25	27	27	28	26	27	28	29	28	28	27	27	28	20	25	25	25	25	25	2 ×	25	25	25	2 2	26	25	25	25	Q 2	C] ¥	25	25	25	25	25	2 2	4 x	26	22	20	21	77	20	21	21	21	22 %	7 77	22	22	22	22	23	21	3 23	22	33	33	24	23	22	24	24	24	8 g	38	39	40	69 Q	<del>9</del> 8	39	38	38	38	40 20	6 9	42	40
1066	1077	1046	1055	1061	1062	1069	1055	1057	1076	1081	1084	1075	1050	1056	1056	1045	1060	1057	1062	1057	1066	1070	1062	1063	1067	1048	1085	1056	1061	1050	/COT	1057	1066	1060	1078	1062	1063	106/	1048	1085	1077	1067	1054	acnt .	1050	1065	1066	1079	1074	1058	1062	1056	10/6	1071	1078	1055	1068	1043	1077	1055	1073	1059	1045	1072	1060	1065	1045	1040	1091	1080	1075	1077	1054	1042	1045	1030	1069	1082	1083	1074
86	91	88	92	91 or	97	91	f 8	91	92	66	95	8	91	97	88 8	8 8	59	53	57	57	62	8	58	59	55	5 5	3 3	61	63	55 5	8 5	20	69	3	59	56	59	s :	¥ 5	2	69	71	69	66 64	67	71	70	72	74	74	76	71	80	78	73	1	80	72	82	81	77	81	83	81	83	8 5	61 20	55	52	61	5 S	8 2	59	z	56	57	53	59	61	56
1103	1017	1070	1000	1108	1011	1069	1126	1069	1182	1077	1011	1044	1077	1014	1077	1052	1019	1068	1026	1033	1010	109/	1020	1101	1026	1091	1043	1035	666	1019	900T	1023	1010	1097	66	1020	1101	1026	1091	1043	1017	1044	1077	760T	1132	1039	1058	1077	1025	1041	1098	1103	1014	1008	1116	1074	1071	1071	1031	1014	1028	1052	1021	1108	1074	1082	1062	1040	1087	1069	1012	1047	1014	1064	1035	1056	1129	1066	1057	1055
0.004	0.0043	0.0042	0.0041	0.0042	0.0042	0.0041	0.0042	0.0043	0.0044	0.0044	0.0045	0.0043	0.0047	0.0041	0.0045	0.0043	0.008	0.0029	0.0028	0.0027	0.0029	500.0	0.0029	0.003	0.003	0.0028	0.0029	0.0027	0.0029	0.003	0.000	27000	0.0029	0,008	0.0029	0.0029	0.003	0.003	0.0028	0.0029	0.0026	0.0023	0.0022	62000	0.0024	0.0025	0.0025	0.0025	0.0024	0.0026	0.0028	0.0024	0.0024	0.0026	0.0027	0.0029	0.0025	0.0027	0.0028	0.008	0.0028	0.0028	0.0028	0.0031	0.0031	0.003	0.0037	0.0036	0.0039	0.0038	0.0038	0.0037	0.0038	0.0036	0.0037	0.0036	0.0038	0.0041	0.0042	0.0039
0.0542	0.055	0.0534	0.0504	0.0538	0.0525	0.0517	0.0526	0.0524	0.055	0.0563	0.0541	0.0528	0.0579	0.0508	0.0568	CHCU.U	0.0559	0.0535	0.0535	0.0556	0.0514	/750.0	0.0535	0.0524	0.0527	0.0543	0.055	0.0537	0.0556	0.0559	10000	0.0556	0.0514	0.0527	0.0536	0.0535	0.0524	0.0227	0.0543	0.055	0.0574	0.0505	0.0539	0.0541	0.0528	0.0538	0.0546	0.0546	0.0538	0.0553	0.0533	0.0524	0.0538	0.0551	0.0534	0.055	0.053	0.0537	0.0536	0.054	0.0524	0.0516	0.0534	0.0528	0.0551	0.0545	0.0523	0.0516	0.057	0.053	0.0553	0.0500	0.0525	0.0519	0.0534	0.0521	0.0515 ^ nE45	0.0562	0.056	0.055
0.0982	0.1979	0.3247	0.2610	0.3147	0.3468	0.3180	0.2644	0.3729	0.3530	0.2714	0.3125	0.2486	0.3351	0.3339	0.4319 0.3445	0.3563	0.1356	0.1925	0.1534	0.1267	0.0918	0.1083	0.2551	0.1381	0.2169	0.1080	0.1851	0.1027	0.2234	0.1365	1/27-0	0.1278	0.080.0	0.0595	0.0919	0.2341	0.1351	0.2183	0.1240	0.2076	0.2907	0.1891	0.1993	0197.0	0.1444	0.1400	0.1270	0.2167	0.0959	0.1768	0.0733	0.2123	0.2249	0.1589	0.2975	0.2679	0.1154	0.2508	0.1331	0.1942	0.2828	0.2171	0.2205	0.1464	0.0892	0.1756	0.3133	0.3138	0.2764	0.2878	0.3952	0.3007	0.2403	0.3401	0.2338	0.3648	0.3413	0.3439	0.4085	0.3739
0.0044	0.0049	0.004/	0.0046	0.0049	0.0050	0.0052	0.0048	0.0050	0.0050	0.0053	0.0051	0.0052	0.0050	0.0050	0.0051	1000.0	0.0046	0.0045	0.0045	0.0046	0.0046	0.0045	0.0046	0.0046	0.0045	0.0046	0.0047	0.0045	0.0045	0.0046	CHOD-D	0.0016	0.0046	0.0046	0.0047	0.0046	0.0046	0.0045	0.0046	0.0047	0.0041	0.0037	0.0039	00000	0.0037	0.0038	0.0039	0.0089	0.0040	0.0040	0.0041	0.0041	0.0040	0.0040	0.0042	0.0039	0.0041	0.0040	0.0042	0.0042	0.0043	0.0042	0.0045	0.0044	0.0043	0.0043	0.0071	0.0069	0.0072	0.0074	0.0072	0.0073	0.0071	0.0070	0.0071	0.0070	0.0074	0.0073	0.0077	0.0073
0.1795	0.1822	0.1263	0.1781	0.1790	0.1793	0.1809	0.1777	0.1781	0.1818	0.1828	0.1831	0.1819	0.1759	0.1785	0.1781	0.1764	0.1790	0.1783	0.1791	0.1784	0.1801	0.107	0.1793	0.1796	0.1801	0.1764	0.1833	0.1782	0.1788	0.1790	C0/T-0	16/10	0.1801	0.1789	0.1821	0.1793	0.1796	1081.0	0.1764	0.1833	0.1817	0.1801	0.1777	8//T-0	0.1771	0.1796	0.1798	0.1825	0.1813	0.1779	0.1794	0.1777	0.1518	0.1806	0.1822	0.1780	0.1805	0.1759	0.1816	0.1781	0.1815	0.1786	0.1789	0.1807	0.1784	0.1794	0.1758	0.1754	0.1844	0.1828	0.1816	0.1820	0.1779	0.1756	0.1763	0.1735	0.1802	0.1821	0.1831	0.1818
0.0700	0.0730	0.0790	0.0750	0.0810	0.0800	0.0780	0.0810	0.0840	0.0780	0.0880	0.0810	0.080.0	0.0800	0.0850	0.0770	0.0800	0.0710	0.0700	0.0700	0.0710	0.0720	06/0.0	0.0720	0.0730	0.0710	0.0690	0.0710	0.0730	0.0770	0.0760	00100	00200	0.0800	0.0790	0.0780	0.0730	0.0780	05/00	0.0750 0	0.0770	0.0680	0.0720	0.0670	0.0050	0.0670	0.0680	0.0690	0.0720	0.0690	0.0710	0.0740	0.0700	05/00	0.0720	0.0750	0.0740	0.0760	0.0710	0.0770	0670.0	0.0740	0.0770	06/0.0	0.0790	0.0780	0.0780	0660.0	0.0970	0.1000	0.1100	0660.0	0.1000	0660.0	0660.0	0960.0	0860.0	0.1000	0.1000	0.1100	0.1000
1.9020	1.8160	1.8950	1.7970	1.8600	18220	1 9650	1.8910	1.8990	1.8360	1.9030	1 8740	1.8200	1.8210	1.8250	1.8360	1.7960	1.8220	1.8630	1.8300	1.8500	1.8450	1 9/30	1.8190	1.8820	1.8540	1.8620	1.9080	1.8400	1.8130	1.8240	T.0/00	1 8570	1.8390	19000	1.8370	1.8190	1.8990	1.8440	1 8150	1.9010	1.8510	1.8550	1.8210	1 80E0	18790	1.8470	1.8410	1.8990	1.8510	1.8180	1.8870	1.8660	1.8790	1.8070	1.9100	1.8510	1.8660	1.8380	1.8440	1.7780	1.8280	1.8260	1.8350	1.9200	1.8370	1.8990	1.8010	1.7940	1.9280	1.9060	1.8590	1 8920	1.8300	1.8400	1.7920	1.8140	1.9020	1.8790	1.8910	1.8910
0.0033	0.0033	0.0034	0.0033	0.0035	0.0035	0.0034	0.0035	0.0034	0.0033	0.0037	0.0034	9600.0	0.0034	0.0035	0.0033	0.0035	050000	0.0029	0:0030	0:0030	0.0031	0:000	0.0029	0.0031	0:0030	1500.0	00000	0.0031	0.0031	0:0030	670000	05000	0.0031	0.0032	0.0030	0.0029	0.0031	0500.0	0.0030	0:0030	0.0025	0.0026	0.0026	97000	0.0026	0.0026	0.0026	0.0027	0.0027	0.0027	0.0029	0.0027	0.0030	0.0028	0.0028	0.0029	020000	0.0027	0.0030	0.0029	0.0028	0:0030	0.0031	0.0031	0.0031	0600.0	0.0026	0.0024	0.0024	0.0026	0.0023	3200.0	0.0025	0.0024	0.0024	0.0025	0.0026	0.0025	0.0026	0.0024
0.0763	0.0731	0.0754	0.0725	0.0745	0.0729	0.0750	0.0772	0.0750	0.0730	0.0753	0.0729	0.0741	0.0753	0.0730	0.0753	10.0744	0.0741	0.0755	0.0743	0.0749	0.0741	0.0730	0.0735	0.0768	0.0753	0.0742	0.0748	0.0746	0.0737	0.0741	00/00	0.07/45	0.0741	0.0773	0.0730	0.0735	0.0768	0.0758	27/0.0	0.0748	0.0731	0.0741	0.0753	0.0755	0.0774	0.0739	0.0746	0.0753	0.0734	0.0740	0.0761	0.0763	05/0.0	0.0728	0.0768	0.0752	0.0751	0.0751	0.0736	0.0730	0.0735	0.0744	0.0751	0.0765	0.0752	0.0755	05/0.0	0.0736	0.0760	0.0756	0.0738	0.0753	0.0739	0.0758	0.0745	0.0760	0.0768	0.0750	0.0754	0.0754
0.1366	0.1476	0.1399	0.1450	0.1529	0.1555	0.1589	0.1520	0.1576	0.1513	0.1586	0.1521	0.1572	0.1616	0.1569	0.1608	0.1575	0.1436	0.1416	0.1408	0.1445	0.1418	0.145/	0.1431	0.1426	0.1387	0.1475	0.1399	0.1417	0.1408	0.1436	014TO	0.1445	0.1418	0.1437	0.1417	0.1431	0.1426	0.138/	0.14/5	0.1399	0.1242	0.1141	0.1235	10 1255	0.1180	0.1178	0.1206	0.1171	0.1217	0.1264	0.1274	0.1298	0.1247	0.1226	0.1265	0.1231	0.1258	0.1293	0.1274	0.1324	0.1305	0.1317	0.1406	0.1348	0.1351	0.1336	0.2297	0.2243	0.2117	0.2215	0.2183	5720 U	0.2243	0.2270	0.2284	0.2325	0.2274	0.2201	0.2297	0.2209
5.5710	5.4885	5.4555	5.6148	5.5866	5.5772	5.5279	5.6275	5.6148	5.5006	5.4705	5.4615	5.4975	5.6850	5.6022	5.6148 c c AAA	5.6689	5.5866	5.6085	5.5835	5.6054	5.5525	1992.5	5.5772	5.5679	5.5525	5.6625	5.4555	5.6117	5.5928	5.5866 r conr	2.0002	2.2835	5,55,5	5.5897	5.4915	5.5772	5.5679	5.5525	5.6680	5.4555	5.5086	5.5525	5.6275	2:0243	5.6465	5.5679	5.5617	5.4795	5.5157	5.6211	5.5741	5.6275	5.5835	5.5371	5.4885	5.6180	5.5402	5.6850	5.5066	5.6148	5.5096	5.5991	5.5897	5.5340	5.6054	5.5741 r cm2	5.6883	5.7013	5.4230	5.4705	5.5066 c.4765	5.4005	5.6211	5.6948	5.6722	5.7637	5.5494 c 7308	5.4915	5.4615	5.5006
0.26	0.27	87.0 X	0.25	0.26	0.26	0.26	0.26	0.27	0.26	0.26	0.25	0.26	0.25	0.25	0.26	0.75	0.26	0.26	0.26	0.26	0.26	Q. 70	0.26	0.26	0.26	2.0	0.26	0.25	0.26	0.26	9.0	97.0	0.26	0.26	0.26	0.26	0.26	0.15	4.0	0.26	0.26	0.26	0.26	07.0	0.26	0.26	0.26	0.26	0.27	9.26	0.27	0.27	0.26	0.26	0.26	0.26	0.26	0.26	0.26	0.26	0.26	0.26	0.27	0.26	0.26	0.27	0.26	0.27	0.26	0.27	0.27	0.26	0.27	0.27	0.26	0.27	0.27	0.27	0.26	0.26
oc6_91500_3	oc6 91500 4	006 91500 5 006 91500 6	oc6_91500_7	oc6_91500_8	oc6_91500_10	006 91500 11	oc6 91500 13	oc6_91500_14	006 91500 15 006 91500 16	oc6 91500 17	006_91500_18	oc6 91500 20	oc6_91500_21	oc6 91500 22	006 91500 23	000 91500 24	ac6 91500 26	oc6 91500 27	oc6_91500_28	oc6 91500 29	006 91500 30	006_91500_31	oc6 91500 33	oc6_91500_34	oc6_91500_35	oc6 91500 36	oc6_91500_38	oc6_91500_39	oc6 91500 40	006 91500 41	24 00016 000	000 91500 43	oc6 91500 45	oc6 91500 46	oc6 91500 47	oc6_91500_48	oc6 91500 49	ocb 91500 50	005 91500 51	oc6 91500 53	oc7_91500_1	oc7_91500_2	oc7_91500_3	9001 61200 E	oc7 91500 6	oc7 91500 7	oc7_91500_8	oc7 91500 9	oc7 91500 10	oc7 91500 12	oc7 91500 13	oc7 91500 14	oc/ 91500 15 oc7 91500 16	oc7 91500 17	007_91500_18	007_91500_19	007 91500 21	oc7 91500 22	oc7_91500_23	007 91500 25	oc7_91500_26	oc7_91500_27	oc/ 91500 28	oc7 91500 30	oc7_91500_31	oc7 91500 32	1 002 91500 2	fe05_91500_3	fe05_91500_4	fe05_91500_5	fe05 91500 6	fent arton 8	fe05 91500 9	fe05_91500_10	fe05_91500_11	fe05_91500_12	fe05 91500 15	fe05_91500_15	fe05 91500 16	fe05_91500_1/

