

FLOOR STIFFENER CRACKING IN
LARGE MINING TRUCK DUMP BODIES

CENTRE FOR NEWFOUNDLAND STUDIES

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LARGE MINING TRUCK DUMP BODIES**

by

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Abstract

Due to the soft nature of the underfoot conditions in an oil sand mine, mobile equipment tends to develop greater amounts of maintenance problems than similar equipment in other types of mines. This is an investigation into cracking of haul truck dump bodies in oil sand mining service using the Finite Element Method (FEM). This work identifies the damage mechanism and source causing this persistent problem, which occurs at the intersection of the widthwise and lengthwise box-style floor stiffeners. In particular, compressive, membrane stresses are setup at these intersections resulting from overall bending of the floor plate from the weight of the ore. Superimposed onto these membrane stresses are localized bending stresses caused by very slight deflections, or twist, within the frame. Depending on the magnitude of twist, these localized bending stresses can overcome the compressive membrane stress producing sufficient tension to propagate a crack in this as-welded, non-heat-treated connection.

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Chapter: 1 Introduction

Syncrude Canada Ltd. (SCL) is the world's largest producer of crude oil from oil sands, and the largest single-source producer in Canada. Its crude oil production facility operates on the immense reserves of the Athabasca oil sand deposit north of Fort McMurray, Alberta, converting bitumen, an asphalt like oil that is as thick as molasses in its natural state, into a marketable crude oil. Oil sand is mined in an open pit using large shovels and heavy hauler trucks. The extraction of bitumen from oil sand involves mixing the ore with hot water and caustic soda, conditioning it for separation as it travels through a hydro-transport pipeline. Once inside the separation vessel, bitumen floats to the surface while the sand settles away. In the upgrading plant, bitumen is converted into a light crude oil by fluid coking, hydroprocessing, hydrotreating and blending. The final product (Syncrude Sweet Blend) is transported by pipeline to Edmonton area refineries and to pipeline terminals, which in turn ship it to other refineries in Canada and the United States.

Syncrude uses some of the largest mining trucks available in the world, known as heavy haulers, for its mining operations in both the Mildred Lake and the Aurora mines. These include such trucks as the Komatsu 930E (Figure 1-1) with a payload rating of 320 tons, and the largest truck in the world, the Caterpillar 797 (380 tons). They move overburden material to storage areas, move ore to the crushers where the process starts, move tailings sand, and even move material back into the mine to reclaim depleted areas. To put it into

perspective, it takes two tons of oil sand to produce one barrel of oil. As well, an equal amount of overburden must be removed to expose that ore. At present, Syncrude produces over 250,000 barrels of crude oil daily, which means that over 1 Million tons of material are moved each day.



Figure 1-1: Komatsu 930E Heavy Hauler Mining Truck

To move such vast amounts of material daily, SCL employs a fleet of almost 80 heavy haulers, all of which were acquired through two local dealerships. The business of developing and selling mining trucks, however, is fiercely competitive. Due to this competitiveness, information beyond standard specifications and promotional material is rarely shared by each of the vendors. When specific information is shared, it is usually used to troubleshoot maintenance activities and is safeguarded from being disclosed to other vendors. The result is an environment of limited communication in which

information does not flow freely. Although it hinders research activities, it is an accepted and essential part of the haul truck business; one that researchers and engineers must learn to work with.

SCL is not in the business of designing better haul trucks; however, to improve the reliability, productivity and safety of the haul truck fleet, it is necessary to understand the mine-specific operating conditions. This thesis should help to develop a more detailed understanding of the nature and magnitude of the forces subjected to a typical haul truck body in Syncrude mining operations. This work should provide information useful with respect to maintenance issues with the existing fleet, and help reduce operational costs. The increased understanding may also guide decisions to purchase future equipment, and may generate better designs for oil sand applications.

The equipment modeled in this study is a Syncrude owned Komatsu 930E heavy hauler mining truck. It is currently the second largest type of mining truck used at the site, and has a payload rating of 320 tons (290 metric tonnes). The truck is equipped with what is referred to as a standard dump body. Strictly speaking, however, the body is not a standard 930E body. Significant modifications have been made to adapt the structure for oil sand mining operations, including the addition of abrasion resistant cladding on the floor and sidewalls, and measures for strengthening the floor structure. Considering the fact that this work is an evaluation of a floor-stiffener cracking problem, it should be recognized that the modifications to the floor structure were quite extensive. All of the

stiffening structure from the hinge pivot to the rear was replaced with materials of twice the original thickness, and one-inch thick plates have been added to both sides of the two main rails. Although floor-stiffener cracking is most prevalent in this body, the problem is observed to lesser degrees in all haul truck bodies on the SCL mine sites. In other words, this thesis should not be considered as a design evaluation of standard 930E dump bodies. Rather, it is an investigation into a persistent problem observed in all types of dump bodies in oil sand service.

Chapter: 2 Basic Concepts

Before we get into the details, it would be helpful to introduce some of the basic concepts and techniques of the finite element method. The finite element method, also known as Finite Element Analysis (FEA), is a numerical method for solving problems in engineering and physics. For many real-world problems, it is impossible to obtain an analytical solution. Analytical solutions generally require the solution of differential equations and auxiliary conditions, which can become cumbersome or even impossible depending on the complexity of the geometry, material properties and boundary conditions for the problem at hand. As a result, engineers and scientists often resort to numerical methods such as the finite element method to obtain acceptable solutions. Some of the areas where FEA is frequently applied include structural analysis, heat transfer, mass transfer, and electromagnetism.

Finite element formulations recast the differential equations normally required to solve real world problems with a series of simultaneous algebraic equations. The underlying concept of FEA is to divide the complex geometry into a system of interconnected bodies, such that a solution for each is approximated. This process of dividing a problem into discrete finite elements is called discretization. Rather than attempting to solve the entire problem in one cumbersome operation, algebraic equations for each element are formulated and then combined to obtain the solution of the entire system¹.

2.1 Finite Element Theory

2.1.1 Basic Principle of Finite Element Analysis (FEA)

To illustrate the basic principle of FEA, we consider the spring displacement system of Figure 2-1. The system consists of three paddles connected together with an arrangement of springs. Each of the three paddles has a single degree of freedom (DOF), which is translation along the horizontal plane, and has an external force applied. The paddles represent nodes in a FEA, while the springs represent the elements interconnecting them. The symbols at the base of the paddles represent the boundary conditions applied to this system. The triangular shaped symbols represent a fixed displacement condition, while the circle shaped symbols represent rollers that imply these paddles are free to move in the horizontal direction only.

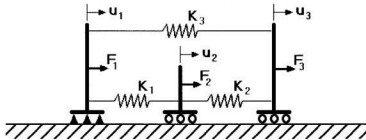


Figure 2-1: Spring Displacement System

The objective is to establish a relationship between displacements and forces.

$$\begin{Bmatrix} u_1 \\ u_2 \\ u_3 \end{Bmatrix} \& \begin{Bmatrix} F_1 \\ F_2 \\ F_3 \end{Bmatrix} \quad (2-1)$$

2.1.1.1 Element Stiffness Matrices

The first step in the finite element method is to discretize the problem and to formulate the element stiffness equations. Figure 2-2 represents the behavior of a generic spring element. The governing equation for a spring is $f = kd$. That is, the force in a spring is proportional to the difference in the end displacements, and the constant of proportionality is referred to as the spring stiffness, k .

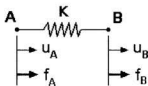


Figure 2-2: Generic Spring Behavior

For this particular element, the relationship between the nodal displacements (u_i) and the nodal forces (f_i) can be expressed as:

$$\begin{bmatrix} K & -K \\ -K & K \end{bmatrix} \begin{Bmatrix} u_A \\ u_B \end{Bmatrix} = \begin{Bmatrix} f_A \\ f_B \end{Bmatrix} \quad (2-2)$$

Similarly, each of the spring elements for the system in Figure 2-1 can be described in terms of the nodal displacements and the element forces, the internal forces within each spring element.

$$\text{Element \#1} \quad K_1 \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{Bmatrix} u_1 \\ u_2 \end{Bmatrix} = \begin{Bmatrix} f_1 \\ f_2 \end{Bmatrix} \quad (2-3)$$

$$\text{Element \#2} \quad K_2 \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{Bmatrix} u_2 \\ u_3 \end{Bmatrix} = \begin{Bmatrix} f_2 \\ f_3 \end{Bmatrix} \quad (2-4)$$

$$\text{Element \#3} \quad K_3 \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{Bmatrix} u_1 \\ u_3 \end{Bmatrix} = \begin{Bmatrix} f_1 \\ f_3 \end{Bmatrix} \quad (2-5)$$

2.1.1.2 Assembly of Element Equations into Global Stiffness Matrix

The objective, however, is to represent the relationship between the nodal displacements and the nodal forces, or the forces applied externally to the nodes of the finite element model. To do this, the element stiffness matrices above must be assembled into one global stiffness matrix formulation. By representing the above element stiffness formulations with all the nodal degrees-of-freedom (DOF) present, it is possible to directly superimpose them forming the global stiffness matrix.

$$K_1 \begin{bmatrix} 1 & -1 & 0 \\ -1 & 1 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{Bmatrix} u_1 \\ u_2 \\ u_3 \end{Bmatrix} + K_2 \begin{bmatrix} 0 & 0 & 0 \\ 0 & 1 & -1 \\ 0 & -1 & 1 \end{bmatrix} \begin{Bmatrix} u_1 \\ u_2 \\ u_3 \end{Bmatrix} + K_3 \begin{bmatrix} 1 & 0 & -1 \\ 0 & 0 & 0 \\ -1 & 0 & 1 \end{bmatrix} \begin{Bmatrix} u_1 \\ u_2 \\ u_3 \end{Bmatrix} = \begin{Bmatrix} F_1 \\ F_2 \\ F_3 \end{Bmatrix} \quad (2-6)$$

$$\begin{bmatrix} K_1 + K_3 & -K_1 & -K_3 \\ -K_1 & K_1 + K_2 & -K_2 \\ -K_3 & -K_2 & K_2 + K_3 \end{bmatrix} \begin{Bmatrix} u_1 \\ u_2 \\ u_3 \end{Bmatrix} = \begin{Bmatrix} F_1 \\ F_2 \\ F_3 \end{Bmatrix} \quad (2-7)$$

2.1.1.3 Boundary Conditions and Solution

The boundary conditions associated with displacement based finite element formulations consist of known displacements and forces (or pressures, etc.) at each node. In order to solve a FEA problem, an externally applied displacement or force must be known for each DOF of each node in the system. Either a displacement or force is specified, or the externally applied force is known to be zero. In the system described in Figure 2-1, the first paddle is fixed. As a result, this nodal displacement is known ($u_1=0$). Considering

this, it is possible to reduce the system by eliminating the row and column of the stiffness matrix associated with this DOF as follows:

$$\begin{bmatrix} \cancel{K_1} & \cancel{K_3} & K_1 & K_3 \\ -\cancel{K_1} & K_1 + K_2 & -K_2 \\ -\cancel{K_3} & -K_2 & K_2 + K_3 \end{bmatrix} \begin{Bmatrix} \cancel{u_1} \\ u_2 \\ u_3 \end{Bmatrix} = \begin{Bmatrix} \cancel{F_1} \\ F_2 + K_1 * u_1 \\ F_3 + K_3 * u_1 \end{Bmatrix} \quad (2-8)$$

$$\begin{bmatrix} K_1 + K_2 & -K_2 \\ -K_2 & K_2 + K_3 \end{bmatrix} \begin{Bmatrix} u_2 \\ u_3 \end{Bmatrix} = \begin{Bmatrix} F_2 + K_1 * u_1 \\ F_3 + K_3 * u_1 \end{Bmatrix} \quad (2-9)$$

With the known displacements accounted for, we are left with the global stiffness matrix relating the nodal displacements to the forces applied at the nodes. Therefore, it is possible to determine the unknown displacements by re-arranging and solving the system of equations as follows:

$$\begin{Bmatrix} u_2 \\ u_3 \end{Bmatrix} = \begin{bmatrix} K_1 + K_2 & -K_2 \\ -K_2 & K_2 + K_3 \end{bmatrix}^{-1} \begin{Bmatrix} F_2 + K_1 * u_1 \\ F_3 + K_3 * u_1 \end{Bmatrix} \quad (2-10)$$

2.1.2 Formulation of a 2D Bar Element Stiffness Matrix

A spring element is perhaps the simplest form of a finite element, which was well suited for describing the overall solution methodology used in FEA. As stated earlier, however FEA is used to solve problems in many different technical disciplines. The first step in any such analysis is to develop the element matrix equations, called stiffness matrices in the structural analysis realm. The following procedure will illustrate the concepts used in structural FEA to develop element stiffness matrices using the case of a one-dimensional bar element, suitable for modeling pin connected truss networks².

2.1.2.1 Definition of the Element Type

Figure 2-3 is a schematic representation of a simple pin connected structural element subjected to the tensile force, T . The pin connections are represented in FEA by nodes, labeled **1** and **2**. Nodal displacements, u_1 and u_2 , represent positive axial displacements at the pinholes, while f_1 and f_2 represent positive axial forces acting on the bar element at the pinholes.

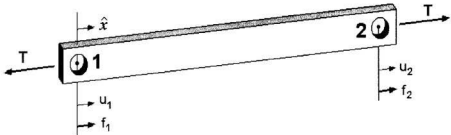


Figure 2-3: One-dimensional Bar Element

The following assumptions have been made in deriving the bar element stiffness matrix³:

1. The bar cannot sustain a shear force.
2. Any effect of transverse displacement is ignored.
3. Hooke's law applies; that is, axial stress σ_x is related to the axial strain ϵ_x by

$$\sigma_x = E\epsilon_x.$$

2.1.2.2 Selection of the Displacement Function

To begin, we must choose a displacement function with the total number of coefficients equal to the number of degrees of freedom associated with the element.

$$u = a_1 + a_2 \hat{x} \quad (2-11)$$

Expressed in matrix form, this equation becomes:

$$u = \begin{bmatrix} 1 & \hat{x} \end{bmatrix} \begin{Bmatrix} a_1 \\ a_2 \end{Bmatrix} \quad (2-12)$$

To express this function in terms of nodal displacements, u_1 and u_2 , we evaluate u at each node solving for a_1 and a_2 as follows:

$$u(0) = u_1 = a_1 \quad (2-13)$$

$$u(L) = u_2 = u_1 + a_2 L \quad (2-14)$$

$$a_2 = \frac{u_2 - u_1}{L} \quad (2-15)$$

which gives:

$$u = u_1 + \left(\frac{u_2 - u_1}{L} \right) \hat{x} \quad (2-16)$$

Expressed in matrix form, u becomes,

$$u = \begin{bmatrix} 1 - \frac{\hat{x}}{L} & \frac{\hat{x}}{L} \end{bmatrix} \begin{Bmatrix} u_1 \\ u_2 \end{Bmatrix} \quad \text{or} \quad u = \begin{bmatrix} N_1 & N_2 \end{bmatrix} \begin{Bmatrix} u_1 \\ u_2 \end{Bmatrix} \quad (2-17)$$

where N_1 and N_2 are called shape functions:

$$N_1 = 1 - \frac{\hat{x}}{L} \quad (2-18a)$$

$$N_2 = \frac{\hat{x}}{L} \quad (2-18b)$$

2.1.2.3 Strain - Displacement and Stress - Strain Relationships

The strain - displacement relationship for this one-dimensional problem is,

$$\varepsilon_x = \frac{du}{d\bar{x}} = \frac{u_2 - u_1}{L} \quad (2-19)$$

and the stress - strain relationship for this uniaxial state of stress is,

$$\sigma_x = E\varepsilon_x \quad (2-20)$$

where E is the modulus of elasticity for the bar material, and σ_x is the axial stress.

2.1.2.4 Element Stiffness Matrix

From mechanics, we know that the tension, T , in the bar is,

$$T = A\sigma_x \quad (2-21)$$

where A is the cross-sectional area of the bar. Using the strain-displacement and stress-strain relationships, the expression becomes

$$T = AE \left(\frac{u_2 - u_1}{L} \right) \quad (2-22)$$

Using the nodal sign convention,

$$f_1 = -T \quad \text{or} \quad f_1 = \frac{AE}{L} (u_1 - u_2) \quad (2-23)$$

Similarly,

$$f_2 = T \quad \text{or} \quad f_2 = \frac{AE}{L} (u_2 - u_1) \quad (2-24)$$

When expressed together, in matrix form, these equations become,

$$\begin{Bmatrix} f_1 \\ f_2 \end{Bmatrix} = \frac{AE}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{Bmatrix} u_1 \\ u_2 \end{Bmatrix} \quad (2-25)$$

For a one-dimensional bar element, the stiffness matrix is:

$$\underline{k} = \frac{AE}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \quad (2-26)$$

2.1.2.5 Transformation into Global Coordinate System

The one-dimensional bar element, as derived above, is not well suited for solving engineering problems in its present form. To solve pin-connected truss networks, it would be helpful to have nodal forces and displacements defined in a bi-axial (planar) coordinate system as opposed to a uniaxial coordinate system (Figure 2-4).

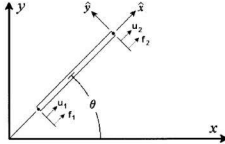


Figure 2-4: Transformation into Global Coordinate System

Transforming the nodal displacements, u_1 and u_2 , into the global (x - y) coordinate system we get,

$$\hat{u}_1 = u_{1x} \cos \theta + u_{1y} \sin \theta \quad (2-27)$$

$$\hat{u}_2 = u_{2x} \cos \theta + u_{2y} \sin \theta \quad (2-28)$$

which can be written in matrix form as⁴,

$$\begin{Bmatrix} \hat{u}_1 \\ \hat{u}_2 \end{Bmatrix} = \begin{bmatrix} C & S & 0 & 0 \\ 0 & 0 & C & S \end{bmatrix} \begin{Bmatrix} u_{1x} \\ u_{1y} \\ u_{2x} \\ u_{2y} \end{Bmatrix} \quad \text{or} \quad \underline{\hat{u}} = \underline{T}^* \underline{u} \quad (2-29)$$

where $C = \cos \theta$ and $S = \sin \theta$. Similarly, the global force vector can be obtained

$$\underline{\hat{f}} = \underline{T}^* \underline{f} \quad (2-30)$$

Substituting the above relations into the equation,

$$\underline{\hat{f}} = \underline{\hat{k}} \underline{\hat{u}} \quad (2-31)$$

yields:

$$\underline{T}^* \underline{f} = \underline{\hat{k}} \underline{T}^* \underline{u} \quad (2-32)$$

In order to determine the expression relating the global forces to global displacements, we must invert \underline{T}^* which is not immediately possible because it is not a square matrix.

Instead, we must expand the element matrices to be consistent with the global coordinates, recognizing the fact that the nodal forces normal to the bar element axis will always be zero. The relationship between element and global displacements becomes,

$$\begin{Bmatrix} \hat{u}_{1x} \\ \hat{u}_{1y} \\ \hat{u}_{2x} \\ \hat{u}_{2y} \end{Bmatrix} = \begin{bmatrix} C & S & 0 & 0 \\ -S & C & 0 & 0 \\ 0 & 0 & C & S \\ 0 & 0 & -S & C \end{bmatrix} \begin{Bmatrix} u_{1x} \\ u_{1y} \\ u_{2x} \\ u_{2y} \end{Bmatrix} \quad \text{or} \quad \underline{\hat{u}} = \underline{T} \underline{u} \quad (2-33)$$

and similarly,

$$\underline{\hat{f}} = \underline{T} \underline{f} \quad (2-34)$$

The element stiffness matrix must also be expanded to the same order, as follows:

$$\begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{1y} \\ \hat{f}_{2x} \\ \hat{f}_{2y} \end{Bmatrix} = \frac{AE}{L} \begin{bmatrix} 1 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 \\ -1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{Bmatrix} \hat{u}_{1x} \\ \hat{u}_{1y} \\ \hat{u}_{2x} \\ \hat{u}_{2y} \end{Bmatrix} \quad (2-35)$$

Now as before, substituting the above relations into the equation,

$$\underline{\hat{f}} = \underline{\hat{k}} \underline{\hat{u}} \quad (2-36)$$

yields:

$$\underline{T} \underline{f} = \underline{\hat{k}} \underline{T} \underline{u} \quad (2-37)$$

By multiplying both sides of this equation by \underline{T}^{-1} , we obtain the relationship between the global forces and global displacements:

$$\underline{f} = \underline{T}^{-1} \underline{\hat{k}} \underline{T} \underline{u} \quad (2-38)$$

However, \underline{T} is an orthogonal matrix, and as a result, the inverse of \underline{T} is equal to its transpose.

$$\underline{T}^{-1} = \underline{T}^T \quad (2-39)$$

Therefore,

$$\underline{f} = \underline{T}^T \underline{\hat{k}} \underline{T} \underline{u} \quad (2-40)$$

From above, we can see that the stiffness matrix in global coordinates, \underline{k} , is

$$\underline{k} = \underline{T}^T \underline{\hat{k}} \underline{T} \quad (2-41)$$

When expanded, \underline{k} becomes

$$\underline{k} = \frac{AE}{L} \begin{bmatrix} C^2 & CS & -C^2 & -CS \\ CS & S^2 & -CS & -S^2 \\ -C^2 & -CS & C^2 & CS \\ CS & -S^2 & CS & S^2 \end{bmatrix} \quad (2-42)$$

2.2 FEA Techniques

2.2.1 Example of a Bar Element Truss Problem

With the global stiffness matrix for a one-dimensional bar element defined in Cartesian coordinates, it is now possible to use this element to solve a pin-connected truss problem. Figure 2-5 is an example of a pin-connected truss. Each of the truss members has a cross-sectional area, A , and a modulus of elasticity, E ; and the truss is subjected to two loads, P and $2P$. The purpose of this problem will be to illustrate the process involved in solving for member forces and displacements using the finite element method, and later, to demonstrate several techniques, used throughout the thesis, that could be utilized to reduce the computational effort required in obtaining this solution.

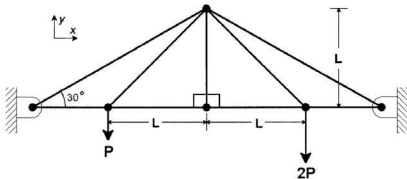


Figure 2-5: Pin-Connected Truss Problem

2.2.1.1 Discretize Geometry and Formulate Element Equations

The first step in the solution process is to break up the geometry into discrete or finite elements. As shown in Figure 2-6, the truss structure has been broken into nine elements (in red) and the pin connections have been designated as nodes (in blue)

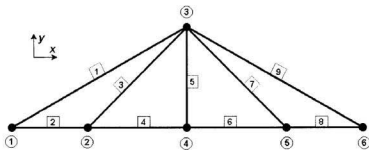


Figure 2-6: Discretized Truss Structure

The second step is to formulate the stiffness equations for each of the nine elements. Element number 1 has a length of $2L$ and $\theta = 30^\circ$, therefore its stiffness matrix is evaluated as follows:

$$\text{Element \#1} \quad \begin{Bmatrix} f_{1x} \\ f_{1y} \\ f_{3x} \\ f_{3y} \end{Bmatrix} = \frac{AE}{8L} \begin{bmatrix} 3 & \sqrt{3} & -3 & -\sqrt{3} \\ \sqrt{3} & 1 & -\sqrt{3} & -1 \\ -3 & -\sqrt{3} & 3 & \sqrt{3} \\ -\sqrt{3} & -1 & \sqrt{3} & 1 \end{bmatrix} \begin{Bmatrix} u_{1x} \\ u_{1y} \\ u_{3x} \\ u_{3y} \end{Bmatrix} \quad (2-43)$$

Element 3 has a length of $\sqrt{2}L$ and $\theta = 45^\circ$, therefore its stiffness matrix is evaluated as follows:

$$\text{Element \#3} \quad \begin{Bmatrix} f_{2x} \\ f_{2y} \\ f_{3x} \\ f_{3y} \end{Bmatrix} = \frac{\sqrt{2}AE}{4L} \begin{bmatrix} 1 & 1 & -1 & -1 \\ 1 & 1 & -1 & -1 \\ -1 & -1 & 1 & 1 \\ -1 & -1 & 1 & 1 \end{bmatrix} \begin{Bmatrix} u_{2x} \\ u_{2y} \\ u_{3x} \\ u_{3y} \end{Bmatrix} \quad (2-44)$$

Element 5 has a length of L and $\theta = 270^\circ$, therefore its stiffness matrix is evaluated as follows:

$$\text{Element \#5} \quad \begin{Bmatrix} f_{3x} \\ f_{3y} \\ f_{4x} \\ f_{4y} \end{Bmatrix} = \frac{AE}{L} \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & -1 \\ 0 & 0 & 0 & 0 \\ 0 & -1 & 0 & 1 \end{bmatrix} \begin{Bmatrix} u_{3x} \\ u_{3y} \\ u_{4x} \\ u_{4y} \end{Bmatrix} \quad (2-45)$$

Element 7 has a length of $\sqrt{2}L$ and $\theta = 315^\circ$, therefore its stiffness matrix is evaluated as follows:

$$\text{Element \#7} \quad \begin{Bmatrix} f_{3x} \\ f_{3y} \\ f_{5x} \\ f_{5y} \end{Bmatrix} = \frac{\sqrt{2}AE}{4L} \begin{bmatrix} 1 & -1 & -1 & 1 \\ -1 & 1 & 1 & -1 \\ -1 & 1 & 1 & -1 \\ 1 & -1 & -1 & 1 \end{bmatrix} \begin{Bmatrix} u_{3x} \\ u_{3y} \\ u_{5x} \\ u_{5y} \end{Bmatrix} \quad (2-46)$$

Element 9 has a length of $2L$ and $\theta = 330^\circ$, therefore its stiffness matrix is evaluated as follows:

$$\text{Element \#9} \quad \begin{Bmatrix} f_{3x} \\ f_{3y} \\ f_{6x} \\ f_{6y} \end{Bmatrix} = \frac{AE}{4L} \begin{bmatrix} 3 & -\sqrt{3} & -3 & \sqrt{3} \\ -\sqrt{3} & 1 & \sqrt{3} & -1 \\ -3 & \sqrt{3} & 3 & -\sqrt{3} \\ \sqrt{3} & -1 & -\sqrt{3} & 1 \end{bmatrix} \begin{Bmatrix} u_{3x} \\ u_{3y} \\ u_{6x} \\ u_{6y} \end{Bmatrix} \quad (2-47)$$

Elements 4 and 6 have lengths of L and $\theta = 0^\circ$, therefore their stiffness matrices are evaluated as follows:

$$\text{Element \#4} \quad \begin{Bmatrix} f_{2x} \\ f_{2y} \\ f_{4x} \\ f_{4y} \end{Bmatrix} = \frac{AE}{L} \begin{bmatrix} 1 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 \\ -1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{Bmatrix} u_{2x} \\ u_{2y} \\ u_{4x} \\ u_{4y} \end{Bmatrix} \quad (2-48)$$

$$\text{Element \#6} \quad \begin{Bmatrix} f_{4x} \\ f_{4y} \\ f_{5x} \\ f_{5y} \end{Bmatrix} = \frac{AE}{L} \begin{bmatrix} 1 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 \\ -1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{Bmatrix} u_{4x} \\ u_{4y} \\ u_{5x} \\ u_{5y} \end{Bmatrix} \quad (2-49)$$

Elements 2 and 8 have lengths of $(\sqrt{3}-1)L$ and $\theta = 0^\circ$, therefore their stiffness matrices are evaluated as follows:

$$\text{Element \#2} \quad \begin{Bmatrix} f_{1x} \\ f_{1y} \\ f_{2x} \\ f_{2y} \end{Bmatrix} = \frac{AE}{(\sqrt{3}-1)L} \begin{bmatrix} 1 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 \\ -1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{Bmatrix} u_{1x} \\ u_{1y} \\ u_{2x} \\ u_{2y} \end{Bmatrix} \quad (2-50)$$

$$\text{Element \#8} \quad \begin{Bmatrix} f_{5x} \\ f_{5y} \\ f_{6x} \\ f_{6y} \end{Bmatrix} = \frac{AE}{(\sqrt{3}-1)L} \begin{bmatrix} 1 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 \\ -1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{Bmatrix} u_{5x} \\ u_{5y} \\ u_{6x} \\ u_{6y} \end{Bmatrix} \quad (2-51)$$

2.2.1.2 Assemble Global Stiffness Matrix

With each of the element equations formulated, it is now possible to assemble the global stiffness matrix. In this particular FEA model, nodal displacements at the two pin supports (nodes 1 and 6) are known to be zero. Since these nodes are inactive, there is no need to include the terms associated with these DOF into the stiffness matrix. For node 2, we wish to assemble the two equations that relate nodal displacement to the global

forces applied to the model at that node. To do this, we must incorporate the stiffness terms related to the global forces, F_{2x} and F_{2y} , from each of the three elements connected to this node (elements 2, 3 and 4) as follows:

$$\frac{AE}{L} \begin{bmatrix} \frac{1}{\sqrt{3}-1} + \frac{\sqrt{2}}{4} + 1 & \frac{\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} & 1 & 0 & 0 & 0 \\ \frac{\sqrt{2}}{4} & \frac{\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} & \frac{\sqrt{2}}{4} & 0 & 0 & 0 & 0 \end{bmatrix} \begin{Bmatrix} u_{2x} \\ u_{2y} \\ u_{3x} \\ u_{3y} \\ u_{4x} \\ u_{4y} \\ u_{5x} \\ u_{5y} \end{Bmatrix} = \begin{Bmatrix} F_{2x} \\ F_{2y} \end{Bmatrix} \quad (2-52)$$