101.08 98.97	102.08 98.66	101.95 99.72	101.05	99.07	99.91	99.07 100.95	100.29	100.45 98.14	101.23	99.43 99.57	98.29	99.13	100.85	90.91	102.07	99.45 200 00	10.256 99.17	100.84	99.53	101.45	26.35 26.08	16:06	100.28	100.09	99.43 100.47	98.74	100.47	100.95	99.62 200 m	100.00	100.68	100.29	50.07	98.10 	101.50	100.09	99.82	100.28	102.05	100.56	98.67 20.55	06.72	101.12	100.37	100.56	100.47	98.05	101.99	47.707	99.53	100.66	102.19	99.81	101.61	100.86	101.82	99.25 08.08	102.42	06'66	%.% %03	99.25	100.66	100.38	98:90	38.08	102.00	101.24	100.48	101.28	100.97	98.79	101.74	100.65 100.85
109.95 100.48	97.91	100.94	102.52 96.83	100.95	100.85	98.71 102.91	101.45	101.60 96.70	105.62	96.61 94.13	99.04	06'96	105.86	104.21	106.59	99.82	10/.36 99.35	105.34	99.62	102.93	70'C6	98.24	101.04	97.29	03.01	96.87	102.88	104.52	101.05	00.29	103.88	104.91	97.61	95,33	108.83	103.15	103.75	104.54	109.50	103.55	97.19	92.40	104.34	102.38	103.76	102.96	97.24	106.22	103.37	99.53	104.21	108.37	100.66	106.85	104.05	104.62	100.66 98.16	108.27	100.10	94,66	97.89	102.00	102.04 08.46	99.45	96.83	108.84	104.72	104.80	103.51	30.41 103.78	101.63	108.25	106.90
R R 1	¥ 12	R 17	12	2 F	: 98	86	18 I	R 8	99	82	61	99	8 6	<i>a</i> 19	r.	88	8 6	8	99	<b>8</b> 8	8 2	5 8	66	8	<del>1</del> 8 H	8	67	67	6	8 18	9 8	18	82	8	88	8	8	8 2	5 68	81	88	8 8	8	87	35 S	8	87	16 %	8 8	88	88 8	8 88	92	88	8	88	8	8	88	8 35	88	81	130	120	120	110	110	8	110	9 18	110	110	81 81
1064	10/9	1057	1027	1114	1082	1067	1041	1082	1079	1010	981	1027	1100	1063	1134	1107	1040	1057	1070	1044	1089	1046	1033	1076	1029	1083	1077	1064	1100	1085	1094	1043	1014	1074	1050	1123	1073	1044	1095	1041	1032	797	1141	1070	1058	1069	1076	1092	1053	1029	1146	1061	1084	1066	1096	1053	1001	1093	1028	1059	1081	1048	1125	121	1115	1049	1018	696	1022	982 982	1000	1074	1106
35	35	37 36	35	36	32	32	30	33	31	80	30	31	90	31	30	32	31	31	32	31	31	31	31	32	32	31	30	8	31	82 00	6 g	29	30	52	28	29	31	8 P	9	30	90	29	28	30	29	6 6	28	30	6 6	30	30	32	30	32	32	31	og og	29	8	29	30	29	29	46	50	47	47	46	45	47	50	45	45
1072	1046	1024	1045	1075	1073	1050	1045	1077	1058	1035	1051	1040	1057	1070	1062	1087	1081	1075	1067	1038	1078	1063	1070	1077	1049	1035	1065	1053	1063	1021	1036	1044	1074	1104	1069	1080	1082	1057	1073	1072	1053	1074	1069	1073	1070	1073	1079	1055	1043	1064	1058	1052	1076	1059	1041	1046	1080	1074	1025	1066	1073	1066	1045	1092	1091	1050	1052	1043	1018	1033	1075	1032	1078
38	39	40	38	39	6 6	39 40	88	39	40	6E 85	38	39	39	38	41	66	41	40	39	4	55 Q	f 88	40	39	66 02	37	39	8	86	8 <u>6</u> 68	40	88	40	<del>6</del>	40	40	40	66	6	40	39	x 4	40	40	40	4	40	40	6 6	40	40	64 1	40	41	39	41	6 4	41	38	66	40	41	40	32	34	31	33	33	32	33	33	32	33
1083	1078	1044	1056	1065	1072	1070	1048	1056	1071	1053	1033	1031	1066	1069	1084	1081	1072	1084	1062	1053	1067	1062	1073	1078	1043	1022	1070	1063	1059	1021	1043	1047	1064	1083	1085	1081	1080	1060	1095	1078	1039	1045	1081	1077	1076	1078	1058	1076	1042	1059	1065	1075	1074	1076	1050	1065	1061	1100	1024	1045	1065	1073	1049	1080	1070	1071	1065	1048	1031	1043	1062	1050	1085
55	2 %	88	51 54	56	55	53 59	49	24 03	5	47	53	£	57	55	54	3, 13	52	55	56	55 5	8 5	52	54	2	8 3	56	48	53	ß	66	89	70	63	59	59	62	70	8 5	8	66	20	\$ 8	64	72	88	8 02	68	74	78	73	76	79	69	74	76	11	70	67	20	67	69	68	69 PZ	74	82	02	8	78	69	20 76	83	74	76
985 1049	974 1054	965 1064	1030	1055	1063	1084	1033	1065	1014	1090	1043	1064	1007	1050	1017	1083	1079	1029	1066	1023	1075	1081	1062	1108	1074	1055	1040	1017	1048	1018	1001	866	1090	1136	1049	1048	1041	1014	1000	1041	1069	1131	1036	1052	1087	1047	1088	1013	1008	1064	1022	992 992	1067	1007	1009	1018	1084	1016	1023	1104	1088	1052	1028	1086	1105	984 1014	1017	1000	996	1005	1045	970	1015 980
0.0038	0.0038	0.0038	0.0038	0.0039	0.0035	0.0036	0.0033	0.0038	0.0035	0.0033	0.0032	0.0034	0.0036	0.0035	0.0038	0.0036	0.0034	0.0035	0.0034	0.0036	0.0034	0.0034	0.0034	0.0035	0.0034	0.0033	0.0035	0.0035	0.0035	0.0041	0.0043	0.0042	0.0041	0.0045	0.0044	0.0047	0.0044	0.0042	0.0045	0.0042	0.0042	0.0041	0.0045	0.0046	0.0044	0.0044	0.0046	0.0048	0.0044	0.0044	0.0046	0.0046	0.0048	0.0045	0.0047	0.0044	0.0042	0.0046	0.0044	0.0044	0.0045	0.0042	0.0045	0.0061	0.0062	0.0059	0.0057	0.0054	0.0056	0.0055	0.0056	0.0059	0.0062
0.0541 0.053	0.0549	0.0534	0.0523	0.0563	0.0547	0.0544	0.0529	0.0552	0.0549	0.0522	0.0499	0.0523	0.0559	0.0538	0.0577	0.0564	0.053	0.0539	0.0541	0.0532	6100.0	0.0533	0.0525	0.0547	0.0521	0.0525	0.0548	0.054	0.0557	0.052/	0.0556	0.0527	0.0516	0.0546	0.0526	0.0574	0.0545	0.0532	0.0559	0.0528	0.0524	0.0487	0.0581	0.0546	0.0539	0.0556	0.0549	0.0556	0.0537	0.0522	0.0581	0.0542	0.0554	0.0479	0.0557	0.0537	0.0507	0.0556	0.0525	0.0538	0.0545	0.0532	0.0535	0.0573	0.0567	0.0536	0.0519	0.0493	0.0516	0.0501	0.051	0.0546	0.0565
0.3029	0.2859	0.2762	0.3531	0.3012	0.3317	0.3570	0.3113	0.3470	0.3288	0.3624	0.3075	0.4118	0.2154	0.3124	0.3311	0.2543	0.1833	0.2866	0.2676	0.3478	0.3046	0.3081	0.1957	0.3277	0.1916	0.1980	0.3210	0.3010	0.2772	0.1824	0.1509	0.1165	0.1811	0.1394	0.1861	0.1677	0660.0	0.1698	0.2109	0.1843	0.1256	0.0124	-0.0216	0.0529	0.1929	0.0941	-0.0632	0.2019	0.0893	-0.0117	0.0511	0.0622	0.1607	0.1681 0.1235	0.0768	0.1964	0.1166	0.1598	0.2007	0.1408	0.2192	0.1697	0.1259	0.1466	0.2296	0.1929	0.1739	0.1143	0.2731	0.2430	0.2728	0.1740	0.1579 0.1132
0.0073	0.0071	0.0073	0.0073	1/0000	0.0073	0.0074	0.00.0	0.0071	0.0073	0.0071	0.0070	0.0071	0.0072	0.0071	0.0075	0.0072	5/000	0.0073	0.0071	0.0072	1/000	0.0071	0.0073	0.0071	0.0072	0.0068	0.0071	0.0070	0.0070	60000	0.0070	0.0070	0.0072	0.0074	0.0074	0.0073	0.0072	0.0072	0.0074	0.0074	0.0072	0.0073	0.0074	0.0074	0.0074	0.0074	0.0072	0.0073	0.0072	0.0071	0.0072	0.0074	0.0074	0.0074	0.0072	0.0075	0.0072	0.0075	0.0069	0.0072	0.0074	0.0076	0.0073	0.0058	0.0063	0.0058	0.0060	0.0061	0.0058	0.0060	0.0059	0.0058	0.0062
0.1831 0.1778	0.1819	0.1761 0.1814	0.1781	0.1797	0.1809	0.1807 0.1788	0.1769	0.1824	0.1806	0.1773	0.1741	0.1733	0.1801	0.1802	0.1835	0.1826	0.1809	0.1833	0.1794	0.1776	0.1801	0.1790	0.1812	0.1822	0.1754	0.1717	0.1807	0.1792	0.1788	0.1710	0.1754	0.1759	0.1792	0.1830	0.1833	0.1825	0.1819	0.1787	0.1852	0.1818	0.1752	0.1762	0.1826	0.1820	0.1816	0.1822	0.1783	0.1819	0.1754	0.1780	0.1797	0.1817	0.1812	0.1816 0.1758	0.1771	0.1797	0.1/89	0.1863	0.1724	0.1759	0.1799	0.1812	0.1769	0.1827	0.1806	0.1807	0.1798	0.1770	0.1735	20.1762	0.1788	0.1766	0.1838 0.1814
0.1000	0.0950	0.0980	0.0980 0.1000	0.1000	006010	0.0920 0.0850	0.0820	0260.0	0.0870	0.0850	0.0840	0.0880	0.0870	0.0890	0.0880	0.0890	0.0880.0	0.0890	0.0880	0.0840	0.0880	0.0870	0.0870	0.0900	0.0850	0.0840	0.0860	0.0840	0.0850	05/00	0.0790	0.0800	0.0820	0.0830	0.0790	0.0830	0.0860	0.0840	0.0830	0.0820	0.0820	0.0840	0.0770	0.0840	0.0820	0.0820	0.0810	0.0860	0.0840	0.0840	0.0860	0.0890	0.0860	0.0870	0.0850	006010	0.08.70	0.0820	0.0820	0.0820	0.0840	0.0820	0.0800	0.1400	0.1400	0.1300	0.1300	0.1300	0.1200	0.1300	0.1400	0.1200	0.1400
1.8660	1.7940	1.7650	1.8190	1.8800	1.8850	1.8200	1.8050	1.9110	1.8430	1.8370	1.8000	1.7970	1.8440	1.8600	1.8520	1.9140	1.9120	1.9000	1.8740	1.7880	1 8920	1.8450	1.8650	1.8930	1.8150	1.7880	1.8600	1.8220	1.8480	1.7350	1.7830	1.7980	1.8730	1.9540	1.8540	1.8950	1.9060	1.8500	1.8780	1.8670	1.8240	1.8920	1.8610	1.8840	1.8780	1.8830	1.8800	1.8280	1.7850	1.8510	1.8370	1.8150	1.8900	1.8460	1.7930	1.8320	1 9130	1.8760	1.7600	1.8560	1.8930	1.8570	1.8240	1.9320	1.9350	1.8310	1.8360	1.8030	1.7340	1.7840	1.8880	1.7700	1.9010
0.0025	0.0025	0.0025	0.0025	0.0024	0.0023	0.0025	0.0020	0.0025	0.0022	0.0021	0.0022	0.0023	0.0023	0.0023	0.0021	0.0023	0.0022	0.0022	0.0023	0.0022	0002	0.0022	0.0022	0.0023	0.0025	0.0023	0.0020	0.0021	0.0021	/200.0	0,0028	0.0028	0.0028	0.0027	0.0027	0.0028	0.0029	0.0029	0.0027	0.0028	0.0030	10000	0.0028	0:0030	0.0028	0.0029	0:0030	0.0031	0.0031	0.0031	0.0031	0.0032	0.0029	0.0031	0:0030	0.0032	0.0032	0.0028	0.0030	00000	0.0031	0.0029	0.0029	0.0035	0.0039	0.0032	0.0037	0.0035	0.0033	0.0035	0.0036	0.0034	0.0036
0.0735	0.0724	0.0731	0.0746	0.0753	0.0758	0.0762	0.0741	0.0750	0.0735	0.0754	0.0750	0.0759	0.0741	0.0748	0.0724	0.0762	0.0760	0.0742	0.0759	0.0735	0.0753	0.0762	0.0752	0.0757	0.0760	0.0752	0.0744	0.0734	0.0747	0.0735	C#200	0.0743	0.0763	0.0772	0.0733	0.0746	0.0747	0.0745	0.0738	0.0745	0.0754	0.0792	0.0743	0.0747	0.0748	0.0747	0.0763	0.0744	0.0732	0.0758	0.0737	0.0723	0.0755	0.0740	0.0741	0.0742	0.0729	0.0728	0.0741	0.0773	0.0773	0.0747	0.0743	0.0763	0.0774	0.0725	0.0752	0.0743	0.0730	0.0734	0.0748	0.0727	0.0745
0.2177	0.2176 0.2345	0.2257	0.2207	0.2199	0.2231	0.2266	0.2237	0.2224	0.2238	0.2259	0.2309	0.2364	0.2220	0.2186	0.2227	0.2159	0.2170	0.2173	0.2206	0.2283	0.2189	0.2216	0.2223	0.2139	0.2340	0.2307	0.2174	0.2180	0.2190	0.2340	0.2340	0.2262	0.2242	0.2210	0.2202	0.2192	0.2176	0.2255	0.2157	0.2239	0.2346	0.2351	0.2219	0.2234	0.2244	0.2229	0.2265	0.2206	0.2340	0.2241	0.2230	0.2241	0.2254	0.2244	0.2296	0.2323	0.2250	0.2161	0.2322	0.2327	0.2286	0.2315	0.2333	0.1738	0.1932	0.1776	0.1856	0.1947	0.1927	0.1933	0.1846	0.1860	0.1835
5.4615 5.6243	5.4975 5.7471	5.5127	5.6148 5.5463	5.5648	5.5279	5.5340 5.5928	5.6529	5.4825 5.6117	5.5371	5.6402	5.7438	5.7703	5.5525 c cc17	5.5494	5.4496	5.4765	5.5279	5.4555	5.5741	5.6306	5.0059	5.5866	5.5188	5.4885	5.7013 5.617	5.8241	5.5340	5.5804	5.5928	5.8241	5.7013	5.6850	5.5804	5.4645	5.4555	5.4795	5.4975	5.5960	5.3996	5.5006	5.7078	5.6754	5.4765	5.4945	5.5066 5.4a75	5.4885	5.6085	5.4975 c c462	5.7013	5.6180	5.5648	5.5036	5.5188	5.5066 5.6883	5.6465	5.5648	5.5697	5.3677	5.8005	5.6850	5.5586	5.5188	5.6529 5.4526	5.4735	5.5371	5.5340	5.5617	5.6497	5.7637	5.6754	5.5928	5.6625	5.5127 5.5127
0.26	0.26	0.27	0.26	0.26	0.28	0.27	0.27	0.27	0.27	0.27	0.27	0.27	0.27	0.27	0.27	0.27	0.27	0.27	0.26	0.27	0.27	0.27	0.27	0.27	0.26	0.27	0.27	0.27	0.27	0.25	0.26	0.26	0.26	0.26	0.26	0.26	0.26	0.27	0.26	0.26	0.26	0.26	0.26	0.26	0.26	0.26	0.26	0.26	0.26	0.25	0.25	0.26	0.26	0.26	0.25	0.25	0.26	0.26	0.25	0.25	0.25	0.25	0.26	0.27	0.27	0.27	0.28	0.27	0.27	0.27	0.27	0.27	0.26
fe05_91500_18 fe05_91500_19	fe05_91500_20 fe05_91500_21	fe05 91500 22 fe05 91500 23	fe05 91500 24 fe05 91500 25	fe05 91500 26	fe05 91500 28	fe05 91500 29 fe05 91500 30	fe05 91500 31	fe05 91500 32 fe05 91500 33	fe05 91500 34	fe05 91500 35	fe05_91500_37	fe05_91500_38	fe05 91500 39	fe05 91500 41	fe05_91500_42	fe05 91500 43	fe05 91500 45	fe05_91500_46	fe05_91500_47	fe05 91500 48	fens 91500 49	fe05_91500_51	fe05_91500_52	fe05_91500_53	fe05 91500 54	fe05 91500 56	fe05_91500_57	fe05_91500_58	fe05_91500_59	mr20_91500_1 mr20_91500_2	mr20 91500 3	mr20_91500_4	mr20_91500_5	mr20_91500_6	mr20_91500_7 mr20_91500_8	mr20_91500_9	mr20_91500_10	mr20_91500_11	mr20 91500 13	mr20_91500_14	mr20_91500_15	mr20 91500 17	mr20_91500_18	mr20_91500_19	mr20 91500 20 mr20 91500 21	mr20 91500 22	mr20_91500_23	mr20_91500_24	mr20 91500 26	mr20 91500 27	mr20_91500_28	mr20_91500_30	mr20 91500 31	mr20 91500 32 mr20 91500 33	mr20 91500 34	mr20_91500_35	mr20 91500 36 mr20 91500 37	mr20 91500 38	mr20 91500 39	mr20 91500 41	mr20 91500 42	mr20_91500_43	mr10_91500_44 mr10_01500_1	mr19 91500 2	mr19_91500_3	mr19_91500_4	mr19_91500_6	mr19_91500_7	mr19_91500_8	mr19 91500 10	mr19 91500 11	mr19 91500 12	mr19 91500 13 mr19 91500 14