For node 3, we must incorporate the stiffness terms related to F_{3x} and F_{3y} from each of the five elements connected to this node (elements 1, 3, 5, 7 and 9) as follows:

$$\frac{AE}{L} \begin{bmatrix} -\frac{\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} & \frac{3}{8} + \frac{\sqrt{2}}{4} + \frac{\sqrt{2}}{4} + \frac{3}{8} & \frac{\sqrt{3}}{8} + \frac{\sqrt{2}}{4} - \frac{\sqrt{2}}{4} - \frac{\sqrt{3}}{8} & 0 & 0 & -\frac{\sqrt{2}}{4} & \frac{\sqrt{2}}{4} \\ -\frac{\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} & \frac{\sqrt{3}}{8} + \frac{\sqrt{2}}{4} - \frac{\sqrt{2}}{4} - \frac{\sqrt{3}}{8} & \frac{1}{8} + \frac{\sqrt{2}}{4} + 1 + \frac{\sqrt{2}}{4} + \frac{1}{8} & 0 & -1 & \frac{\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} \end{bmatrix} \begin{Bmatrix} u_{2x} \\ u_{2y} \\ u_{3x} \\ u_{3y} \\ u_{4x} \\ u_{4y} \\ u_{5x} \\ u_{5y} \end{Bmatrix} = \begin{Bmatrix} F_{3x} \\ F_{3y} \end{Bmatrix} \quad (2-53)$$

which simplifies to,

$$\frac{AE}{L} \begin{bmatrix} -\frac{\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} & \frac{3+2\sqrt{2}}{4} & 0 & 0 & 0 & -\frac{\sqrt{2}}{4} & \frac{\sqrt{2}}{4} \\ -\frac{\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} & 0 & \frac{5+2\sqrt{2}}{4} & 0 & -1 & \frac{\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} \end{bmatrix} \begin{Bmatrix} u_{2x} \\ u_{2y} \\ u_{3x} \\ u_{3y} \\ u_{4x} \\ u_{4y} \\ u_{5x} \\ u_{5y} \end{Bmatrix} = \begin{Bmatrix} F_{3x} \\ F_{3y} \end{Bmatrix} \quad (2-54)$$

For node 4, we must incorporate the stiffness terms related to F_{4x} and F_{4y} from each of the three elements connected to this node (elements 4, 5 and 6) as follows:

$$\frac{AE}{L} \begin{bmatrix} -1 & 0 & 0 & 0 & 2 & 0 & -1 & 0 \\ 0 & 0 & 0 & -1 & 0 & 1 & 0 & 0 \end{bmatrix} \begin{Bmatrix} u_{2x} \\ u_{2y} \\ u_{3x} \\ u_{3y} \\ u_{4x} \\ u_{4y} \\ u_{5x} \\ u_{5y} \end{Bmatrix} = \begin{Bmatrix} F_{4x} \\ F_{4y} \end{Bmatrix} \quad (2-55)$$

Lastly, for node 5, we must incorporate the stiffness terms related to F_{5x} and F_{5y} from each of the three elements connected to this node (elements 6, 7 and 8) as follows:

$$\frac{AE}{L} \begin{bmatrix} 0 & 0 & -\frac{\sqrt{2}}{4} & \frac{\sqrt{2}}{4} & -1 & 0 & \frac{1}{(\sqrt{3}-1)} + \frac{4+\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} \\ 0 & 0 & \frac{\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} & 0 & 0 & -\frac{\sqrt{2}}{4} & \frac{\sqrt{2}}{4} \end{bmatrix} \begin{Bmatrix} u_{2x} \\ u_{2y} \\ u_{3x} \\ u_{3y} \\ u_{4x} \\ u_{4y} \\ u_{5x} \\ u_{5y} \end{Bmatrix} = \begin{Bmatrix} F_{5x} \\ F_{5y} \end{Bmatrix} \quad (2-56)$$

Then, combining these expressions for nodal forces, we obtain the global stiffness matrix:

$$\frac{AE}{L} \begin{bmatrix} \frac{1}{(\sqrt{3}-1)} + \frac{4+\sqrt{2}}{4} & \frac{\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} & -1 & 0 & 0 & 0 \\ \frac{\sqrt{2}}{4} & \frac{\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} & 0 & 0 & 0 & 0 \\ -\frac{\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} & \frac{3+2\sqrt{2}}{4} & 0 & 0 & 0 & -\frac{\sqrt{2}}{4} & \frac{\sqrt{2}}{4} \\ -\frac{\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} & 0 & \frac{5+2\sqrt{2}}{4} & 0 & -1 & \frac{\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} \\ -1 & 0 & 0 & 0 & 2 & 0 & -1 & 0 \\ 0 & 0 & 0 & -1 & 0 & 1 & 0 & 0 \\ 0 & 0 & -\frac{\sqrt{2}}{4} & \frac{\sqrt{2}}{4} & -1 & 0 & \frac{1}{(\sqrt{3}-1)} + \frac{4+\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} \\ 0 & 0 & \frac{\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} & 0 & 0 & -\frac{\sqrt{2}}{4} & \frac{\sqrt{2}}{4} \end{bmatrix} \begin{Bmatrix} u_{2x} \\ u_{2y} \\ u_{3x} \\ u_{3y} \\ u_{4x} \\ u_{4y} \\ u_{5x} \\ u_{5y} \end{Bmatrix} = \begin{Bmatrix} F_{2x} \\ F_{2y} \\ F_{3x} \\ F_{3y} \\ F_{4x} \\ F_{4y} \\ F_{5x} \\ F_{5y} \end{Bmatrix}$$

$$\text{or } \underline{Ku} = \underline{F} \quad (2-57)$$

2.2.1.3 Nodal Displacements

The next portion of the FEA solution process involves applying the specified boundary conditions and solving for nodal displacements. The supporting boundary conditions for this FEA model have already been accounted for. As was mentioned earlier, the DOF associated with nodes 1 and 6 are constrained to be zero by the pin boundary conditions. As a result, these DOF are inactive and have been omitted from the global stiffness matrix formulation. There are, however, two vertical loads applied to nodes on the bottom of the truss frame. Represented in vector form and adhering to the nodal sign convention, the force vector for this FEA problem is:

$$\underline{F} = \begin{Bmatrix} F_{2x} \\ F_{2y} \\ F_{3x} \\ F_{3y} \\ F_{4x} \\ F_{4y} \\ F_{5x} \\ F_{5y} \end{Bmatrix} = P \begin{Bmatrix} 0 \\ -1 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ -2 \end{Bmatrix} \quad (2-58)$$

To solve for nodal displacements, we must rearrange equation 2-57 by multiplying both sides with the inverse of the stiffness matrix

$$\underline{K}^{-1} \underline{K} \underline{u} = \underline{K}^{-1} \underline{F} \quad (2-59)$$

which becomes

$$\underline{u} = \underline{K}^{-1} \underline{F} \quad (2-60)$$

To compute the nodal displacement vector, we simply need to carry out the matrix multiplication resulting in

$$\underline{u} = \begin{Bmatrix} u_{2x} \\ u_{2y} \\ u_{3x} \\ u_{3y} \\ u_{4x} \\ u_{4y} \\ u_{5x} \\ u_{5y} \end{Bmatrix} = \frac{PL}{AE} \begin{Bmatrix} \frac{1}{6} \frac{\sqrt{3}(\sqrt{3}-1)(5\sqrt{3}-3)}{2\sqrt{3}-1} \\ \frac{1}{9} \frac{\sqrt{3}(-36\sqrt{2}-219+44\sqrt{3}+6\sqrt{2}\sqrt{3})}{2\sqrt{3}-1} \\ \frac{4}{3} \\ -12 \\ \frac{1}{2} \frac{\sqrt{3}-1}{2\sqrt{3}-1} \\ -12 \\ -\frac{1}{6} \frac{\sqrt{3}(\sqrt{3}-1)(7\sqrt{3}-3)}{2\sqrt{3}-1} \\ \frac{1}{9} \frac{\sqrt{3}(-276+55\sqrt{3}-72\sqrt{2}+12\sqrt{2}\sqrt{3})}{2\sqrt{3}-1} \end{Bmatrix} = \frac{PL}{AE} \begin{Bmatrix} 0.485 \\ -14.0 \\ 1.33 \\ -12.0 \\ 0.149 \\ -12.0 \\ -0.783 \\ -19.8 \end{Bmatrix} \quad (2-61)$$

This portion of the results is referred to as the *nodal solution*.

2.2.1.4 Solve for Element Forces

Having determined the nodal displacements, we may now go back to the element level to determine the forces present within each element. Substituting the now known nodal displacements into the element stiffness equations and solving, we obtain what is referred to as the *element solution*. For example, the element stiffness equations for element number 1 were:

$$\begin{Bmatrix} f_{1x} \\ f_{1y} \\ f_{3x} \\ f_{3y} \end{Bmatrix} = \frac{AE}{8L} \begin{bmatrix} 3 & \sqrt{3} & -3 & -\sqrt{3} \\ \sqrt{3} & 1 & -\sqrt{3} & -1 \\ -3 & -\sqrt{3} & 3 & \sqrt{3} \\ -\sqrt{3} & -1 & \sqrt{3} & 1 \end{bmatrix} \begin{Bmatrix} u_{1x} \\ u_{1y} \\ u_{3x} \\ u_{3y} \end{Bmatrix} \quad (2-62)$$

Substituting in the nodal displacements,

$$\begin{Bmatrix} f_{1x} \\ f_{1y} \\ f_{3x} \\ f_{3y} \end{Bmatrix} = \frac{AE}{8L} \begin{bmatrix} 3 & \sqrt{3} & -3 & -\sqrt{3} \\ \sqrt{3} & 1 & -\sqrt{3} & -1 \\ -3 & -\sqrt{3} & 3 & \sqrt{3} \\ -\sqrt{3} & -1 & \sqrt{3} & 1 \end{bmatrix} \frac{PL}{AE} \begin{Bmatrix} 0 \\ 0 \\ \frac{4}{3} \\ -12 \end{Bmatrix} \quad (2-63)$$

and carrying out the multiplication yields:

$$\begin{Bmatrix} f_{1x} \\ f_{1y} \\ f_{3x} \\ f_{3y} \end{Bmatrix} = P \begin{Bmatrix} -\frac{1}{2} + \frac{3\sqrt{3}}{2} \\ \frac{3}{2} - \frac{\sqrt{3}}{6} \\ \frac{1}{2} - \frac{3\sqrt{3}}{2} \\ -\frac{3}{2} + \frac{\sqrt{3}}{6} \end{Bmatrix} \approx P \begin{Bmatrix} 2.10 \\ 1.21 \\ -2.10 \\ -1.21 \end{Bmatrix} \quad (2-64)$$

Since element 1 is situated on an angle, we must find the resultant of the nodal force components to determine the tensile or compressive inline force within the element. The resultant, R , of the force components f_{1x} and f_{1y} is

$$R = P \sqrt{\left(-\frac{1}{2} + \frac{3\sqrt{3}}{2}\right)_x^2 + \left(\frac{3}{2} - \frac{\sqrt{3}}{6}\right)_y^2} = P \left(-\frac{1}{2} + \frac{3\sqrt{3}}{2}\right) \left(\frac{3}{2} - \frac{\sqrt{3}}{6}\right) = 2.54P \quad (2-65)$$

and from the direction of these force components we can ascertain that element #1 is in compression. This procedure is then repeated to determine the forces in each of the remaining elements, and with these forces it is possible to evaluate the stress and strain within each element.

2.2.2 Symmetry Considerations

The truss problem suggested in Section 2.2.1 was geometrically symmetrical about a line drawn down the center of the structure. If the loading applied to the truss had been symmetrical about this centerline as well (Figure 2-7), then the principle of symmetry could be used to reduce the computational effort required to solve the problem. When subjected to a symmetrical set of loads, the results will be a mirror image on both sides of line of symmetry. To take advantage of this property, the model may be cut along line of symmetry, and only half of the model needs to be processed to obtain a solution. By reducing the number of active DOF required to solve the problem, the size of the stiffness matrix that must be assembled has also been reduced. When used in FEA software to solve large problems, the advantages include faster solution times and a reduction in

storage requirements, or the ability to produce finer mesh densities or larger models within computer hardware and software limitations.

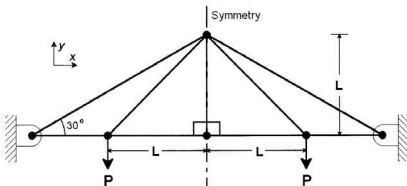


Figure 2-7: Symmetrical Truss Problem

In this half model analysis, symmetry boundary conditions are applied to nodes along the cut boundary, and the vertical element is reduced in cross-sectional area by one-half. In general, symmetry boundary conditions consist of constraining nodal displacements normal to the line (or plane) of symmetry, while permitting displacement along this line (or plane). If rotational degrees of freedom were used, then the rotational DOF out of the plane of symmetry would be constrained. For this particular model, the symmetry boundary conditions are simply the condition, $u_x = 0$, applied to the nodes along the line of symmetry (Figure 2-8).

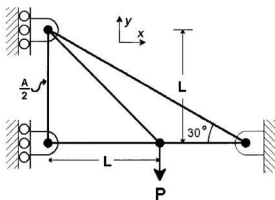


Figure 2-8: Truss Half Model with Symmetry Boundary Conditions

Figure 2-9 shows the discretization used to solve this half model analysis. The element and node numbering has been chosen to be consistent with the full model analysis in Section 2.1.1. As a result, the equations for element numbers 6 thru 9 will be the same.

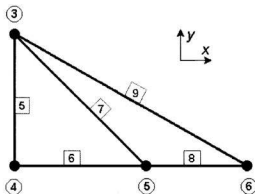


Figure 2-9: Truss Half Model Discretization

In this half model analysis, however, element 5 has half the cross-sectional area of the element 5 in the full model problem. Therefore, the equations for this element must be adjusted as follows:

$$\begin{Bmatrix} f_{3x} \\ f_{3y} \\ f_{4x} \\ f_{4y} \end{Bmatrix} = \frac{AE}{2L} \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & -1 \\ 0 & 0 & 0 & 0 \\ 0 & -1 & 0 & 1 \end{bmatrix} \begin{Bmatrix} u_{3x} \\ u_{3y} \\ u_{4x} \\ u_{4y} \end{Bmatrix} \quad (2-66)$$

As before, the global stiffness matrix must be assembled, but needs only the terms corresponding to the active DOF included. The global stiffness equations for this half model analysis with symmetry boundary conditions are:

$$\frac{AE}{L} \begin{bmatrix} \frac{1}{2} + \frac{\sqrt{2}}{4} + \frac{1}{8} & -\frac{1}{2} & \frac{\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} \\ -\frac{1}{2} & \frac{1}{2} & 0 & 0 \\ \frac{\sqrt{2}}{4} & 0 & 1 + \frac{\sqrt{2}}{4} + \frac{1}{\sqrt{3}-1} & -\frac{\sqrt{2}}{4} \\ -\frac{\sqrt{2}}{4} & 0 & -\frac{\sqrt{2}}{4} & \frac{\sqrt{2}}{4} \end{bmatrix} \begin{Bmatrix} u_{3y} \\ u_{4y} \\ u_{5x} \\ u_{5y} \end{Bmatrix} = \begin{Bmatrix} F_{3y} \\ F_{4y} \\ F_{5x} \\ F_{5y} \end{Bmatrix} \quad (2-67)$$

which can be simplified to

$$\frac{AE}{L} \begin{bmatrix} \frac{5+2\sqrt{2}}{8} & -\frac{1}{2} & \frac{\sqrt{2}}{4} & -\frac{\sqrt{2}}{4} \\ -\frac{1}{2} & \frac{1}{2} & 0 & 0 \\ \frac{\sqrt{2}}{4} & 0 & \frac{4+\sqrt{2}}{4} + \frac{1}{\sqrt{3}-1} & -\frac{\sqrt{2}}{4} \\ -\frac{\sqrt{2}}{4} & 0 & -\frac{\sqrt{2}}{4} & \frac{\sqrt{2}}{4} \end{bmatrix} \begin{Bmatrix} u_{3y} \\ u_{4y} \\ u_{5x} \\ u_{5y} \end{Bmatrix} = \begin{Bmatrix} F_{3y} \\ F_{4y} \\ F_{5x} \\ F_{5y} \end{Bmatrix} \quad (2-68)$$

The force vector for this half model symmetry analysis is

$$\underline{F} = \begin{Bmatrix} F_{3y} \\ F_{4y} \\ F_{5x} \\ F_{5y} \end{Bmatrix} = P \begin{Bmatrix} 0 \\ 0 \\ 0 \\ -1 \end{Bmatrix} \quad (2-69)$$

To solve for nodal displacements, we must carry out the matrix multiplication of equation 2-60 resulting in:

$$\underline{u} = \begin{Bmatrix} u_{3y} \\ u_{4y} \\ u_{5x} \\ u_{5y} \end{Bmatrix} = \frac{PL}{AE} \begin{Bmatrix} -8 \\ -8 \\ -\frac{1}{3}\sqrt{3}(\sqrt{3}-1) \\ -\frac{1}{6}(9\sqrt{2}\sqrt{3}-\sqrt{2}+4\sqrt{3})\sqrt{2}\sqrt{3} \end{Bmatrix} \approx \frac{PL}{AE} \begin{Bmatrix} -8.00 \\ -8.00 \\ -0.423 \\ -11.3 \end{Bmatrix} \quad (2-70)$$

2.2.3 Anti-symmetry Considerations

Another useful technique in FEA uses the principle of anti-symmetry. In Section 2.2.2, it was shown that a symmetrical FEA model with a symmetrical load set could be solved by applying appropriate boundary conditions to a reduced FEA model. The same can be done if the loading applied to the symmetrical model was anti-symmetrical about the line of symmetry. An anti-symmetrical load set consists of forces (or pressures, displacements, etc.) applied to mirrored locations on either side of the line of symmetry that are equal and opposite in magnitude and direction. For example, an anti-symmetric load set applied to the same truss arrangement as earlier could look like Figure 2-10. Note that the applied loads are in opposite directions on either side.

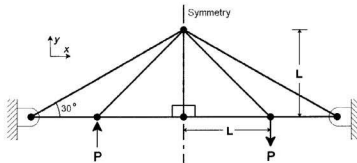


Figure 2-10: Truss Problem with Anti-Symmetric Load Set

Like the symmetrical analysis of Section 2.2.2, the solution for this scenario can be obtained by applying appropriate boundary conditions to a half model analysis. Again, this half model analysis will have a reduced number of active DOF, which reduces the computational effort required in obtaining a solution. In general, anti-symmetry boundary conditions consist of constraining nodal displacements in the line (or plane) of symmetry, while permitting displacement perpendicular to this line (or plane). If rotational degrees of freedom were used, then the rotational DOF within the plane of symmetry would be constrained. For this particular model, the anti-symmetry boundary conditions are simply the condition, $u_y = 0$, applied to the nodes along the line of symmetry (Figure 2-11).

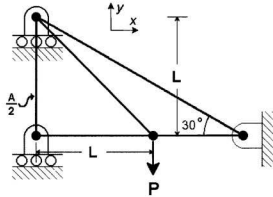


Figure 2-11: Truss Half Model with Anti-Symmetry Boundary Conditions

The same discretization used for the symmetry analysis in Section 2.2.2 (Figure 2-9) will be used for this half model analysis. As before, the global stiffness matrix must be assembled, but needs only the terms corresponding to the active DOF included. The global stiffness equations for this half model analysis with anti-symmetry boundary conditions are:

$$\frac{AE}{L} \begin{bmatrix} \frac{3+2\sqrt{2}}{8} & 0 & -\frac{\sqrt{2}}{4} & \frac{\sqrt{2}}{4} \\ 0 & 1 & -1 & 0 \\ -\frac{\sqrt{2}}{4} & -1 & \frac{4+\sqrt{2}}{4} + \frac{1}{\sqrt{3}-1} & -\frac{\sqrt{2}}{4} \\ \frac{\sqrt{2}}{4} & 0 & -\frac{\sqrt{2}}{4} & \frac{\sqrt{2}}{4} \end{bmatrix} \begin{Bmatrix} u_{3x} \\ u_{4x} \\ u_{5x} \\ u_{5y} \end{Bmatrix} = \begin{Bmatrix} F_{3x} \\ F_{4x} \\ F_{5x} \\ F_{5y} \end{Bmatrix} \quad (2-71)$$

And the force vector for this FEA problem is:

$$\underline{F} = \begin{Bmatrix} F_{3x} \\ F_{4x} \\ F_{5x} \\ F_{5y} \end{Bmatrix} = P \begin{Bmatrix} 0 \\ 0 \\ 0 \\ -1 \end{Bmatrix} \quad (2-72)$$

To solve for nodal displacements, we must carry out the matrix multiplication of equation 2-60 resulting in:

$$\underline{u} = \begin{Bmatrix} u_{3x} \\ u_{4x} \\ u_{5x} \\ u_{5y} \end{Bmatrix} = \frac{PL}{AE} \begin{Bmatrix} \frac{8}{3} \\ 1 - \sqrt{3} \\ 1 - \sqrt{3} \\ -\frac{1}{6}(3\sqrt{2}\sqrt{3} + 5\sqrt{2} + 12)\sqrt{2} \end{Bmatrix} = \frac{PL}{AE} \begin{Bmatrix} 2.67 \\ -0.732 \\ -0.732 \\ -6.23 \end{Bmatrix} \quad (2-73)$$

2.2.4 Superposition Considerations

The final FEA technique to be described, utilizes the principle of superposition. The properties of superposition are that FEA results are both additive and linear. In other words, the analysis results arising from separate load vectors applied to the same FEA model may be added together, or superimposed, and the combined results would be the same as if both load vectors had been superimposed and solved simultaneously. For instance, the truss frame example in Section 2.2.1 was subjected a load vector (\underline{F}) that can be expressed as a superposition of two separate load vectors (\underline{F}_S and \underline{F}_A), as follows:

$$\underline{F} = \begin{Bmatrix} F_{2x} \\ F_{2y} \\ F_{3x} \\ F_{3y} \\ F_{4x} \\ F_{4y} \\ F_{5x} \\ F_{5y} \end{Bmatrix} = P \begin{Bmatrix} 0 \\ -1 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ -2 \end{Bmatrix} = \underline{F}_S + \underline{F}_A = \frac{3P}{2} \begin{Bmatrix} 0 \\ -1 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ -1 \end{Bmatrix}_S + \frac{P}{2} \begin{Bmatrix} 0 \\ 1 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ -1 \end{Bmatrix}_A \quad (2-74)$$

where \underline{F}_S and \underline{F}_A are symmetric and anti-symmetric, respectively, about the centerline of the model. Using the principle of superposition, it is possible to solve these load vectors separately; and considering the fact that FEA results are linear, it is possible to scale the results of results of in Sections 2.2.2 and 2.2.3 to obtain equivalent results, as would be produced from the vectors above. Therefore, it is now possible to obtain the identical results of the full truss problem subjected to the unsymmetrical load vector, \underline{F} , without assembling the full FEA model, but by superimposing the results of two half model analyses instead.

The results of the symmetry analysis in Section 2.2.2 (\underline{u}_s) expanded to the same order of the full truss problem can be expressed as,

$$\underline{u}_s = \begin{Bmatrix} u_{2x} \\ u_{2y} \\ u_{3x} \\ u_{3y} \\ u_{4x} \\ u_{4y} \\ u_{5x} \\ u_{5y} \end{Bmatrix} = \frac{PL}{AE} \begin{Bmatrix} \frac{1}{3}\sqrt{3}(\sqrt{3}-1) \\ -\frac{1}{6}(9\sqrt{2}\sqrt{3}-\sqrt{2}+4\sqrt{3})\sqrt{2}\sqrt{3} \\ 0 \\ -8 \\ 0 \\ -8 \\ -\frac{1}{3}\sqrt{3}(\sqrt{3}-1) \\ -\frac{1}{6}(9\sqrt{2}\sqrt{3}-\sqrt{2}+4\sqrt{3})\sqrt{2}\sqrt{3} \end{Bmatrix} \approx \frac{PL}{AE} \begin{Bmatrix} 0.423 \\ -11.3 \\ 0 \\ -8.00 \\ 0 \\ -8.00 \\ -0.423 \\ -11.3 \end{Bmatrix} \quad (2-75)$$

taking into consideration the effect of the symmetry conditions on the results of the un-modeled portion of the truss. To obtain the results of the full truss problem subjected to the load vector \underline{F}_s , we simply need to multiply the results of Section 2.2.2 by the appropriate linearity constant:

$$\underline{U}_s = \frac{3}{2}\underline{u}_s = \frac{3}{2} \begin{Bmatrix} u_{2x} \\ u_{2y} \\ u_{3x} \\ u_{3y} \\ u_{4x} \\ u_{4y} \\ u_{5x} \\ u_{5y} \end{Bmatrix} = \frac{3}{2} \frac{PL}{AE} \begin{Bmatrix} \frac{1}{3}\sqrt{3}(\sqrt{3}-1) \\ -\frac{1}{6}(9\sqrt{2}\sqrt{3}-\sqrt{2}+4\sqrt{3})\sqrt{2}\sqrt{3} \\ 0 \\ -8 \\ 0 \\ -8 \\ -\frac{1}{3}\sqrt{3}(\sqrt{3}-1) \\ -\frac{1}{6}(9\sqrt{2}\sqrt{3}-\sqrt{2}+4\sqrt{3})\sqrt{2}\sqrt{3} \end{Bmatrix} \approx \frac{PL}{AE} \begin{Bmatrix} 0.634 \\ -16.9 \\ 0 \\ -12.0 \\ 0 \\ -12.0 \\ -0.634 \\ -16.9 \end{Bmatrix} \quad (2-76)$$

Similarly, the results of the anti-symmetry analysis in Section 2.2.3 (\underline{u}_a) expanded to the same order of the full truss problem can be expressed as

$$\underline{u}_a = \begin{Bmatrix} u_{2x} \\ u_{2y} \\ u_{3x} \\ u_{3y} \\ u_{4x} \\ u_{4y} \\ u_{5x} \\ u_{5y} \end{Bmatrix} = \frac{PL}{AE} \begin{Bmatrix} 1-\sqrt{3} \\ \frac{1}{6}(3\sqrt{2}\sqrt{3}+5\sqrt{2}+12)\sqrt{2} \\ \frac{8}{3} \\ 0 \\ 1-\sqrt{3} \\ 0 \\ 1-\sqrt{3} \\ -\frac{1}{6}(3\sqrt{2}\sqrt{3}+5\sqrt{2}+12)\sqrt{2} \end{Bmatrix} = \frac{PL}{AE} \begin{Bmatrix} -0.732 \\ 6.23 \\ 2.67 \\ 0 \\ -0.732 \\ 0 \\ -0.732 \\ -6.23 \end{Bmatrix} \quad (2-77)$$

taking into consideration the effect of the anti-symmetry conditions on the results of the un-modeled portion of the truss. And, we may obtain the results of the full truss problem subjected to the load vector \underline{F}_A by multiplying the results of Section 2.2.3 by the appropriate linearity constant:

$$\underline{U}_A = \frac{1}{2}\underline{u}_a = \frac{1}{2} \begin{Bmatrix} u_{2x} \\ u_{2y} \\ u_{3x} \\ u_{3y} \\ u_{4x} \\ u_{4y} \\ u_{5x} \\ u_{5y} \end{Bmatrix} = \frac{1}{2} \frac{PL}{AE} \begin{Bmatrix} 1-\sqrt{3} \\ \frac{1}{6}(3\sqrt{2}\sqrt{3}+5\sqrt{2}+12)\sqrt{2} \\ \frac{8}{3} \\ 0 \\ 1-\sqrt{3} \\ 0 \\ 1-\sqrt{3} \\ -\frac{1}{6}(3\sqrt{2}\sqrt{3}+5\sqrt{2}+12)\sqrt{2} \end{Bmatrix} = \frac{PL}{AE} \begin{Bmatrix} -0.366 \\ 3.11 \\ 1.34 \\ 0 \\ -0.366 \\ 0 \\ -0.366 \\ -3.11 \end{Bmatrix} \quad (2-78)$$

To obtain the same results as the full model analysis in Section 2.2.1, we simply must superimpose the results of the above half model analyses to obtain:

$$\underline{U} = \underline{U}_S + \underline{U}_A = \begin{Bmatrix} u_{2x} \\ u_{2y} \\ u_{3x} \\ u_{3y} \\ u_{4x} \\ u_{4y} \\ u_{5x} \\ u_{5y} \end{Bmatrix} = \frac{PL}{AE} \begin{Bmatrix} 0.634 \\ -16.9 \\ 0 \\ -12.0 \\ 0 \\ -12.0 \\ -0.634 \\ -16.9 \end{Bmatrix} + \begin{Bmatrix} -0.366 \\ 3.11 \\ 1.34 \\ 0 \\ -0.366 \\ 0 \\ -0.366 \\ -3.11 \end{Bmatrix} = \frac{PL}{AE} \begin{Bmatrix} 0.268 \\ -13.8 \\ 1.34 \\ -12.0 \\ -0.366 \\ -12.0 \\ -1.00 \\ -20.0 \end{Bmatrix} \quad (2-79)$$

Note that any discrepancy between the results above and those of Section 2.2.1 is due to rounding errors in expressing the exact solution in decimal form using floating-point arithmetic. This discrepancy was also expected considering the fact that the decimal solution has been presented to only three significant figures. A check of this analysis indicated that there is no discrepancy between the exact solutions.

Chapter: 3 Design and Performance of Heavy Hauler Bodies

3.1 Construction and Fabrication

The standard dump body for most mining trucks is a welded, steel plate structure consisting of flat floor, sidewall and canopy components with an intricate pattern of box-style stiffeners on the outer sides of each. An array of floor stiffeners (called bolsters) run from side to side, while two main rails (called stringers) run lengthwise. Where the two intersect, the main rails are cut to fit over the bolsters and the intersection seam is continuously welded. The floor bolsters are not of a regular, constant cross-section. Instead, they vary in cross-section providing greater stiffness towards the centerline of the structure.

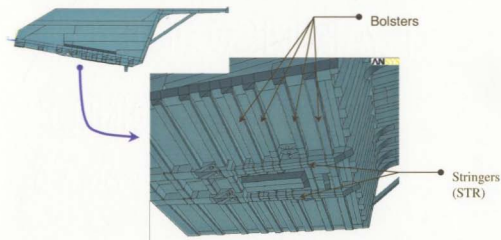


Figure 3-1: Floor Stiffening Arrangement

Size restrictions, imposed by transportation limitations, prevent the entire truck from being assembled at the manufacturing facility. The only way to access or transport goods to the mine sites north of Fort McMurray, Alberta is by a provincial highway. Considering the fact that a fully assembled haul truck is too large to be driven on conventional highways, it is impossible to deliver them in one piece. Instead, large portions are assembled at the factory and transported to the site by tractor-trailer. Final assembly occurs on-site where manufacturing and assembly tools are limited in comparison to the manufacturing facility. In the case of the dump body, the body arrives in several separate pieces and is arranged for welding upside down supported by jacks and blocks, often outdoors on the ground.

Weld repairs, as well, are quite often carried out with the dump body laid upside down outdoors. Cracks and cracked welds are ground away completely with hand-held grinders, and the original volume of material is replaced with multiple weld passes until the original weld fillet is built-up. In some circumstances, SCL replaces the original weld specifications with heavier, more robust weld sizes. Although it is possible to stress relieve such weld repairs with strap-on heat packs, no stress relieving of any sort is carried out on these repairs. The result is that the replacement welds themselves are no better suited to resist cracking, and the cracks quickly return.

3.2 Operational Performance

It is a full time effort for SCL's truck maintenance group to keep these heavy hauler mining trucks running continuously. Haul truck operators work on 12-hour shifts taking only 1-hour worth of breaks daily. At end of each shift, another operator takes over keeping the truck in constant service. These trucks, however, do come out of service on a regular basis for scheduled maintenance. Things like engine oil changes, gearbox oil changes, electrical system inspection and maintenance, and recharging of the suspension strut pressures are necessary to keep the truck operating properly. After a certain number of operating hours, even the engine module gets rebuilt. Because of the lead-time required to rebuild an engine module, a spare engine module is used to keep the fleet operating constantly.

All regularly scheduled maintenance repairs occur at a specified number of operating hours. Quite often, however, repairs are required for incidental occurrences. From time to time, certain items like handrails, stairs and brackets need repair. Other times, trucks are damaged by accidents such as contact with other mining equipment; for example, the shovel operator may contact the haul box while loading. While such repairs are a common part of heavy hauler operation, they are all caused by circumstances outside of what would be referred to as 'regular service'. All heavy haulers at Syncrude mine sites, however, develop some degree of cracking in the dump body during regular service, which requires weld repair on a regular basis. Although these repairs are required regularly, they should not be considered a part of regular truck maintenance. At present,

these non-incidental repairs are a continuous cost of operation, and should be reduced if not eliminated in the future.

This perpetual cracking occurs in the welds forming the intersections between the widthwise and lengthwise floor stiffeners (bolsters and stringers respectively). These regions of interest will hereafter be referred to as bolster-stringer intersections. Cracking seems to develop first on the inside of the stringers, near the hinge pivots, even after very short periods of regular service (Figure 3-2). If left un-repaired, the cracks will propagate until all of the bolster-stringer intersection welds have eventually cracked.

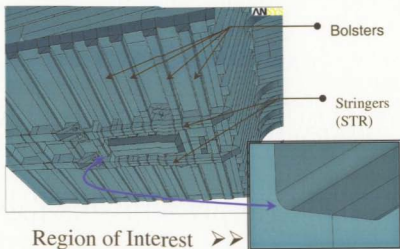


Figure 3-2: Location of Floor Stiffener Cracking

3.3 Weld Repair Costs

Heavy hauler floor stiffener cracking is such a problem in oil sand mining operations that trucks are inspected with Non-Destructive Testing (NDT) to track the extent of crack

growth whenever the truck undergoes routine maintenance such as oil changes. In the case of the Komatsu 930E fleet in operation in the Mildred Lake mines, \$248,753 was spent on welding crack repairs alone in these eight trucks over a period of 2 years and 9 months, according to the work orders entered into the Syncrude process information system (Appendix A). In terms of shop time, 3473 man-hours in total were put in to repairing the cracked welds in the Syncrude maintenance shops. Not included in these costs are the charges of getting work done at an outside contractor's site, where the bulk of large repair overhauls and modification work is done.

To minimize the downtime impact on production required to continually repair floor stiffener cracking, a spare body is used. For a fleet of eight trucks, the ninth (spare) body is continuously out-of-service getting weld repairs. Although fleet downtime is significantly reduced with this spare body, it does represent another \$306,000 in a capital expense. In short, floor stiffener cracking is an ongoing and very expensive problem associated with running a fleet of heavy haulers. The company is currently investigating several options to reduce or minimize these costs, including purchasing new body designs. This work is providing insight as to the cause of these problems, which will assist in the decision making process.

Chapter: 4 Stress and Deformation Modeling

4.1 Modeling Methodology

4.1.1 Requirements and Limitations

The primary factors that govern the complexity of a FEA model are the structural geometry, loading conditions, and the information to be extracted from the model. The intricate pattern of reinforcement in this structure need only be included in sufficient detail to model the results of interest. Incorporating a level of detail beyond this would waste both model creation time and valuable computational resources. The information of primary interest from this FEA model is the state of stress at the many bolster-stringer intersections, where cracking is a continual problem. To investigate the stress at these locations, the overall deformation of the haul body floor must be accurately modeled in the analysis. To capture this deformation, the flat plate stiffening arrangement has been modeled in detail.

During regular mining operations, the entire truck structure experiences a combination of static, dynamic and impact loading. While dynamic and impact loading would produce stresses within the structure greater than that of static loading, a static analysis has been used for the purpose of this investigation. The reason for this is that although a dynamic analysis would better reflect the nature of the loading, it would also require an analytical effort well beyond what was achievable in the desired timeline. In addition, a

prerequisite for any dynamic analysis is to understand the static response in detail. This work identifies, for the first time, the damage mechanism and source responsible for floor stiffener cracking.

Since FEA is a numerical analysis technique, the limitations of the computer software and hardware must also be considered. A significant effort has been put into making this FEA model as efficient as possible. This includes efficiency in data storage, computational effort, and overall serviceability and adaptability of the model. Perhaps the most valuable feature of the ANSYS 5.5.3 finite element software package used in this analysis is the ability to use input files. Input files are standard text files containing a sequence of commands to be executed by the software. Instead of saving the FEA model database files directly, a much smaller text file containing the commands used to assemble the model can be stored instead. At present, the ANSYS software does not have a simple 'undo' command for correcting simple mistakes made during model creation. Using input files, small mistakes may be corrected easily by editing the text file. In addition, using the ANSYS parametric design language (APDL) it is possible to include logic statements, program loops, as well as statements calling other input files to be read.

All of the geometry creation, material property selection, mesh sizing, and even analysis commands used in this analysis have been assembled into a hierarchy of thirty-six such text based input files. The first input file (called I_MAIN_INPUT) is at the top of the

hierarchy, and breaks the work into discrete sections such as geometry creation and meshing. Each section then contains call statements for input files that contain the appropriate commands for that portion. The 2_series of files setup the analysis options and build the model geometry. The 3_series of files assign the appropriate material thickness settings to the geometry areas. The 4_series of files apply the element mesh and boundary conditions for the analysis. While the 5_series of files contain commands for viewing and analyzing the results of the haul body analysis. The 6_series of files contain commands for a shell-to-solid sub-model analysis, which will be discussed later. The 7_series of files were used to model the frame of the haul truck supported on uneven strut forces, and as will be discussed later the 8_series of files combine both the frame and body FEA models. A printed copy of these thirty-six text based files is contained in Appendix B.

As mentioned previously, the software used for this analysis was ANSYS version 5.5.3. This software is licensed for use at SCL's Edmonton Research Center. Unlike university versions that are restricted to 32,000 nodes, this software does not restrict the size of the FEA models that can be analyzed. Instead, computer hardware offers the only modeling limitations. The platform on which the software runs is a DEC Personal Workstation 600au (EV 5/6chip 600 MHz) with a Digital Unix alpha 4.0D operating system. With 1.256Gb of physical memory, 1.270Gb of swap disk space, and 28Gb of storage capacity in a Raid disk, this platform was more than sufficient to solve the largest FEA models used in this analysis.

4.1.2 Element Selection

Two groups of elements are applicable for this type of analysis: shell and solid elements. Shell elements efficiently model the behavior of thin plates provided that the assumptions made in the element formulation are acceptable, and offer a significant reduction in computational effort when compared to a similar analysis using solid elements. The SHELL93 element has a quadratic displacement shape function that produces a linear strain distribution within the element. Bending stresses vary linearly through the thickness, while the transverse shear stresses are assumed constant through the element. This element is well suited to efficiently model the global behavior of the steel plate structure.

Shell elements are limited, however, in that they represent stresses through the material thickness as a linear variation from one surface to another. If greater detail is required, then shell elements will not suffice. In a three-dimensional model, such information can only be obtained through a discretization of volume elements. When compared to an equivalent shell element model, the number of elements and DOF associated with a volume element analysis is enormous. Conducting a volume element analysis of the entire body structure is beyond the solution capabilities of the computer hardware used in this project; hence, it simply was not feasible.

If required later, a Shell-to-Solid sub-model analysis using SOLID95 elements could be used. In a sub-model analysis, results of a larger and coarser global model are used to

form the boundary conditions for a smaller and more refined sub-model. This technique makes it possible to analyze specific regions in detail without having to refine and resolve the entire FEA model. By using solid elements in the sub-model, it is possible to see the results of interest in greater detail than is possible with a shell element analysis alone. The shell element or global model would adequately describe the structural response of the entire body to various loading scenarios, while the solid element sub-model would 'feed' off of these results to reveal the state of stress in localized regions in much greater detail. Presently, however, such detail has not been required and this analysis option has not been used.

4.1.3 Meshing

Meshing is the term used to describe the discretization of the model geometry into discrete or 'finite' elements. Two meshing options are available in the ANSYS software package: free and mapped meshing. Mapped meshing allows the user to directly control the element size and pattern during the discretization process. Through such control, clean, uniform and efficient meshes are possible resulting in lower solution times. Free meshing uses computer algorithms to automatically discretize the model geometry. These algorithms respond to the geometry, refining the mesh near regions of detail such as small curves and angles. The primary advantage of free meshing is the speed of mesh generation. By adjusting the algorithm parameters, meshes of varying density can be generated quickly, which is particularly useful in establishing convergence.

The meshing technique used in this model, however, was a combination of both. In the ANSYS software package, it is possible to exercise direct control of the mesh sizing at some locations of the model, while allowing the free meshing routines to generate the mesh and discretize the remaining geometry automatically. In this way, the advantages of both meshing options are exploited.

4.2 Boundary Conditions

The accuracy of FEA results are highly dependant on the accuracy of the boundary conditions (BCs) applied to the model. It is therefore, a major concern of this study to adequately represent the support and load conditions on a working haul truck box. Often, the results of interest are sensitive to some BCs and not sensitive to others. It is important to understand this sensitivity in order to effectively evaluate the effect assumptions have on the results of interest. For BCs that are not sensitive, general engineering judgment may be sufficient, whereas BCs that are sensitive to the results of interest may require a much more judicial effort.

4.2.1 Symmetry

If a model is symmetrical about one or more planes, in terms of both loading and geometry, then symmetry BCs can be used to dramatically reduce the computational effort required in obtaining a solution. A 930E haul body is geometrically symmetrical about a single plane down the middle of the structure. For analyses in which both the applied loading and support conditions are symmetrical about this plane as well, only half of the structure needs to be modeled (see Figure 4-1). Along the plane of symmetry, BCs

are applied to represent the effects of the other half of the model. More specifically, the nodal displacements are not permitted to cross the plane of symmetry, and nodal rotations out of the plane of symmetry are held at zero.

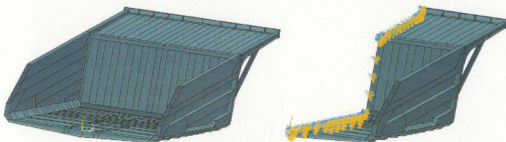


Figure 4-1: 930E Body Full Model Geometry and Symmetry Model with BCs

In situations where the applied loading or the support BCs are not symmetrical about this plane, the symmetry condition cannot be used. If the applied load or displacement is equal and opposite on the other symmetrical half of the model, on the other hand, anti-symmetry conditions may be used along the cut plane. Symmetrical and anti-symmetrical loads may be analyzed separately and superimposed to study the combined effect of each. This technique was used extensively in the trial analyses that identified the need to study support displacement in detail, which will be discussed in Chapter 5.

For asymmetrical loading situations, or verification of superimposed half-model results, a full finite element model has to be assembled. The input routines used for this FEA model have been created in such a way that this poses no significant challenge.

However, solution times of a full model FEA are as much as four times that of a half model analysis. Whenever possible, half model analyses were conducted to save time.

4.2.2 Initial Supporting Conditions

In order to obtain a solution, initial supporting conditions were applied to the model geometry. These conditions are meant to simulate the supporting effect the frame has on the haul body when the truck is stationary sitting on level ground, an ideal situation. It later became evident that frame displacement is a source of structural loading, and an entirely different means of supporting the body structure in a FEA will be discussed in detail later. The following initial supporting conditions were used to start the analysis process.

Haul truck dump bodies have three support locations: a hinged pin connection at the rear of the truck frame, a rubber pad distributed support condition along the main beams of the frame, and hinged pivot connections to the hoist cylinders. For this analysis, the lowered box position only will be considered, so the effect of the hoist cylinder supports in this position has been ignored. The distributed support condition of the rubber pads along the front stringers of the frame has been represented by constraining the displacement in the vertical direction $U_y=0$ on the areas representing the stringer bottom plate (see Figure 4-2). Such solid-model BCs are transferred to the nodes of the finite element mesh when a solution is initiated.

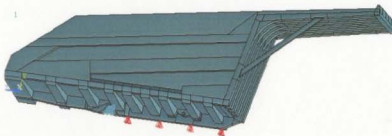


Figure 4-2: Stringer Distributed Support Boundary Condition

Representing hinge pivot conditions effectively is often a considerable challenge. For the present load case, the structure is not expected to rotate significantly about the center axis of the hinge pin. Rather, the bearing forces of the weight resting on the pin were deemed significant. The weight resting on the pin was represented by constraining $U_y=0$ on the lines that make up the top of the hinge pivot holes. To resist any forward motion, due to the 9° slope of the floor, the constraint $U_z=0$ was applied to the lines that make up the rear of the same pivot holes (see Figure 4-3).

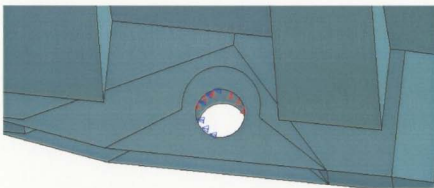


Figure 4-3: Hinged Pin Boundary Conditions

4.2.3 Ore Load Application

The most significant force that is applied to a truck body is pressure on the inside faces due to the weight of a full load of oil sand. This pressure distribution is a function of the oil sand soil mechanics and the pile shape. The version of FEA software used is limited in that pressure gradients may be specified on only one coordinate direction at a time. To apply the distributed load of a rounded pile of oil sand, some amount of discretization and approximation was necessary. One option was to break the inside face areas into a number of sections, applying appropriate face pressures as required. While this manual discretization would be effective, a more adaptive, adjustable concept proved to be much more useful.

An ANSYS algorithm that applies face pressures to elements based on their location within the structure was developed. The result is a much finer pressure discretization than would be attempted manually, and one that is directly proportional to the mesh density of the inside face areas. With this algorithm, rounded pressure distributions were now possible, circumventing the ANSYS single gradient limitation. Most importantly, the algorithm allows for adjustments in the pressure distribution with minimal effort. In this way, the effect of off-center loads and oversized loads can be investigated for a variety of soil types and conditions.

4.2.3.1 Approximate Profile Shape

The only established standards for haul box design are the Society of Automotive Engineers (SAE) Standard J1363⁵ and the International Standards Organization (ISO)

Standard 6483⁶, which is the same as the SAE standard adopted without modification. The interesting thing about these standards is that both are capacity ratings only. They make no reference to the types of material being hauled, no reference to the forces expected in service, and specify nothing with respect to structural strength. Instead, they specify a detailed way to measure the volumetric rating, or the volume of material that the body can carry, for any given body geometry. While the volumetric rating is useful in comparing the capacity ratings of different bodies, it has little relevant use in haul body design. The ore load shape specified suggests a 2:1 slope above the haul body sidewalls and a 1:1 slope near the rear (Figure 4-4). Such a shape is impossible because no known material would form two separate slopes when poured naturally.

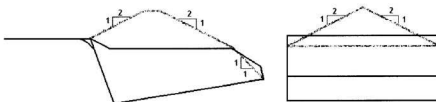


Figure 4-4: SAE J1363 Capacity Rating

In addition, using this shape as a load profile has been shown to be a poor estimator of the true center-of-gravity location. Philipi-Hagenbuch, a producer of patented lightweight haul body designs, suggests that the center-of-gravity location predicted by the established standards is not accurate when compared to on-site investigations⁷. The result of this is that the true center-of-gravity location is offset from the location for

which the truck has been designed, and the weight distribution onto the frame is affected accordingly. To develop lightweight bodies that also correct the center-of-gravity location onto the truck frame, Philipi-Hagenbuch uses a patented profiled shape that more accurately represents the load shapes seen on individual customer sites.

For similar reasons, it was decided that a more realistic shape than the established standards should be used in this analysis. From a recent payload study⁸, side profile and rear profile pictures were collected for a number of oil sand payloads along with their corresponding weigh scale weights. Some minor editing of the pictures was done to accentuate the features of interest, namely the floor and front wall lines, and the oil sand pile profile lines. The trend line fitting feature of Microsoft Excel was used to determine relative functions describing the geometry (Figures 4-5 and 4-6).

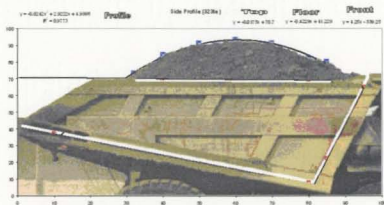


Figure 4-5: Side Profile Shape from Payload Study Picture



Figure 4-6: Rear Profile Shape from Payload Study Picture

Using symbolic math software, the picture rotation effect was subtracted from the shape functions, and known box dimensions were used to return to a true scale. Once scaled, it was then possible to create a three-dimensional function to approximate the payload observed. The average of nine different approximate payload functions was used to develop a simplified shape function (Figure 4-7) shown here along with the floor and front wall planes.

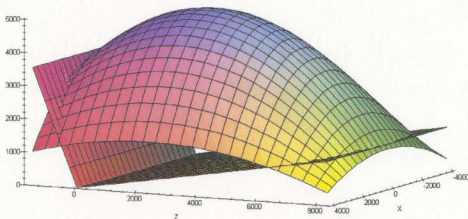


Figure 4-7: Approximate Profile Shape Function

Mathematically, the above function can be described in mm units as follows:

$$PROFILE = MaxHeight * \left[1 - \left(\frac{X - XPeak}{4850} \right)^2 \right] * \left[1 - \left(\frac{Z - ZPeak}{6650} \right)^2 \right] \quad (4-1)$$

where *XPeak* is the location of the pile peak offset from the centerline of the truck, *ZPeak* is the location of the pile peak measured from the floor - front wall edge, and *MaxHeight* is the height of the pile peak from that same floor - front wall edge. *MaxHeight* in mm can be expressed as a function of oil sand mass and density in the range of interest (250 ~ 400 short tons):

$$MaxHeight = \left(22.2 * \frac{Mass}{Density} \right) + 1020 \quad (4-2)$$

where *Mass* is expressed in metric tonnes (te) and *Density* is expressed in metric tonnes per cubic meter (te/m^3).

In a word of caution, it should be noted that this is not meant to be a statistical representation of the ore shapes expected in an oil sand mine. It does not include such factors as seasonal soil properties, large lumps, rocks, etc. This representation is not intended to be used for any other purposes such as the studies used to optimize shovel-loading practices. It does, however, provide an easily adjustable load shape that is more representative of reality than the established SAE standards.

4.2.3.2 Soil Mechanics

The next step in the ore load application scheme was to determine the pressures on the inside faces as a function of this approximate load shape. Using the same soil mechanics principles used in foundation design, the pressures on the walls of this dump box can be broken down into vertical and lateral components. The vertical pressure σ_v is simply:

$$\sigma_v = \rho gh \quad \text{or} \quad \sigma_v = \gamma h \quad (4-3)$$

where ρ is the density of oil sand (kg/m^3), g is the acceleration due to gravity (9.81 m/sec^2), and h is the height of the column of soil directly above the area in question (Figure 4-8).

The horizontal or lateral load exerted on a frictionless, vertical wall varies linearly with a maximum pressure at the base (see Figure 4-8). According to Das in *Principles of Foundation Engineering*, the Rankine lateral earth pressure at the base is $\sigma_h = K_a \sigma_v$ where K_a is the Rankine active pressure coefficient⁹:

$$K_a = \tan^2(45 - \phi/2) \quad \text{or} \quad K_a = (1 - \sin \phi)/(1 + \sin \phi) \quad (4-4)$$

and σ_v is the vertical pressure evaluated at the base of the wall. The angle ϕ refers to the angle of repose, or the soil friction angle. The commonly accepted value for oil sand from the Athabasca oil sand deposit is 33° .

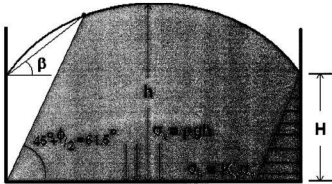


Figure 4-8: Soil Pressure Components

The presence of a sloped pile near the wall has the effect of applying a surcharge to the lateral earth pressure. According to Bowles in *Foundation Analysis and Design*, this effect is incorporated as an increase in the Rankine active pressure coefficient as follows¹⁰:

$$K_a = \cos \beta \frac{\cos \beta - \sqrt{\cos^2 \beta - \cos^2 \phi}}{\cos \beta + \sqrt{\cos^2 \beta - \cos^2 \phi}} \quad (4-5)$$

where β is the average slope angle for the active wedge as defined in Figure 4-8. Theoretically, it is impossible for the angle β to be greater than the angle of friction ϕ . Since β is usually a few degrees less than ϕ , the value $\beta \approx 30^\circ$ was chosen as a good estimate resulting in $K_a \approx 0.5$.

4.2.3.3 Load Application Algorithm

The final step in this load application scheme was to write an algorithm that would autonomously apply an appropriate pressure to the face of each element based on its location within the structure. An overview of the algorithm is as follows.

First, a number of parameters are set to allow for adjustment including total payload, density, K_a , as well as the location of the pile peak (for off center loads). The areas that form the inside face of the floor, side and front walls are selected and defined as components for ease of selection later. A specific component (e.g. the front wall) is selected for load application and all the elements making up that component are selected as well. The algorithm then enters a loop indexing through all of the selected elements, executing the commands below.

The algorithm addresses each element by indexing through the elements numbers of the currently selected element set. Entering the loop, the element index is set at the minimum selected element number. After processing that element, ANSYS APDL commands are issued which set the element index to the next selected element number, and the process commands are repeated. Once all the selected elements have been processed, the APDL commands will deliver a value of zero for the next available element number, which causes the loop to be exited.

The first step in processing each element is to determine the appropriate lateral and vertical pressure components for that element. APDL commands are issued which collect the three-dimensional coordinate location of the element centroid. The height of the column of soil directly above the element centroid is determined by evaluating the height of the load shape function by substituting in the element X and Z coordinates into the function stated earlier, and subtracting the Y co-ordinate of the element centroid. The vertical pressure on the element is then calculated by substituting this column height into the equation $\sigma_v = \rho gh$.

Calculating the lateral pressure on the element is a little more involved. As described earlier, the lateral pressure varies linearly from a maximum pressure at the base. For each element location, this base pressure must first be determined. The base pressure is defined as $\sigma_h = K_a \rho g H$ where H is the vertical height up the sloped wall where the oil sand surface and the wall intersect (see Figure 4-8). The appropriate lateral pressure for the element location is then determined using the ratio of element centroid Y co-ordinate to the active height H .

Lastly, the calculated pressures are applied directly to the element face as a constant pressure. This is done by superimposing the normal-to-face components. The normal-to-face component of the vertical pressure is $\sigma_v \cos \theta$ where θ is the angle between the wall and the horizontal plane (see Figure 4-9), and $\sigma_h \sin \theta$ is the normal-to-face component of the lateral pressure. The pressure components along the element face are

neglected since the wall is assumed frictionless. This assumption is valid in the presence of vibration since any friction effects on the walls will dissipate as the oil sand settles.

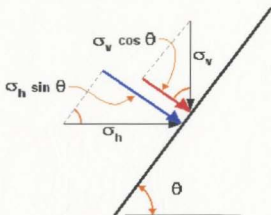


Figure 4-9: Superposition of Normal-To-Face Components

The above process is repeated for all selected elements until appropriate pressures have been applied to all of the elements within the component. Then, the next component is selected (e.g. the floor) and the process is continued with a similar methodology. The result is a well discretized pressure profile on the inside element faces (Figure 4-10).

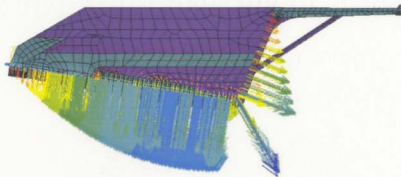


Figure 4-10: FEA Model After Pressure Application

4.3 Mesh Convergence

4.3.1 Preliminary Mesh

There is a need to demonstrate convergence of the results from a finite element mesh. The mesh must be such that further refinements are not justified since no significant improvement in the results can be expected. To demonstrate this, a suitable quantifier is needed. The initial concept was to refine the mesh until convergence of the stress pattern in an area of interest was achieved. A coarse mesh of the entire geometry was produced (Figure 4-11) with the applied loading and initial support conditions described above, and a solution was initiated.

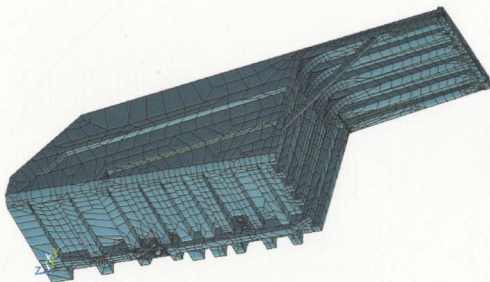


Figure 4-11: Coarse Mesh of 930E Box Structure

Bending stresses are setup in the floor due to the weight resting outside of the central supports resulting in a near uniaxial state of stress in the lower plate of the closed-form bolster stiffeners. Given the simplicity of the stress in this region and its proximity to the troublesome bolster-stinger intersections, this location was isolated as a suitable region to demonstrate convergence of the finite element mesh. The state of stress in one such bolster stiffener may be examined by mapping the mid-plane stress results to a path function or a line drawn down the centerline of the lower bolster plate (see Figure 4-12). Mapping the mid-plane stress results omits the effects of localized bending near the bolster-stinger intersections, which will be discussed in detail later. At this time, the overall bending, or global deformation, of the floor stiffener is the result of interest.

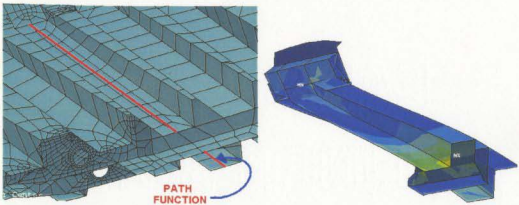


Figure 4-12: Path Function on Bolster, and Plot of Stress Results

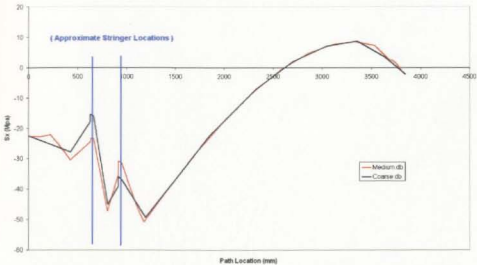


Figure 4-13: Bolster Path Mid-Plane Stress Results

Figure 4-13 is a plot of the mid-plane stress results with respect to the path length for the test case examined. As expected, the central portion of the stress pattern resembles that of a bending moment diagram for a beam subjected to a distributed load. Compressive stress in the lower plate increases in magnitude towards the direction of the stringer, or main rail. As the bolster passes through the stringer, some discontinuity is expected. The tension seen in the lower plate near the outside of the bolster path can be explained due to the deformed shape of the stiffener. The outer portion of the floor is attached to the sidewall of the body. As the floor plate deforms downward, one would expect the wall to rotate outward. However, the sidewall resists deflection since it is attached to the front wall, and as a result, there is a change in the curvature of the floor. This effect is less

pronounced in bolster stiffeners further away from the front wall where the sidewall stiffness is considerably less.

With respect to mesh quality, the stress pattern along the span of the bolster is smooth and seems to change little with mesh refinement. Near the stringer intersection, on the other hand, the results are very erratic, discontinuous, and change significantly with mesh refinement. For these reasons, it is obvious that further mesh refinement in this area is required. In addition to this, this location is precisely the location of the persistent floor stiffener cracking problems. Therefore, demonstrating a reliable convergence in the results of this region is of particular importance. Uniformly refining the mesh over the entire structure produced cumbersome models, excessive solution times, and minimal improvements in the results of this region. In order to produce a suitably converged mesh, within the limitations of the computer hardware, an efficient refinement methodology was required.