99.05	99.63	102.10	100.00	98.97	102.09	100.19	00 810	100.39	100.94	100.83	100.65	102.01	100.29	100 E7	99.91	00.67	99.82	100.28	98.89	99.17	98.97	97.59	99.72	98.26	99.72	100.09	100.85	99,444 100 AE	97.82	98.78	98.22	99.52	100.09	101.02	100.67	101 JA	40.43	100.67	101.62	102.46	101.97	98.71	100.83	100.47	98.88	101.06	100.37 100.7E	101.05	98.13	100.38	98.88	101.44	98.45	98,49 07.75	c/./2	100.78	100.18	100.19	102.50	100.09
100.19	97.26	107.96	104.20	96.53	109.23	101.43	106.3U	98.30	101.99	102.15	98.02	105.34	100.48	58.65 103 EU	08.43 08.43	90.00	99.54	103.21	98.16	98.72	98.78	94.93	102.50	100.19	103.90	102.46	105.94	110 A6	95.90	99.72	98.77	97.30	105.91	104.52	104.03	102.01	16:001	99.81	104.62	103.08	103.91	96.10	102.50	98.41 101 37	99.17	99.11	99.98 77 001	100.77 102 51	93.17	100.44	94.37	104.53	96.05	11.d9	34.12 100.48	101.82	98.70	99.73 as an	107.90	98.97
110	120	120	110	110	69	74	66 66	61	68	71	69	8	63	99 93	8 6	2	5 69	22	70	89	67	65	70	70	74	20	7	7 72	رد 55	3 99	88	70	69	99	67	69	5	62	63	72	73	71	99	/4 65	20	73	5	71		02	74	89	65	4 B	7/	74	74	72	., 26	79
1066	1124	1030	1020	1038	1119	1058	1001	1027	1052	1054	1085	1054	971	1034	1050	1050	1070	1070	1060	1072	1052	1043	1075	1092	1105	1095	1104	1109	1050	1042	1063	1044	1058	1079	1066	1801	1078	1013	1004	1107	1044	1039	1036	1/01	1037	1068	1080	1111	1067	1059	1091	1030	1018	1001	696	1072	1087	1074	1085	1043
46	46	47	51	64	38	88 6	۶ ۶	8 88	37	38	88	39	36	dč S	37	۲¢	6E	8 88	37	36	37	36	37	39	37	38	37	8 8	8 £	37	38	37	40	39	36	85 8	8 8	37	37	39	39	42	39	40	6	40	6	₽ 8	67	6	40	41	66 :	9	37	40	41	39	40	41
1058	1068	1050	1068	1068	1055	1059	1037	1037	1064	1086	1081	1044	1041	1050	1068	1054	1083	1090	1077	1085	1067	1037	1067	1089	1069	1082	1061	10 /U	1053	1063	1066	1050	1092	1075	1052	1050	1056	1038	1048	1056	1064	1089	1078	1056	1069	1040	1067	1051	1067	1053	1075	1042	1032	1060	1017	1030	1084	1069	1079	1075
36	33	35	33	\$ \$	49	47	49	46	48	50	49	48	46	6 <del>1</del>	45 15	e e	47	48	46	47	47	45	47	47	47	47	47	4/	÷ 5	47	46	46	49	48	46	48	÷ 4	47	48	51	51	20	12	7 5	20	50	89 2	16	f 5	3	50	49	48	<del>5</del> 5	8 8	50	20	49 5-1	72	20
1048	1064	1072	1068	1057	1077	1061 1085	1035	1041	1074	1095	1088	1065	1044	1021	1067	1050	1081	1093	1065	1076	1056	1012	1064	1070	1066	1083	1070	1004	1030	1050	1047	1045	1093	1086	1059	1062	1050	1045	1065	1082	1085	1075	1087	1062	1057	1051	1071	1062	1047	1057	1063	1057	1016	1044	1016	1038	1086	1071	1106	1076
77	75	80	94	80	72	71	6/	69	62	69	68	72	67	63 7.4	ť 5	69	72	67	64	61	63	60	62	75	69	65	64	را 89	20	66	70	67	84	69	61	71	12	68	71	62	68	78	67	//	72	65	62 7F	c/ 12	80	20	72	70	70	76	75	72	74	70	74	69
1046	1094	993	1025	1095	986	1046	1058	1059	1053	1072	1110	1011	1039	1035	1084	1060	1086	1059	1085	1090	1069	1066	1038	1068	1026	1057	1010	10U5 985	1074	1053	1060	1074	1032	1039	1018	1020	1106	1047	1018	1050	1044	1119	1060	1050	1066	1060	10/1	000T	1124	1052	1126	1011	1058	1098	1011	1019	1100	1074	1025	1087
0.0059	0.0065	0.0061	0.006	0.0057	0.0036	0.0039	10035	0.0032	0.0036	0.0037	0.0036	0.0036	0.0033	0.0036	2 200.0	10033	0.0036	0.0037	0.0037	0.0036	0.0035	0.0034	0.0036	0.0037	0.0039	0.0037	0.0037	0.0037	0.0034	0.0034	0.0035	0.0036	0.0036	0.0034	0.0035	0.0035	0.0034	0.0032	0.0033	0.0038	0.0038	0.0037	0.0035	0.0038	0.0036	0.0038	0.0037	0000	0.0035	0.0036	0.0038	0.0036	0.0034	0.0034	0.0036	0.0039	0.0039	0.003 /	0.004	0.0042
0.0542	0.0573	0.0526	0.0518	0.0527	0.0569	0.054	0.051	0.0523	0.0534	0.0533	0.0554	0.0533	0.0492	0.0577	17000	0.0535	0.0546	0.0546	0.0541	0.0546	0.0536	0.0529	0.0548	0.0555	0.0565	0.0559	0.0563	0.0564	0.0535	0.0529	0.0542	0.0532	0.0537	0.0548	0.0541	010100	0.0549	0.0516	0.0509	0.0563	0.0532	0.053	0.0528	0.0523	0.0529	0.0545	0.0549	2950.0	0.0542	0.054	0.0555	0.0525	0.0518	0.0507	0.0493	0.0547	0.0555	0.0548	0.0554	0.0537
0.2064	0.2061	0.2104	0.1105	0.1768	0.2491	0.1254 0.100F	0.1808	0.1624	0.1447	0.2025	0.0748	0.1931	0.2057	0.1341	CTCD/0	1238	0.0040	0.0323	0.0598	0.0899	0.0482	0.0842	0.1521	0.0733	0.0724	0.1566	0.1187	0.1513	0101 C	0.1460	0.1595	0.1751	0.0581	0.0945	0.1587	01200	1101	9060.0	0.0635	0.3839	J. 3449	0.2416	0.2342	1122.0	0.1907	0.2837	0.3589	1 2077	0.2486	0.2384	0.2756	0.3316	0.2635	0.1903	0.1660	0.3793	0.2706	0.2642 1 1067	0.1935	0.3104
0.0067	0.0061	0.0064	0.0060	0.0061	0600.0	0.0086	0.0085	0.0085	0.0088	0.0092	0600.0	0.0088	0.0085	7800.0	0.000	0.0085	0.0087	0.0088	0.0086	0.0087	0.0085	0.0081	0.0086	0.0087	0.0086	0.0087	0.0086	0.008b	0.0082	0.0085	0.0084	0.0085	0.0089	0.0088	0.0085	0.0086	0.0086	0.0085	0.0088	0.0094	0.0033	0.0093	0.0093	2600.0	0.001	0.0092	16000		1600.0	0.0092	0.0092	0600.0	0.0087	06000	1600.0	0.0091	0.003	0.0091	9600.0	0.003
0.1772	0.1797	0.1815	0.1802	0.1784	0.1822	0.1789 0.182F	CCOT.U	0.1756	0.1814	0.1853	0.1840	0.1800	0.1757	C1/10	16/17.0	0.1771	0.1827	0.1846	0.1794	0.1815	0.1777	0.1701	0.1796	0.1805	0.1799	0.1831	0.1808	0.1/9/	0.1734	0.1771	0.1764	0.1762	0.1851	0.1835	0.1785	0.1704	0 1771	0.1762	0.1799	0.1826	0.1837	0.1815	0.1838	0.1800	0.1776	0.1771	0.1801	1783	0.1768	0.1787	0.1798	0.1786	0.1711	0.1760	0.1702	0.1751	0.1831	0.1812	0.1873	0.1815
0.1300	0.1300	0.1300	0.1400	0.1300 0.1300	0.1100	0.1100	01001	0.1000	0.1000	0.1100	0.1100	0.1100	0.1000	0/60.0	01100	0 1000	0.1100	0.1100	0.1000	0.1100	0.1000	0660.0	0.1000	0.1100	0.1100	0.1100	0.1000	0.1100	0,1000	0.1100	0.1100	0.1000	0.1200	0.1100	0.1000	0.1000	0 1000	0.1000	0.1000	0.1100	0.1100	0.1200	0.1100	0.1100	0.1100	0.1100	0.1100	01100	0.1200	0.1100	0.1200	0.1100	0.1100	0.1100	0.1100	0.1100	0.1200	0.1200	0.1200	0.1100
1.8340	1.8790	1.8260	1.8730	1.8790	1.8470	1.8350	1 7940	1.7870	1.8600	1.9170	1.9070	1.8120	1.7570	1 9500	1 8850	1 8450	1.9190	1.9190	1.8800	1.9110	1.8520	1.7940	1.8480	1.9440	1.8710	1.9150	1.8630	1.8800	1.8420	1.8620	1.8560	1.8240	1.9270	1.8990	1.8140	1 2710	1 8230	1.7850	1.8020	1.8530	1.8670	1.9300	1.8920	1.8690	1.8670	1.8070	1.8670	1 8210	1.8770	1.8100	1.8790	1.8090	1.7700	1.8430	1.7260	1.7760	1.9140	1.8660	1.9010	1.8840
0.0037	0.0036	0.0037	0.0039	0.0038	0.0026	0.0027	0.0025	0.0026	0.0024	0.0026	0.0027	0.0027	0.0025	0.0024	0.0075	0.0024	0.0027	0.0027	0.0026	0.0025	0.0026	0.0025	0.0024	0.0029	0.0025	0.0026	0.0025	0.0026	0.0023	0.0026	0.0027	0.0026	0.0031	0.0026	0.0024	0.0026	0.0020	0.0027	0.0027	0.0023	0.0025	0:0030	0.0025	7200.0	0.0027	0.0024	0.0023	0.0026	0.0020	0.0026	0.0028	0.0025	0.0026	0500.0	0.0027	0.0026	0.0028	0.0028	0.0027	0.0026
0.0750	0.0761	0.0733	0.0743	0.0773	0.0735	0.0752	0.0743	0.0749	0.0748	0.0753	0.0764	0.0736	0.0741	0.0753	2570.0	0.075.4	0.0763	0.0749	0.0768	0.0772	0.0757	0.0751	0.0746	0.0763	0.0733	0.0754	0.0742	0.0/34	0.0760	0.0745	0.0754	0.0760	0.0746	0.0753	0.0737	0.0743	0.0766	0.0751	0.0738	0.0743	0.0741	0.0769	0.0747	0.0743	0.0749	0.0747	0.0740	0.0738	0.0771	0.0744	0.0772	0.0729	0.0746	0.0765	0.0729	0.0732	0.0762	0.0760	0.0734	0.0757
0.2134	0.1889	0.1943	0.1848	0.1917	0.2711	0.2687	0 2795	0.2757	0.2674	0.2679	0.2658	0.2716	0.2753	0.2604	0.2654	0.7710	0.2606	0.2582	0.2672	0.2641	0.2692	0.2799	0.2666	0.2670	0.2657	0.2595	0.2631	0.2005	7272 N	0.2710	0.2699	0.2738	0.2598	0.2613	0.2668	0.2673	2/02/0	0.2738	0.2719	0.2819	0.2756	0.2823	0.2753	c/82.0	0.2885	0.2933	0.2806	1.201/	0.2911	0.2881	0.2846	0.2821	0.2972	0.2928	0.2969	0.2968	0.2774	0.2772	0.2737	0.2823
5.6433	5.5648	5.5096	5.5494	5.6054	5.4885	5.5897	5.7330	5.6948	5.5127	5.3967	5.4348	5.5556	5.6915	5.8309	3.3040 5.555.6	5 AAFE	5.4735	5.4171	5.5741	5.5096	5.6275	5.8789	5.5679	5.5402	5.5586	5.4615	5.5310	5.5548	0.767.0	5.6465	5.6689	5.6754	5.4025	5.4496	5.6022	5.4705	256455	5.6754	5.5586	5.4765	5.4437	5.5096	5.4407	5.5897	5.6306	5.6465	5.5525	20000	5.6561	5.5960	5.5617	5.5991	5.8445	5.698U 5.6818	5.8754	5.7110	5.4615	5.5188	5.3390	5.5096
0.26	0.27	0.27	0.27	0.26	0.25	0.26	0.20	0.26	0.27	0.26	0.26	0.27	0.26	0.25	0.26	0.26	0.25	0.26	0.26	0.25	0.26	0.25	0.26	0.26	0.26	0.26	0.25	0.25	0.25	0.26	0.25	0.26	0.26	0.26	0.26	0.25	0.26	0.26	0.26	0.26	0.26	0.26	0.27	0.27	0.26	0.25	0.26	0.20	0.26	0.27	0.26	0.27	0.26	12.0	0.26	0.26	0.27	0.26	0.27	0.26
mr19 91500 15	mr19_91500_16	mr19_91500_17	mr19_91500_18	mr19 91500 20	mr19_91500_21	mr19_91500_22	mr19 91500 23	mr19 91500 25	mr19_91500_26	mr19_91500_27	mr19_91500_28	mr19_91500_29	mr19_91500_30	mr 19 91500 31	mr10 01500 32	mr19 91500 34	mr19 91500 35	mr19 91500 36	mr19 91500 37	mr19 91500 38	mr19_91500_39	mr19_91500_40	mr19_91500_41	mr19_91500_42	mr19_91500_43	mr19_91500_44	mr19_91500_45	mr19_91500_40	mr19 91500 48	mr19 91500 49	mr19_91500_50	mr19_91500_51	mr19_91500_52	mr19_91500_53	mr19_91500_54	mr19 91500 55	mr19 91500 57	mr19 91500 58	mr19_91500_59	mr30_91500_1	mr30_91500_2	mr30_91500_3	mr30_91500_4	mr30_91500_5	mr30 91500 7	mr30_91500_8	mr30_91500_9	mr30 91500 11	mr30 91500 12	mr30 91500 13	mr30_91500_14	mr30_91500_15	mr30_91500_16	mr30_91500_1/	mr30 91500 19	mr30_91500_20	mr30_91500_21	mr30_91500_22	mr30 91500 24	mr30_91500_25