4.3.2 Estimating Solution Error

The error approximation technique included in the ANSYS software is an elegant means of proving reliable convergence. It estimates the amount of solution error due specifically to mesh discretization. The structural energy error (SERR) is a measure of the discontinuity in the stress field from element to element, while the percentage error (SEPC) indicates the relative amount of error due to a particular discretization.

The continuity assumption used in many displacement-based finite element formulations results in a continuous displacement field from element to element, but a discontinuous stress field. To obtain more acceptable stresses, averaging of the element nodal stresses is done within the ANSYS software. *Element nodal* data consist of the element derived data, such as stresses and strains, calculated at the interior integration points and then extrapolated to the nodes¹¹. The POST1 postprocessor averages component tensor or vector data at nodes used by more than one element to arrive at a smoothened *nodal solution*.

The error approximation technique incorporated into the ANSYS software package is similar to that given by Zienkiewicz and Zhu¹². Using these averaged nodal stresses, the processor returns to the element level and evaluates the discrepancy between the averaged results and the results of each element. The stresses at each node of each element are processed to yield:

$$\{\Delta\sigma_n^i\} = \{\sigma_n^a\} - \{\sigma_n^i\} \quad (4-6)$$

where: $\{\Delta\sigma_n^i\}$ = stress error vector at node n of element i

$$\{\sigma_n^a\} = \frac{\sum_{i=1}^{N_e^n} \{\sigma_n^i\}}{N_e^n} \text{ averaged stress vector at node } n$$

N_e^n = number of elements connecting to node n

$\{\sigma_n^i\}$ = stress vector of node n of element i

Then for each element, the energy associated with this stress error (structural energy error, or SERR) is evaluated similar to the concept of strain energy:

$$e_i = \frac{1}{2} \int_{vol} \{\Delta\sigma\}^T [D]^{-1} \{\Delta\sigma\} d(vol) \quad (4-7)$$

where: e_i = energy error for element i

vol = volume of the element

$[D]$ = constitutive matrix

$\{\Delta\sigma\}$ = stress error vector at points as needed (evaluated from all $\{\Delta\sigma_n\}$ of this element).

The total energy associated with discontinuity in the stress field, or energy error, is:

$$e = \sum_{i=1}^{N_e} e_i \quad (4-8)$$

where: e = energy error over the entire (or part of the) model.

N_e = number of elements in the model or part of model.

Energy error can be normalized against the total strain energy to give some measure of the effect on the results of interest. This can be defined over the entire solution domain, or for element subdomains. When calculated over localized regions, it is more meaningful.

$$E = 100 \left(\frac{e}{U + e} \right)^{\frac{1}{2}} \quad (4-9)$$

where: E = percentage error in energy norm (or SEPC)

$U = \sum_{i=1}^{N_e} E_{ei}^{po}$ strain energy over the entire (or part of the) model

E_{ei}^{po} = strain energy of element i

Although it is a good indicator of mesh quality, the percentage error in energy norm (or SEPC) gives little direct information about the stresses. An estimation of the upper and lower stress bounds considering the effect of discretization error is available. Again, these results are more meaningful when evaluated over a localized element subdomain rather than the entire solution domain.

$$\sigma_j^{min} = \min(\sigma_{j,n}^a - \Delta\sigma_n) \quad (4-10)$$

$$\sigma_j^{max} = \max(\sigma_{j,n}^a + \Delta\sigma_n) \quad (4-11)$$

where min and max are defined over the selected nodes, and:

σ_j^{min} = output quantity for nodal minimum of stress (SMNB)

σ_j^{max} = output quantity for nodal maximum of stress (SMXB)

j = subscript for particular stress component or combined stress component

$\sigma_{j,n}^a$ = averaged stress quantity j at node n

$\Delta\sigma_n$ = root mean square of all $\Delta\sigma_i$ from elements connecting to node n

$\Delta\sigma_i$ = maximum absolute value of any component $\Delta\sigma_n^i$ for all nodes of the element

4.3.3 Adaptive Refinement

The above ANSYS error estimation technique gives the user the tools necessary to evaluate the effectiveness of a FEA discretization, to decide where the mesh should be refined, and the effect discretization error has on the results of interest. When applied to the initial mesh of the 930E body bolster stiffener region, the drastic need for mesh refinement can clearly be seen. A plot of the structural energy error (SERR) reported for

each element clearly shows which regions of the structure are highly stressed and have a large stress discontinuity, and thus require significant mesh refinement (see Figure 4-14).

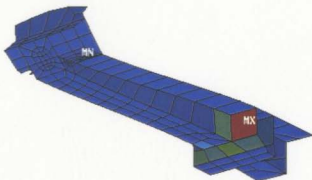


Figure 4-14: Coarse Mesh SERR in Bolster Stringer Region

With each refinement iteration, the SERR values reported for each element steered the refinement efforts into the region where the bolster stiffener and the stringer main rail intersect. After considerable refinement in this region, the mesh shown in Figure 4-15 was produced. Note the extensive refinement in the lower edge of the outer bolster-stringer intersection.

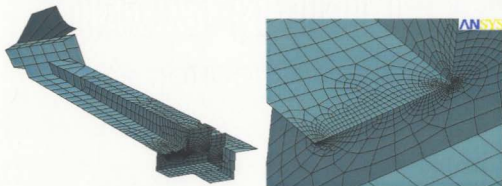


Figure 4-15: Refined Mesh in Bolster Stringer Region

Although mesh refinement reduced the structural energy error in the bolster-stringer region considerably, it was noticed that some error always remained in the sharp corner regardless of the level of refinement (Figure 4-16).

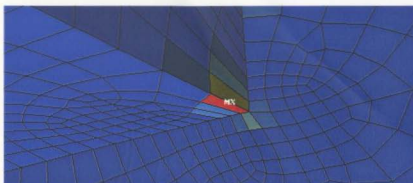


Figure 4-16: SERR in Sharp Corner

The explanation for this has to do with the way that ANSYS estimates solution error. As stated previously, the post-processor averages the element nodal stresses, and the discrepancy between the individual element results and the averaged results is used to evaluate discretization error. In a corner section, shell elements in two or more intersecting planes share common nodes. During the element nodal solution averaging process, component stresses in three separate planes are averaged. The problem arises from relative magnitudes. When subjected to displacements along a particular plane, the elements in that plane will develop large stresses in comparison to the elements experiencing out-of-plane displacement. The result is a discontinuity in the element nodal solution. Since this averaged solution is used to estimate discretization error, some error will always be predicted in shell element corner transitions.

The need to demonstrate a suitable convergence of the results in this region remains. As before, the mid-plane stress results of this refined mesh were mapped to a path function in the location shown in Figure 4-12. By comparing the results alongside those of an unrefined mesh, considerable refinement especially in the region of interest can be clearly seen (Figure 4-17). The two spikes in the solution data correspond to the location of the bolster-stringer intersections.

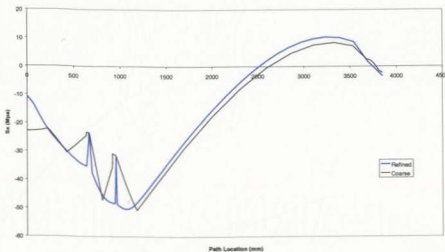


Figure 4-17: Bolster Path Mid-plane Stress Results

To understand the structural behavior in this region, in light of this numerical discontinuity, let us zoom in on this region of interest to have a closer look (path length: 625mm–975mm). The *Element Nodal Solution* line represents data mapped from the averaged element nodal results, while the *Element Solution* line represents data mapped from the element solution directly with no averaging of results (Figure 4-18). In order to explain the spike in the element solution results, an explanation of how ANSYS maps

results to path function is necessary. For each path point, elements are searched to find elements containing that geometric location¹³ and the results from the first element found are mapped to the path. Therefore, within an element thickness of the intersection, element solution data may be obtained from stringer elements rather than the bolster elements. A sharp transition from a compressed state to a near zero stress state can be seen at both intersection locations, because un-averaged stress results are mapped from the out-of-plane stringer elements instead. The averaged results at these intersections appear as less sharp spikes in the otherwise continuous plot.

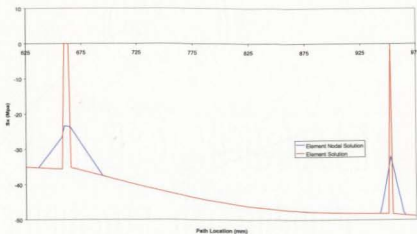


Figure 4-18: Path Mid-plane Stress Results (Bolster - Stringer Intersection)

To confirm this explanation, a similar path results plot was produced with only the bolster stiffener elements selected (Figure 4-19). The result: the intersection effect in the averaging of element nodal data has been eliminated because the out-of-plane stringer elements are no longer selected. Since the structural energy error in this region is less

than other, less important regions and the numerical discontinuity effects have been accounted for, the mesh was considered sufficiently converged.

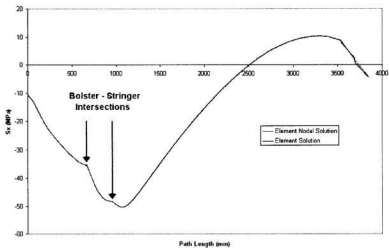


Figure 4-19: Path Results with Only Bolster Elements Selected

Chapter: 5 Analysis, Results and Implications

5.1 Bolster-Stringer Stress

Away from the bolster-stringer intersection, the compressive stresses in the bolster are relatively uniform across the bolster width. At the bolster-stringer intersection, however, the compressive stresses are greatest in the two corners near the bolster sidewalls (Figure 5-1). In order to interpret useful information from this region, a better understanding of the state of stress needed to be developed. Searching for an explanation of this stress, trials were conducted on a simplified geometry with similar support conditions. This smaller, more efficient model enabled faster manipulation of geometry, boundary conditions, and FEA modeling techniques.

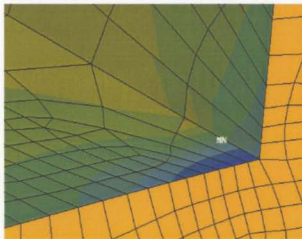


Figure 5-1: Compressive Stresses at a Bolster-Stringer Intersection

5.1.1 Rounded Corner Trial Analysis

The first trial was a shell element representation very similar to the bolster stiffener of the full FEA model. Some subtle differences include the fact that the tapered bolster is replaced with a stiffener of uniform cross section, and the stringer wall is modeled as a single plate in this investigation. When subjected to load conditions similar to the full FEA model, (pressure on the top surface and $U_y=0$ on the base of the stringer plate) this trial structure develops a similar state of stress at the bolster-stringer intersection (Figure 5-2).

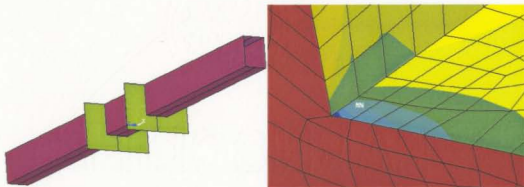


Figure 5-2: Square Section (Bolster-Stringer Stress Trial)

In reality, however, this sharp corner does not exist. On the dump body studied here, bolsters are formed from a single piece of steel with a 38mm rounded corner in this region. The box-like representation above was a geometric modeling simplification. As it will be demonstrated shortly, this representation of the corner does adversely affect the results, and as a result, this oversimplification had to be revisited. The second trial

5.1.2 Solid Element Trial Analysis

In the analyses thus far, the geometry has been modeled using shell type elements that cannot geometrically represent the fillet weld in this region. To validate whether shell elements effectively model the stress in this region, another trial was conducted using solid-volume brick elements (SOLID95) and the same loading conditions as the two previous trials (Figure 5-4). This time, however, the 12 mm full penetration fillet weld that exists in this region was included.

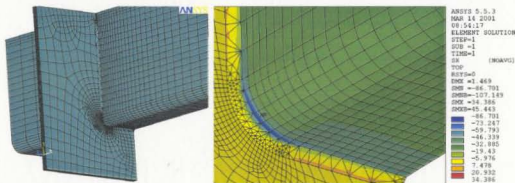


Figure 5-4: Solid Section (Bolster-Stringer Stress Trial)

To explain the stresses near this welded joint, it is helpful to consider the rounded corner section separately. Vertical stresses exist in this region that are set up to equilibrate the vertical load applied to the truck box floor. These vertical forces cause an upward deflection in the plate, which results in a highly localized bending stress (Figure 5-5).



Figure 5-5: Localized Bending (Bolster-Stringer Stress Trial)

Figure 5-6 is a plot of the stress results in the direction of the bolster centerline (σ_x). Bending stresses appear as a variation of σ_x through the thickness of the material. When superimposed over the $\approx 45\text{MPa}$ of compressive membrane stress set up due to the global bending of the bolster stiffener, this secondary bending stress reduces the magnitude of σ_x on the inside surface of the bolster plate to $\approx 7\text{MPa}$, and increases the magnitude of σ_x on the outside surface to $\approx 87\text{MPa}$ of compression.

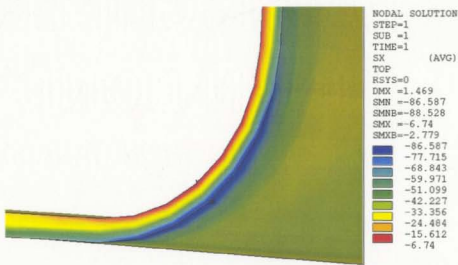


Figure 5-6: Stress Variation through Material Thickness

The purpose of these trial analyses was to shed some light on the state of stress in the bolster-stringer intersection region, and to evaluate whether a shell element finite element model is suitable to study the same. The rounded corner trial indicated the need to correct the oversimplification in the bolster-stringer intersection corner in order to obtain meaningful FEA results. The solid element trial solution linked the high stresses in the corner to the presence of localized bending in the region. And, a comparison of the results of the shell element and solid element trial solutions indicate a difference in the outer compression magnitudes of only 5%. With this it was concluded, that the shell element model does reasonably predict the presence and magnitude of both the global and localized stresses in the corner region. By retrofitting the haul body FEA model with proper rounded bolsters, meaningful results at the many troublesome bolster-stringer intersections can be obtained.

5.2 Frame Twist as a Source of Structural Loading

With the shell element model corrected, it was possible to model the stresses present within the structure set up to equilibrate the applied loading and the resulting deformations. Figure 5-7 is a rear-view, schematic diagram of a typical section of a dump body floor. Under the weight of the ore load, the stiffened floor arrangement deflects slightly as illustrated by the exaggerated deformation shown in red. Resulting from this 'global deformation', a slight tensile stress exists in the floor plate, stresses vary linearly down the stiffener sidewalls, and a uniform, compressive membrane stress is setup through the thickness of the stiffener lower plate.

In addition to this, there is some 'local deformation' in the immediate vicinity of the bolster-stringer intersection. The curvature of the plate results in a bending stress component superimposed onto the compressive membrane stress in the area (Figure 5-7). For both the ore load and the self-weight of the structure, the membrane and local bending stresses in this region combine to form compression throughout the plate thickness. Compression, however, does not explain the source of the extensive cracking problems in this area.

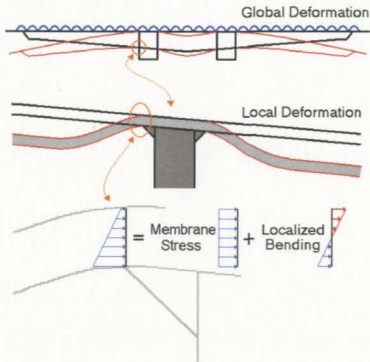


Figure 5-7: Localized Bending at Bolster-Stringer Intersection

Crack growth is usually caused by some form of alternating tension. In order to explain the extensive crack growth observed in the floor stiffener intersections, a state of stress producing tension at the outer edge of the material thickness must be demonstrated. At this stage, the hypothesis was that localized bending could be present in the region that is in reverse to the bending demonstrated thus far. If present in sufficient magnitudes, this localized bending could overcome the compressive membrane stress in the area resulting in a variation through the thickness with tension present at the outside edge (Figure 5-8).

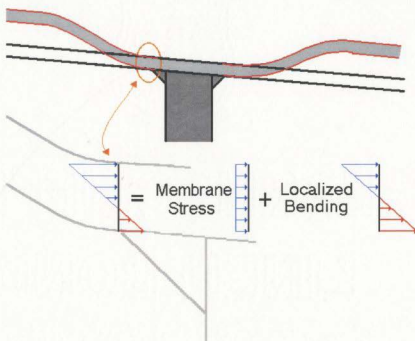


Figure 5-8: Reversed Localized Bending

5.2.1 Frame Displacement Trial Analyses

The frame or chassis of any heavy hauler mining truck is essentially the backbone of the entire truck structure. When a fully loaded haul truck with a gross vehicle weight of over

one million pounds drives over uneven ground, the frame is subjected to some very intense forces. As the wheels drive over bumps and sink into holes, a certain amount of deflection within the frame can be expected. Deflection within the frame directly translates into displacement of the dump body supports, which is a form of structural loading.

At this stage, the magnitude and mode shape of the frame deflections that could be expected during regular service were not known. Instead, trial mode shapes were applied to see what effect they would have on structural loading. Two modes of frame displacement were investigated using a half model with anti-symmetry conditions along the center plane. With this scenario, any force, pressure or displacement applied to the half model has the effect of being accompanied by an equal and opposite load applied to the other half. In other words, the frame displacements studied are assumed anti-symmetrical about the truck centerline.

Mode #1 (Figure 5-9) is a representation of frame twist, defined as a displacement arrangement in which the vertical deflection varies linearly from a 2mm difference at the stringer nose to an equal and opposite 2mm difference at the hinge pin. Mode #2 (Figure 5-10) is a uniform frame displacement of 2mm from the stringer nose to the hinge pin. These two trial displacement modes may be scaled and or superimposed to represent other feasible displacement patterns, and superimposed with the ore load and self-weight

to investigate the combined effect on the structural deformation. Studying their effects separately, however, offers more insight into the damage mechanisms seen in service.

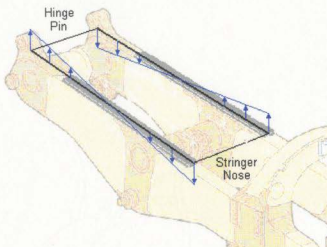


Figure 5-9: Trial Frame Displacement Mode - Twist

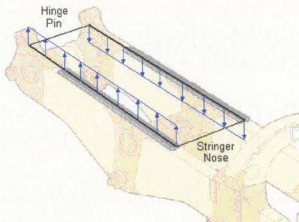


Figure 5-10: Trial Frame Displacement Mode – Uniform

The uniform displacement mode resulted in negligible stresses. The reason for this is that a shear displacement pattern in the frame will not be transmitted to the body through the rubber support pads. As each side deflects upward or downward, the stringers are free to rotate which causes a slight roll producing no significant stresses within the structure.

Initially, the frame twist results produced a similar state of stress to that of the ore load, but larger in magnitude. That is, global bending of the floor plate resulting in a compressive membrane stress in the lower plate of the bolster, and localized bending at the stringer intersection resulting in a variation of the in-plane stresses through the material thickness. The combined state of stress at the intersection weld is, again, predominately in compression.

According to the anti-symmetry assumption, however, the frame twist applied to the other side is in the opposite direction. To investigate the response of the other side, the frame twist displacement mode can be inverted by multiplication with a scale factor of -1. This inverted frame twist produced equal-and-opposite results, this time, with the state of stress predominately in tension. The implication is that frame twist does produce reversed localized bending in the bolster-stringer intersections that may explain the cracking in this region.

In reality, this frame twist structural loading would coexist with the ore load. When superimposed, this 2mm trial mode of frame displacement was more than sufficient to

overcome the compression results of the ore-load, producing tension at the outside edge of the material thickness at the fillet weld toe (Figure 5-11). It is important to note, however, that these findings were the result of an assumed shape and magnitude of frame displacement. The frame deflections present in reality may produce different results. Nonetheless, this analysis does demonstrate the fact that frame twist can explain the cracking problems present, and a more detailed analysis to determine the true extent of frame deflections was warranted.

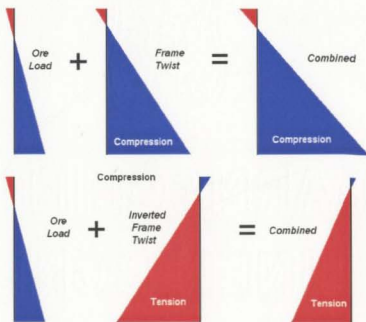


Figure 5-11: Superimposed Ore Load and Trial Frame Twist Results

5.2.2 Frame Displacement Verification

Initially, the extent of frame deflection was to be determined through a direct measurement. The data collected would have served as an excellent input, validating the support boundary conditions of the analyses. Although multiple means of measuring frame deflections were proposed, no feasible alternatives were found. The most promising concept involved a beam welded to both sides of the frame main rails and instrumented with strain gauges to monitor deflection within the beam. The concept was ruled out, however, due to the inability to differentiate between relative vertical deflection and rotation of the ends of the beam. The need to gather physical inputs to validate the results remained, despite the fact that there was no feasible means of directly measuring frame deflection. The alternative was to model the frame of the haul truck using FEA and using strut pressure data as the physically collected input.

The frame of a typical haul truck consists of box section main rails, tubular cross members, and castings at critical stress transition zones. Near the front, a rigid horse collar structure accommodates the strut mounts while providing clearance for the engine and associated propulsion equipment. For the purpose of this analysis, frame stresses at critical locations are not of interest; rather, capturing the true deflection shape is the intent. Hence, the model created represents the overall dimensions and metal thickness properly. However, details and features that would have little effect on the overall deformation of the frame have been omitted (see Figure 5-12). The de-featured FEA

model is sufficient to capture the true deflection shape, but frame stresses at transition regions should be ignored.

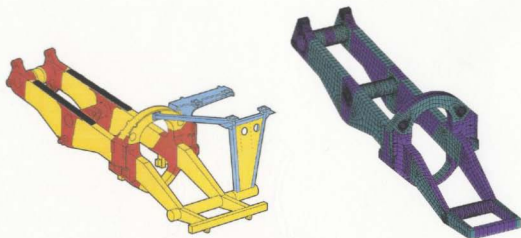


Figure 5-12: Haul Truck Frame¹⁴ and De-featured FEA Model

5.2.2.1 Strut Force Boundary Conditions

Modern haul trucks are equipped with telemetry capable of monitoring most of the onboard vital systems. The truck investigated here was equipped with pressure transducers in each of the four hydro-pneumatic suspension struts for use in a payload metering system. By attaching a laptop to the onboard payload meter, it was possible to acquire real-time pressure data at a rate of 50 Hz. It was then possible to determine the corresponding forces and moments applied to the frame using the strut active areas collected from the manufacturer, and relevant dimensions (moment arms) that were measured directly.

In the FEA, the four struts are modeled as spring elements. At the rear, the struts are attached to the frame with a clevis pin mounted in a spherical bushing. This ensures a straight line-force with no significant moment applied to the frame. In the FEA, the line-forces from the spring elements are distributed evenly over the nodes representing the clevis pinhole. At the front, the upper strut housing is rigidly bolted to the horse collar at four locations. Here, both a vertical force component and an associated moment are transferred to the frame structure (Figure 5-13). In the FEA, a rigid region is defined between the nodes of the strut mount and a node located the appropriate distance away to capture the moment arm effect. This way, the vertical strut force present in the spring element is transferred to the horse collar as both a vertical force and moment.

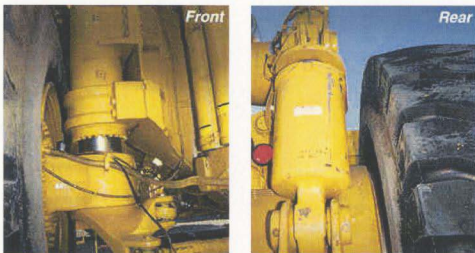


Figure 5-13: Front and Rear Suspension Struts¹⁵

Much of the strut pressure data collected for this investigation was collected with the truck moving. For the most part, this was done to interfere with normal production as little as possible. By multiplying the force difference between the right and left struts by

the appropriate moment arm, moments about the truck centerline exerted onto the frame by the front and rear strut-pairs can be plotted (Figure 5-14). As can be seen, these forces are dynamic in nature. This analysis, however, is purely static. Each haul run begins with the truck parked next to the shovel getting loaded with ore (see Figure 6-1). The underfoot conditions at this location are characterized by soft uneven ground. The data used for this FEA was the static strut pressures after the last shovel bucket of ore is placed into the dump body, and the truck is stationary momentarily before being cleared to proceed along the haul route (shown in red, Figure 5-14).

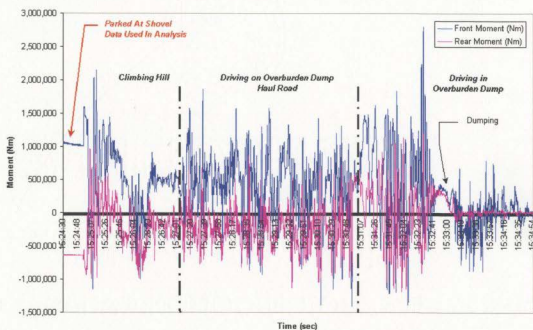


Figure 5-14: Front and Rear Moment Data Calculated from Strut Pressure Data

A large component of the raw strut pressure data, however, is the weight of haul truck including the engine, propulsion systems, etc. To remove this component, averages of

dynamic data were collected with the truck 'running empty' along a relatively smooth portion of the haul road. These running empty average pressures were then subtracted from the raw data leaving only the ore load component of the strut forces. In the FEA, the self-weight of the body and frame were neglected, leaving only the ore load to be in equilibrium with these strut forces. The end result was that the frame twist demonstrated in this analysis is due solely to the way the ore load is distributed onto the four struts while the truck is parked on uneven ground.

5.2.2.2 Haul Body - Frame Interaction

Modeling the interaction between the frame and the haul body using conventional boundary conditions (forces, pressures, displacements, etc.) would have been difficult. The weight of the body and ore load is distributed onto the hinge pins and rubber pads, and this distribution changes significantly as the frame twists. Since a FEA model of the dump body was already in existence, the simplest solution was to import the model combining both body and frame into a single FEA, leaving it to the software to work out the appropriate force transfer between them.

The rubber pad support was modeled by meshing the region between the dump body stringers and the main rails of the frame with solid elements. Modeling the hinge pin connection, however, was a little more difficult. It was necessary to form a connection between the two models that accurately represented the force transfer and allowed free rotation about the pin axis. Defining a rigid region comprised of the nodes representing the pinholes, would accomplish the force transfer. Without allowing the rotation DOF

about the hinge, however, there was a risk of over-constraining the FEA model. Instead, the following hinge-pin representation scheme was devised.

The pinholes for the body and frame are nearly concentric in the FEA model because in the real structure there is a slight clearance to allow for rotation about the hinge. For each hole, a node was placed in the center of the circle and a series of very stiff springs connect this center node to the outer nodes of the circle forming a 'wagon wheel' pattern. For each near pair of holes, all of the center node degrees of freedom were coupled using constraint equations with the exception of rotation about the pin axis. Thus, the nodes in this region are forced to behave much like a real pin connection (Figure 5-15).

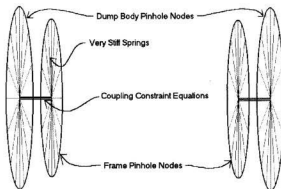


Figure 5-15: 'Wagon Wheel' Representation of Hinge Pin Connections

Ideally, these very stiff springs would have been defined as rigid regions. Problems were encountered, however, in that the master node of a rigid region cannot be used in other constraint equations. The reason for this has to do with how constraint equations are

handled by the solution process. Constraint equations define a relationship between the nodal DOF of a group of nodes called slave nodes and one master node. When processed by the software, the nodal DOF for each of the slave nodes are condensed out of the element stiffness matrix, keeping only those of the master node. If a master node for one constraint equation is used as a slave node in another, errors occur. What happened here was that the constraint equations coupling the DOF at the center would be processed, condensing one of the center nodes out of the stiffness matrix. When the constraint equations defining the rigid region were processed, a master node was named that no longer existed in the stiffness matrix, and the solution would terminate. This scenario would work as long as the constraint equations were processed in the right order. The ANSYS software, however, offered no means of controlling the order of constraint equation processing. The problem was circumvented by replacing the rigid region links between the pinhole and center nodes with a series of very stiff springs instead.

There was also a concern that adding large stiffness constants may adversely affect the condition of the element stiffness matrix, which would in turn adversely affect the reliability of the results. This was addressed by choosing a spring constant that was stiff enough to be considered rigid with respect to this region of the FEA model, but was no larger than the highest pivot term reported by the solver in previous solutions. In other words, the large terms added to the matrix for these stiff springs were no larger than the largest already there, and the condition of the matrix was not adversely affected.

5.2.2.3 Combined Frame - Body FEA Results

Figure 5-16 is a picture of the frame and body FEA model used for the frame twist analysis. The many colored arrows indicate the pressure applied to the inside faces of the body by the weight of the ore load. The spring elements representing the four struts can be seen in light blue. At the top of each spring element, rigid region constraint equations distribute the line-forces onto the appropriate nodes of the frame. At the lower ends of each strut spring, displacement boundary conditions constrain all nodal displacements.

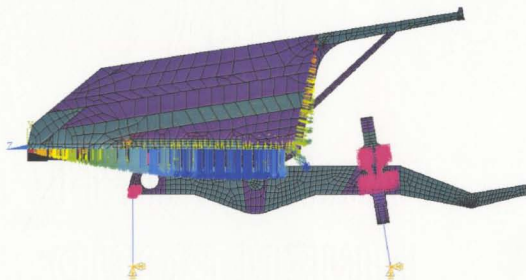


Figure 5-16: Frame and Dump Body FEA Model

The most pronounced shape of displacement observed with this frame analysis was torsion about the truck centerline. That is, the frame twists like a corkscrew in response to the opposing moments applied by a difference in the two front strut forces and the two

rear strut forces. In the FEA, front and rear strut force differences were applied as vertical displacement differences in the lower nodes of the front and rear strut springs.

According to the collected strut pressure data, the moments about the truck centerline for the front and rear struts do not balance. This means, there is a significant moment component coming from the fact that the ore load is placed slightly off-center in the body. Even though the moment arm of ore load resulting force is a little as 145mm (the dump body is 8m wide), this moment must be taken into consideration in order to capture the true frame torsion present. It was possible to capture this effect by offsetting the load shape slightly in the load application algorithm. This would require, however, integrating the load shape function to determine the appropriate amount to offset the load. Instead, time was saved by applying a force couple that balanced the front and rear moments. This couple was applied as line forces acting along both outer edges of the body floor, far away from any regions of particular interest.

Ideally, we would like to re-run this analysis with an offset load shape rather than a force couple correction. Unfortunately, the resources required to re-solve the FEA model are no longer available. The version of ANSYS used by Memorial University of Newfoundland is the University high option, and is limited to 32,000 nodes. This finite element model was assembled and solved on an unlimited version of the ANSYS software licensed for use at SCL's Edmonton Research Center. The combined frame and dump body FEA model described here has over 930,000 nodes. Re-meshing the model to

fit under the 32,000 node restriction would have detrimental effects on the convergence of the results.

The effect that frame torsion had on the dump body was as expected. Frame torsion causes localized bending in some bolster-stringer intersections, which result in tensile stresses. Furthermore, this occurs most extensively near the hinge pivots. This result is supported, at least in Syncrude's experience, by the fact that the bolster-stringer intersections in this region develop cracks first, regardless of the make or model of the haul truck. Under static conditions, parked fully loaded on uneven ground, the intersection between the sixth bolster from the front and the left-hand-side stringer had the greatest amount of tension present. To be more specific, the tension was present on the inside edge and the rearward-most rounded corner of the innermost bolster-stringer intersection (see Figure 3-2).

The bolster stiffeners in this hinge pin region are slightly different from those described earlier in that they are slightly smaller and are not tapered. Instead, they have a constant cross-section from the outer edge of the one stringer to the outer edge of the other. Outward from the stringers, these bolster stiffeners have a tapered cross-section like the rest. As described by Figure 5-17, the exaggerated results of the shell element model indicate the presence of localized bending stresses in this bolster-stringer intersection. The hypothesis presented earlier was that this bending would be reversed completely from that described in Figure 5-7, and would look similar to Figure 5-8. When subjected

to a realistic frame deflection, however, the results were in fact a combination of both. Nonetheless, at the outer edge of this intersection, the bolster bottom plate is deformed upward, which is the appropriate direction to produce tension in the material near the weld toe.

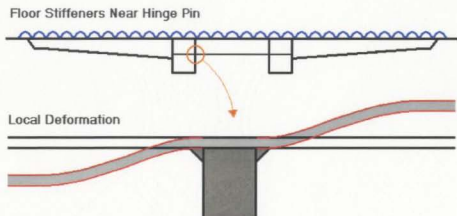


Figure 5-17: Floor Stiffener Deformation near Hinge Pins

The top and bottom results of the shell elements on either side of the stringer intersection indicate the state of stress through the bolster, with the assumption of a linear variation through the material thickness. From the trial analyses of Section 5.1, it was noted that the stress results at the corner intersection of a shell element analysis were not significantly different than the variation of stress through the thickness near the weld toe in a solid element model of the same region. It was therefore concluded that the shell element model does adequately represent this region, and the results obtained can be interpreted as follows:

The top and bottom results on the inward side of the intersection are -70 MPa and -170 MPa respectively (see Figure 5-18). The interpretation of this is that superimposed onto 120 MPa of uniform, compressive membrane stress in this area is 50 MPa of a pure bending stress. The combined state of stress, however, is entirely in compression. On the outer edge, where cracking commonly occurs, the situation is different. This time, the top and bottom results indicate -168 MPa and $+100$ MPa respectively. Again, a secondary bending stress is superimposed onto a compressive membrane stress, however, this time the bending stress of 134 MPa is great enough to overcome the 34 MPa of compression, producing tension near the weld toe. This tension is causing the crack propagation problems of the area.

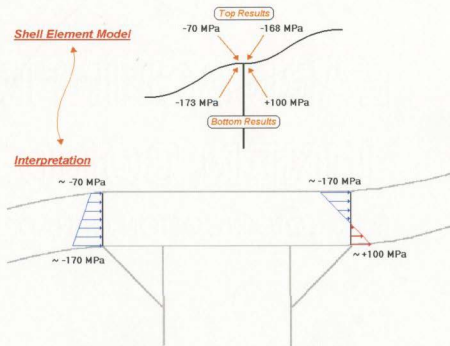


Figure 5-18: Interpretation of Shell Element Model Results

Again, it should be noted that this was an analysis of a static situation only. To reiterate slightly, the above analysis indicated that the frame of a mining truck does deflect under normal operating conditions, resulting in a displacement of the dump body supports, which is a form of structural loading. In response to this support displacement, localized bending stresses in some bolster-stringer intersections near the hinge pivots reverse with sufficient magnitude to produce tensile stresses. As a fully loaded haul truck drives over uneven ground, the frame can be expected to deflect similar to this, but back and forth, causing the stress at the weld toe to alternate between tension and compression. In addition to this, under dynamic conditions, one would expect the peak tension to be greater than that seen here under static conditions. It is the presence of alternating tensile stresses greater than 100 MPa, at the toe of a weld with poor fatigue resistance, that is causing the extensive cracking problems observed in this area.

Chapter: 6 Conclusions and Future Directions

The static analysis presented in this work, models the frame deflection of a fully loaded haul truck, parked at the shovel on uneven ground, prior to commencing a haul run (similar to Figure 6-1). In addition, this analysis models the effect this deflection has on the dump body, and the results indicate the presence of tensile stresses in the floor stiffener intersections. Since this deflection is actually a twist along the truck frame, we can expect that it will twist back and forth, as the truck drives over uneven ground, resulting in an alternating state of compression and tension. The magnitudes observed would easily explain fatigue cracking if present in a dynamic environment; and it is expected that a dynamic analysis of this truck would produce stresses greater than observed here. In conclusion, frame deflections caused by normal service conditions are the primary cause of fatigue cracking in the bolster-stringer intersections of mining truck dump bodies in oil sand operations.



Figure 6-1: Haul Truck Parked at Shovel, Receiving Last Load Pass

The frame, being the backbone of the entire truck structure, is the most crucial, most studied, and most analyzed part of the trucks design. Changing frame designs to better suit the dump body is not something that is likely to happen. The haul body, being significantly cheaper, is much more likely to be modified. It is the recommendation of this work to account for movement in the haul body supports when analyzing or designing future mining truck haul bodies.

New and improved haul truck designs, however, will do nothing to reduce the cost of maintaining existing fleets. Many companies, such as SCL, have large fleets of mining trucks currently in service. What can be done to mitigate the cost of weld repairs to these floor stiffener intersections? Several feasible alternatives exist including: replacing the current dump body design with one chosen specifically for its ability to accommodate frame deflections, and modifying existing body designs to improve the fatigue strength of the floor stiffener intersections.

6.1 Entire Body Replacement

Most standard haul truck bodies have a traditional box-style bolster-stringer floor stiffening arrangement, which has been demonstrated to not respond well to the normal frame deflections of the truck during service. Other stiffening arrangements, however, may accommodate frame torsions better. One such body design, by the Chilean manufacturer Dicsa-Tricon, is called the DT-HiLoad (shown in Figure 6-1). The DT-

HiLoad is a lightweight design with an unconventional floor stiffening arrangement currently being considered by SCL's truck maintenance group to replace the existing bodies for the entire 930E fleet.

The most notable difference in this design with respect to conventional designs is the reduction in the need for external wall stiffeners by utilizing the stiffness of curved plates. Although the floor does contain external stiffeners, they are of an I-Beam construction. Most significantly, the way these widthwise stiffeners intersect with the lengthwise stiffeners is different from traditional designs in that the intersection is not welded in place. Instead, reinforced contact pads are placed at the intersection (Figure 6-2). By allowing slight movements at this location, the cracking problems of traditional designs may be reduced.



Figure 6-2: DT-HiLoad Body Design - Close-up of Floor Stiffener Intersection

Synchrude Canada Limited has purchased one such body for trial purposes to see how this design will perform in oil sand mine operating conditions. In addition to this, there is a request from the truck maintenance group to investigate the relative performance of this new design when subjected to the same loading conditions. The recommendation for future work in this area is to conduct a FEA of this lightweight design, applying the same loading conditions studied earlier, and to compare the structural response of both designs. Together with the performance of the trial body soon to be in service, an educated decision should be possible as to which body design should be purchased as a replacement for the entire 930E fleet.

6.2 Modification of Existing Bodies

The other option to reduce the costs of weld repair would be to modify current designs. As stated before, localized bending in bolster-stringer intersections causes high stresses that the welds in the region are unable to withstand. Modifying the structural arrangement to reduce or eliminate this localized bending would be a cumbersome task, and one that is not feasible. Current cracking problems exist, however, not because high stresses exist in this region, but because a weld is located there as well. Intuitively, one could remedy the problem by removing the weld instead of the high stresses.

Although this is much easier said than done, the solution is quite ingenious. Simply cut out the troubled sections of the haul bodies and replace these sections with integral

one-piece components of the same geometry. In the corners currently referred to as the bolster-stringer intersection, localized bending will continue to cause high stresses. These components, however, would be fabricated without welding and would replace the fillet welds of the intersection with rounded corners. This way, the fatigue life of the region would be substantially enhanced. Such components would have to be welded into place, but they can be welded with full-penetration butt-welds at locations away from the localized bending. Under much lower stress conditions, the fatigue life of these welds ought to be satisfactory.

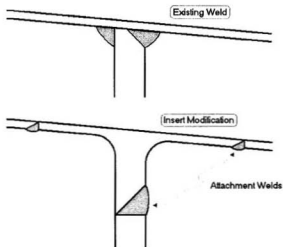


Figure 6-3: Modification Details

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- ¹⁵ 930E-2 Specifications, Komatsu Mining Systems Inc., 2000

Appendix A

Weld Repair Costs

EQUIPMENT	REG_HOURS	OT_HOURS	ACTUAL_COST	EST_HOURS	DESCRIPTION	DATE_BEGIN	DATE_END
45-17-81	10	0 \$	439.41	5	WELDING REPAIRS.		1999/03/06 0:00
45-17-81	6	0 \$	292.39	4	WELDING	1999/05/29 0:00	1999/05/29 0:00
45-17-81	12	0 \$	611.62	6	FIX BOX CRACKS	1999/12/21 0:00	1999/12/21 0:00
45-17-81	4	24 \$	1,797.56	24	REPAIR CRACKS IN BOX AS PER INSPECTION REPORT.	1999/01/05 0:00	1999/01/05 0:00
45-17-81	44	0 \$	2,088.13	24	REPAIR CRACKS IN BOX AS PER INSPECTION REPORT	1999/02/09 0:00	1999/02/09 0:00
45-17-81	14	60 \$	4,838.46	24	REPAIR CRACKS, FAB. AND INSTALL PLATES ON BACK END OF BOX.	1999/04/20 0:00	1999/04/20 0:00
45-17-81	0	0 \$	-	12	REPAIR FRAME AND BOX CRACKS AS PER INSPECTION REPORT.	1999/05/25 0:00	1999/05/25 0:00
45-17-81	1	0 \$	48.48	12	REPAIR CRACKS AS PER INSPECTION REPORT.	1999/09/07 0:00	1999/09/07 0:00
45-17-81	0	0 \$	-	16	REPAIR CRACKS. CHANGE BUSHINGS.	1999/10/12 0:00	1999/10/12 0:00
45-17-81	62	18 \$	4,210.77	24	COMPLETE WELDING REPAIRS AS PER INSPECTION REPORT	1999/11/16 0:00	1999/11/16 0:00
45-17-81	30	0 \$	1,308.60	24	COMPLETE WELDING REPAIRS AS PER INSPECTION REPORT	1999/12/21 0:00	1999/12/21 0:00
45-17-81	273	12 \$	21,983.13	24	WELDING MODS TO DUMP BODY	2000/03/03 0:00	2000/03/03 0:00
45-17-81	105	12 \$	6,809.59	72	COMPLETE WELD REPAIRS ON BOX AS PER INSPECTION REPORT	2000/04/06 0:00	2000/04/07 0:00
45-17-81	18	0 \$	862.05	5	REPAIR BOX CRACKS AS PER REPORT	2000/04/17 0:00	2000/04/17 0:00
45-17-81	0	0 \$	-	5	REPAIR BOX MAIN FRAME CRACKS	2000/06/13 0:00	2000/06/13 0:00
45-17-81	202	0 \$	23,656.91	24	REPLACE DUMP BODY DUE TO FATIGUE AND DAMAGE	2000/07/17 0:00	2000/07/17 0:00
45-17-81	12	6 \$	1,149.20	12	COMPLETE WELDING REPAIRS AS PER INSPECTION REPORT	2000/09/26 0:00	2000/09/26 0:00
Totals:	793	132 \$	70,096.32	317		<i>02 Years 07 Months 23 Days</i>	
45-17-82	20	0 \$	997.43	12	REPAIR CRACKS AS PER INSPECTION REPORT.	1999/12/08 0:00	1999/12/08 0:00
45-17-82	0	0 \$	-	12	REPAIR CRACKS IN BOX AS PER INSPECTION REPORT	1999/01/12 0:00	1999/01/12 0:00
45-17-82	20	0 \$	1,027.39	8	REPAIR CRACKS IN MAIN FRAME OF BOX AS PER INSPECTION REPORT	1999/02/16 0:00	1999/02/16 0:00
45-17-82	0	0 \$	-	8	REPAIR CRACKS ON REAR OF BOX	1999/03/23 0:00	1999/03/23 0:00
45-17-82	0	0 \$	-	8	FIX BOX MAIN BEAM CRACKS AS PER REPORT	1999/07/06 0:00	1999/07/06 0:00
45-17-82	48	0 \$	2,376.22	3	COMPLETE WELDING REPAIRS AS PER INSPECTION REPORT	1999/09/18 0:00	1999/09/18 0:00
45-17-82	24	0 \$	1,086.48	6	WELDING P.M. REPAIRS AS PER INSPECTION REPORT.	2000/02/01 0:00	2000/02/01 0:00
45-17-82	3	0 \$	144.12	3	REPAIR CRACKS AS PER REPORT	2000/05/16 0:00	2000/05/16 0:00
45-17-82	24	0 \$	1,398.77	36	REPAIR CRACKS AS PER INSPECTION REPORT.	2000/06/20 0:00	2000/06/20 0:00
45-17-82	12	0 \$	675.54	12	COMPLETE WELDING REPAIRS ON BOX AS PER INSPECTION REPORT	2000/10/02 0:00	2000/10/02 0:00
45-17-82	11	0 \$	611.55	24	REPAIR CRACKS AS PER INSPECTION REPORT	2000/11/11 0:00	2000/11/11 0:00
45-17-82	0	0 \$	-	3	REPAIR CRACK AS PER REPORT	2000/11/11 0:00	2000/11/11 0:00
Totals:	162	0 \$	8,317.50	135		<i>01 Years 12 Months 04 Days</i>	
45-17-83	0	0 \$	-	36	REPAIR CRACKS IN BOX AS PER INSPECTION REPORT.	1999/03/30 0:00	1999/03/30 0:00
45-17-83	25	2 \$	1,412.22	12	COMPLETE WELDING REPAIRS AS PER INSPECTION REPORT	1999/09/21 0:00	1999/09/21 0:00
45-17-83	149	2 \$	7,245.82	24	REPLACE CANOPY STIFFENER PLATES AND REPAIR CRACKS AS PER INS	1999/10/26 0:00	1999/10/26 0:00
45-17-83	20	0 \$	1,003.44	18	REPAIR CRACKS AS PER INSPECTION REPORT.	1999/11/30 0:00	1999/11/30 0:00
45-17-83	8	0 \$	362.16	8	COMPLETE WELDING REPAIRS AS PER INSPECTION REPORT	2000/03/15 0:00	2000/03/15 0:00
45-17-83	4	0 \$	181.08	6	REPAIR CRACKS AS PER INSPECTION REPORT.	2000/04/18 0:00	2000/04/18 0:00
45-17-83	36	0 \$	2,283.48	24	BOX WELDING AS PER INSPECTION	2000/09/05 0:00	2000/09/05 0:00
45-17-83	36	12 \$	4,797.49	24	REPAIR CRACKS AS PER INSPECTION REPORT.	2000/10/10 0:00	2000/10/10 0:00
45-17-83	0	0 \$	-	12	REPAIR CRACKS AS PER INSPECTION REPORT.	2000/11/14 0:00	2000/11/14 0:00
Totals:	278	16 \$	17,285.69	164		<i>01 Years 08 Months 17 Days</i>	
45-17-84	0	0 \$	-	5	FIX BOX CRACKS AND LADDER	1999/12/22 0:00	1999/12/22 0:00
45-17-84	0	0 \$	-	6	WELDING REPAIRS TO BOX	1999/01/26 0:00	1999/01/26 0:00
45-17-84	0	0 \$	-	12	REPAIR CRACKING AND FISH PLATE REAR OF BOX	1999/04/06 0:00	1999/04/06 0:00

45-17-84	0	0 \$	-	18 REPAIR BOX CRACKING AND EVALUATE WHEEL MOTOR CRACK.	1999/04/06 0:00
45-17-84	0	0 \$	-	12 WELD BOX CRACKS AS PER INSPECTION	1999/05/11 0:00
45-17-84	0	0 \$	-	8 FIX BOX CRACKS	1999/06/15 0:00
45-17-84	0	0 \$	-	7 REPAIR CRACKS AS PER REPORT	1999/07/22 0:00
45-17-84	0	0 \$	-	16 COMPLETE WELD REPAIRS AS PER INSPECTION REPORT	1999/08/24 0:00
45-17-84	36	34 \$	10,185.92	18 COMPLETE WELD REPAIRS AS PER INSPECTION REPORT	1999/12/07 0:00
45-17-84	24	15 \$	2,569.90	24 REPAIR CRACKS AS PER INSPECTION REPORT	2000/01/11 0:00
45-17-84	20	18 \$	2,669.90	24 REPAIR CRACKS TO CANOPY AND MAIN BOX BEAMS.	2000/01/28 0:00
45-17-84	143	33.5 \$	3,496.01	24 COMPLETE WELD REPAIRS ON BOX AS PER INSPECTION REPORT	2000/09/12 0:00
45-17-84	98	6 \$	17,056.29	36 REMOVE AND FLIP BOX TO REPAIR CRACKING	2000/09/12 0:00
45-17-84	8	0 \$	9,810.86	12 REPAIR BOX CRACKING AS PER REPORT	2000/09/12 0:00
45-17-84	41	0 \$	632.56	12 REPAIR BOX CRACKS AS PER INSPECTION REPORT.	2000/10/17 0:00
45-17-84	0	0 \$	2,600.64	24 REPLACE BOX WITH SPARE BOX DUE TO CRACKING	2000/11/23 0:00
Totals:	384	107.5 \$	49,044.58		
01 Years 12 Months 02 Days					
45-17-85	14	0 \$	677.87	8 FIX CRACKS IN BOX	1999/11/24 0:00
45-17-85	12	0 \$	514.20	16 REPAIR CRACKS IN BOX AND INSTALL FISH PLATE AS PER INSPECTIO	1999/05/25 0:00
45-17-85	0	0 \$	-	16 REPAIR BOX CRACKS AS PER ATTACHED REPORT.	1999/06/22 0:00
45-17-85	0	0 \$	-	16 REPAIR BOX CRACKS AS PER ATTACHED REPORT.	1999/07/27 0:00
45-17-85	28	2 \$	3,314.40	8 REPAIR BOX CRACKS AS PER REPORT	1999/09/01 0:00
45-17-85	11	0 \$	526.32	12 REPAIR CRACKS AS PER INSPECTION REPORT.	1999/11/09 0:00
45-17-85	48	6.5 \$	3,186.39	4 REPAIR CRACK TO LEFT SIDE BOX PIN CASTING	2000/03/28 0:00
45-17-85	116	8 \$	6,900.52	18 REPAIR TWO CRACKS IN BOX MAIN FAL	2000/03/28 0:00
45-17-85	36	0 \$	1,828.50	12 COMPLETE WELDING REPAIRS AS PER INSPECTION REPORT	2000/05/02 0:00
45-17-85	24	0 \$	1,229.16	24 REPAIR CRACKS AS PER REPORT	2000/07/11 0:00
45-17-85	34	0 \$	2,156.62	24 REPAIR CRACKS AS PER INSPECTION	2000/08/15 0:00
45-17-85	66	102.5 \$	12,312.29	48 REPAIR BOX CRACKS AS PER INSPECTION REPORT.	2000/09/19 0:00
45-17-85	0	0 \$	-	12 REPAIR BOX CRACKS AS PER REPORT	2000/10/23 0:00
45-17-85	30	0 \$	1,524.12	5 REPAIR BOX CRACKS AS PER REPORT	2000/10/23 0:00
45-17-85	0	0 \$	-	16 COMPLETE WELD REPAIRS ON BOX AS PER INSPECTION REPORT	2000/10/30 0:00
Totals:	419	119 \$	33,870.59		
01 Years 12 Months 06 Days					
45-17-86	0	0 \$	-	36 REPAIR CRACKS, FABRICATE AND INSTALL FISH PLATE	1999/06/28 0:00
45-17-86	0	0 \$	-	36 COMPLETE WELDING REPAIRS AS PER INSPECTION REPORT	1999/08/24 0:00
45-17-86	0	0 \$	-	24 REPAIR CRACKS AT REAR OF BOX	1999/09/09 0:00
45-17-86	0	24 \$	1,751.52	12 BOX WELDING	2000/01/01 0:00
45-17-86	30	12 \$	8,638.36	16 COMPLETE WELDING REPAIRS TO BOX AS PER INSPECTION REPORT	2000/02/10 0:00
45-17-86	78	48 \$	2,261.48	36 REPAIR BOX CRACKS	2000/03/01 0:00
45-17-86	219	2 \$	12,246.70	12 REPAIR CRACKS AS PER INSPECTION REPORT.	2000/03/25 0:00
45-17-86	0	0 \$	-	5 REPAIR CRACK IN OUTBOARD SIDE OF LEFT BOX PIN CASTING.	2000/05/10 0:00
45-17-86	6	0 \$	286.24	8 REPAIR CRACKS AND BROKEN GENERATOR BRACKETS	2000/06/14 0:00
45-17-86	0	0 \$	-	5 REPAIR CRACKS AS PER REPORT	2000/08/24 0:00
45-17-86	134.5	21 \$	11,604.66	24 REPAIR BOX CRACKS AS PER INSPECTION REPORT.	2000/11/01 0:00
45-17-86	3	0 \$	117.00	8 REPAIR CRACKS AS PER REPORT	
Totals:	470.5	107 \$	36,907.86		
01 Years 05 Months 06 Days					
45-17-87	0	0 \$	-	8 REPAIR CRACKS IN UNIT AS PER INSPECTION REPORT	1999/03/25 0:00

45-17-87	0	22 \$	1,592.80	12 REPAIR CRACKS AS PER INSPECTION REPORT.	1999/06/02 0:00
45-17-87	24	0 \$	1,186.17	12 REPAIR CANOPY CRACK AND BOX CRACKS AS PER REPORT	1999/06/28 0:00
45-17-87	14	0 \$	840.00	12 REPAIR 2 LARGE BOX MAIN BEAM CRACKS AND OTHERS IF TIME PERMI	1999/10/09 0:00
45-17-87	44.5	0 \$	1,968.83	24 REPAIR CRACKS AT BACK OF BOX AS MARKED.	1999/10/20 0:00
45-17-87	14	0 \$	2,877.82	24 REPAIR CRACKS IN REAR OF BOX AS PER INSPECTION REPORT	1999/11/24 0:00
45-17-87	14	0 \$	840.00	24 REPAIR CRACKS IN JUNT AS PER INSPECTION REPORT	1999/11/24 0:00
45-17-87	28	41 \$	4,582.71	24 REPAIR CRACKS AS PER ATTACHED REPORT	1999/12/05 0:00
45-17-87	0	0 \$	-	12 REPAIR BOX CRACK AS PER INSPECTION REPORT	2000/01/05 0:00
45-17-87	2	0 \$	96.08	8 MODIFICATION AND REPAIR CRACKS AS PER REPORT	2000/05/17 0:00
45-17-87	26	6.5 \$	2,155.21	9 REPAIR CRACKS AS PER REPORT	2000/07/26 0:00
45-17-87	23	0 \$	1,458.89	18 REPAIR CRACKS AS PER REPORT	2000/10/04 0:00
45-17-87	2	0 \$	114.85	12 REPAIR CRACKS AS PER REPORT	2000/11/10 0:00
45-17-87	0	0 \$	-	12 COMPLETE WELDING REPAIRS AS PER INSPECTION REPORT	2000/11/11 0:00
Totals:	217.5	69.5 \$	16,923.46	01 Years 08 Months 19 Days	
45-17-88	0	0 \$	-	8 PM REPAIRS (WELDING ON BOX) TRANSWEST	1999/02/25 0:00
45-17-88	0	0 \$	-	24 REPAIR CRACKS IN BOX AS PER INSPECTION REPORT.	1999/03/31 0:00
45-17-88	0	0 \$	-	36 BOX WELDING - MODIFY RAILS	1999/04/21 0:00
45-17-88	0	0 \$	-	24 WELDING ON BOX BY TRANSWEST (CRACKING AT REAR)	1999/05/07 0:00
45-17-88	38	4 \$	2,569.60	24 COMPLETE WELDING REPAIRS AS PER INSPECTION REPORT	1999/05/22 0:00
45-17-88	0	0 \$	-	24 REPAIR DAMAGE & CRACKING TO BOX	1999/09/22 0:00
45-17-88	6	0 \$	404.46	12 SANDBLAST BOX AROUND CRACK	1999/10/14 0:00
45-17-88	24	0 \$	1,236.12	48 REPAIR CRACKING IN BOX AND FRAME	1999/10/27 0:00
45-17-89	18	35 \$	3,499.34	24 COMPLETE WELDING REPAIRS AS PER INSPECTION REPORT	1999/11/03 0:00
45-17-89	6	0 \$	5,276.39	4 COMPLETE WELDING REPAIRS AS PER INSPECTION REPORT	1999/11/25 0:00
45-17-89	8	0 \$	362.16	12 COMPLETE WELDING REPAIRS AS PER INSPECTION REPORT	2000/03/16 0:00
45-17-89	0	0 \$	-	36 REPAIR CRACKS IN BOX	2000/03/19 0:00
45-17-89	0	0 \$	-	36 REPAIR BOX CRACKS AT REAR OF BOX	2000/03/26 0:00
45-17-89	45	0 \$	2,127.61	12 REPAIR BOX CRACKS AS PER INSPECTION REPORT.	2000/05/24 0:00
45-17-89	0	0 \$	-	12 REPAIR WELDING AS PER INSPECTION REPORT	2000/06/28 0:00
45-17-89	12	2 \$	831.24	12 REPAIR CRACKS AND INSTALL STIFFENER PLATES AS PER INSPECTION	2000/07/25 0:00
45-17-89	0	0 \$	-	12 COMPLETE WELDING REPAIRS AS PER INSPECTION REPORT	2000/10/12 0:00
Totals:	157	41 \$	16,306.92	01 Years 08 Months 17 Days	

Summary:

Total Cost: \$ 248,753
Cost/Unit: \$ 31,094
Total Cost / Year \$ 86,775
Total Cost / Unit / Year \$ 11,097

Down Time: 3473 Hrs
Down Time / Unit: 43.3 Hrs
Down Time / Year: 1239 Hrs
Down Time / Unit / Year: 155 Hrs