% Concordancy (206Pb-238U	age/207Pb-235U age) *100	100.6	100.8	101.2	5'86	101.3	103.9	98.8 Mr	100.2	100.5	97.1	99.5	93:8 100 J	2.001	101.4	101.6	98.7	101.2	103.9	100.3	99.3	101.7	102.1	9.85	587 2013	88	100.4	98.1	0'66	103.1	102.4	99.4	5.95	0:1601	5.05	21200	90 F	2.8	9.66	93.6	98.6	101.6	99.1	99.3	99.2 00 f	5.95 F 80	36:4 101:0	99.3 2	98.8	98.5	100.6	0.001	2.16	97.4	99.4 20.0	101.8	98.9 101.7	98.8	102.4	100.3	101.7	9/./ 00.6	101.2	98.5	100.6	5.85 c 2	00:30 08:30	100.4	100.5	99.2	99.1	103.2	38.5	100.5	C:001	9).4 101.5	100.1	8.66	100.4	96.7	101.0	C.UUI E.90	102.3	100.2	101.2	101.9
% Concordancy (206Pb-238U	age/207Pb-20GPb age)*100	97.4	115.1	152	33.1 88.0	98.7	121.8	82.2	52.3 95.3	106.7	80.7	97.4	43.4	819	117.8	123.0	94.3	1116	172.3	94.6	102.3	132.7	124.2	93.3	1044	72.7	108.2	88.3	94.6	139.3	111.7	87.3	75	1221	102	07.0	1010	04.6	104.5	98.3	90.9	116.9	101.0	96.6	104.5	98.3	30.9	97.2	90.2	86.5	108.9	03.6	67.1	76.8	102.7	110.3	86.1 121.3	94.7	120.6	110.4	1114	97.4	127.1	90.9	115.3	87.5	74.2 83.8	105.8	131.2	93.5	97.3	142.7	100.6	104.U	0.70T	1144	108.6	102.4	109.2	79.5	1128	106.7	121.4	105.0	121.0	119.9 1
	ZE	18	11	9 :	17	17	18	18	18	17	17	17	10	18	18	18	19	18	18	18	18	18	50	20	19	5	18	19	20	21	20	22	2	77	17	27	12	13	2 2	13	13	13	12	13	E :	n 5	n 11	7	6	80	-	, u	6	10	10	11 \$	9 ø	6	6	6	:::::::::::::::::::::::::::::::::::::::	11	18	18	18	8	18	18	18	17	18	17	17	17	10	91	16	17	17	18	16	16 16	16	17	16	16
	<sup>03</sup> Pb/ <sup>232</sup> Th	306	293	567	299	300	305	309	322	305	315	302	015	CPC	289	290	305	283	289	278	286	283	302	298	305	273	274	287	297	307	295	314	197	200	coc	300	202	300	296	295	303	306	293	295	296	505	306	300	289	298	287	167	304	298	298	299	289	294	292	295	288	305	299	303	305	306	797	303	296	290	298	290	307	314	667	208	294	312	320	331	296	203 203	300	307	295	291
	2SE	5	<del>ن</del> ا ت	e :	a ti	15	16	16 16	n ta	16	15	16	9	r (	3 00	6	10	6	10	6	9	9	9	=	9 6	a 0	Π	10	10	11	9	12	:	4 4	4 5	1 5	4 =	; ₽	9 0	01	10	10	п	Ħ	# :	<b>1</b> \$	a 8	6	10	6	6	a ¢	9 9	0	9	9 Ş	a 6	9	10	10	= :	1	4	14	14	s :	4 1	4	13	13	4	13	r :	7 F	4 5	1 1	17	12	12	11 : 1	а :	4 5	12	12	# :	12
sa	0 <sup>207</sup> Pb/ <sup>235</sup> U	297	285	582	296	295	298	302	301	303	302	305	300	200	291	287	299	286	284	293	294	230	162	295	285	294	280	294	298	295	292	300	301	107	100	007 CUE	206	200	280	296	297	298	295	296	291	202	12 000	297	292	296	230	002	308	303	290	290	106	562	289	295	293	308	302	305	302	303	311	301	302	301	307	296	606	305	202	29.5	294	301	304	304	299	2967 3012	293	298	294	294 294
Dat	2SE	15	14	a :	14	15	16	15	15	15	14	15	Q +	, r	7	7	7	7	7	7	2	-			, -	-	7	7	7	8	7	80	0	•	• •	0 0	2		, 7	7	7	2	7	7	-	\ r	~ ~	9	9	9	9	o 4	9	9	9	7	9	9	9	9	7	o (	12	12	12	=	12	11	11	11	12	12	12	12	77	11	11	11	11	12	: : :	11	п	11	=:	11
	<sup>205</sup> Pb/ <sup>233</sup> U	299	288	867	927 593	299	310	298	301	305	293	304	900	65	295	291	295	289	295	294	292	295	162	291	283	278	281	288	295	304	562	298	222	82	t v	50	100	707	289	292	293	E0E	292	294	582	767	903 303	294	289	292	292	202	293	295	289	295	902 903	295	296	296	298	54 LG	305	301	303	66Z	305	303	80E	298	304	305	304	202	300	262	57	300	305	294	302	947 266	300	298	298	300
	2SE	82	72	8	73	78	90	84	78	79	75	82	11	59	53	62	60	58	64	61	65	62	69	72	50	59	77	59	95	110	102	110	HOT	511	100	112	63	8 5	59	58	57	57	63	57	59	8	57	74	77	77	80	26 86	80	83	84	89 or	cs 18	87	90	84	93	52	5	55	52	23	40	47	45	48	51	47	51	25	40	48	50	45	43	62	50	44	47	46	43	44
	PP/922 PP	307	250	667	333	303	254	88	316	285	363	312	3.60	356	250	237	313	259	171	311	285	22 I	539	312	202	382	260	326	312	218	268	342	915	857	orc WC	102	080	304	276	297	322	259	289	304	276	167	342	303	320	337	268	216	436	385	281	268	945 050	312	245	268	268	375	240	331	263	342	564 264	286	231	319	312	214	302	167	F67	260	271	293	279	370	268	275 275	247	284	246	250
1	ZSE	0.0009	600000	0.0008	0.0008	0.0009	0.0009	0.0009	0.0009	0.0008	600000	0.0008	60000	00000	00000	600000	0.0010	0.0009	600000	0:0000	600000	600000	0.0010	0.0010		00000	600000	0.0010	0.0010	0.0011	0.0010	0.0011	01000	TINNIN		11000	0,0006	00000	0.0007	0.0006	0.0007	0.0006	0.0006	0.0007	0.0007	00000	0.0006	0.0004	0.0004	0.0004	0.0004	10000	0.0004	0.0005	0.0005	0.0005	00000	0.0004	0.0004	0.0005	0.0006	0,000	0.0009	0.0009	0.0009	60000		00000	0.0009	0.0009	0.0009	600000	0.0008	A0000	00000	0,000	0.0008	0.0009	0.0009	600000	0.0008	0.0008	0.0008	0.0008	0.0008	0.0008
	<sup>ua</sup> Pb/ <sup>44</sup> Th	0.0153	0.0146	0.0147	0.0149	0.0150	0.0152	0.0154	0.0161	0.0152	0.0157	0.0151	0.0145	0.0145	0.0144	0.0144	0.0152	0.0141	0.0144	0.0138	0.0142	0.0141	0.0150	0.0149	0.0148	0.0136	0.0137	0.0143	0.0148	0.0153	0.0147	0.0157	0.0143	6670.0	0.0146	0.0140	0.0146	201010	0.0147	0.0147	0.0151	0.0153	0.0146	0.0147	0.0148	0.0161	1210.0	0.0150	0.0144	0.0149	0.0143	0.0140	0.0152	0.0149	0.0148	0.0149	0.0144	0.0146	0.0145	0.0147	0.0144	0.0155	0.0149	0.0151	0.0152	0.0153	0.0148	0.0151	0.0148	0.0145	0.0148	0.0145	0.0153	0.0140	0.0162	50T0-0	0.0147	0.0156	0.0160	0.0165	0.0148	0.0145	0.0149	0.0153	0.0147	0.0145
	Rho	0.1667	0.4220	0.2521	0.2397	0.3063	0.2874	0.2263	0.3598	0.3139	0.4072	0.2251	+TT7-0	0.2898	0.2838	0.1794	0.3313	0.3314	0.2339	0.2987	0.3458	0.2234	0.2935	0.1239	0.2500	0.2503	0.2094	0.2006	0.1915	0.1720	0.2328	0.2558	0.3452	0.2750	01110	0.0272	0.0431	0.1375	0.1287	0.0668	0.0747	0.0570	0.0373	0.1509	0.1323	61200	0.0786	0.1445	0.1736	0.1528	0.0385	2142.0	0.1764	0.2335	0.1957	0.1860	0.1315	0.1802	0.1881	0.1126	0.1005	0.3935	0.3175	0.2696	0.3261	0.2855	0.3525	0.3572	0.3952	0.3652	0.3621	0.4730	0.2201	0.4077	1/04/0	0.3385	0.3182	0.3158	0.3048	0.2437	0.2554	0.3705	0.3444	0.3240	0.3682	0.3741
Iplot	2SE	0.0024	0.0023	470000	0.0023	0.0024	0.0025	0.0024	0.0024	0.0025	0.0024	0.0024	C20000	0.0011	0.0011	0.0012	0.0012	0.0011	0.0012	0.0012	0.0012	0.0011	0.0012	110000	0001	0.0011	0.0012	0.0011	0.0011	0.0013	0.0012	0.0013	71000	51000	C1000	00014	0.0011	0.0012	0.0011	0.0011	0.0011	0.0012	0.0012	0.0012	0.0011	TTOOOD	0.0012	600000	0.0009	0.0009	0.0010		0.0010	0.0010	600000	0.0011	0100.0	0.0010	0.0010	0.0010	0.0011		0.0019	0.0019	0.0019	6100.0	51000	6100.0	0.0018	0.0018	0.0019	0.0019	0.0019	020000	STOO O	81000	0.0018	0.0019	0.0019	0.0019	0.0019	9T0000	0.0018	0.0018	0.0018	0.0018
r Wetheril	<sup>205</sup> Pb/ <sup>238</sup> U	0.0475	0.0456	0.04/3	0.0465	0.0474	0.0493	0.0474	0.0478	0.0483	0.0465	0.0482	0.0450	0.0463	0.0468	0.0462	0.0469	0.0459	0.0467	0.0467	0.0463	0.0467	0.0472	0.0462	0.0449	0.0442	0.0446	0.0457	0.0468	0.0482	0.0475	0.0474	0.0470	0.0470	0.0469	0.0478	0.0464	0.0466	0.0457	0.0463	0.0464	0.0481	0.0464	0.0466	0.0457	0.0463	0.0481	0.0467	0.0458	0.0463	0.0463	TOMON	0.0465	0.0466	0.0458	0.0469	0.0482	0.0469	0.0470	0.0469	0.0474	0.0488	0.0485	0.0478	0.0482	0.0475	0.0485	0.0481	0.0482	0.0474	0.0483	0.0486	0.0483	0.0468	0.0470	0.0473	0.0467	0.0476	0.0484	0.0466	0.0480	0.0476	0.0476	0.0474	0.0473	0.0476
Data fc	2SE	0.0200	0.0200	0.0200	0.0200	0.0200	0.0210	0.0220	0.0210	0.0220	0.0210	0.0220	0170.0	0.0130	0.0110	0.0120	0.0130	0.0120	0.0130	0.0130	0.0130	0.0130	0.0130	0.0140	0.0120	0.0120	0.0140	0.0130	0.0130	0.0150	0.0140	0.0160	OCTO:O	OCTO:O	0.01000	0.00.60	0.0140	OT M D	0.0140	0.0140	0.0130	0.0140	0.0150	0.0140	0.0140	01/11/10	0.0140	0.0120	0.0120	0.0120	0.0120	0.0100	0.0130	0.0140	0.0130	0.0140	0.0130	0.0140	0.0130	0.0130	0.0140	0.0140	0.0180	0.0190	0.0190	0.0180	0.0100	0.0180	0.0180	0.0180	0.0190	0.0180	0.0160	0/10/0	0.010.0	0.01500	0.0150	0.0150	0.0150	0.0170	0.0160	OSTO O	0.0160	0.0150	0.0150	0.0150
	<sup>207</sup> Pb/ <sup>235</sup> U	0.3398	0.3250	0.33.00	0.3400	0.3376	0.3430	0.3480	0.3440	0.3510	0.3440	0.3510	arce 0	0126.0	0.3327	0.3291	0.3440	0.3270	0.3220	0.3340	0.3350	0.3320	0.3310	0.3380	033300	0.3370	0.3180	0.3370	0.3409	0.3380	0.3360	0.3440	0.1110	0.3230	01000	OTCON	03410	03282	03304	0.3386	0.3405	0.3400	0.3363	0.3381	0.3308	0.3391	0.3430	0.3390	0.3341	0.3398	0.3308	JTCCD	0.3570	0.3484	0.3318	0.3330	0.34450	0.3450	0.3310	0.3367	0.3350	0.3551	0.3451	0.3525	0.3456	0.3468	0.3508	0.3453	0.3472	0.3431	0.3543	0.3392	0.3550	0.3550	51250	19880	0.3344	0.3458	0.3491	0.3476	0.3434	0.3505	0.3368	0.3400	0.3356	0.3379
olot	2SE	0.0019	0.0016	0.0018	0.0017	0.0018	0.0020	0.0020	0.0018	0.0018	0.0018	0.0019	2100 0	100.0	0.0015	0.0018	0.0017	0.0017	0.0018	0.0018	0.0018	0.0018	0.0018	0.0020	2100.0	0.0018	0.0022	0.0018	0.0022	0.0024	0.0023	0.0026	0.0024	C200-0	10000	0.006	0.003	0.001	0.0022	0.0022	0.0021	0.0021	0.0023	0.0021	0.0022	770010	0.001	0.0017	0.0018	0.0018	0.0018	00000	0.0020	0.0020	0.0019	0.0020	0.0018	0.0020	0.0020	0.0019	0.0021	0.0016	0.0016	0.0017	0.0016	0.0017	/100.0	0.0015	0.0014	0.0016	0.0016	0.0014	0.0015	9700.0	5T00.0	0.0014	0.0014	0.0013	0.0013	0.0018	0.0015	2100.0	0.0014	0.0014	0.0013	0.0013
asserburg	<sup>307</sup> Pb/ <sup>206</sup> Pb	0.0525	0.0512	0.0514	0.0531	0.0524	0.0513	0.0538	0.0527	0.0520	0.0538	0.0526	0.0500	60000	0.0514	0.0512	0.0528	0.0513	0.0496	0.0533	0.0522	0.0509	0.0512	0.0526	17500	0.0548	0.0519	0.0533	0.0526	0.0505	0.0516	0.0533	0.0527	2010.0	0.0510	30300	0.0528	0.0530	0.0518	0.0526	0.0530	0.0514	0.0528	0.0530	0.0518	0.0520	0.0514	0.0524	0.0528	0.0532	0.0516	61000	0.0556	0.0543	0.0519	0.0516	0.0512	0.0526	0.0511	0.0516	0.0516	0.0531	0.0512	0.0532	0.0516	0.0540	65500	0.0521	0.0506	0.0533	0.0530	0.0504	0.0528	97500	0.05.40	0.0516	0.0519	0.0525	0.0521	0.0542	0.0522	12500	0.0516	0.0520	0.0516	0.0516
for Tera-W	2SE	1.0637	1.1061	1.072/	1.0637	1.0682	1.0286	1.0682	1.0504	1.0716	1.1100	1.0330	1:050	0.5140	0.5029	0.5617	0.5458	0.5226	0.5498	0.5509	0.5600	0.5037	0.5396	0.5156	0 5454	0.5641	0.6044	0.5267	0.5031	0.5603	0.5328	0.5789	0.55/0	0.1000	0.000	76130	0.5118	0.5532	0.5258	0.5122	0.5100	0.5182	0.5583	0.5533	0.5258	0.5122	0.5180	0.4165	0.4333	0.4297	0.4480	C10450	0.4584	0.4601	0.4485	0.5001	0.4745	0.4552	0.4525	0.4552	0.4900	0.7901	0.8081	0.8316	0.8178	0.8418	1/10/0	0.8226	0.7757	0.8012	0.8161	0.8061	0.8151	0.7005	0.7550	0.8060	0.8243	0.8386	0.8097	0.8753	0.8243	0.8000	0.7938	0.8028	0.8056	0.7958
Data	<sup>238</sup> U/ <sup>205</sup> Pb	21.0526	21.9298	21.141/	21.5054	21.0971	20.2840	21.0971	20.9205	20.7039	21.5054	20.7469	10/2/17	21 6170	21.3812	21.6357	21.3265	21.7960	21.4041	21.4270	21.6029	21.3995	21.2044	21.6497	22.5668	22.6449	22.4417	21.8818	21.3858	20.7598	21.0704	21.1015	01401777	21.2302	21 2701	17/0772	21 5203	21 4781	21.8627	21.5796	21.5332	20.7814	21.5703	21.4731	21.8627	21.5/20	20.7814	21.3950	21.8198	21.6123	21.6029	21 5227	21.5193	21.4500	21.8436	21.3220	21.1327	21.3356	21.2721	21.3356	21.1060	21.4392 20.5086	20.6228	20.9205	20.7469	21.0482	20.7363 20.6186	20.8073	20.7598	21.0971	20.7254	20.5973	20.7125	20.5852	211 7676	21.1640	213995	21.0084	20.6441	21.4638	20.8290	21.1005	20.9996	21.1193	21.1551	21.0261
1	Ŗ	0.51	0.54	0.55	0.55	0.55	0.55	0.54	5.0	0.55	0.54	0.56	0.35	86.0	0.46	0.54	0.46	0.54	0.51	0.53	0.50	0.52	0.51	0.41	0.55	0.45	0.47	0.35	0.37	0.43	0.40	0.39	06-0 6	747	30.00	60	0.0	070	0.38	0.38	0.36	0.37	0.39	0.40	0.38	97.0 26.0	0.37	0.37	0.34	0.35	0.53	80.0	0.39	0.37	0.35	0.36	0.47	0.53	0.52	0.53	0.36	0.30	0.56	0.51	0.55	0.57	0.64	80	0.61	0.57	0.56	0.62	0.55	0.52	50	500	0.50	0.71	0.74	0.55	6.53	0.73 0.66	0.55	0.60	0.66	0.61
:	Identifier	mr30_02123_1	mr30_02123_2	mr30_02123_3	mr30_02123_5	mr30_02123_6	mr30_02123_7	mr30 02123 8	mr30 02123 10	mr30_02123_11	mr30_02123_12	mr30 02123 13	mr30_02123_14	or14 02123 1	oc14 02123 3	oc14 02123 4	oc14 02123 5	oc14_02123_6	oc14 02123 7	oc14_02123_8	oc14 02123 9	oc14_02123_10	oc14 02123 11	oc14 02123 12	0C14 02123 13	oc14 02123 15	oc14 02123 16	oc14 02123 17	oc6_02123_1	oc6_02123_2	oc6_02123_3	oc6_02123_4	000 07173 2	0.000 000 000	000 (6112 0	000 00123 0	OCE (0123-10	OCE 02122 10	oc6 (2123-12	oc6 02123 13	oc6_02123_14	oc6_02123_15	oc6_02123_16	oc6_02123_17	oc6 02123 18	000 00123 19	006 02123 20	oc7_02123_1	oc7_02123_2	oc7_02123_3	oc7 02123 4	00/ 00122 5	007 02123 7	oc7_02123_8	oc7 02123 9	oc7 02123 10	0C/ 02123 11 0C7 02123 12	oc7_02123_13	oc7_02123_14	oc7_02123_15	007_02123_16	60/ W123 1	fe05_02123_2	fe 05_02123_3	fe05_02123_4	fe 05 02123 5	ferce 02123_0	fe05 02123 8	fe05_02123_9	fe 05_02123_10	fe 05_02123_11	fe05_02123_12	fe 05 02123 13	fack (0123 15	facts 00172 15	ferts 02123 10	fe05 02123 18	fe05 02123 19	fe05_02123_20	fe05_02123_21	fe05_02123_22	fack 00123 24	fe05_02123_25	fe05_02123_26	fe05_02123_27	fe 05 02 123 29

# <u>02123 zircon</u>

			Т					T	Γ												Γ			T							Т											Τ			Т	Τ	Т	Π	Т					Π		Т	П	_
6.66	98.9	99.7	102.0	100.2	101.0	9.66	98.4 oo o	100.6	2:00	101.9	98.6 101.6	0.101	101.8	102.7	99.1	100.5	103.6	100.2	98.6	101.5	0.66	99.3	98.8 101 2	98.86	101.2	100.9	9.66	100.9	98.4	9.66	99.3	100.5	91.2 91.2	100.1	29.7	101.7	100.9	99.5	99.8 101.5	99.5	100.2	101.6	2.99.7	97.8	99.2	100.1	100.5	101.4	99.5 98.3	6.66	100.3	102.5	101.5	98.8	100.3	58.6	8.66	102.2
	~									~																																-	_															_
112.3	101.8	110.8	110.1	108.4	116.4	97.2	89.3	112.6	98.1	111.8	96.4	98.2	120.5	148.0	88.5	104.7	119.0	103.6	91.3	101.6	90.7	93.1	91.1	103.5	108.3	121.6	105.6	1001 /	86.7	107.1	93.0	103.6	51.9	103.9	93.7	124.4	105.9	91.7	91.5	106.0	116.2	117.3	114.4	94.2	107.6	101.0	107.4	106.3	98.0	92.0	101.5	139.2	83 1	109.4	107.7	98.3	113.5	131.7
15	16	15	51 K	19	20	19	19	50 50	20	20	21	19	20	20	20	20	7 R	19	20	20	20	20	30	28	28	28	8 8	07 DZ	38	14	13	15	16	14	13	51 ¥	ц Ю	14	15	14	15	15	15	14	14	15	14	14	14	4	11	11	11 01	10	10	10	11	11
287	292	288	9/7	288	288	283	283	293	298	291	301	282	202	293	289	289	262	282	290	295	285	277	304	299	302	300	313	305 305	202	298	284	295	328	278	273	285	296	282	301	291	291	295	306	289	290	297	287	283	290	307	299	304	762	282	288	286	290	300
12	12	12	1	11	11	11	н н	12	12	12	1 1	11	: 1 ::	12	12	E1 5	7 F	11	11	11	1 1	12	19	8	17	18	18	0 0	9 8	14	14	15	4 5	14	14	15	14	14	14	14	14	14	15	14	14	14	14	14	15	74 T	. ~	7	9 9	6	9 ~	, 9	7	9
292	294	293	182	290	290	283	289 276	293	298	289	299 205	283	291	287	295	290	289	288	299	289	281	293	307	293	295	294	303	866	303	298	294	301	313	284	282	289	300	284	288 295	302	289	291	302	304	302	300	294 294	291	301	300	302	296	307	301	297 205	298	294	293
11	11	11	11	11	11	11	11	11	12	12	12	11	11	11	11	11	11	11	11	11	11	12	01 o	n 6	∞	6	10	η σ	n 6	14	13	14	а £1	13	13	14	14	13	14	14	13	14	14	14	14	14	ц £	13	14	CT ~	• ∞	8	/	7	۲ ۲	, r	7	7
292	291	292	280	291	293	282	285 276	2.95	297	294	295	282	202	295	292	291	298	288	295	294 276	278	291	303	290	299	297	302	301	298	297	292	303	286	285	281	294	303	283	287 299	300	289	296	301	298	299	300	295	295	300	209	302	304	300	298	298 206	293	294	299
51	45	49	7	65	64	61	64	57	72	74	12 22	69	65	74	74	F 1	2 12	99	64	69	19	73	87	88	55	65	2 2	20 28	3 22	54	22	8	с 99	60	28	72	6	55	62	63	55 S	28 8	99	8 8	57	8 2	22	99	62	8 %	74	78	2 6	71	39 52	2 2	76	73
260	286	263	04b2	268	252	290	319	262	303	263	306	287	246	199	330	278	241	278	323	289	307	313	333	279	276	244	286	282	344	277	314	292	222	274	300	236	286	308	314	283	249	252	263	316	278	297	304 275	277	306	303	299	218	259	272	316	565	259	227
0.0008	0.0008	0.0008	0.0000	6000'0	0.0010	0.0010	6000.0	0.0010	0.0010	0.0010	0.0010	0,0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0015	0.0014	0.0014	0.0014	0.0015	0.0015	0.0014	0.0007	0.0007	0.0007	0.0008	0.0007	0.0007	0.0007	0.0008	0.0007	0.0007	0.0007	0.0007	0.0007	0.0008	0.0007	0.0007	0.0008	0.0007	0.0007	0.0007	0.0006	0.0005	0.0006	0.0005	0.0005	0.0005	0.0005	0.0005	0.0006
0.0143	0.0146	0.0144	0.0150	0.0143	0.0144	0.0141	0.0141	0.0146	0.0149	0.0145	0.0150	0.0140	0.0145	0.0146	0.0144	0.0144	0.01446	0.0141	0.0145	0.0147	0.0142	0.0138	0.0152	0.0149	0.0151	0.0149	0.0156	0.0152	0.0148	0.0148	0.0141	0.0147	0.0163	0.0138	0.0136	0.0142	0.0148	0.0141	0.0147	0.0145	0.0145	0.0147	0.0152	0.0144	0.0145	0.0148	0.0143	0.0141	0.0145	0510.0	0.0149	0.0151	0.0148	0.0141	0.0144	0.0143	0.0144	0.0150
0.3579	0.3568	0.2102	0.2/23	0.1116	0.1370	0.1844	-0.0981	0.2519	0.1240	0.0894	0.0505	0.1880	0.0663	0.0116	0.0310	0.1193	0.1354	0.1577	0.1439	0.0598	0.1642	0.1303	0.2291	0.2084	0.3481	0.2128	0.1046	0.1847	0.1325	0.1411	0.2356	0.1085	0.1133	0.1033	0.1742	0.0997	0.0484	0.1939	0.1386 0.1161	0.1127	0.2239	0.0618	0.0495	0.1909	0.1450	0.1477	0.1546	0.0560	0.1340	0.3649	0.3830	0.3322	0.3990	0.3956	0.4223	0.3182	0.2823	0.2926
0.0018	0.0018	0.0018	0.0010	0.0018	0.0018	0.0018	0.0018	0.0019	0.0019	0.0019	0.0019	0.0018	0.0018	0.0019	0.0019	0.0018	0.0018	0.0018	0.0019	0.0018	0.0018	0.0019	0.0016	0.0014	0.0014	0.0015	0.0016	0.0015	0.0015	0.0022	0.0022	0.0023	0.0022	0.0022	0.0021	0.0022	0.0023	0.0021	0.0022	0.0023	0.0022	0.0022	0.0022	0.0022	0.0022	0.0022	0.0022	0.0022	0.0022	0.0012	0.0012	0.0012	0.0012	0.0012	0.0012	0.0011	0.0012	0.0012
0.0463	0.0462	0.0463	0.0453	0.0461	0.0466	0.0447	0.0452	0.0468	0.0472	0.0466	0.0468	0.0447	0.0471	0.0468	0.0464	0.0462	0.0455	0.0457	0.0468	0.0466	0.0441	0.0462	0.0482	0.0460	0.0475	0.0470	0.0480	0.04078	0.0474	0.0471	0.0463	0.0481	0.0453	0.0452	0.0446	0.0466	0.0481	0.0448	0.0456	0.0476	0.0459	0.0469	0.0478	0.0473	0.0475	0.0477	0.0469	0.0468	0.0476	0.0476	0.0481	0.0482	0.0476	0.0473	0.0473	0.0465	0.0466	0.0476
0.0160	0.0150	0.0150	0.0150	0,0140	0.0140	0.0140	0.0140	0.0150	0.0160	0.0160	0.0160	0.0150	0.0150	0.0160	0.0150	0.0160	0.0150	0.0150	0.0150	0.0150	0.0150	0.0150	0.0250	0.0230	0.0230	0.0230	0.0240	0.0250	0.0240	0.0180	0.0180	0.0200	0.0200	0.0180	0.0180	0.0190	0.0190	0.0170	0.0180	0.0190	0.0180	0.0180	0.0200	0.0190	0.0180	0.0190	0.0180	0.0180	0.0190	9600'0	0.0086	0.0088	0.0084	0.0080	0.0082	0.0081	0.0086	0.0084
0.3336	0.3359	0.3328	0.3196	0.3323	0.3328	0.3222	0.3303	0.3370	0.3400	0.3310	0.3440	0.3240	0.3290	0.3260	0.3360	0.3300	0.3180	0.3280	0.3430	0.3310	0.3200	0.3340	0.3550	0.3344	0.3393	0.3353	0.3480	0.3440	0.3490	0.3421	0.3358	0.3460	0.3620	0.3234	0.3207	0.3300	0.3429	0.3235	0.3296	0.3462	0.3295	0.3327	0.3470	0.3494	0.3445	0.3440	0.3360	0.3308	0.3480	0.3437	0.3464	0.3388	193391	0.3467	0.3417	0.3422	0.3363	0.3354
0.0015	0.0013	0.0014	2100.0	2100.0	0.0015	0.0015	0.0019	0.0019	0.0021	0.0022	0.0021	0.0021	0.0019	0.0021	0.0022	0.0022	0.0021	0.0020	0.0020	0.0020	0.0020	0.0022	0.0025	0.0023	0.0021	0.0023	0.0024	2200.0	0.0025	0.0014	0.0014	0.0015	0.0019	0.0017	0.0016	0.0015	0.0018	0.0015	0.0017	0.0017	0.0016	0.0015	0.0018	0.0016	0.0015	0.0016	0.0015	0.0016	0.0017	0.0018	0.0017	0.0017	0.0016	0.0016	0.0015	0.0016	0.0017	0.0016
0.0516	0.0523	0.0519	0.0514	0.0523	0.0515	0.0524	0.0531	0.0515	0.0529	0.0517	0.0525	0.0526	0.0512	0.0499	0.0536	0.0519	0.0515	0.0520	0.0531	0.0522	0.0530	0.0536	0.0531	0.0519	0.0523	0.0514	0.0526	0.0526	0.0531	0.0523	0.0530	0.0525	0.0587	0.0524	0.0530	0.0513	0.0520	0.0527	0.0530	0.0525	0.0515	0.0515	0.0517	0E30.0	0.0519	0.0525	0.0519	0.0520	0.0529	0.0524	0.0523	0.0505	0.0514	0.0517	0.0518	0.0523	0.0514	0.0507
5 0.8382	0.8422	3 0.8408	0.8/60	0.8470	7 0.8303	4 0.9005	7 0.8818	3 0.8660	5 0.8521	0.8742	5 0.8675	0.9005	5 0.8128	8 0.8690	3 0.8840	0.8422	4 0.8710	3 0.8638	3 0.8664	2 0.8289 7 0.8274	2 0.9268	0.8890	0.6887	1 0.6616	9 0.6213	0.6790	3 0.6944	0.65.65	0.6676	4 0.9909	3 1.0249	3 0.9958	9 1.0726	5 1.0787	5 1.0557	2 1.0131	7 0.9937	4 1.0477	9 1.0603 3 0.9738	8 1.0134	1.0433	0.9933	0.9629	0.9850	8 0.9742	5 0.9681	1 1.0010	4 1.0066	8 0.9693	1 0.5305	3 0.5195	7 0.5157	0.5292	1 0.5366	7 0.5359	0.5081	2 0.5526	5 0.5307
21.579	21.631	21.612	22.060	21.692	21.477	22.366	22.133	21.349	21.177	21.450	21.367	22.366	21.249	21.385	21.570	21.631	21.997	21.905	21.353	21.459	22.691	21.631	20.746	21.739	21.065	21.276	20.833	21.422	21.097	21.222	21.584	20.807	22.079	22.143	22.421	21.459	20.785	22.336	21.953	20.990	21.777	21.312	20.920	21.159	21.043	20.977	21.331	21.390	20.990	21.026	20.807	20.729	20.999	21.146	21.132	21.491	21.459	21.030
30 0.60	31 0.63	32 0.60	33 U.51	2 0.54	3 0.53	4 0.51	5 0.55 6 0.57	7 0.54	8 0.53	0 0.50	10 0.51	12 0.50	13 0.53	14 0.54	15 0.50	16 0.55	1/ 0.5b 18 0.49	19 0.56	20 0.57	21 0.53	23 0.51	_24 0.50	1 0.52 2 0.56	3 0.59	4 0.67	5 0.60	- 0.60	10.0 ×	09.0	10 0.63	11 0.63	12 0.58 13 0.56	14 0.60	15 0.57	16 0.57	17 0.54 18 0.50	19 0.52	20 0.53	21 0.50	23 0.57	24 0.54	26 0.57	27 0.57	29 0.53	30 0.57	31 0.55	32 U.54 33 0.54	34 0.57	35 0.56	1 0.56	2 0.60	3 0.59	-4 0.62 5 0.56	6 0.61	-7 0.61 • 0.57	09.0	10 0.61	11 0.53
fe05_02123_	fe05_02123_	fe05_02123	TeU5_02123	mr20_02123	mr20_02123	mr20_02123	mr20_02123	mr20_02123	mr20 02123	mr20_02123	mr20_02123	mr20_02123	mr20_02123	mr20_02123	mr20_02123	mr20_02123	mr20_02123	mr20_02123	mr20_02123_	mr20_02123	mr20_02123	mr20_02123	mr19_02123	mr19_02123	mr19_02123	mr19_02123	mr19_02123	mr19 02123	mr19_02123	mr19_02123_	mr19_02123	mr19_02123	mr19 02123	mr19_02123	mr19_02123	mr19_02123	mr19_02123	mr19_02123	mr19_02123	mr19_02123_	mr19_02123	mr19_02123	mr19_02123	mr 19_02123	mr19_02123	mr19_02123	mr19_02123	mr19_02123	mr19_02123	in 13_02123	jn 13_02123	jn 13_02123	in 13_02123	jn 13_02123	jn 13_02123 in 13_02123	in 13_02123	jn13_02123_	jn13_02123_
02123	zircon	continued																																																								
-------	--------	-----------																																																								