Appendix B

ANSYS Input Files

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❖ **Filename: 1_Main_INPUT**

```
! FEA of 930E Truck Box Structure

*****

!----- Geometry Creation -----
:build
! Setting Analysis Options, Element types, and Material Properties
FINISH
/CLEAR
/CLEAR
/FILNAM,geom
/INPUT,2_1_setup_INPUT,,,setup,0
! /NERR,0,, ! Error Message Suppression
! Creating Geometry and Saving Database
/INPUT,2_2_build_floor_INPUT,,,,0 ! Floor
/INPUT,2_3_build_wall_INPUT,,,,0 ! Wall
/INPUT,2_4_build_front_INPUT,,,,0 ! Front
/INPUT,2_5_build_canopy_INPUT,,,,0 ! Canopy
/INPUT,2_6_round_corners_INPUT,,,,0 ! Rounding Bolster Corners
/INPUT,2_7_SCL_mods_INPUT,,,,0 ! SCL Modifications
! Assigning Thickness and Material Properties to All Areas
/INPUT,3_1_assignprop_floor_INPUT,,,,0 ! Floor
/INPUT,3_2_assignprop_wall_INPUT,,,,0 ! Wall
/INPUT,3_3_assignprop_front_INPUT,,,,0 ! Front
/INPUT,3_4_assignprop_canopy_INPUT,,,,0 ! Canopy
/INPUT,3_5_add_guidepin_INPUT,,,,0 ! Canopy
SAVE
/EOF

!----- Finite Element Model -----
:mesh
FINISH
FINISH
/CLEAR
RESUME,geom.db
! /NERR,0,10000, ! Error Message Suppression
! FE Meshing
/INPUT,4_1_FEA_manual_mesh_INPUT,,,,0 ! Meshing Routine
/FILNAME,mesh
SAVE
/EOF
! Saving Mesh.db
:bcs
FINISH
FINISH
/CLEAR
RESUME,mesh.db
! Boundary Conditions
*SET,hingetyp,2 ! 1=Bearing Forces 2=Rigid about Center
*SET,STRtyp,3 ! 1=Distributed 2=Line 3=Rubber
*SET,lyPin,0,0 ! 1 Ux Applied at HingePin
*SET,lyKeeq,0,0 ! 1 Uy Applied at Nose
*SET,Shim,0 ! 0=Off 1=On
*SET,Amt_Shim,1,0 ! Amount Of Steel Shim Added or Subtracted
*SET,Loadcell,0 ! 0=Off 1=On

/INPUT,4_3_FEA_support_INPUT,,,,0 ! Support BC's
```

```

/INPUT,4_4_FEA_load_algorithm_INPUT,,/home/dw11589/930E_Full,1,
      ! Symmetry Conditions
/INPUT,4_5_FEA_symm_INPUT,,,0      ! Symmetry BC's
/INPUT,4_6_FEA_antisymm_INPUT,,,,0 ! Anti-Symm. BC's

/FILNAM,BATCH
/SAVE                                ! Saving FEA.db

/SOLU
/PIVCHECK,1      ! Pivot Check (Off=0) (On=1)
/ISOLVE          ! Solve Current Load Step
/LSOLVE,1,3,1,   ! Solve Load Steps 1 thru 3, incr 1
/FINISH

/DELETE,BATCH,emat,
/DELETE,BATCH,esav,
/DELETE,BATCH,mntr,
/DELETE,BATCH,stat,
/DELETE,BATCH,trn,      ! Cleanup

/EOF !*****

:post
!-----
!----- Post Processing -----
!-----

/INPUT,5_1_post_StressPath_INPUT,,,0 ! Bolster Path Routine
/INPUT,5_2_post_USUM_INPUT,,,0      ! Plot USUM Routine

/EOF
!-----
!-----
!-----

!-----
!-----
!-----
FINISH
FINISH
/FILNAM,test
/SAVE                                ! Saving test.db
/EOF

:here
FINISH
FINISH
/CLEAR
/RESUME,test.db
/PREP7
/APLOT

!-----
!-----

```

❖ Filename: 2_1_Setup_INPUT

```

!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
!
!                               Analysis Setup
!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!

:setup
/TITLE,Analysis Setup

/NOPR
KEYW,PR_SET,1
KEYW,PR_STRUC,1
/COM,Preferences for GUI filtering have been set to display:
/COM, Structural

/PREP7
ET,1,SHELL93           ! Defining Shell Element Type
KEYOPT,1,4,0
KEYOPT,1,5,0
KEYOPT,1,6,0

! Defining Real Constants
R,3,3,.....           ! 1/8" Exhaust Plenum
R,5,5,.....           ! 5mm Thickness
R,8,8,.....           ! 8mm Thickness
R,9,9,.....           ! 9mm Thickness
R,12,12,.....         ! 12mm Thickness
R,14,14,.....         ! 14mm Thickness
R,16,16,.....         ! 16mm Thickness
R,18,17.7,.....       ! 5mm + 1/2" Thickness
R,19,19,.....         ! 3/4" Thickness
R,21,20.7,.....       ! 8mm + 1/2" Thickness
R,22,21.7,.....       ! 9mm + 1/2" Thickness
R,25,25,.....         ! 1" Thickness
R,29,28.575,.....     ! 5/8" + 1/2" Thickness or 1 1/8" Plate
R,35,35,.....         ! 1 1/8" Thickness
R,38,38,.....         ! 38mm Thickness
R,44,44,.....         ! 3/4" + 1"
R,54,54,.....         ! 1 1/8" + 1" FishPlate
R,63,63.5,.....       ! 1.5" + 1" Thickness
R,90,90,.....         ! 90mm Thickness

! Material Properties
! Material #1
! 690 MPa Tensile Strength
! 620 Mpa Yield Strength
! Elongation in 50mm - 18%
! Modulus is Unknown
UIIMP,1,EX,,207000,    ! Modulus in N/mm^2
UIIMP,1,DENS,,.00000786, ! Density in kg/mm^3
UIIMP,1,PRXY,,.3,

! Material #2
! 1379 MPa Tensile Strength
! Yield Strength Unknown
! Elongation in 50mm - Unknown
! Modulus is Unknown
UIIMP,2,EX,,207000,    ! Modulus in N/mm^2
UIIMP,2,DENS,,.00000786, ! Density in kg/mm^3
UIIMP,2,PRXY,,.0,3,

FINISH
/EOF

```


❖ Filename: 2_2_build_floor_INPUT

```

*****
*****
! FEA of 930E Truck Box Structure
! Floor Geometry Construction Routine

:build

FINISH
FINISH

!CLEAR
!NERR,0,, ! Warning
!Supression
!RESUME,setup.db
!FILNAM,build_floor
!RESUME,geom.db

:/FILNAM,geom
!/TITLE,Building Floor Geometry

/!PREP7

!-----
!----- Floor Construction
!-----
! Defined Parameters

*SET,bxlength,8105
*SET,bxwidth,7915
*SET,tonnes,320

! Creating Keypoints

K,1,0,0,0,
K,2,bxwidth/2,0,0,
K,3,bxwidth/2,0,-bxlength,
K,4,0,0,-bxlength,

FLST,2,4,3 ! Floor Plate Area
FITEM,2,1
FITEM,2,2
FITEM,2,3
FITEM,2,4
A,P51X
CM,_Y,AREA
ASEL,,,1
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 15, 2, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1

!-----
!----- Bolsters
!-----

RH Item #16 ! EG9394 Angle, Rear
! Keypoints

K,5,0,-340,0,
K,6,(bxwidth/2)-120,-115,0,
FLST,2,4,3
FITEM,2,1
FITEM,2,5
FITEM,2,6

FITEM,2,2
A,P51X ! Bottom Area

APLOT
/VIEW,1,1,1,1
/USER,1
/VIEW,1,-0.391990212388,-0.705334606237,
0.590632514036
/ANG,1,174.710908189
/AUTO,1
/REP

! EG9379 Bolster, Rear

RH Item #14
FLST,3,1,5,ORDE,1
FITEM,3,2
AGEN,2,P51X,,-1535,,0! Copying Rear Area to
Location
FLST,3,1,5,ORDE,1
FITEM,3,5
FLST,3,1,5,ORDE,1
FITEM,3,5
AGEN,2,P51X,,-350,,0 ! Copying Area to other
side
FLST,2,4,3
FITEM,2,13
FITEM,2,17
FITEM,2,16
FITEM,2,12
A,P51X ! Creating Bottom

FLST,3,3,5,ORDE,2 ! Item #12
FITEM,3,5
FITEM,3,-7
AGEN,2,P51X,,-2740+1535,,0

FLST,3,3,5,ORDE,2 ! Item #11
FITEM,3,5
FITEM,3,-7
AGEN,2,P51X,,-3690+1535,,0

FLST,3,3,5,ORDE,2 ! Item #10
FITEM,3,5
FITEM,3,-7
AGEN,2,P51X,,-4360+1535,,0

FLST,3,3,5,ORDE,2 ! Item #9
FITEM,3,5
FITEM,3,-7
AGEN,2,P51X,,-5035+1535,,0

FLST,3,3,5,ORDE,2 ! Item #7
FITEM,3,5
FITEM,3,-7
AGEN,2,P51X,,-5705+1535,,0

```


[illegible]

FITEM,2,109				FITEM,2,117	
A,P51X	! Creating Forward			FITEM,2,118	
Stringer				FITEM,2,114	
				FITEM,2,113	
				A,P51X	
FLST,2,15,5,ORDE,2				FLST,3,5,5,ORDE,5	
FITEM,2,14				FITEM,3,15	
FITEM,2,28				FITEM,3,17	
FLST,2,15,5,ORDE,2				FITEM,3,19	
FITEM,2,14				FITEM,3,21	
FITEM,2,28				FITEM,3,23	
FLST,3,2,5,ORDE,2				ASBA, 72,P51X	
FITEM,3,6				FLST,3,5,5,ORDE,5	
FITEM,3,72				FITEM,3,14	
ASBA,P51X,P51X, ,KEEP	! Dividing Bolster Areas			FITEM,3,16	
				FITEM,3,18	
FLST,2,4,3				FITEM,3,20	
FITEM,2,148				FITEM,3,22	
FITEM,2,147				ASBA, 6,P51X	! Removing Bolster Holes in Front
FITEM,2,149				Stringer	
FITEM,2,150					
A,P51X				LANG, 191, 146,90,0, 0.9878158211681047E-01	
FLST,2,4,3				LANG, 187, 147,90,0, 0.1071629505009111	
FITEM,2,145				KL,190,5, ,	
FITEM,2,146				KL,186,5, ,	
FITEM,2,152				FLST,2,3,3	
FITEM,2,151				FITEM,2,154	
A,P51X				FITEM,2,156	
FLST,2,4,3				FITEM,2,111	
FITEM,2,136				A,P51X	
FITEM,2,135				FLST,2,3,3	
FITEM,2,141				FITEM,2,153	
FITEM,2,142				FITEM,2,155	
A,P51X				FITEM,2,109	
FLST,2,4,3				A,P51X	
FITEM,2,133					
FITEM,2,134				ASBA, 15, 6	
FITEM,2,144				ASBA, 24, 14	! Chopping Stringer Edge
FITEM,2,143				Angle Area	
A,P51X					
FLST,2,4,3				FLST,2,4,3	
FITEM,2,137				FITEM,2,107	
FITEM,2,138				FITEM,2,105	
FITEM,2,131				FITEM,2,153	
FITEM,2,132				FITEM,2,154	
A,P51X				A,P51X	
FLST,2,4,3				FLST,2,4,3	
FITEM,2,139				FITEM,2,153	
FITEM,2,140				FITEM,2,155	
FITEM,2,130				FITEM,2,156	
FITEM,2,129				FITEM,2,154	
A,P51X				A,P51X	
FLST,2,4,3				FLST,2,4,3	
FITEM,2,128				FITEM,2,110	
FITEM,2,127				FITEM,2,112	
FITEM,2,123				FITEM,2,156	
FITEM,2,124				A,P51X	! Closing Front Stringer (Added
A,P51X				Outer Plates)	
FLST,2,4,3					
FITEM,2,125					
FITEM,2,126					
FITEM,2,122					
FITEM,2,121					
A,P51X					
FLST,2,4,3					
FITEM,2,120					
FITEM,2,119					
FITEM,2,115					
FITEM,2,116					
A,P51X					
FLST,2,4,3					

	----- Pivot Structure	

K, 48°20.5,-370,-2740+50,		
K, 48°20.5,-440,-2740-370,		
K, 48°20.5,-440,-4090,		
K, 48°20.5,0,-4090,		

K, 48*20.5,0,-2740+50, IK, 970,-370,-2740+50, IK, 970,-440,-2740-370, IK, 970,-440,-4090, IK, 970,0,-4090, IK, 970,0,-2740+50,		FITEM,3,303 LGEN,2,P51X, , , , ,275, ,0 Lines	! Construction
FLST,2,5,3 FITEM,2,109 FITEM,2,111 FITEM,2,157 FITEM,2,158 FITEM,2,159 A,P51X Structure Side Area	! Pivot	FLST,2,1,4,ORDE,1 FITEM,2,287 FLST,3,1,4,ORDE,1 FITEM,3,38 LSBL,P51X,P51X, , ,KEEP FLST,2,1,4,ORDE,1 FITEM,2,303 FLST,3,1,4,ORDE,1 FITEM,3,39 LSBL,P51X,P51X, , ,KEEP LSBL, 38, 41 LSBL, 39, 43 LSTR, 177, 162 LSTR, 173, 164 FLST,2,2,4,ORDE,2 FITEM,2,38 FITEM,2,302 LDELE,P51X, , ,1 Lines	
FLST,2,6,5,ORDE,2 FITEM,2,8 FITEM,2,-13 FLST,3,1,5,ORDE,1 FITEM,3,18 ASBA,P51X,P51X, , ,DELETE,KEEP FLST,2,6,5,ORDE,6 FITEM,2,19 FITEM,2,21 FITEM,2,24 FITEM,2,-25 FITEM,2,27 FITEM,2,118 ADELE,P51X, , ,1 Bolsters Inside Pivot	! Deleting	FLST,2,4,3 FITEM,2,160 FITEM,2,162 FITEM,2,177 FITEM,2,169 A,P51X FLST,2,4,3 FITEM,2,164 FITEM,2,166 FITEM,2,172 FITEM,2,173 A,P51X FLST,2,1,5,ORDE,1 FITEM,2,9 FLST,3,1,5,ORDE,1 FITEM,3,12 ASBA,P51X,P51X, , ,KEEP FLST,2,1,5,ORDE,1 FITEM,2,10 FLST,3,1,5,ORDE,1 FITEM,3,13 ASBA,P51X,P51X, , ,KEEP Areas	! Dividing
FLST,3,1,5,ORDE,1 FITEM,3,18 AGEN,2,P51X, , , -383, , , ,0 Otherside	! Creating		
FLST,2,4,3 FITEM,2,160 FITEM,2,162 FITEM,2,163 FITEM,2,161 A,P51X FLST,2,4,3 FITEM,2,165 FITEM,2,164 FITEM,2,166 FITEM,2,167 A,P51X FLST,2,1,5,ORDE,1 FITEM,2,18 FLST,3,2,5,ORDE,2 FITEM,3,9 FITEM,3,-10 ASBA,P51X,P51X, , ,KEEP Outside Area	! Divided	FLST,3,2,5,ORDE,2 FITEM,3,12 FITEM,3,-13 AGEN,2,P51X, , , -48*20.5, , , ,0 FLST,2,4,3 FITEM,2,19 FITEM,2,175 FITEM,2,169 FITEM,2,160 A,P51X FLST,2,4,3 FITEM,2,175 FITEM,2,174 FITEM,2,177 FITEM,2,169 A,P51X FLST,2,4,3 FITEM,2,177 FITEM,2,174 FITEM,2,23 FITEM,2,162	! Dividing
FLST,3,2,4,ORDE,2 FITEM,3,295 FITEM,3,306 FLST,3,2,4,ORDE,2 FITEM,3,31 FITEM,3,33 LGEN,2,P51X, , , -234, , , ,0 FLST,3,1,4,ORDE,1 FITEM,3,287 LGEN,2,P51X, , , -275, , ,0 FLST,3,1,4,ORDE,1			

A,P51X		FITEM,2,333	
FLST,2,4,3		FLST,3,1,4,ORDE,1	
FITEM,2,27		FITEM,3,28	
FITEM,2,180		LSBL,P51X,P51X, , ,KEEP	! Const. Lines
FITEM,2,173		KWPLAN,-1, 187, 189, 186	
FITEM,2,164		KWPLAN,-1, 189, 186, 187	
A,P51X		PCIRC,83.5, ,0,360,	! Circle for
FLST,2,4,3		Pivot Hole	
FITEM,2,173			
FITEM,2,180		FLST,3,1,4,ORDE,1	
FITEM,2,179		FITEM,3,28	
FITEM,2,172		LGEN,2,P51X, , , ,133, ,0	
A,P51X		FLST,3,1,4,ORDE,1	
FLST,2,4,3		FITEM,3,28	
FITEM,2,166		LGEN,2,P51X, , , ,133, ,0	
FITEM,2,172		FLST,2,2,4,ORDE,2	
FITEM,2,179		FITEM,2,334	
FITEM,2,31		FITEM,2,339	
A,P51X		FLST,2,1,4,ORDE,1	
FLST,2,2,5,ORDE,2		FITEM,2,339	
FITEM,2,10		FLST,3,1,4,ORDE,1	
FITEM,2,19		FITEM,3,334	
ADELE,P51X, , ,1	! Creating Tapered	LSBL,P51X,P51X, , ,KEEP	
Bolsters Inside Pivot		FLST,2,1,4,ORDE,1	
		FITEM,2,340	
		FLST,3,1,4,ORDE,1	
		FITEM,3,335	
		LSBL,P51X,P51X, , ,KEEP	! Construction
		Lines	
FLST,2,3,5,ORDE,3		LARC,198,199,186,133,	
FITEM,2,21		FLST,3,1,4,ORDE,1	
FITEM,2,24		FITEM,3,340	
FITEM,2,25		LGEN,2,P51X, , , ,30, ,0	
FLST,3,1,5,ORDE,1		FLST,3,1,4,ORDE,1	
FITEM,3,8		FITEM,3,27	
ASBA,P51X,P51X, , ,KEEP		LGEN,2,P51X, , , ,600-380, ,0	
FLST,2,3,5,ORDE,3		FLST,2,5,4,ORDE,5	
FITEM,2,27		FITEM,2,28	
FITEM,2,118		FITEM,2,334	
FITEM,2,119		FITEM,2,335	
FLST,3,1,5,ORDE,1		FITEM,2,339	
FITEM,3,8		FITEM,2,341	
ASBA,P51X,P51X, , ,KEEP	! Dividing	LDELE,P51X, , ,1	
Tapered Bolsters		LDELE, 340, , ,1	
		FLST,2,1,4,ORDE,1	
		FITEM,2,343	
		FLST,3,1,4,ORDE,1	
		FITEM,3,344	
		LSBL,P51X,P51X, , ,KEEP	
		FLST,2,1,4,ORDE,1	
		FITEM,2,342	
		FLST,3,1,4,ORDE,1	
		FITEM,3,344	
		LSBL,P51X,P51X, , ,KEEP	
		FLST,2,2,4,ORDE,2	
		FITEM,2,28	
		FITEM,2,335	
		LDELE,P51X, , ,1	
		LSTR, 202, 199	
		LSTR, 198, 24	
		LDELE, 345, , ,1	
		FLST,2,1,4,ORDE,1	
		FITEM,2,25	
		FLST,3,1,4,ORDE,1	
		FITEM,3,28	
		LSBL,P51X,P51X, , ,KEEP	! Creating Lines 4 Pivot
		Reinforced Area	
FLST,3,1,4,ORDE,1		FLST,3,5,4,ORDE,5	
FITEM,3,27			
LGEN,2,P51X, , , ,600, ,0			
FLST,3,1,4,ORDE,1			
FITEM,3,25			
LGEN,2,P51X, , , ,180, ,0			
FLST,2,1,4,ORDE,1			

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FITEM,3,28
FITEM,3,334
FITEM,3,335
FITEM,3,339
FITEM,3,344
LGEN,2,P51X, ,383, ,0
!LGEN,2,P51X, ,380, ,0
FLST,3,1,5,ORDE,1
FITEM,3,8
AGEN,2,P51X, ,383, ,0
!AGEN,2,P51X, ,380, ,0
FLST,2,1,4,ORDE,1
FITEM,2,191
FLST,3,1,4,ORDE,1
FITEM,3,25
LSBL,P51X,P51X, ,KEEP ! Copied Lines and Hole
to Otherside

FLST,2,6,4
FITEM,2,28
FITEM,2,334
FITEM,2,344
FITEM,2,339
FITEM,2,335
FITEM,2,340
AL,P51X
NUMMRG,KP, ,
FLST,2,6,4
FITEM,2,351
FITEM,2,25
FITEM,2,342
FITEM,2,346
FITEM,2,345
FITEM,2,343
AL,P51X
FLST,2,1,5,ORDE,1
FITEM,2,11
FLST,3,1,5,ORDE,1
FITEM,3,129
ASBA,P51X,P51X, ,KEEP
FLST,2,1,5,ORDE,1
FITEM,2,129
FLST,3,1,5,ORDE,1
FITEM,3,127
ASBA,P51X,P51X, ,DELETE
FLST,2,1,5,ORDE,1
FITEM,2,119
FLST,3,1,5,ORDE,1
FITEM,3,128
ASBA,P51X,P51X, ,KEEP
FLST,2,1,5,ORDE,1
FITEM,2,128
FLST,3,1,5,ORDE,1
FITEM,3,8
ASBA,P51X,P51X, ,DELETE ! Finish
Dividing Areas Reinforced Area

FLST,3,1,4,ORDE,1
FITEM,3,351
LGEN,2,P51X, ,400, ,0
FLST,3,1,4,ORDE,1
FITEM,3,282
LGEN,2,P51X, ,580, ,0
LSBL, 171, 144
FLST,3,1,4,ORDE,1
FITEM,3,284
LGEN,2,P51X, ,133, ,0
LSTR, 109, 100
LSTR, 100, 204
LSTR, 204, 185

FLST,2,3,4,ORDE,3
FITEM,2,144
FITEM,2,181
FITEM,2,191
LDELETE,P51X, ,1 ! Creating Lines for Pivot
Indent

FLST,2,1,4,ORDE,1
FITEM,2,353
FLST,3,2,4,ORDE,2
FITEM,3,292
FITEM,3,295
LSBL,P51X,P51X, ,KEEP
FLST,2,1,4,ORDE,1
FITEM,2,354
FLST,3,2,4,ORDE,2
FITEM,3,298
FITEM,3,306
LSBL,P51X,P51X, ,KEEP
ASBL, 18, 191
FLST,3,2,4,ORDE,2
FITEM,3,144
FITEM,3,171
ASBL, 130,P51X
FLST,3,2,4,ORDE,2
FITEM,3,181
FITEM,3,355
ASBL, 129,P51X
ASBL, 9, 356
ASBL, 131, 353 ! Dividing Lines and Areas on Side
for Mesh reasons

FLST,2,7,4,ORDE,7 ! Sweeping Pivot Indent
Accros
FITEM,2,144
FITEM,2,171
FITEM,2,181
FITEM,2,191
FITEM,2,353
FITEM,2,355
FITEM,2,356
ADBRAG,P51X, , , , , , 309

! Dividing Lines and Areas on Other Side for
Mesh reasons
FLST,2,1,5,ORDE,1
FITEM,2,127
FLST,3,7,4,ORDE,7
FITEM,3,306
FITEM,3,363
FITEM,3,365
FITEM,3,367
FITEM,3,369
FITEM,3,371
FITEM,3,373
ASBL,P51X,P51X, ,KEEP

NUMMRG,KP, , ! Merging Co-incident Keypoints

FLST,2,4,3
FITEM,2,20
FITEM,2,109
FITEM,2,84
FITEM,2,95
A,P51X
FLST,2,4,3
FITEM,2,109
FITEM,2,84

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FITEM,2,83
FITEM,2,159
A,P51X
FLST,2,4,3
FITEM,2,20
FITEM,2,95
FITEM,2,94
FITEM,2,168
A,P51X      ! Attaching Pivot Structure to Rear
Stringer

FLST,2,4,3
FITEM,2,158
FITEM,2,108
FITEM,2,107
FITEM,2,157
A,P51X
FLST,2,4,3
FITEM,2,32
FITEM,2,106
FITEM,2,105
FITEM,2,28
A,P51X
FLST,2,4,3
FITEM,2,185
FITEM,2,202
FITEM,2,28
FITEM,2,157
A,P51X
FLST,2,4,3
FITEM,2,157
FITEM,2,28
FITEM,2,105
FITEM,2,107
A,P51X      ! Attaching Pivot Structure to Front
Stringer

!-----
!----- Dividing Floor Plate Areas - Near Stringer
!-----

FLST,2,1,5,ORDE,1
FITEM,2,31
FLST,3,2,4,ORDE,2
FITEM,3,2
FITEM,3,160
ASBL,P51X,P51X,,KEEP
FLST,2,1,5,ORDE,1
FITEM,2,33
FLST,3,6,4,ORDE,6
FITEM,3,35
FITEM,3,135
FITEM,3,148
FITEM,3,318
FITEM,3,377
FITEM,3,-378
ASBL,P51X,P51X,,KEEP
FLST,2,1,5,ORDE,1
FITEM,2,35
FLST,3,2,4,ORDE,2
FITEM,3,37
FITEM,3,332
ASBL,P51X,P51X,,KEEP
FLST,2,1,5,ORDE,1
FITEM,2,36
FLST,3,2,4,ORDE,2
FITEM,3,33
FITEM,3,301
ASBL,P51X,P51X,,KEEP
FLST,2,1,5,ORDE,1

FITEM,2,34
FLST,3,2,4,ORDE,2
FITEM,3,31
FITEM,3,296
ASBL,P51X,P51X,,KEEP
FLST,2,1,5,ORDE,1
FITEM,2,37
FLST,3,6,4,ORDE,6
FITEM,3,34
FITEM,3,47
FITEM,3,69
FITEM,3,317
FITEM,3,379
FITEM,3,381
ASBL,P51X,P51X,,KEEP
FLST,2,1,5,ORDE,1
FITEM,2,39
FLST,3,2,4,ORDE,2
FITEM,3,57
FITEM,3,74
ASBL,P51X,P51X,,KEEP
FLST,2,1,5,ORDE,1
FITEM,2,41
FLST,3,2,4,ORDE,2
FITEM,3,61
FITEM,3,76
ASBL,P51X,P51X,,KEEP
FLST,2,1,5,ORDE,1
FITEM,2,43
FLST,3,2,4,ORDE,2
FITEM,3,81
FITEM,3,85
ASBL,P51X,P51X,,KEEP
FLST,2,1,5,ORDE,1
FITEM,2,45
FLST,3,2,4,ORDE,2
FITEM,3,67
FITEM,3,79
ASBL,P51X,P51X,,KEEP
FLST,2,1,5,ORDE,1
FITEM,2,30
FLST,3,2,4,ORDE,2
FITEM,3,51
FITEM,3,71
ASBL,P51X,P51X,,KEEP

!-----
!----- Corner Stringer
!-----

FLST,3,18,4,ORDE,18
FITEM,3,95
FITEM,3,-96
FITEM,3,99
FITEM,3,101
FITEM,3,103
FITEM,3,105
FITEM,3,107
FITEM,3,109
FITEM,3,111
FITEM,3,113
FITEM,3,115
FITEM,3,117
FITEM,3,119
FITEM,3,121
FITEM,3,123
FITEM,3,125
FITEM,3,127
FITEM,3,129
LGEM,2,P51X,,,-32*10,,0

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FLST,3,18,4,ORDE,18
 FITEM,3,95
 FITEM,3,96
 FITEM,3,98
 FITEM,3,101
 FITEM,3,103
 FITEM,3,105
 FITEM,3,107
 FITEM,3,109
 FITEM,3,111
 FITEM,3,113
 FITEM,3,115
 FITEM,3,117
 FITEM,3,119
 FITEM,3,121
 FITEM,3,123
 FITEM,3,125
 FITEM,3,127
 FITEM,3,129
 LGEN,2,P51X,,-8*10,32*10,,0
 FLST,3,18,4,ORDE,2
 FITEM,3,403
 FITEM,3,420
 LGEN,2,P51X,,-23*10,-15*10,,0
 FLST,3,18,4,ORDE,2
 FITEM,3,421
 FITEM,3,438
 LGEN,2,P51X,,-16*10,-2.5*10,,0
 Copying Lines

FLST,2,5,3
 FITEM,2,215
 FITEM,2,272
 FITEM,2,234
 FITEM,2,253
 FITEM,2,70
 A,P51X
 FLST,2,5,3
 FITEM,2,230
 FITEM,2,287
 FITEM,2,249
 FITEM,2,268
 FITEM,2,72
 A,P51X
 FLST,2,5,3
 FITEM,2,229
 FITEM,2,286
 FITEM,2,248
 FITEM,2,267
 FITEM,2,62
 A,P51X
 FLST,2,5,3
 FITEM,2,228
 FITEM,2,285
 FITEM,2,247
 FITEM,2,266
 FITEM,2,64
 A,P51X
 FLST,2,5,3
 FITEM,2,227
 FITEM,2,284
 FITEM,2,246
 FITEM,2,265
 FITEM,2,58
 A,P51X
 FLST,2,5,3
 FITEM,2,226
 FITEM,2,283
 FITEM,2,245
 FITEM,2,264

FITEM,2,54
 A,P51X
 FLST,2,5,3
 FITEM,2,225
 FITEM,2,282
 FITEM,2,244
 FITEM,2,263
 FITEM,2,50
 A,P51X
 FLST,2,5,3
 FITEM,2,224
 FITEM,2,281
 FITEM,2,243
 FITEM,2,262
 FITEM,2,46
 A,P51X
 FLST,2,5,3
 FITEM,2,223
 FITEM,2,280
 FITEM,2,242
 FITEM,2,261
 FITEM,2,42
 A,P51X
 FLST,2,5,3
 FITEM,2,222
 FITEM,2,279
 FITEM,2,241
 FITEM,2,260
 FITEM,2,38
 A,P51X
 FLST,2,5,3
 FITEM,2,221
 FITEM,2,278
 FITEM,2,240
 FITEM,2,259
 FITEM,2,34
 A,P51X
 FLST,2,5,3
 FITEM,2,220
 FITEM,2,277
 FITEM,2,239
 FITEM,2,258
 FITEM,2,30
 A,P51X
 FLST,2,5,3
 FITEM,2,219
 FITEM,2,276
 FITEM,2,238
 FITEM,2,257
 FITEM,2,26
 A,P51X
 FLST,2,5,3
 FITEM,2,218
 FITEM,2,275
 FITEM,2,237
 FITEM,2,256
 FITEM,2,22
 A,P51X
 FLST,2,5,3
 FITEM,2,217
 FITEM,2,274
 FITEM,2,236
 FITEM,2,255
 FITEM,2,18
 A,P51X
 FLST,2,5,3
 FITEM,2,216
 FITEM,2,273
 FITEM,2,235
 FITEM,2,254