101.9	100.4	100.6	0.99.0	103.2	100.2	100.8	101.5	100.2	0.99	5'66	98.5	96.8	100.9	8.86	99.2	96.8	99.7	97.9	96.8	101.9	98.6	102.0	99.1	98.1	99.4	5'66	1.99.1	99.9	101.7
121.0	105.0	103.9	88.6	110.3	102.5	114.1	118.6	118.0	93.9	89.6	98.5	84.8	105.5	95.0	90.9	83.0	94.7	83.2	83.2	110.6	85.5	117.8	90.6	83.8	99.2	96.8	86.1	92.5	108.3
10	11	11	11	14	14	14	14	14	13	14	14	14	15	15	15	15	16	14	14	16	16	15	15	15	14	16	16	16	16
285	299	303	290	298	297	294	293	294	288	282	291	290	303	295	276	294	293	289	291	295	285	282	279	284	280	287	288	292	293
9	9	9	7	8	6	6	8	8	8	6	6	6	6	6	6	10	10	6	6	10	11	9	10	6	6	10	10	10	10
297	299	295	302	291	297	293	292	289	296	296	303	303	294	300	285	311	300	301	294	291	300	294	297	295	289	295	297	293	285
7	7	7	7	8	8	8	8	8	8	6	8	8	6	8	8	9	6	9	8	6	9	9	6	8	6	6	6	6	6
302	300	296	299	300	297	295	296	290	293	295	298	293	297	296	283	301	299	295	284	296	296	300	294	290	287	293	294	292	290
72	70	75	72	75	75	80	76	11	78	81	74	80	84	82	87	84	91	84	76	68	93	85	6	85	83	96	68	91	6
250	285	285	337	272	290	259	250	245	312	329	303	346	281	312	312	363	316	354	342	268	346	254	325	346	290	303	342	316	268
0.0005	0.0005	0.0005	0.0005	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0007	0.0008	0.0008	0.0007	0.0008	0.0008	0.0007	0.0007	0.0008	0.0008	0.0008	0.0008	0.0007	0.0007	0.0008	0.0008	0.0008	0.0008
0.0142	0.0149	0.0151	0.0145	0.0149	0.0148	0.0146	0.0146	0.0147	0.0143	0.0141	0.0145	0.0144	0.0151	0.0147	0.0138	0.0146	0.0146	0.0144	0.0145	0.0147	0.0143	0.0140	0.0139	0.0141	0.0139	0.0143	0.0144	0.0145	0.0146
0.3027	0.4073	0.2486	0.4323	0.3684	0.2719	0.2560	0.3480	0.2662	0.3453	0.4094	0.3270	0.2454	0.3515	0.2754	0.2457	0.2967	0.2855	0.1071	0.4033	0.3160	0.0543	0.3258	0.2474	0.3050	0.3746	0.0334	0.2178	0.4039	0.1738
0.0012	0.0011	0.0012	0.0012	0.0013	0.0013	0.0013	0.0013	0.0013	0.0013	0.0014	0.0014	0.0013	0.0014	0.0013	0.0014	0.0014	0.0015	0.0014	0.0013	0.0014	0.0015	0.0014	0.0014	0.0014	0.0014	0.0014	0.0014	0.0014	0.0014
0.0480	0.0476	0.0470	0.0474	0.0477	0.0472	0.0468	0.0470	0.0460	0.0465	0.0467	0.0474	0.0466	0.0471	0.0470	0.0449	0.0479	0.0474	0.0468	0.0451	0.0470	0.0469	0.0476	0.0467	0.0460	0.0456	0.0466	0.0467	0.0464	0.0461
0.0084	0.0086	0.0081	0.0090	0.0110	0.0120	0.0110	0.0110	0.0100	0.0110	0.0120	0.0110	0.0120	0.0120	0.0120	0.0120	0.0130	0.0130	0.0120	0.0120	0.0130	0.0140	0.0120	0.0140	0.0120	0.0120	0.0130	0.0140	0.0130	0.0130
0.3403	0.3418	0.3364	0.3457	0.3345	0.3410	0.3346	0.3340	0.3296	0.3383	0.3390	0.3480	0.3478	0.3370	0.3427	0.3229	0.3600	0.3450	0.3467	0.3343	0.3360	0.3480	0.3380	0.3430	0.3409	0.3312	0.3390	0.3430	0.3380	0.3270
0.0016	0.0016	0.0017	0.0017	0.0017	0.0017	0.0018	0.0017	0.0017	0.0018	0.0019	0.0017	0.0019	0.0019	0.0019	0.0020	0.0020	0.0021	0.0020	0.0018	0.0020	0.0022	0.0019	0.0021	0.0020	0.0019	0.0022	0.0021	0.0021	0.0021
0.0512	0.0520	0.0520	0.0532	0.0517	0.0521	0.0514	0.0512	0.0511	0.0526	0.0530	0.0524	0.0534	0.0519	0.0526	0.0526	0.0538	0.0527	0.0536	0.0533	0.0516	0.0534	0.0513	0.0529	0.0534	0.0521	0.0524	0.0533	0.0527	0.0516
0.5215	0.4849	0.5425	0.5341	0.5709	0.5838	0.5933	0.5888	0.6152	0.6017	0.6408	0.6229	0.5989	0.6308	0.5890	0.6951	0.6109	0.6676	0.6384	0.6400	0.6338	0.6819	0.6176	0.6417	0.6616	0.6733	0.6455	0.6411	0.6505	0.6599
20.8464	20.9952	21.2630	21.0971	20.9556	21.1909	21.3630	21.2811	21.7533	21.5146	21.3950	21.0926	21.4638	21.2269	21.2857	22.2816	20.8899	21.0971	21.3538	22.1877	21.2766	21.3220	21.0040	21.4087	21.7391	21.9298	21.4731	21.3995	21.5564	21.7108
0.58	0.61	0.61	0.62	0.60	0.60	0.60	0.62	0.61	0.61	0.54	0.55	0.60	0.48	0.38	0.36	0.43	0.38	0.67	0.60	0.45	0.36	0.36	0.35	0.35	0.34	0.33	0.34	0.34	0.37
jn13_02123_12	jn13_02123_13	jn13_02123_14	jn13_02123_15	jn26_02123_1	jn26_02123_2	jn26_02123_3	jn26_02123_4	jn26_02123_5	jn26_02123_6	jn26_02123_7	jn26_02123_8	jn26_02123_9	jn26_02123_10	jn26_02123_11	jn26_02123_12	jn26_02123_13	jn26_02123_14	jn26_02123_15	jn26_02123_16	jn26_02123_17	jn26_02123_18	jn26_02123_19	jn26_02123_20	jn26_02123_21	jn26_02123_22	jn26_02123_23	jn26_02123_24	jn26_02123_25	jn26_02123_26