FITEM,2,14		FLST,3,1,4,ORDE,1
A,P51X		FITEM,3,393
FLST,2,5,3		ASBL,P51X,P51X,,KEEP
FITEM,2,213		FLST,2,1,5,ORDE,1
FITEM,2,270		FITEM,2,35
FITEM,2,232		FLST,3,1,4,ORDE,1
FITEM,2,251		FITEM,3,392
FITEM,2,10		ASBL,P51X,P51X,,KEEP
A,P51X		FLST,2,1,5,ORDE,1
FLST,2,4,3		FITEM,2,153
FITEM,2,206		FLST,3,1,4,ORDE,1
FITEM,2,231		FITEM,3,391
FITEM,2,250		ASBL,P51X,P51X,,KEEP
FITEM,2,2		FLST,2,1,5,ORDE,1
A,P51X	! Creating Internal Stiffeners	FITEM,2,157
	! Dividing Floor Plate Areas Near	FLST,3,1,4,ORDE,1
		FITEM,3,390
Corner Stringer		ASBL,P51X,P51X,,KEEP
FLST,2,1,5,ORDE,1		FLST,2,4,5,ORDE,4
FITEM,2,169		FITEM,2,31
FLST,3,1,4,ORDE,1		FITEM,2,-32
FITEM,3,386		FITEM,2,62
ASBL,P51X,P51X,,KEEP		FITEM,2,148
FLST,2,1,5,ORDE,1		FLST,3,4,4,ORDE,3
FITEM,2,46		FITEM,3,3
FLST,3,1,4,ORDE,1		FITEM,3,387
FITEM,3,402		FITEM,3,-389
ASBL,P51X,P51X,,KEEP		ASBL,P51X,P51X,,KEEP
FLST,2,1,5,ORDE,1		
FITEM,2,167		FLST,2,4,3
FLST,3,1,4,ORDE,1		FITEM,2,206
FITEM,3,401		FITEM,2,231
ASBL,P51X,P51X,,KEEP		FITEM,2,232
FLST,2,1,5,ORDE,1		FITEM,2,213
FITEM,2,44		A,P51X
FLST,3,1,4,ORDE,1		FLST,2,4,3
FITEM,3,400		FITEM,2,216
ASBL,P51X,P51X,,KEEP		FITEM,2,213
FLST,2,1,5,ORDE,1		FITEM,2,232
FITEM,2,166		FITEM,2,235
FLST,3,1,4,ORDE,1		A,P51X
FITEM,3,399		FLST,2,4,3
ASBL,P51X,P51X,,KEEP		FITEM,2,217
FLST,2,1,5,ORDE,1		FITEM,2,216
FITEM,2,42		FITEM,2,235
FLST,3,1,4,ORDE,1		FITEM,2,236
FITEM,3,398		A,P51X
ASBL,P51X,P51X,,KEEP		FLST,2,4,3
FLST,2,1,5,ORDE,1		FITEM,2,217
FITEM,2,163		FITEM,2,236
FLST,3,1,4,ORDE,1		FITEM,2,237
FITEM,3,397		FITEM,2,218
ASBL,P51X,P51X,,KEEP		A,P51X
FLST,2,1,5,ORDE,1		FLST,2,4,3
FITEM,2,40		FITEM,2,219
FLST,3,1,4,ORDE,1		FITEM,2,218
FITEM,3,396		FITEM,2,237
ASBL,P51X,P51X,,KEEP		FITEM,2,236
FLST,2,1,5,ORDE,1		A,P51X
FITEM,2,161		FLST,2,4,3
FLST,3,1,4,ORDE,1		FITEM,2,220
FITEM,3,395		FITEM,2,219
ASBL,P51X,P51X,,KEEP		FITEM,2,236
FLST,2,1,5,ORDE,1		FITEM,2,239
FITEM,2,38		A,P51X
FLST,3,1,4,ORDE,1		FLST,2,4,3
FITEM,3,394		FITEM,2,220
ASBL,P51X,P51X,,KEEP		FITEM,2,239
FLST,2,1,5,ORDE,1		FITEM,2,240
FITEM,2,34		FITEM,2,221

FITEM,2,256
 A,P51X
 FLST,2,4,3
 FITEM,2,26
 FITEM,2,30
 FITEM,2,258
 FITEM,2,257
 A,P51X
 FLST,2,4,3
 FITEM,2,30
 FITEM,2,34
 FITEM,2,259
 FITEM,2,258
 A,P51X
 FLST,2,4,3
 FITEM,2,34
 FITEM,2,38
 FITEM,2,260
 FITEM,2,259
 A,P51X
 FLST,2,4,3
 FITEM,2,38
 FITEM,2,42
 FITEM,2,261
 FITEM,2,260
 A,P51X
 FLST,2,4,3
 FITEM,2,42
 FITEM,2,46
 FITEM,2,262
 FITEM,2,261
 A,P51X
 FLST,2,4,3
 FITEM,2,46
 FITEM,2,50
 FITEM,2,263
 FITEM,2,262
 A,P51X
 FLST,2,4,3
 FITEM,2,50
 FITEM,2,54
 FITEM,2,264
 FITEM,2,263
 A,P51X
 FLST,2,4,3
 FITEM,2,54
 FITEM,2,58
 FITEM,2,265
 FITEM,2,264
 A,P51X
 FLST,2,4,3
 FITEM,2,58
 FITEM,2,64
 FITEM,2,266
 FITEM,2,265
 A,P51X
 FLST,2,4,3
 FITEM,2,64
 FITEM,2,62
 FITEM,2,267
 FITEM,2,266
 A,P51X
 FLST,2,4,3
 FITEM,2,62
 FITEM,2,72
 FITEM,2,268
 FITEM,2,267
 A,P51X
 FLST,2,4,3
 FITEM,2,72

FITEM,2,70
 FITEM,2,253
 FITEM,2,268
 A,P51X
 FLST,2,4,3
 FITEM,2,70
 FITEM,2,3
 FITEM,2,252
 FITEM,2,253
 A,P51X
 Plate Areas
 FLST,2,4,3
 FITEM,2,250
 FITEM,2,251
 FITEM,2,232
 FITEM,2,231
 A,P51X
 FLST,2,4,3
 FITEM,2,251
 FITEM,2,254
 FITEM,2,235
 FITEM,2,232
 A,P51X
 FLST,2,4,3
 FITEM,2,254
 FITEM,2,255
 FITEM,2,236
 FITEM,2,235
 A,P51X
 FLST,2,4,3
 FITEM,2,255
 FITEM,2,256
 FITEM,2,237
 FITEM,2,236
 A,P51X
 FLST,2,4,3
 FITEM,2,256
 FITEM,2,257
 FITEM,2,238
 FITEM,2,237
 A,P51X
 FLST,2,4,3
 FITEM,2,257
 FITEM,2,258
 FITEM,2,239
 FITEM,2,238
 A,P51X
 FLST,2,4,3
 FITEM,2,258
 FITEM,2,259
 FITEM,2,240
 FITEM,2,239
 A,P51X
 FLST,2,4,3
 FITEM,2,259
 FITEM,2,260
 FITEM,2,241
 FITEM,2,240
 A,P51X
 FLST,2,4,3
 FITEM,2,260
 FITEM,2,261
 FITEM,2,242
 FITEM,2,241
 A,P51X
 FLST,2,4,3
 FITEM,2,261
 FITEM,2,262
 FITEM,2,243

! Adding Lower Outside

FITEM,2,242
 A,P51X
 FLST,2,4,3
 FITEM,2,262
 FITEM,2,263
 FITEM,2,244
 FITEM,2,243
 A,P51X
 FLST,2,4,3
 FITEM,2,263
 FITEM,2,264
 FITEM,2,245
 FITEM,2,244
 A,P51X
 FLST,2,4,3
 FITEM,2,264
 FITEM,2,265
 FITEM,2,246
 FITEM,2,245
 A,P51X
 FLST,2,4,3
 FITEM,2,265
 FITEM,2,266
 FITEM,2,247
 FITEM,2,246
 A,P51X
 FLST,2,4,3
 FITEM,2,266
 FITEM,2,267
 FITEM,2,248
 FITEM,2,247
 A,P51X
 FLST,2,4,3
 FITEM,2,267
 FITEM,2,268
 FITEM,2,249
 FITEM,2,248
 A,P51X
 FLST,2,4,3
 FITEM,2,268
 FITEM,2,253
 FITEM,2,234
 FITEM,2,249
 A,P51X
 FLST,2,4,3
 FITEM,2,253
 FITEM,2,252
 FITEM,2,233
 FITEM,2,234
 A,P51X
 Plate Areas
 FLST,2,4,3
 FITEM,2,6
 FITEM,2,9
 FITEM,2,10
 FITEM,2,2
 A,P51X
 FLST,2,4,3
 FITEM,2,13
 FITEM,2,17
 FITEM,2,18
 FITEM,2,14
 A,P51X
 FLST,2,4,3
 FITEM,2,21
 FITEM,2,25
 FITEM,2,26
 FITEM,2,22
 A,P51X

! Adding Upper Outside

FLST,2,4,3
 FITEM,2,29
 FITEM,2,33
 FITEM,2,34
 FITEM,2,30
 A,P51X
 FLST,2,4,3
 FITEM,2,37
 FITEM,2,41
 FITEM,2,42
 FITEM,2,38
 A,P51X
 FLST,2,4,3
 FITEM,2,45
 FITEM,2,49
 FITEM,2,50
 FITEM,2,46
 A,P51X
 FLST,2,4,3
 FITEM,2,53
 FITEM,2,61
 FITEM,2,58
 FITEM,2,54
 A,P51X
 FLST,2,4,3
 FITEM,2,63
 FITEM,2,60
 FITEM,2,62
 FITEM,2,64
 A,P51X
 FLST,2,4,3
 FITEM,2,71
 FITEM,2,69
 FITEM,2,70
 FITEM,2,72
 A,P51X
 Bolster Ends

! Closing

!-----
 !----- Hoist Pivot
 !-----

FLST,3,3,4,ORDE,3
 FITEM,3,121
 FITEM,3,123
 FITEM,3,125
 LGEN,2,P51X,,,-bwidth/2+1177.6,...,0
 FLST,3,2,4,ORDE,2
 FITEM,3,599
 FITEM,3,601
 LGEN,2,P51X,,,-300,...,0
 FLST,2,4,3
 FITEM,2,322
 FITEM,2,319
 FITEM,2,316
 FITEM,2,320
 A,P51X
 FLST,2,5,4,ORDE,2
 FITEM,2,599
 FITEM,2,-603
 LDELE,P51X,,1
 Lines
 FLST,3,1,5,ORDE,1
 FITEM,3,269
 AGEN,2,P51X,,,-249,...,0
 FLST,2,9,5,ORDE,9
 FITEM,2,44
 FITEM,2,86
 FITEM,2,88

! Construction

FITEM,2,-89		FITEM,2,627	
FITEM,2,91		FITEM,2,621	
FITEM,2,93		AL,P51X	! Stiffeners
FITEM,2,95		Inside Bolsters	
FITEM,2,192			
FITEM,2,194		KL,623,0.4, .	
FLST,3,2,5,ORDE,2		KL,625,0.6, .	
FITEM,3,269		FLST,3,1,3,ORDE,1	
FITEM,3,-270		FITEM,3,328	
ASBA,P51X,P51X	! Cutting	KGEN,2,P51X, , , , -240, -255, ,0	
Bolster Areas		KL,646,0.6, .	
		KL,648,0.4, .	
FLST,3,1,3,ORDE,1		FLST,3,1,3,ORDE,1	
FITEM,3,321		FITEM,3,334	
KGEN,2,P51X, , , , -164, -72, ,0		KGEN,2,P51X, , , , -240, -255, ,0	
FLST,3,1,3,ORDE,1		LSTR, 343, 345	
FITEM,3,317		LSTR, 345, 344	
KGEN,2,P51X, , , ,0,-60, ,0		LSTR, 336, 340	
FLST,2,6,3		LSTR, 340, 339	
FITEM,2,321		FLST,2,4,4,ORDE,4	
FITEM,2,317		FITEM,2,623	
FITEM,2,320		FITEM,2,625	
FITEM,2,334		FITEM,2,646	
FITEM,2,325		FITEM,2,648	
FITEM,2,324		FLST,3,4,4,ORDE,4	
A,P51X		FITEM,3,466	
FLST,3,1,3,ORDE,1		FITEM,3,478	
FITEM,3,318		FITEM,3,549	
KGEN,2,P51X, , , , -164, 72, ,0		FITEM,3,-560	
FLST,3,1,3,ORDE,1		LSBL,P51X,P51X, , , ,KEEP	
FITEM,3,322		FLST,2,5,4	
KGEN,2,P51X, , , ,0,60, ,0		FITEM,2,651	
FLST,2,6,3		FITEM,2,466	
FITEM,2,318		FITEM,2,476	
FITEM,2,322		FITEM,2,652	
FITEM,2,323		FITEM,2,632	
FITEM,2,335		AL,P51X	
FITEM,2,327		FLST,2,5,4	
FITEM,2,326		FITEM,2,606	
A,P51X		FITEM,2,549	
FLST,3,6,4,ORDE,6		FITEM,2,550	
FITEM,3,223		FITEM,2,607	
FITEM,3,229		FITEM,2,615	
FITEM,3,232		AL,P51X	! Pivot Areas
FITEM,3,-233			
FITEM,3,238			! Punching Holes Through Hoist
FITEM,3,-239		Pivot and Front Stringer	
LGEN,2,P51X, , , , -249, , ,0		FLST,3,1,3,ORDE,1	
IFLST,2,6,4		FITEM,3,334	
FITEM,2,255		KGEN,2,P51X, , , , -140, -260, ,0	
FITEM,2,551		KWPLAN,-1, 346, 334, 335	
FITEM,2,599		PCIRC,60, ,0,360,	
FITEM,2,623		FLST,2,1,5,ORDE,1	
FITEM,2,626		FITEM,2,95	
FITEM,2,618		VEXT,P51X, , , -2000,0,0, , ,	
IAL,P51X		FLST,2,4,5,ORDE,4	
NUMMRG,KP, , ,		FITEM,2,5	
FLST,2,6,4		FITEM,2,16	
FITEM,2,623		FITEM,2,91	
FITEM,2,626		FITEM,2,93	
FITEM,2,618		ASBV,P51X, 1	
FITEM,2,255			
FITEM,2,551			
FITEM,2,599			
AL,P51X			
FLST,2,6,4			
FITEM,2,600			
FITEM,2,601			
FITEM,2,602			
FITEM,2,625			

----- Correcting Angles at Ends of Corner Stringer

KWPLAN,-1, 2, 206, 250

wpro,5.000000,

wpro,5.000000,

wpro,1.000000,

FLST,2,3,5,ORDE,3					FITEM,2,259	
FITEM,2,31					FITEM,2,301	
FITEM,2,206					ADELE,P51X	
FITEM,2,242					FLST,2,9,4,ORDE,9	
ASBW,P51X					FITEM,2,87	
FLST,2,4,5,ORDE,4					FITEM,2,404	
FITEM,2,6					FITEM,2,422	
FITEM,2,16					FITEM,2,566	
FITEM,2,187					FITEM,2,597	
FITEM,2,192					FITEM,2,-598	
ADELE,P51X,,1					FITEM,2,660	
FLST,2,4,4					FITEM,2,668	
FITEM,2,655					FITEM,2,670	
FITEM,2,659					LDELE,P51X,,1	
FITEM,2,653					LDELE, 672,,1	
FITEM,2,545					LDELE, 440,,1	
AL,P51X				! Correcting Rear End of	LSTR, 253, 366	
Corner STR					LSTR, 234, 365	
					NUMMRG,KP,,,	
KWPLAN,-1, 112, 110, 156					FLST,2,4,4	
wpro,,12,500000,					FITEM,2,96	
FLST,2,3,5,ORDE,3					FITEM,2,671	
FITEM,2,15					FITEM,2,65	
FITEM,2,301					FITEM,2,460	
FITEM,2,-302					AL,P51X	
ASBW,P51X					FLST,2,4,4	
FLST,2,4,5,ORDE,4					FITEM,2,386	
FITEM,2,16					FITEM,2,669	
FITEM,2,-17					FITEM,2,87	
FITEM,2,31					FITEM,2,567	
FITEM,2,192					AL,P51X	
ADELE,P51X,,1					FLST,2,4,4	
FLST,2,4,4					FITEM,2,459	
FITEM,2,542					FITEM,2,65	
FITEM,2,656					FITEM,2,675	
FITEM,2,403					FITEM,2,87	
FITEM,2,189					AL,P51X	
AL,P51X				! Correcting Front of	FLST,2,4,4	
Stringer					FITEM,2,671	
					FITEM,2,548	
FLST,3,3,5,ORDE,3					FITEM,2,669	
FITEM,3,223					FITEM,2,675	
FITEM,3,241					AL,P51X	! Correcting Front End of
FITEM,3,259					Corner STR	
AGEN,2,P51X,,,,-375,,0						
FLST,2,3,5,ORDE,3					WPCSYS,-1,0	
FITEM,2,16						
FITEM,2,-17					NUMMRG,ALL,,,	! Merging Coincident
FITEM,2,31					Items	
ASBW,P51X					NUMCMP AREA	
FLST,2,3,5,ORDE,3					NUMCMP LINE	
FITEM,2,269					NUMCMP,KP	! Compressing Numbers
FITEM,2,-270						
FITEM,2,298					FINISH	
ADELE,P51X,,1					ISAVE	
FLST,2,6,5,ORDE,6					/EOF	
FITEM,2,192						
FITEM,2,223						
FITEM,2,241						
FITEM,2,-242						

❖ *Filename: 2_3_build_wall_INPUT*

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*****
! FEA of 130E Truck Box Structure
! Side Wall Construction Routine

:build

FINISH
FINISH
I/CLEAR
I/INERR,0,
I/RESUME,build_floor.db
I/FILNAM,build_wall
I/RESUME,geom.db
I/FILNAM,geom

/TITLE,Building Wall Geometry

/PREP7

/VIEW,1,1,1,1
/ANG,1
/REP,FAST
/USER,1
/VIEW,1,0.784420712192,-0.258767530301,0.563669683011
/ANG,1,-1.85612833420
/AUTO,1
APlot

-----
----- Wall Construction
-----

*AFUN,DEG
WPSTYLE,1,0
FLST,3,1,3,ORDE,1
FITEM,3,366
KGEN,2,P51X,,.21*20.5*sin(90-13)-.21*20.5*cos(90-13),0
FLST,3,1,3,ORDE,1
FITEM,3,356
KGEN,2,P51X,,.79*20.5*sin(39.5)-.79*20.5*cos(39.5),0
FLST,3,1,3,ORDE,1
FITEM,3,354
KGEN,2,P51X,,.123*20.5*sin(89.25)-.123*20.5*cos(89.25),0
FLST,3,1,3,ORDE,1
FITEM,3,354
KGEN,2,P51X,,.160*20.5*sin(77.5)-.160*20.5*cos(77.5),0

LSTR,366,356
LSTR,356,357
LSTR,357,358
LSTR,358,359
LSTR,354,359

FLST,2,23,4
FITEM,2,646
FITEM,2,401
FITEM,2,402
FITEM,2,403
FITEM,2,404
FITEM,2,405
FITEM,2,406
FITEM,2,407

FITEM,2,408
FITEM,2,409
FITEM,2,410
FITEM,2,411
FITEM,2,412
FITEM,2,413
FITEM,2,414
FITEM,2,415
FITEM,2,416
FITEM,2,87
FITEM,2,662
FITEM,2,661
FITEM,2,660
FITEM,2,659
FITEM,2,658

AL,P51X

! Side Wall Plate

-----
----- Top Tapered Bolster
-----

FLST,3,1,3,ORDE,1
FITEM,3,356
KGEN,2,P51X,,.230,,.0
LSTR,356,360
LSTR,360,347
KL,659,29.5/79,,
FLST,3,1,3,ORDE,1
FITEM,3,361
KGEN,2,P51X,,.230,,.0
LSTR,362,361

! Lines Near
Tail End.

FLST,2,1,4,ORDE,1
FITEM,2,659
FLST,3,1,4,ORDE,1
FITEM,3,665
LSBL,P51X,P51X,,KEEP
Line

! Dividing Back

LSTR,360,362

FLST,3,1,3,ORDE,1
FITEM,3,361
KGEN,2,P51X,,.1564,34,-10000,.0
LSTR,361,363
FLST,2,1,4,ORDE,1
FITEM,2,668
FLST,3,1,4,ORDE,1
FITEM,3,662
LSBL,P51X,P51X,,KEEP
FLST,2,1,4,ORDE,1
FITEM,2,662
FLST,3,1,4,ORDE,1
FITEM,3,670
LSBL,P51X,P51X,,DELETE
Horizontal Line

FLST,3,1,3,ORDE,1
FITEM,3,364
KGEN,2,P51X,,.230,,.0
LSTR,364,363
LSTR,363,362
FLST,3,3,3,ORDE,2
FITEM,3,357
FITEM,3,-359
KGEN,2,P51X,,.230,,.0

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LSTR, 365, 357		LSBW,P51X	
LSTR, 366, 358		LSTR, 358, 359	
LSTR, 367, 359		LSTR, 367, 369	
LSTR, 362, 365		LSTR, 369, 358	! Making
LSTR, 365, 366		Tapered Section	
LSTR, 366, 367		WPCSYS,-1,0	
LSTR, 367, 363	! Box Section		
Lines		FLST,2,3,4	
KL,675,0.56, ,		FITEM,2,661	
LSTR, 368, 357		FITEM,2,660	
FLST,3,1,3,ORDE,1		FITEM,2,680	
FITEM,3,368		AL,P51X	
KGEN,2,P51X, ...,1564.34,-10000, ,0		FLST,2,6,4	
LSTR, 368, 369		FITEM,2,662	
FLST,2,1,4,ORDE,1		FITEM,2,675	
FITEM,2,675		FITEM,2,676	
FLST,3,1,4,ORDE,1		FITEM,2,674	
FITEM,3,680		FITEM,2,677	
LSBL,P51X,P51X, ,KEEP		FITEM,2,660	
FLST,2,4,4,ORDE,4		AL,P51X	
FITEM,2,672		FLST,2,4,4	
FITEM,2,-673		FITEM,2,678	
FITEM,2,676		FITEM,2,671	
FITEM,2,682		FITEM,2,680	
LDELE,P51X, , ,1		FITEM,2,683	
FLST,2,1,4,ORDE,1		AL,P51X	
FITEM,2,680		FLST,2,3,4	
FLST,2,1,4,ORDE,1		FITEM,2,678	
FITEM,2,678		FITEM,2,676	
FLST,2,1,4,ORDE,1		FITEM,2,672	
FITEM,2,680		AL,P51X	
FLST,3,1,4,ORDE,1		FLST,2,4,4	
FITEM,3,678		FITEM,2,683	
LSBL,P51X,P51X, ,KEEP		FITEM,2,672	
FLST,2,1,4,ORDE,1		FITEM,2,674	
FITEM,2,678		FITEM,2,661	
FLST,3,1,4,ORDE,1		AL,P51X	
FITEM,3,673		FLST,2,5,4	
LSBL,P51X,P51X, ,DELETE		FITEM,2,673	
ADELE, 294		FITEM,2,680	
LDELE, 660, , ,1		FITEM,2,677	
FLST,2,2,4,ORDE,2		FITEM,2,669	
FITEM,2,661		FITEM,2,667	
FITEM,2,677		AL,P51X	
LDELE,P51X, , ,1		FLST,2,4,4	
FLST,3,1,3,ORDE,1		FITEM,2,665	
FITEM,3,357		FITEM,2,667	
KGEN,2,P51X, ...,1564.34,-10000, ,0		FITEM,2,679	
LSTR, 357, 358		FITEM,2,681	
FLST,2,1,4,ORDE,1		AL,P51X	
FITEM,2,671		FLST,2,4,4	
FLST,2,1,4,ORDE,1		FITEM,2,673	
FITEM,2,660		FITEM,2,682	
FLST,3,1,4,ORDE,1		FITEM,2,679	
FITEM,3,671		FITEM,2,683	
LSBL,P51X,P51X, ,KEEP		AL,P51X	
FLST,2,1,4,ORDE,1		FLST,2,4,4	
FITEM,2,671		FITEM,2,665	
FLST,3,1,4,ORDE,1		FITEM,2,669	
FITEM,3,673		FITEM,2,670	
LSBL,P51X,P51X, ,DELETE		FITEM,2,662	
LSTR, 365, 366		AL,P51X	
		FLST,2,5,4	
		FITEM,2,670	
		FITEM,2,682	
		FITEM,2,681	
		FITEM,2,678	
		FITEM,2,675	
		AL,P51X	
		Areas	
*AFUN,DEG			
KWPLAN,-1, 359, 367, 366			
wprot,0,-33.35,0			
FLST,2,2,4,ORDE,2			
FITEM,2,661			
FITEM,2,672			

! Creating Top Tapered Bolster

<pre> ----- ----- Rear Bolster Section ----- </pre>		<pre> ASBL,P51X,P51X,,KEEP Existing Areas </pre>		<pre> Dividing </pre>
<pre> KL,669,57.5/391.5, KWPAVE, 370 *AFUN,DEG wpro,,-50.500000, </pre>		<pre> Placing Workplane </pre>		<pre> KL,646,23.5/77, FLST,3,1,3,ORDE,1 FITEM,3,373 KGEN,2,P51X,,1564.34,-10000,,0 LSTR, 373, 375 </pre>
<pre> FLST,2,4,4,ORDE,4 FITEM,2,646 FITEM,2,-647 FITEM,2,669 FITEM,2,-670 LSBW,P51X divide lines </pre>		<pre> Using Workplane to </pre>		<pre> FLST,2,1,4,ORDE,1 FITEM,2,692 FLST,3,1,4,ORDE,1 FITEM,3,668 LSBL,P51X,P51X,,KEEP FLST,2,1,4,ORDE,1 FITEM,2,668 FLST,3,1,4,ORDE,1 FITEM,3,694 LSBL,P51X,P51X,,DELETE FLST,2,1,4,ORDE,1 FITEM,2,646 FLST,3,1,4,ORDE,1 FITEM,3,693 LSBL,P51X,P51X,,KEEP Line </pre>
<pre> WPSTYLE,.....,0 NUMMRG,KP,, LSTR, 371, 370 LSTR, 370, 374 LSTR, 374, 372 LSTR, 372, 371 </pre>		<pre> Creating Lines </pre>		<pre> FLST,3,1,4,ORDE,1 FITEM,3,693 LGEN,2,P51X,,230,,0 LSTR, 375, 373 LSTR, 377, 376 FLST,2,1,4,ORDE,1 FITEM,2,669 FLST,3,1,4,ORDE,1 FITEM,3,696 LSBL,P51X,P51X,,KEEP Lines </pre>
<pre> FLST,2,4,4 FITEM,2,658 FITEM,2,663 FITEM,2,664 FITEM,2,648 AL,P51X FLST,2,4,4 FITEM,2,666 FITEM,2,663 FITEM,2,659 FITEM,2,665 AL,P51X FLST,2,4,4 FITEM,2,669 FITEM,2,646 FITEM,2,647 FITEM,2,670 AL,P51X FLST,2,5,4 FITEM,2,688 FITEM,2,646 FITEM,2,686 FITEM,2,658 FITEM,2,666 AL,P51X FLST,2,5,4 FITEM,2,684 FITEM,2,659 FITEM,2,689 FITEM,2,669 FITEM,2,687 AL,P51X Areas </pre>		<pre> Horizontal Line </pre>		<pre> Top Area </pre>
<pre> FLST,2,1,5,ORDE,1 FITEM,2,302 FLST,3,1,4,ORDE,1 FITEM,3,647 ASBL,P51X,P51X,,KEEP FLST,2,1,5,ORDE,1 FITEM,2,95 FLST,3,1,4,ORDE,1 FITEM,3,670 </pre>		<pre> Creating </pre>		<pre> KL,693,2019.25/7362.2, KWPAVE, 378 WPCSYS,-1.0 WPSTYLE,.....,0 KWPAVE, 378 wpro,,9.000000, Workplane </pre>
<pre> FLST,2,4,4,ORDE,4 FITEM,2,405 FITEM,2,421 FITEM,2,646 FITEM,2,693 LSBW,P51X Divide Lines </pre>		<pre> Moving </pre>		<pre> Using WorkPlane to </pre>
<pre> NUMMRG,KP,, WPSTYLE,.....,0 LSTR, 378, 379 LSTR, 379, 380 LSTR, 380, 382 LSTR, 382, 378 Lines </pre>		<pre> Creating </pre>		<pre> FLST,2,2,5,ORDE,2 FITEM,2,244 FITEM,2,306 </pre>

FLST,3,2,4,ORDE,2			
FITEM,3,421			
FITEM,3,696			
ASBL,P51X,P51X,,KEEP	! Dividing		
Existing Areas			
FLST,2,9,4			
FITEM,2,694			
FITEM,2,684			
FITEM,2,401			
FITEM,2,402			
FITEM,2,403			
FITEM,2,404			
FITEM,2,669			
FITEM,2,405			
FITEM,2,703			
AL,P51X			
FLST,2,9,4			
FITEM,2,646			
FITEM,2,701			
FITEM,2,420			
FITEM,2,419			
FITEM,2,418			
FITEM,2,417			
FITEM,2,685			
FITEM,2,698			
FITEM,2,704			
AL,P51X			
FLST,2,4,4			
FITEM,2,696			
FITEM,2,704			
FITEM,2,703			
FITEM,2,693			
AL,P51X			
FLST,2,4,4			
FITEM,2,646			
FITEM,2,421			
FITEM,2,405			
FITEM,2,693			
AL,P51X	! Creating		
Areas			

----- Middle Bolster Section - Block Along Side -----			

KL,405,24*20.5/631.6,,			
FLST,3,1,3,ORDE,1			
FITEM,3,381			
KGEN,2,P51X,,,-10000*tan(9),-10000,,0			
LSTR, 381, 383			
FLST,2,1,4,ORDE,1			
FITEM,2,707			
FLST,3,1,4,ORDE,1			
FITEM,3,692			
LSBL,P51X,P51X,,KEEP			
FLST,2,1,4,ORDE,1			
FITEM,2,692			
FLST,3,1,4,ORDE,1			
FITEM,3,709			
LSBL,P51X,P51X,,DELETE			
FLST,2,1,4,ORDE,1			
FITEM,2,405			
FLST,3,1,4,ORDE,1			
FITEM,3,708			
LSBL,P51X,P51X,,KEEP			
FLST,3,1,4,ORDE,1			
FITEM,3,707			
FLST,2,1,4,ORDE,1			
FITEM,2,706			
AL,P51X			
Areas			