%Concordancy (206Pb-238U	age/207Pb-235U age) *100	100.9	100.7	102.9	101.7	102.2	100.4	101.2	101.1	102.0	101.1 99.5	100.8	0.99	103.0 98.7	200	99.5	98.6	101.0	95.9	101.3	98.4	100.4	102.0	100.5	98.9	98.6	98.8	97.0 a7 1	98.3	97.5	98.9	97.9	90.0 000	6:66	100.0	2.99.7	98.5	102.6	101.8	98.7	8.69 0.60	96.7	101.8	101.3	101.7	100.6	100.9	102.1	101.3	100.2	101.3	102.4	99.5	101.9	100.8	99.2	100.9	100.5	99.4	98.5	97.8 98.8	103.3
% Concordancy (206Pb-238U	age/207Pb-206Pb age)*100	101.6	100.8	104.8	102.8	103.3	100.5	101.8	101.9	103.5	102.2 99.6	101.1	98.5	105.5 98.6	99.6	99.4	97.9	101.8	93.4	101.8	97.6	100.4	102.8	100.5	98.2	98.0	98.1	95.1 oc.2	0.79	96.6	98.7	96.7	100.4	100.4	100.5	98.7	1.79	22	103.0	98.4	100.1	95.4	102.4	101.5	102.6	100.4	101.5	101./	102.2	100.2	102.1	103.8	99.5	103.0	101.4	99.4	102.1	101.2	99.1	96.7	96.8 98.1	105.2
	2SE	210	200	210	200	210	200	200	200	200	210	210	180	170	170	170	220	210	220	260	210	240	380	250	240	210	210	210	230	300	340	320	340	310	310	160	150	150	150	150	150	140	140	140	110	250	110	110	120	110	150	160	150	150	170	150	150	170	170	260	180	190
	<sup>208</sup> Pb/ <sup>232</sup> Th	3901	3732	3894	3630	3569	3747 3683	3820	3733	3759	3922	3962	3732	3944	3458	3587	3809	3685	3645	4427	3720	3967	5800	4488	4085	3608	3556	3582	3944	3370	3957	3753	3937	3655	3602	3563	3409	3724	3676	3818	3849	3528	3517	3630	3845	5100	3827	3840	4175	3728	3732 3638	3920	3614	3647	3962	3622	3678	3592 3651	3544	4340	3701	3995
	2SE	56	8 ×	2	27	3 89	27	49	48	53	49	<del>1</del>	40	45	4	4	æ	ж ғ	7 F	8 R	33	¥	47	<del>3</del> %	55	32	8	75 A	5 8	25	62	8	86	8 8	61	49	<del>8</del> 6	6 14	47	89	8	46	47	47	÷ 🕄	24	я ;	51 F	14	17	х х	រង	- 72	56	ধ দ	8	25	55 F	ទ	25 5	8 8	¥ 8
sa	<sup>207</sup> Pb/ <sup>235</sup> U	3479	3475 3518	3526	3514 2500	3475	3499	3484	3484	3522	3518 3490	3481	3455	3530	3460	3472	3468	3497	3402	3480	3449	3464	3486	3476	3474	3457	3461	3409	3447	3458	3479	3444	3502	3488	3481	3455	3425 3420	3531	3510	3455	3484 3475	3433	3498	3481	3501	3512	3502	3484	3516	3471	3497 3480	3518	3449	3495	3503	3490	3518	3454 3476	3451	3422	3450	3546
Dat	ZSE	60	58		63	110	62 76	100	001	110	01 01	001	100	011	90	100	100	0 <u>1</u>	66 66	110	100	100	140	110	100	100	100	00	90	110	81	85	88 6	78	79	130	071	130	120	120	120	120	130	120	64	84	65	64	66	99	73	76	74	73	79	75	77	130	130	160	130	140
	<sup>206</sup> pb/ <sup>238</sup> U	3512	3501	3630	3572	3552	3513	3525	3453	3594	3558 3471	3510	3422	3637	3451	3454	3420	3531	3262	3525	3395	3478	3555	3493	3435	3407	3421	3307	3389	3371	3441	3372	3500	3486	3482	3445	33/3	3623	3572	3410	34/8	3318	3562	3525	3559	3532	3534	3529	3562	3477	3542 3534	3601	3431	3562	3532	3461	3551	3472 3546	3431	3370	3375 3434	3664
	2SE	18	16	21	19	32	20	18	18	17	15	16	15	13	14	13	11	12	11	16	11	17	27	18	16	14	16	16	15	45	26	25	27	24	24	22	17	6	10	12	10	10	12	6	36	45	36	37	37	37	92 50	9	40	40	40	40	40	33	3 66	51	30	31
	<sup>07</sup> Pb/ <sup>206</sup> Pb	3458	3472	3465	3474	3439	3495 3483	3462	3472	3474	3483	3473	3474	3448 3478	3464	3474	3494	3469	3493	3462	3478	3464	3457	3474	3499	3476	3486	3478	3495	3489	3488	3487	3486	3471	3465	3489	34/4	3478	3469	3466	34/3 3480	3479	3478	3472	3469	3517	3481	34/1	3485	3469	3471	3470	3448	3460	3482	3483	3477	3429 3433	3462	3486	3486	3483
	ZSE	0.0130	0.0120	0.0130	0.0120	0.0120	0.0120	0.0120	0.0120	0.0120	0.0120	0.0130	0.0110	0.0120	0.0097	0.0100	0.0130	0.0130	0.0120	0.0160	0.0130	0.0140	0.0250	0.0160	0.0150	0.0120	0.0120	0.0120	0.0140	0.0180	0.0200	0.0190	0.0200	0.0180	0.0180	0.0094	0.0084	0.0089	0.0089	0.0093	4600.0	0.0084	0.0084	0.0087	0.0065	0.0170	0.0067	0.0067	0.0074	0.0064	0.0089 n nn88	0.0096	0.0089	0.0088	0.0000	0.0088	0.0089	0.0099	0.0099	0.0160	0.0100	0.0110
	<sup>28</sup> Pb/ <sup>232</sup> Th	0.2131	0.2027	0.2126	0.1970	0.1933	0.2038	0.2080	0.2027	0.2042	0.2140	0.2167	0.2028	0.2157	0.1867	0.1944	0.2074	0.2002	0.1977	0.2448	0.2020	0.2168	0.3320	0.2486	0.2244	0.1956	0.1925	0.1941	0.2157	0.1816	0.2162	0.2040	0.2150	0.1982	0.1951	0.1930	0.1835	0.2024	0.1992	0.2081	0.2136	0.1907	0.1901	0.1967	0.2094	0.2910	0.2086	0.2095	0.2297	0.2026	0.2030 n 1975	0.2137	0.1960	0.1977	0.2005	0.1962	0.1994	0.1945 ^ 1985	0.1914	0.2400	0.2004	0.2186
ľ	Rho	0.6451	0.6809	0.6474	0.6988	0.7636	0.6772	666970	0.7186	0.7523	0.7567	16/7.0	0.7090	0.7442	0.7366	0.8016	0.6788	0.5059	0.877	0.7849	0.7194	0.5788	0.8603	0.7641	0.6275	0.6098	0.5173	0.7370	0.6325	0.5682	0.5910	0.6891	0.6450	0.5481	0.5612	0.5730	0.6380	0.6063	0.5216	0.7465	0.7239	0.7289	0.4668	0.5513	0.6809	0.5444	0.6432	0.6617	0.6695	0.6725	0.6819 0.7362	0.6921	0.6232	0.6550	0.7038	0.6748	0.6573	0.5527 n.6096	0.6352	0.6452	0.6248	0.5933
plot	2SE	0.0160	0.0160	0.0180	0.0170	0.0280	0.0170	0.0280	0.0280	0.0290	0.0280	0.0280	0.0270	0.0300	0.0270	0.0270	0.0270	0.0280	0570 0	0.0290	0.0270	0.0280	0.0360	0.0300	0.0270	0.0270	0.0270	0.0260	0.0270	0.0290	0.0220	0.0220	0.0230	0.0210	0.0210	0.0340	0.0320	0.0340	0.0340	0.0320	0.0330	0.0310	0.0340	0.0330	0.0170	0.0230	0.0180	0.01/0	0.0180	0.0170	0.0200	0.0210	0.0200	0.0200	0.0200	0.0200	0.0210	0.0350 ^ / /370	0.0360	0.0420	0.0350	0.0380
r Wetherill	<sup>206</sup> pb/ <sup>238</sup> U	0.7250	0.7232	0.7590	0.7410	0.7350	0.7270	0.7280	0.7320	0.7480	0.7390	0.7220	0.7012	0.7540	0.7088	0.7095	0.6994	0.7296	0.6921	0.7270	0.6934	0.7155	0.7390	0.7190	0.7041	0.6963	0.7010	0.6705	0.6920	0.6900	0.7050	0.6900	0.7220	0.7180	0.7150	0.7080	0.68/0	0.7531	0.7404	0.6981	0.7047	0.6738	0.7380	0.7281	0.7390	0.7320	0.7310	0.7430	0.7400	0.7150	0.7320	0.7520	0.7050	0.7370	0.7280	0.7110	0.7360	0.7150	0.7030	0.6850	0.6880	0.7620
Data fo	2SE	0.7900	0.7800	0.8800	0.8500	1.2000	0.8400	1.5000	1.5000	1.6000	1.5000	1.5000	1.2000	1 2000	1,2000	1.2000	0.9800	1.0000	001510	1.0000	0.9700	1.0000	1.4000	1.1000	1.0000	0.9700	0.9800	0.9600	0.9800	1.9000	1.9000	1.9000	2.0000	1,9000	1.9000	1.5000	1.4000	1,5000	1.5000	1.4000	1.4000	1.4000	1.5000	1,4000	0.4100	0.7500	0.4200	0.4100	0.4500	0.4300	0.7600	0.8100	0.7400	0.7800	0./800	0.8000	0.7900	1 6000	1.6000	1.8000	1.6000	1.7000
	<sup>207</sup> Pb/ <sup>235</sup> U	29.7900	30 9900	31.3100	30.8900	29.5600	30.5500	29.9600	30.6300	31.2500	30.9400	29.9000	29.1300	31.2900	29.2700	29.5100	29.4600	30.3200	28.6400	29.7400	28.9000	29.4100	30.1000	29.7900	29.6200	29.1000	29.2500	27.8100	28.8600	29.2000	29.8000	28.8300	30.5400	30.0600	29.8500	29.1300	28.2400	31.3800	30.7100	29.0800	29.6800	28.3800	30.4000	29.8300	30.5500	30.8000	30.4300	30.0900	30.9500	29.5200	30.3500 29 9600	31.0400	28.9100	30.2800	30.5300	30.2200	30.8900	28.9800	29.0400	28.2000	28.9400 79.6800	31.8900
lot	2SE	0.0054	0.0053	0.0059	0.0056	0.0072	0.0057	0.0062	0.0062	0.0062	0.0060	0.0060	0.0049	0.0052	0.0048	0.0047	0.0064	0.0064	con0.0	0.0067	0.0064	0.0068	0.0079	0/00/0	0.0069	0.0066	0.0068	0.0066	0.0068	0.0130	0.0100	0.0100	0.0100	660000	0.0099	0.0052	0.0044	0.0034	0.0035	0.0037	0.0035	0.0035	0.0037	0.0034	0.0070	0.0091	0.0071	0/00/0	0.0073	0.0072	0.0075	0.0078	0.0077	0.0076	0.0078	0.0079	0.0077	0.0053	0.0058	0.0100	0.0056	0.0061
asserburg p	<sup>607</sup> Pb/ <sup>206</sup> Pb	0.2978	0.3008	0.2994	0.3013	0.2913	0.3047	0.2978	0.3002	0.3017	0.3029	0.3004	0.3002	0.2962	0.2993	0.3009	0.3045	0.2990	0.3049	0.2982	0.3015	0.2988	0.2969	0.3011	0.3058	0.3014	0.3035	0.3018	0.3051	0.3063	0.3037	0.3016	0.3039	0.3003	0.2998	0.3039	0.3014	0.3016	0.2998	0.2994	0.3008	0.3020	0.3015	0.3004	0.2997	0.3092	0.3021	0.3001	0.3028	0.2998	0.3001 n 2961	0.3000	0.2957	0.2980	0.3023	0.3024	0.3013	0.2922 n 7929	0.2984	0.3030	0.3030	0.3024
for Tera-W	2SE	0.0304	0.0306	0.0312	0.0310	0.0518	0.0322	0.0528	0.0523	0.0518	0.0513	0.0537	0.0549	0.0528	0.0537	0.0536	0.0552	0.0526	0/5/00	0.0549	0.0562	0.0547	0.0659	0.0580	0.0545	0.0557	0.0549	0.0578	0.0564	0.0609	0.0443	0.0462	0.0441	0.0407	0.0411	0.0678	0.0671	0.0599	0.0620	0.0657	0.0645	0.0683	0.0624	0.0622	0.0311	0.0429	0.0337	0.03/21	0.0329	0.0333	0.0373 n n393	0.0371	0.0402	0.0368	0.03/b	0.0396	0.0388	0.0685 n n689	0.0728	0.0895	0.0739	0.0654
Data	<sup>238</sup> U/ <sup>206</sup> Pb	1.3793	1.3827	1.3175	1.3495	1.3605	1.3755	1.3736	1.3661	1.3369	1.3532	1.3850	1.4261	1.3263	1.4108	1.4094	1.4298	1.3706	1.4449	1.3755	1.4422	1.3976	1.3532	1.3908	1.4203	1.4362	1.4265	1.4912	1.4451	1.4493	1.4184	1.4493	1.3850	1.3928	1.3986	1.4124	1.4556	1.3278	1.3506	1.4325	1.4190	1.4841	1.3550	1.3734	1.3532	1.3661	1.3680	1.3/30	1.3514	1.3986	1.3661	1.3298	1.4184	1.3569	1.3550	1.4065	1.3587	1.3986	1.4225	1.4599	1.4535	1.3123
:	- N/H	0.40	0.31	0.30	0.56	0.79	0.51	0.46	0.54	0.61	0.51	0.58	0.84	0.51	0.74	0.78	1.04	0.56	101	0.65	0.79	0.50	0.75	0.86	0.53	0.52	0.96	0.68	0.65	0.62	0.87	0.88	0.76	0.81	0.95	0.46	0.68	0.59	0.57	0.73	0.78	0.83	0.91	0.81	0.94	0.42	0.44	0.77	0.57	0.67	0.85 0.64	0.52	0.74	0.78	1/10	0.88	0.81	0.95 n ag	0.83	0.07	0.59	1.06
:	Identifier	Z0G1_1_0C14	Z0G1_2_0C14 Z0G1_3_0C14	Z0G1_4_oc14	Z0G1_5_0C14	Z0G1_7_0C14	Z0G1 8_oc14 Z0G1 9_oc14	ZOG1 1 fe05	Z0G1_3_fe05	Z0G1_4_fe05	ZOG1_5_fe05 ZOG1_6_fe05	Z0G1_7_fe05	Z0G1_8_fe05	ZOG1 9 fe05 ZOG1 10 fe05	ZOG1 11 fe05	Z0G1_12_fe05	z_0G1_1_mr20	Z_0G1_2_mr20	7 061 4 mr 20	Z 0G1 5 mr 20	Z_0G1_6_mr20	Z_0G1_7_mr20	Z 0G1 8 mr20	2 061 10 mr20	.0G1_11_mr20	2_0G1_12_mr20	0G1 13 mr20	2 0G1 14 mr20	061 16 mr20	Z0G1_1_mr19	Z0G1_2_mr19	Z0G1_3_mr19	Z0G1 4 mr19	ZOG1 6 mr19	Z0G1_7_mr19	Z0G1_8_mr19	2061_9_mr19	2061 11 mr 19	Z0G1_11_mr19	Z0G1_11_mr19	2061 11 mr19 2061 11 mr19	Z0G1_11_mr19	Z0G1_11_mr19	Z0G1_11_mr19 Z0G1_11_mr19	061 1 jn13	0G1_2_n13	061_3_jn13	061 5 in13	0G1_6_n13	0G1_7_in13	0G1_1_n26	061_3_n26	0G1_4_In26	0G1_5_in26	061_6_n26	0G1_8_In26	0G1_9_n26	OG1 1 mr30	0G1_3_mr30	0G1_4_mr30	OG1 5 mr30	0G1_7_mr30

# OG-1 zircon

_																																_		_	_	_						_						_	_	_			_	_			_	_	_	_	_	_	_	_		_	_	_	_	_	_	_
%Concordancy (206Pb-238U	age/207Pb-235U age)*100	100.9	99.9	101.2	1.001	99:66 1.00 E	99.5	100.6	100.7	99.3 101 2	98.4	96.8	98.2	99.0	101.4	99.4	100.0	101.0	98.9	100.6	100.2	100.5	00.0	90.1	99.4	6'66	99.8	99.7	100.1	99.8	99.8	98.6	00 2	100.8	100.2	99.7	99.6	98.7	39.2 98.8	38 r.	99.2	9366	101.1	99.0	101.2	36./ 99.5	101.4	100.0	100.0	101.2	100.7	99.5	100.5	98.8 2.5	38.6	99.5	100.1	99.7	100.2	5.95 7.99	100.3	96.3	101.3	98.3	101.0	99.5 02.7	36.z 101.1	100.6	98.9	6.69	8/./	36.0
% Concordancy (206Pb-238U	age/207Pb-206Pb age)*100	111.7	104.2	115.7	32.2	99.99	102.2	115.5 27.5	97.5	96.1	27.707	84.2	88.6	27.7	109.0	39.66	104.4	105.3	98.7	106.3	108.8	113.2	11015	C.001	104.0	100.9	98.8	97.5	111.5	111.1	105.1	91.8		103.2	106.6	101.2	99.5	93.5	016	0.00	96.7	94.3	111.9	96.8	123./ 05.3	0.99	111.7	114.7	99.2	112.7	9/.4 104.3	103.2	106.2	107.4	0:40 886	95.6	97.7	94.7	96.1	105.U 95.3	102.5	81.5	103.7	94.6	104.6	106.8	91.7 108.6	107.1	95.0	93.5	51.1 00.7	34.1
	2SE	3 2	25	33	2 22	23	53	33	54	24	2 2	11	13	12	17	: =	15	13	15	21	8	12	77	21	12	22	20	19	18	19	22	57	5	3	24	26	25	26	2 2	ж	24	25	24	8	\$	37	8	36	18	17	29 E	8	19	81 Ç	el 8	19	19	17	14	14	17	8	17	89	81 %	20	7 8	12	8	21	85	77
	<sup>%</sup> Pb/ <sup>232</sup> Th	341	376	336	341	343	336	334	340	349	353	381	346	333	353	330	334	340	326	341	333	336	241	330	337	367	351	337	327	342	354	332	565	352	352	365	351	373	328	385	344	350	349	351	330	370	367	361	361	345	359	370	366	355	351	331	337	333	355	351	340	353	343	337	336	345	349	354	344	360	633 246	340
	2SE 26	0 00	6	6	n o	6 0	0 00	10	1 01	10	9 0	6	6	6	م م	6	6	6	10	15	14	÷ ۲	d t	a f	14	13	13	13	12	12	9	01 6	3 5	19	10	10	11	11	9 6	2 E	10	11	10	19	19	2 2	61	19	15	14	ม ม	15	15	15	14	14	14	15	5	n ر.	, «	8	••	80	6	ь «	8 16	16	16	17	16	0T
	7pb/ <sup>235</sup> U	336	361	345	346	347	335	333	335	343	351	345	341	343	330	688	334	329	336	346	344	351	361	353	347	360	353	351	347	351	332	333	248	343	344	350	350	356	575 576	357	349	351	348	345	340	354	349	345	358	351	35	356	352	349	jije	337	336	340	351	352	346	353	342	346	343	346	232	336	349	351	397	240
Dates	2SE 20	0	8		0 00	00 F	~ 80	80 O			• •	9	9	9 1	, -	9	7	9	7	13	13 13	EI C	d 6	4 E	ព	14	13	13	13	13	12	11 ;	4 6	i El	13	13	13	13	1 6	4 6	13	13	13	10	01 0	9	1 01	10	16	16	16	16	16	15	а н	15	15	15		20 00	, 61	6	10	6	10	01 ¢	10 16	17	17	17	17	1/1
	<sup>5</sup> Pb/ <sup>238</sup> U	339	361	349	347	346	333	335	337	341	52 57	334	335	340	595 595	337	334	333	333	349	345	352	350	350	8 <del>1</del>	359	352	350	347	350	331	329	346	346	344	349	348	352	325	351	346	350	352	342	344	352	354	345	358	355	\ <del>3</del>	354	354	345	ŧ	336	336	339	351	352	347	340	347	340	347	344	343	388	345	351	348	340
	2SE 200	8 8	43	42	4	66 8	90 40	8 5	88	58 6	88	30	35	R 2	\$ 9	8	43	37	43	34	8	R 7	ħ 5	5 6	31	35	33	33	28	31	ж :	99 99	S 17	36	36	34	40	37	R 8	3 6	37	36	36	41	4/	47	47	50	38	8	30	32	32	36	8 8	36	34	35	65	37 E9	5	61	64	8	58 5	2 G	79 295	25	20	25 E	33 5	\$
	b/ <sup>206</sup> Pb	303	346	302	329	346	326	290	346	354	384	396	378	348	30/ 315	338	320	316	337	328	317	311	217	346	331	356	356	359	311	315	315	358	101	335	323	345	350	376	357	387	358	371	314	353	2/2	356	317	301	361	315	338	343	333	321	345	351	344	358	366	342	339	417	334	359	331	322	3/8 316	316	363	375	189	30/
$\left  \right $	2SE 207	0011	0013	0012	0012	0012	0012	0012	0012	0012	0012	9000	2000	9000	000	9000	8000	0007	0007	0010	0010	1100	1100	0100	0010	0011	0010	0010	6000	0010	0013	2100	7100	0013	0012	0013	0013	0013	1100	0013	0012	0012	0012	0018	/100	6T 00	0018	0018	6000	6000	6000	0010	0010	6000	6000	0011	6000	6000	0007	000/	6000	6000	6000	6000	6000	0010	0009 0010	0010	0010	0011	0019	1 01100
	4L-0/0	0 0170	0188 0	0168 0	0170 0	0171 0	0168 0	0167 0	0170 0	0174 0	0176 0	0191 0	0173 0	0166 0	0 9210	0165 0	0167 0	0169 0	0163 0	0170 0	0166 0	0168 0	0 0210	0 0110	0168 0	0183 0	0175 0	0168 0	0163 0	0171 0	0176 0	0166 0	1046 0	0176 0	0176 0	0182 0	0175 0	0186 0	0 164 0	0119.2	0172 0	0175 0	0174 0	0175 0	0165 0	0185 0	0183 0	0180 0	0180 0	0172 0	0 1/10	0185 0	0183 0	0177 0	0 122	0163 0	0168 0	0166 0	0177 0	01/5 v	0170 0	0176 0	0171 0	0168 0	0168 0	0172 0	016/ 0	0177 0	0172 0	0180 0	0318 U	01/3 J v
502	d q	682 0.	491 0.	243 0.	577 0.	188 0.0	104 0.	836 0.	932 0.	300	268 0.	865 0.	569 0.	271 0.	820 0.	164 0.	231 0.	126 0.	155 0.	781 0.	094 0.	397 0.	562 0.	735 0	876 0.	501 0.	059 0.	845 0.	932 0.	357 0.	759 0.	522 U.	184	759 0.	993 0.	480 0.	559 0.	691 0.	579 0.	778	053 0.	505 0.	806 0.	556 0.	400 0.1	419 0.	468 0.	391 0.	953 0.	785 0.	380 0.	620 0.	943 0.	0.08 0.0	694 0.	305 0.	.0 086	0.094 0.0	830 0.	0 889 U	933 0.	572 0.	315 0.	437 0.	851 0.	109 0.1	985 0.	429 0.	308 0.	324 0.	368 U.	0/4 J v.
	SE	0.12 0.4	013 0.3	013 0.4	013 0.3	013 0.5	012 0.4	013 0.4	013 0.3	013 0.5	013 0.4	010 0.2	010 0.2	010 0.3	20 TTO	010 0.2	011 0.2	010 0.3	0011 0.3	022 0.5	0.6	0.22 0.5	1200	N21 0.4	021 0.5	023 0.5	0.022 0.5	021 0.4	021 0.5	021 0.5	020 0.1	020 0.2	100	0.1	0.1 0.1	021 0.2	021 0.0	0.1 0.1	2.0 02.0	N21 0.1	021 0.2	021 0.2	021 0.1	016 0.3	0.16 0.1 0.16 0.3	2'0 2T00	017 0.3	017 0.3	0.1	0.26 0.2	0.26 0.1	0.1	0.1	0.1	0.1 0.1	025 0.2	0.1	025 0.2	014 0.4	013 U.4	016 0.5	015 0.5	016 0.5	015 0.4	017 0.7	015 U.4	01b U.V	0.27 0.4	027 0.4	0.28 0.3	0.28 U.4	1027 JU27
therill plo	o/ <sup>238</sup> U 2	539 0.0	576 0.0	657 0.(	552 0.0	551 0.(	531 0.0	533 0.0	537 0.0	542 0.0	550 0.0	531 0.0	533 0.0	542 0.0	547 0.0	536 0.0	532 0.0	530 0.0	529 0.0	555 0.0	550 0.0	561 0.0		518	549 0.0	573 0.0	561 0.0	559 0.0	553 0.0	558 0.0	527 0.0	523 U.I	551 0.0	551 0.0	549 0.0	557 0.0	555 0.0	560 0.0	517 0.0	240 010	652 0.0	557 0.0	561 0.0	545 0.0	548 0.0	10 160	565 0.0	551 0.0	571 0.0	567 0.0	562 0.0	565 0.0	564 0.0	549 0.0	543 0.0	534 0.0	536 0.0	540 0.0	561 0.0	561 U.V	552 0.0	542 0.0	553 0.(	541 0.0	553 0.0	546 0.0	553 U.V.	539 0.0	549 0.0	559 0.0	555 U.V	~~ I T#G
Data for We	SE <sup>206</sup> PI	110 0.0	11.20 0.0	120 0.0	120 0.0	120 0.0	120 0.0	0140	140 0.0	0.0	140 0.0	11.20 0.0	120 0.0	0.0	170 01	120 0.0	130 0.0	11.20 0.0	1130 0.0	200 0.0	1200 0.0	0.0		010	200 0.0	180 0.0	170 0.0	170 0.0	170 0.0	170 0.0	140 0.0	140 0.1		140 0.0	140 0.0	1150 0.0	1150 0.0	1150 0.0	140 0.0	010	140 0.0	1150 0.0	0.0	260 0.0	1260 0.C	270 0.0	270 0.0	12.70 0.0	12.10 0.0	210 0.0	200 0.0	210 0.0	1200 0.0	200 0.0	200 0.0	200 0.0	1200 0.0	200 0.0	0.0 690	073 U.1 0.0	110 0.0	110 0.0	110 0.0	120 0.0	120 0.0	0.0 0.0	120 0C0	220 0.0	230 0.0	230 0.0	10, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0	120 0.02
ľ	o/ <sup>235</sup> U 2	933 0.0	276 0.0	045 0.0	049 0.0	075 0.0	908 0.0	893 0.0	921 0.0	037 0.0	134 0.0	042 0.0	971 0.0	022	961 0.0	961 0.0	899 0.0	835 0.0	928 0.0	063 0.0	037 0.0	122 0.0	122 0.0	156 0.0	020	245 0.0	157 0.0	132 0.0	063 0.0	123 0.0	875 0.0	88/ U.L	700	022 0.0	035 0.0	121 0.0	117 0.0	198 0.0	875 0.0	100	106 0.0	120 0.0	088 0.0	055 0.0	173 0.C	172 0.0	108 0.0	061 0.0	231 0.0	115 0.0	150 0.0	195 0.0	140 0.0	0.0 0.0	0.0 0.0	951 0.0	931 0.0	972 0.0	130 0.0	129 0.0	056 0.0	162 0.0	019 0.0	053 0.0	058 0.0	049 0.0	973 0,0	936 0.0	103 0.0	109 0.0	750 U.L	-v- I CSD
╞	SE <sup>207</sup> Pt	012 0.3	013 0.4	013 0.4	013 0.4	012 0.4	013 0.3	020 0.3	020 0.3	020 0.4	020 0.4	014 0.4	015 0.3	015 0.4	015 0.3	015 0.3	016 0.3	015 0.3	016 0.3	012 0.4	012 0.4	012 0.4	70 210	70 210	012 0.4	011 0.4	011 0.4	011 0.4	010 0.4	010 0.4	013 0.3	014 0.5		014 0.4	014 0.4	013 0.4	015 0.4	014 0.4	014 0.3	20 210	013 0.4	014 0.4	013 0.4	019 0.4	0.19 0.13	020 0.4	019 0.4	020 0.4	011 0.4	010 0.4	010 010	009 0.4	009 0.4	010 0.4	010 0.4	011 0.3	010 0.3	010 0.3	014 0.4	014 U.4	015 0.4	015 0.4	015 0.4	015 0.4	015 0.4	015 0.4		012 0.3	012 0.4	014 0.4	016 U.4	013 J V.
burg plot	<sup>206</sup> Pb 2	528 0.0	535 0.0	526 0.0	535 0.0	539 0.0	533 0.0	521 0.0	534 0.0	536 0.0	543 0.0	549 0.0	544 0.0	538 0.0	28 0.0	532 0.0	530 0.0	528 0.0	538 0.0	532 0.0	531 0.0	0.0	20 000	20	533 0.0	539 0.0	539 0.0	538 0.0	528 0.0	530 0.0	530 0.0	540 U.C	230	532 0.0	532 0.0	536 0.0	538 0.0	543 0.0	536 0.C	200	538 0.0	543 0.0	529 0.0	541 0.0	270 010	540 0.0	530 0.0	527 0.0	541 0.0	530 0.0	533 0.0	536 0.0	532 0.0	0.0	10 10	539 0.0	538 0.0	541 0.0	539 0.0	533 UL	532 0.0	551 0.0	531 0.0	537 0.0	531 0.0	528 U.C	527 0,0	527 0.0	538 0.0	541 0.0	522 U.L	1 1 1 1 1
ra-Waser	E <sup>207</sup> Pb/	26 0.0	24 0.0	87 0.0	66 0.0	79 0.0	61 0.0	0.0	10 0.0	22 0.0	93 0.0	43 0.0	16 0.0	0.0	83 0.0	76 0.0	90 0.0	63 0.0	31 0.0	50 0.0	50 0.0	03 0.0	20 0		67 0.0	95 0.0	85 0.0	32 0.0	79 0.0	47 0.0	93 0.0	15 0.0	20 0 0	12 0.0	78 0.0	81 0.0	15 0.0	89 0.0	0.0 0.0		94 0.0	69 0.0	84 0.0	87 0.0	20.0	02 0.0	25 0.0	99 0.0	66 0.0	02 0.0	23 0.0	56 0.0	79 0.0	0.0	88 0.0	57 0.0	18 0.0	80 0.0	55 0.0	75 0.0	45 0.0	04 0.0	32 0.0	35 0.0	59 0.0	24 0.0	24 0.0	94 0.0	58 0.0	61 0.0	90 U.U	
Data for Te	<sup>%</sup> Pb 2SI	126 0.41	32 0.39	69 0.41	59 0.42	122 0.42	30 0.42	177 0.45	54 0.45	134 0.44	19 0.42	18 0.35	12 0.35	04 0.34 5 0.34	0.0 136 0.36	128 0.34	141 0.38	51 0.35	136 0.39	78 0.71	17 0.69	112 0.70	12 0.00	47 0.67	49 0.69	69.0 86	90 0.69	151 0.67	96 0.68	44 0.67	45 0.71	10.73	090 UC	122 0.69	82 0.69	95 0.67	.48 0.68	176 0.66	73 0.74	710 0 92	92 0.68	33 0.67	112 0.66	86 0.53	52.0 28 22.0 28	53 0.54	91 0.53	88 0.55	139 0.79	23 0.81	141 0.80	17 0.81	68 0.81	83 0.82	64 0.84	61 0.87	41 0.87	54 0.85	80 0.44	12 0.41	61 0.52	68 0.51	32 0.52	14 0.51	132 0.55	0.50	2C:0 10	29 0.92	49 0.89	91 0.89	USU 08.	43 U.24
$\left  \right $	<sup>238</sup> U/ <sup>2</sup>	9 18.54	9 17.37	9 17.94	9 18.11	9 18.1	9 18.8	9 18.72	9 18.62	18.4	9 18.17	9 18.82	8 18.75	18.46	18.20	9 18.6	9 18.80	9 18.87	8 18.90	0 18.02	0 18.19	17.8	17.00	179.1	1 18.2	9 17.4	0 17.83	0 17.90	0 18.05	8 17.92	18.96	19.1	1816	8 18.14	9 18.27	9 17.96	8 18.03	8 17.8	19.21	17.8	9 18.1	9 17.95	1 17.8	8 18.3	18.2	17.82	8 17.65	8 18.14	1 17.50	2 17.65	17.71 B	8 17.7	8 17.75	18.20	9 18.42	8 18.73	8 18.67	9 18.52	9 17.8	9 17.92	8 18.10	9 18.4	8 18.06	8 18.50	18.06	18.3	9 18.28	9 18.55	9 18.21	9 17.85	10,01	9 I 10-14
Ļ	È	2 0.0	3 0.0	e 4 0.0	6 0.0	2 0.0	0.0	1 0.0	3 0.0	4 0.1	0.0	1 0.0	2 0.0	000 E	4 5	-00 9	7 0.0	8 0.0	9 0.0	2_1 0.1	2 0.1	2 0.1		- 0 - 9	7 0.1	8 0.0	9 0.1	10 0.1	11 0.1	12 0.0	e_1 0.1	e_2 0.0		= 2 0.0	e_6 0.0	e_7 0.0	e_8 0.0	e_9 0.0	00	10 01	13 0.0	_14 0.0	15 0.1	e_1 0.0	e_2 0.0	2 4 0.0	e_5 0.0	e_6 0.0	e_7 0.1	e_8 0.1	10 0.0	11 0.0	12 0.0	13 0.0	15 0.0	16 0.0	17 0.0	18 0.0	1 0.0	3 0.0	1 0.0	2 0.0	3 0.0	4 0.0	5 0.0	- 0.U	- / 0.0	2 0.0	e_3 0.0	e_4 0.0	e 5 0.0	
	Identifier	oc14_Plesovice	oc14 Plesovice	oc14 Plesovice	oc14_Plesovice	oc14 Plesovice	oc14_Plesovice	oc6 Plesovice	oc6_Plesovice	oc6 Plesovice	oc6 Plesovice	oc7_Plesovice	oc7_Plesovice	oc7 Plesovice	oc/_Plesovice	oc7 Plesovice	oc7 Plesovice	oc7_Plesovice	oc7_Plesovice	fe05_Plesovice	fe05 Plesovict	fe05 Plesovict	falls Plasovice	fall5 Plasovice	fe05 Plesovice	fe05 Plesovice	fe05_Plesovice	e05_Plesovice	fe05 Plesovice	e05_Plesovice	mr20_Ple sovic	mr20_Plesovic	mr20 Plasovic	mr20 Ple sovict	mr20_Ple sovici	mr20_Ple sovic	mr20_Ple sovic.	mr20_Plesovic	nr20 Ple sovice	mr20 Plasovice	mr20_Ple sovice	nr 20 Ple sovice	mr20_Ple sovice	mr19_Ple sovio	mr19_Plesovic	mr19 Ple sovict	mr19_Ple sovict	mr19_Ple sovic	mr19_Ple sovic.	mr19_Ple sovic	mr19 Plesovic	mr19_Ple sovice	mr19_Ple sovice	mr19_Ple sovice	mr19 Plesovice	mr19 Ple sovice	mr19_Ple sovice	mr19_Ple sovice	jn13_Plesovice	in13 Plesovice	in26 Plesovice	jn26_Plesovice	jn26_Plesovice	jn26 Plesovice	jn26_Plesovice	in 26 Plesovi ce	mr30 Plesovice	mr30_Ple sovict	mr30_Plesovic	mr30_Plesovic	mr30_Ple sovic	mr.su_rie suvic

# **Plesovice zircon**

# <u>Concordia Diagrams – All Data</u>

#### Baccalieu I-78 (4500 m) sample



### South Tempest G-88 (3837.3 m) sample





## Lancaster G-70 (4405 m) sample – uncorrected Concordia

Lancaster G-70 (4405 m) sample - Andersen corrected



## Baccalieu I-78 (4142.2 m) sample



### Baccalieu I-78 (4135.29 m) sample



#### Panther P-52 (3210 m) sample



South Tempest G-88 (4195.8 m) sample



## **Concordia Diagrams and Calculated Ages – Reference Standards**



#### 91500 Zircon









## OG-1 Zircon





## **Plesovice Zircon**





283