----- Lower Corner Bolster -----			

FLST,2,5,4			
FITEM,2,705			
FITEM,2,703			
FITEM,2,668			
FITEM,2,691			
FITEM,2,695			
AL,P51X			
Area			! Upper Unstiffened Wall

FLST,3,1,4,ORDE,1			
FITEM,3,708			
LGEN,2,P51X,,,-550*cos(9),,,0			! Copy Line
Down			
FLST,2,1,4,ORDE,1			
FITEM,2,715			
FLST,3,1,4,ORDE,1			
FITEM,3,707			
LSBL,P51X,P51X,,KEEP			
FLST,2,1,4,ORDE,1			
FITEM,2,707			
FLST,3,1,4,ORDE,1			
FITEM,3,717			
LSBL,P51X,P51X,,DELETE			
FLST,2,1,4,ORDE,1			

FITEM,2,716			FITEM,2,406	
FLST,3,1,4,ORDE,1			FITEM,2,700	
FITEM,3,411			FITEM,2,709	
LSBL,P51X,P51X,,KEEP			FITEM,2,708	
LDELE, 707,,,1	Cleanup Constr. Line		FITEM,2,718	
			FITEM,2,719	
KL,717,(2582-82.5*20.5)/2582,			AL,P51X	Lower Unstiffened Wall Area
FLST,3,1,3,ORDE,1				
FITEM,3,386				
KGEN,2,P51X,, ,230,,,0				
LSTR, 389, 386				
FLST,2,1,4,ORDE,1				
FITEM,2,717				
FLST,3,1,4,ORDE,1			*AFUN,DEG	Work in Degrees
FITEM,3,707			FLST,3,1,3,ORDE,1	
LSBL,P51X,P51X,,KEEP			FITEM,3,359	
LDELE, 716,,,1	Trim Line to Right		KGEN,2,P51X, , , ,327*20.5*sin(9),327*20.5*cos(9), ,0	
Length				
FLST,3,1,3,ORDE,1			LSTR, 357, 390	
FITEM,3,388			LSTR, 390, 359	
KGEN,2,P51X, , ,230,,,0				
LSTR, 388, 387			FLST,3,1,3,ORDE,1	
LSTR, 387, 355			FITEM,3,390	
LSTR, 387, 389			KGEN,2,P51X, , ,230,,,0	Keypoints
LSTR, 386, 244				
LSTR, 389, 262	Creating		LSTR, 368, 391	
Lines			LSTR, 391, 367	
			LSTR, 391, 390	Lines
FLST,2,7,4			FLST,2,4,4	
FITEM,2,715			FITEM,2,727	
FITEM,2,87			FITEM,2,724	
FITEM,2,416			FITEM,2,726	
FITEM,2,415			FITEM,2,674	
FITEM,2,414			AL,P51X	
FITEM,2,721			FLST,2,4,4	
FITEM,2,719			FITEM,2,661	
AL,P51X			FITEM,2,673	
FLST,2,4,4			FITEM,2,723	
FITEM,2,719			FITEM,2,724	
FITEM,2,720			AL,P51X	
FITEM,2,716			FLST,2,4,4	
FITEM,2,707			FITEM,2,679	
AL,P51X			FITEM,2,723	
FLST,2,4,4			FITEM,2,725	
FITEM,2,721			FITEM,2,727	
FITEM,2,467			AL,P51X	
FITEM,2,722			FLST,2,4,4	
FITEM,2,707			FITEM,2,726	
AL,P51X			FITEM,2,725	
FLST,2,7,4			FITEM,2,682	
FITEM,2,430			FITEM,2,672	
FITEM,2,431			AL,P51X	Areas
FITEM,2,432				
FITEM,2,65				
FITEM,2,717				
FITEM,2,720				
FITEM,2,722				
AL,P51X				
Areas	Creating			
FLST,2,14,4			ADALE, 295, , ,1 Deleting Unneeded Area	
FITEM,2,721				
FITEM,2,413			NUMMRG,ALL, , ,	Merging Coincident Items
FITEM,2,412			NUMCMP,AREA	
FITEM,2,411			NUMCMP,LINE	
FITEM,2,410			NUMCMP,KP	Compressing Numbers
FITEM,2,409				
FITEM,2,408			FINISH	
FITEM,2,407			/SAVE	
			/EOF	

❖ Filename: 2_4_build_front_INPUT

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*****
! FEA of 930E Truck Box Structure
! Front Wall Construction Routine

:build

FINISH
FINISH

!CLEAR
!NERR,0,,
!RESUME_build_wall.db
!FILNAM_build_front
!RESUME_geom.db
!FILNAM_geom

/TITLE,Building Front Wall Geometry

/REP7
*AFUN,DEG

/USER, 1
/VIEW, 1, 0.484264822294, -0.192301274690, -,
0.853526684785
/ANG, 1, 20.5950751333
/REPO
/FOC, 1, 811.708286462, 2215.46451192, -,
5428.73841967
/VIEW, 1, 0.484264822294, -0.192301274690, -,
0.853526684785
/REPO
/VIEW, 1, 0.484264822294, -0.192301274690, -,
0.853526684785
/DIST, 1, 2341.72159713
/ANG, 1, 13.6350751333
/REPO
/FOC, 1, 654.212217908, 2313.76522174, -,
5540.24419816
/VIEW, 1, 0.484264822294, -0.192301274690, -,
0.853526684785
APLOT

!-----
!----- Top Bolster - Lines Only
!-----

KL,676,(872.3-6*20.5)/872.3,
KL,676,(872.3-15*20.5)/872.3, ! Keypoints on Lines

FLST,3,1,3,ORDE,1
FITEM,3,393
KGEN,2,P51X,,,-12.5*20.5*sin(21.5-9),-
12.5*20.5*cos(21.5-9),0

LSTR, 394, 393
LSTR, 393, 392

FLST,3,1,3,ORDE,1
FITEM,3,392
KGEN,2,P51X,,,-13.5*20.5*sin(9),-13.5*20.5*cos(9),
0

LSTR, 392, 395
LSTR, 394, 395
LDELE, 729,,1

FLST,3,3,4,ORDE,3 ! Copying Lines into Middle

FITEM,3,728
FITEM,3,730
FITEM,3,-731
LGEN,2,P51X,,,-0.4127500000E+04,,0

LSTR, 392, 398
LSTR, 395, 399
LSTR, 393, 397
LSTR, 394, 396
LSTR, 398, 397 ! Creating Lines

FLST,2,1,4,ORDE,1
FITEM,2,676
FLST,3,2,4,ORDE,2
FITEM,3,728
FITEM,3,730
LSBL,P51X,P51X,, ,KEEP ! Dividing Line on Side Wall

!-----
!----- Outside Bolster Construction
!-----

FLST,3,1,3,ORDE,1
FITEM,3,393
KGEN,2,P51X,,,-16.5*20.5,,0 ! Width of Bolster

FLST,3,1,3,ORDE,1 ! Line Down Front Wall
FITEM,3,400
KGEN,2,P51X,,,-
0.3225329675E+04,0.7150384185E+03,,0
LSTR, 401, 400

FLST,2,1,4,ORDE,1
FITEM,2,660
FLST,3,2,4,ORDE,2
FITEM,3,734
FITEM,3,736
LSBL,P51X,P51X,, ,KEEP
FLST,2,2,4,ORDE,2
FITEM,2,734
FITEM,2,736
FLST,3,1,4,ORDE,1
FITEM,3,744
LSBL,P51X,P51X,, ,KEEP ! Dividing Lines Near Top
Edge

FLST,2,4,4
FITEM,2,660
FITEM,2,742
FITEM,2,674
FITEM,2,740
AL,P51X
FLST,2,4,4
FITEM,2,741
FITEM,2,744
FITEM,2,660
FITEM,2,745
AL,P51X
FLST,2,4,4
FITEM,2,739
FITEM,2,745
FITEM,2,743
FITEM,2,671
AL,P51X
FLST,2,4,4
FITEM,2,675
FITEM,2,671

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FITEM,2,677
FITEM,2,662
AL,P51X
LSTR, 363, 377
LSTR, 385, 387
FLST,2,4,4
FITEM,2,734
FITEM,2,662
FITEM,2,695
FITEM,2,697
AL,P51X
FLST,2,4,4
FITEM,2,714
FITEM,2,710
FITEM,2,697
FITEM,2,713
AL,P51X
FLST,2,4,4
FITEM,2,736
FITEM,2,713
FITEM,2,718
FITEM,2,716
AL,P51X
FLST,2,4,4
FITEM,2,716
FITEM,2,715
FITEM,2,657
FITEM,2,717
AL,P51X
FLST,2,1,4,ORDE,1
FITEM,2,676
FLST,3,1,4,ORDE,1
FITEM,3,655
LSBL,P51X,P51X,,KEEP
FLST,2,1,5,ORDE,1
FITEM,2,192
FLST,3,1,4,ORDE,1
FITEM,3,749
ASBL,P51X,P51X,,KEEP
FLST,2,1,4,ORDE,1
FITEM,2,746
FLST,3,1,4,ORDE,1
FITEM,3,748
LSBL,P51X,P51X,,KEEP
FLST,2,9,4
FITEM,2,655
FITEM,2,677
FITEM,2,743
FITEM,2,748
FITEM,2,695
FITEM,2,710
FITEM,2,718
FITEM,2,715
FITEM,2,752
AL,P51X ! Areas & Lines for Wall Behind Bolster
FLST,3,1,4,ORDE,1
FITEM,3,730
LGEN,2,P51X,,,-230,,0
! Line for Canopy Edge Stiffener

FLST,3,2,3,ORDE,2
FITEM,3,400
FITEM,3,401
KGEN,2,P51X,,,-10*20.5,,0
LSTR, 407, 408
KWPLAN,-1, 394, 393, 400
LSBW, 753
LDELE, 754,,1
WPCSYS,-1,0

FLST,3,2,3,ORDE,2
FITEM,3,3
FITEM,3,355
KGEN,2,P51X,,,-10*20.5,,0
LSTR, 410, 407
LSTR, 407, 408
LSTR, 408, 401
LSTR, 407, 3
LSTR, 410, 355
FLST,3,1,3,ORDE,1
FITEM,3,409
KGEN,2,P51X,,,-16.5*20.5,,0
LSTR, 411, 410
LSTR, 411, 409
LSTR, 409, 400
FLST,2,1,4,ORDE,1
FITEM,2,728
FLST,3,1,4,ORDE,1
FITEM,3,760
LSBL,P51X,P51X,,KEEP ! Lines 4 Bolster

FLST,2,5,4
FITEM,2,760
FITEM,2,755
FITEM,2,759
FITEM,2,753
FITEM,2,754
AL,P51X
FLST,2,4,4
FITEM,2,756
FITEM,2,754
FITEM,2,757
FITEM,2,751
AL,P51X
FLST,2,4,4
FITEM,2,656
FITEM,2,753
FITEM,2,757
FITEM,2,758
AL,P51X
FLST,2,9,4
FITEM,2,758
FITEM,2,759
FITEM,2,717
FITEM,2,736
FITEM,2,714
FITEM,2,734
FITEM,2,675
FITEM,2,739
FITEM,2,762
AL,P51X
FLST,2,5,4
FITEM,2,762
FITEM,2,745
FITEM,2,655
FITEM,2,761
FITEM,2,760
AL,P51X
FLST,2,5,4
FITEM,2,761
FITEM,2,748
FITEM,2,755
FITEM,2,749
FITEM,2,756
AL,P51X
! Areas For Bolster

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 ----- First Inside Bolster Construction

FLST,3,3,4,ORDE,3
 FITEM,3,755
 FITEM,3,-756
 FITEM,3,761
 LGEN,2,P51X,,,-776.6,, ,0

FLST,3,3,4,ORDE,3
 FITEM,3,728
 FITEM,3,764
 FITEM,3,-765
 LGEN,2,P51X,, ,16.5*20.5,, ,0

LSTR, 416, 412
 LSTR, 417, 413
 LSTR, 414, 415
 LSTR, 419, 418 | Constructing Lines

FLST,2,1,4,ORDE,1
 FITEM,2,538
 FLST,2,2,4,ORDE,2
 FITEM,2,538
 FITEM,2,540
 FLST,3,4,4,ORDE,4
 FITEM,3,764
 FITEM,3,-765
 FITEM,3,767
 FITEM,3,-768
 LSLBL,P51X,P51X,, ,KEEP | Dividing Lines

FLST,2,5,4
 FITEM,2,776
 FITEM,2,748
 FITEM,2,750
 FITEM,2,774
 FITEM,2,772
 AL,P51X
 FLST,2,4,4
 FITEM,2,778
 FITEM,2,772
 FITEM,2,771
 FITEM,2,777
 AL,P51X
 FLST,2,4,4
 FITEM,2,768
 FITEM,2,770
 FITEM,2,765
 FITEM,2,778
 AL,P51X
 FLST,2,4,4
 FITEM,2,769
 FITEM,2,767
 FITEM,2,764
 FITEM,2,777
 AL,P51X
 FLST,2,4,4
 FITEM,2,772
 FITEM,2,766
 FITEM,2,768
 FITEM,2,767
 AL,P51X
 FLST,2,4,4
 FITEM,2,765
 FITEM,2,764
 FITEM,2,728
 FITEM,2,771
 AL,P51X

FLST,2,4,4
 FITEM,2,770
 FITEM,2,728
 FITEM,2,768
 FITEM,2,769
 AL,P51X | Areas

 ----- 2nd & 3rd Inside Bolsters

FLST,3,10,4,ORDE,3 | Copying Lines
 FITEM,3,728
 FITEM,3,764
 FITEM,3,-772
 LGEN,3,P51X,,,-776.6,, ,0

FLST,2,2,4,ORDE,2
 FITEM,2,773
 FITEM,2,775
 FLST,3,8,4,ORDE,8
 FITEM,3,540
 FITEM,3,779
 FITEM,3,781
 FITEM,3,-782
 FITEM,3,788
 FITEM,3,-789
 FITEM,3,791
 FITEM,3,-792
 LSLBL,P51X,P51X,, ,KEEP
 FLST,2,4,4
 FITEM,2,771
 FITEM,2,769
 FITEM,2,786
 FITEM,2,800
 AL,P51X
 FLST,2,4,4
 FITEM,2,785
 FITEM,2,786
 FITEM,2,801
 FITEM,2,803
 AL,P51X
 FLST,2,4,4
 FITEM,2,803
 FITEM,2,784
 FITEM,2,779
 FITEM,2,782
 AL,P51X
 FLST,2,4,4
 FITEM,2,781
 FITEM,2,783
 FITEM,2,540
 FITEM,2,801
 AL,P51X
 FLST,2,4,4
 FITEM,2,780
 FITEM,2,786
 FITEM,2,782
 FITEM,2,781
 AL,P51X
 FLST,2,4,4
 FITEM,2,540
 FITEM,2,785
 FITEM,2,538
 FITEM,2,779
 AL,P51X
 FLST,2,4,4
 FITEM,2,784
 FITEM,2,783
 FITEM,2,780

LSBL,P51X,P51X,,KEEP
 LSTR, 397, 4
 LSTR, 4, 442
 FLST,3,1,4,ORDE,1
 FITEM,3,819
 LGEN,2,P51X,,290,,0
 LSTR, 445, 443
 LSTR, 444, 442
 FLST,3,2,4,ORDE,2
 FITEM,3,821
 FITEM,3,-822
 LGEN,2,P51X,,290,,0
 LSTR, 446, 448
 NUMMRG,KP...
 FLST,2,2,4,ORDE,2
 FITEM,2,382
 FITEM,2,808
 FLST,3,2,4,ORDE,2
 FITEM,3,826
 FITEM,3,-827
 LSBL,P51X,P51X,,KEEP
 Lines

FLST,2,4,4
 FITEM,2,832
 FITEM,2,828
 FITEM,2,830
 FITEM,2,815
 AL,P51X
 FLST,2,4,4
 FITEM,2,828
 FITEM,2,729
 FITEM,2,831
 FITEM,2,829
 AL,P51X
 FLST,2,4,4
 FITEM,2,827
 FITEM,2,825
 FITEM,2,822
 FITEM,2,829
 AL,P51X
 FLST,2,4,4
 FITEM,2,831
 FITEM,2,824
 FITEM,2,821
 FITEM,2,826
 AL,P51X
 FLST,2,4,4
 FITEM,2,823
 FITEM,2,828
 FITEM,2,826
 FITEM,2,827
 AL,P51X
 FLST,2,4,4
 FITEM,2,729
 FITEM,2,819
 FITEM,2,822
 FITEM,2,821
 AL,P51X
 FLST,2,4,4
 FITEM,2,823
 FITEM,2,819
 FITEM,2,824
 FITEM,2,825
 AL,P51X

! Areas

 ----- Misc and Inside Front Angle Plate

FLST,2,24,4
 FITEM,2,763
 FITEM,2,780
 FITEM,2,761
 FITEM,2,776
 FITEM,2,768
 FITEM,2,770
 FITEM,2,765
 FITEM,2,800
 FITEM,2,782
 FITEM,2,784
 FITEM,2,779
 FITEM,2,804
 FITEM,2,792
 FITEM,2,794
 FITEM,2,789
 FITEM,2,809
 FITEM,2,775
 FITEM,2,807
 FITEM,2,773
 FITEM,2,832
 FITEM,2,826
 FITEM,2,824
 FITEM,2,820
 FITEM,2,737
 AL,P51X

! Bottom Area of Top Bolster

FLST,3,1,3,ORDE,1
 FITEM,3,4
 KGEN,2,P51X,,190,0
 KL,729,(3303.6-190)/3303.6,
 FLST,3,2,3,ORDE,2
 FITEM,3,405
 FITEM,3,447
 KGEN,2,P51X,,10000,,0
 FLST,2,4,3
 FITEM,2,447
 FITEM,2,405
 FITEM,2,449
 FITEM,2,450
 A,P51X

! Front Angle Plate

FLST,2,1,5,ORDE,1
 FITEM,2,385
 FLST,3,1,5,ORDE,1
 FITEM,3,17
 ASBA,P51X,P51X,,KEEP
 ADELE, 387,,1
 FLST,2,1,5,ORDE,1
 FITEM,2,17
 FLST,3,1,5,ORDE,1
 FITEM,3,386
 ASBA,P51X,P51X,,KEEP
 FLST,2,10,5,ORDE,10
 FITEM,2,347
 FITEM,2,-348
 FITEM,2,354
 FITEM,2,-355
 FITEM,2,361
 FITEM,2,-362
 FITEM,2,368
 FITEM,2,-369
 FITEM,2,377
 FITEM,2,-378
 FLST,3,1,5,ORDE,1
 FITEM,3,386

ASBA,P51X,P51X,,KEEP

FLST,2,3,5,ORDE,3

FITEM,2,45

FITEM,2,170

FITEM,2,188

FLST,3,1,5,ORDE,1

FITEM,3,386

ASBA,P51X,P51X,,KEEP ! Dividing Areas

NUMMRG,ALL,, ,

Items

NUMCMP,AREA

NUMCMP,LINE

NUMCMP,KP

! Merging Coincident

! Compressing Numbers

FINISH

!SAVE

/EOF

[]

[]

Cleanup

[]

❖ *Filename: 2_5_build_canopy_INPUT*

```

*****
!      FEA of 930E Truck Box Structure
!      Canopy Construction Routine

:build

FINISH

/FILNAM,geom
/TITLE,Building Canopy Geometry

/PREP7
*AFUN,DEG

/VIEW,1,1,1,1
/ANG,1
/REP,FAST
/AUTO,1
/REP
/USER,1
/FOC,1,3101.70013053,4316.90917962,-
10130.9161949
/VIEW,1,0.577350269190,0.577350269190,
0.577350269190
/REPLO
/DIST,1,2537.46312511
/ANG,1,-3.46000000000
APLOT

-----
Outer Bolster
-----

KL,728,(283.9-12.5*20.5)/283.9,,
FLST,3,1,3,ORDE,1
FITEM,3,462
KGEN,2,P51X,,,-16.5*20.5,,0
LSTR,462,463
LSBL,728,863
FLST,3,1,4,ORDE,1
FITEM,3,865
LGEN,2,P51X,,,-16.5*20.5,,0
FLST,2,1,4,ORDE,1
FITEM,2,732
FLST,3,2,4,ORDE,2
FITEM,3,728
FITEM,3,743
LSBL,P51X,P51X,,KEEP
LSTR,464,462! Lines in Top Corner

FLST,3,2,4,ORDE,2
FITEM,3,863
FITEM,3,867
LGEN,2,P51X,,,-4225*sin(9),-4225*cos(9),0
LSTR,395,465
LSTR,406,466
LSTR,463,467! Lines out canopy

FLST,3,2,3,ORDE,2
FITEM,3,465
FITEM,3,467
KGEN,2,P51X,,,-5*20.7*cos(9),-5*20.7*sin(9),0
LSTR,462,468
LSTR,464,469
LSTR,469,467
LSTR,468,465
LSTR,468,469! Lines 4 Lower Bolster

FLST,3,1,4,ORDE,1
FITEM,3,868
LGEN,2,P51X,,,-5*20.7*cos(9),-5*20.7*sin(9),0
LSTR,466,471
LSTR,465,470
LSTR,471,359
LSTR,367,470! Lines 4 Upper Bolster

FLST,2,5,4
FITEM,2,865
FITEM,2,732
FITEM,2,728
FITEM,2,867
FITEM,2,863
AL,P51X
FLST,2,4,4
FITEM,2,732
FITEM,2,874
FITEM,2,873
FITEM,2,877
AL,P51X
FLST,2,5,4
FITEM,2,875
FITEM,2,869
FITEM,2,868
FITEM,2,876
FITEM,2,877
AL,P51X
FLST,2,4,4
FITEM,2,728
FITEM,2,874
FITEM,2,872
FITEM,2,875
AL,P51X
FLST,2,4,4
FITEM,2,876
FITEM,2,873
FITEM,2,870
FITEM,2,865
AL,P51X
FLST,2,4,4
FITEM,2,869
FITEM,2,872
FITEM,2,871
FITEM,2,867
AL,P51X
FLST,2,4,4
FITEM,2,870
FITEM,2,871
FITEM,2,863
FITEM,2,868
AL,P51X
FLST,2,5,4
FITEM,2,881
FITEM,2,871
FITEM,2,879
FITEM,2,743
FITEM,2,739
AL,P51X

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FLST,2,5,4		FITEM,2,918	
FITEM,2,737		FITEM,2,915	
FITEM,2,870		FITEM,2,937	
FITEM,2,727		AL,P51X	
FITEM,2,882		FLST,2,5,4	
FITEM,2,880		FITEM,2,937	
AL,P51X		FITEM,2,917	
FLST,2,4,4		FITEM,2,916	
FITEM,2,727		FITEM,2,913	
FITEM,2,657		FITEM,2,912	
FITEM,2,743		AL,P51X	
FITEM,2,863		FLST,2,4,4	
AL,P51X		FITEM,2,919	
FLST,2,4,4		FITEM,2,930	
FITEM,2,671		FITEM,2,939	
FITEM,2,881		FITEM,2,927	
FITEM,2,882		AL,P51X	
FITEM,2,878		FLST,2,5,4	
AL,P51X	! Creating Areas	FITEM,2,939	
-----		FITEM,2,929	
----- Interior Bolsters		FITEM,2,928	
-----		FITEM,2,925	
FLST,3,4,5,ORDE,2		FITEM,2,924	
FITEM,3,401		AL,P51X	! Completing Bolster Areas
FITEM,3,-404		-----	
AGEN,5,P51X,,-776.6,.,.,0 ! Copying Areas		----- Middle Bolsters	

FLST,2,1,4,ORDE,1		FLST,3,6,4,ORDE,6	
FITEM,2,866		FITEM,3,919	
FLST,3,8,4,ORDE,8		FITEM,3,-620	
FITEM,3,891		FITEM,3,923	
FITEM,3,894		FITEM,3,925	
FITEM,3,903		FITEM,3,929	
FITEM,3,906		FITEM,3,-930	
FITEM,3,915		LGEM,2,P51X,,-682.85,.,.,0	
FITEM,3,918		FLST,2,1,4,ORDE,1	
FITEM,3,927		FITEM,2,730	
FITEM,3,930		FLST,3,1,4,ORDE,1	
LSBL,P51X,P51X,.,.,KEEP ! Dividing Top Bolster Line		FITEM,3,866	
FLST,2,4,4		LSBL,P51X,P51X,.,.,KEEP	
FITEM,2,891		LSTR, 512, 399	
FITEM,2,883		LSTR, 511, 508	
FITEM,2,894		LSTR, 512, 513	
FITEM,2,933		LSTR, 511, 510	
AL,P51X		FLST,2,1,4,ORDE,1	
FLST,2,5,4		FITEM,2,931	
FITEM,2,933		FLST,3,1,4,ORDE,1	
FITEM,2,893		FITEM,3,944	
FITEM,2,892		LSBL,P51X,P51X,.,.,KEEP	! Lines
FITEM,2,889			
FITEM,2,888		FLST,2,4,4	
AL,P51X		FITEM,2,866	
FLST,2,4,4		FITEM,2,944	
FITEM,2,903		FITEM,2,950	
FITEM,2,935		FITEM,2,946	
FITEM,2,906		AL,P51X	
FITEM,2,895		FLST,2,4,4	
AL,P51X		FITEM,2,866	
FLST,2,5,4		FITEM,2,947	
FITEM,2,904		FITEM,2,940	
FITEM,2,935		FITEM,2,949	
FITEM,2,905		AL,P51X	
FITEM,2,901		FLST,2,4,4	
FITEM,2,900		FITEM,2,943	
AL,P51X		FITEM,2,940	
FLST,2,4,4		FITEM,2,944	
FITEM,2,907		FITEM,2,942	
		AL,P51X	

FLST,2,4,4		FITEM,2,828	
FITEM,2,948		FITEM,2,827	
FITEM,2,949		FITEM,2,735	
FITEM,2,941		FITEM,2,744	
FITEM,2,942		AL,P51X	! Area Inside Box
AL,P51X			
FLST,2,4,4		FLST,2,14,4	
FITEM,2,730		FITEM,2,743	
FITEM,2,947		FITEM,2,744	
FITEM,2,941		FITEM,2,729	
FITEM,2,946		FITEM,2,950	
AL,P51X		FITEM,2,951	
FLST,2,4,4		FITEM,2,939	
FITEM,2,950		FITEM,2,938	
FITEM,2,730		FITEM,2,937	
FITEM,2,943		FITEM,2,936	
FITEM,2,948		FITEM,2,935	
AL,P51X	! Areas	FITEM,2,934	
		FITEM,2,933	
!-----		FITEM,2,932	
!----- Closing Top Bolster		FITEM,2,867	
!-----		AL,P51X	! Top Area
FLST,2,24,4		!-----	
FITEM,2,734		!----- Outer Lip	
FITEM,2,945		!-----	
FITEM,2,866			
FITEM,2,944		FLST,3,1,3,ORDE,1	
FITEM,2,951		FITEM,3,512	
FITEM,2,927		KGEN,2,P51X, , , 230*cos(9),230*sin(9), ,0	
FITEM,2,919		LSTR, 512, 515	
FITEM,2,930		FLST,3,1,3,ORDE,1	
FITEM,2,938		FITEM,3,515	
FITEM,2,915		KGEN,2,P51X, , , -75*sin(9),75*cos(9), ,0	
FITEM,2,907		LSTR, 516, 515	
FITEM,2,918		FLST,3,1,3,ORDE,1	
FITEM,2,936		FITEM,3,512	
FITEM,2,903		KGEN,2,P51X, , , -140*cos(9),-140*sin(9), ,0	
FITEM,2,895		LSTR, 517, 511	
FITEM,2,906		KL,730,190/4225, ,	
FITEM,2,934		FLST,3,1,3,ORDE,1	
FITEM,2,891		FITEM,3,518	
FITEM,2,883		KGEN,2,P51X, , , -140*cos(9),-140*sin(9), ,0	
FITEM,2,894		LSTR, 519, 518	
FITEM,2,932		LSTR, 519, 517	! Shape of Lip
FITEM,2,728			
FITEM,2,732		FLST,3,3,4,ORDE,3	
FITEM,2,864		FITEM,3,952	
AL,P51X	! Front Area	FITEM,3,954	
		FITEM,3,955	
FLST,2,6,4		LGEN,2,P51X, , , 4127.5, , , 0 ! Copy to Outside	
FITEM,2,738			
FITEM,2,727		LSTR, 516, 520	
FITEM,2,865		LSTR, 521, 515	
FITEM,2,864		LSTR, 517, 524	
FITEM,2,760		LSTR, 522, 519	! Connecting Lines
FITEM,2,759		LSTR, 523, 520	
AL,P51X	! Side Area	LSTR, 521, 470	
		LSTR, 468, 524	
FLST,2,14,4			
FITEM,2,741		FLST,2,2,5,ORDE,2	
FITEM,2,652		FITEM,2,404	
FITEM,2,773		FITEM,2,409	
FITEM,2,775		FLST,2,3,4,ORDE,3	
FITEM,2,797		FITEM,2,870	
FITEM,2,800		FITEM,2,873	
FITEM,2,801		FITEM,2,882	
FITEM,2,803		FLST,3,2,4,ORDE,2	
FITEM,2,806		FITEM,3,957	
FITEM,2,807		FITEM,3,963	

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SBL,P51X,P51X,,KEEP
FLST,2,2,4,ORDE,2
FITEM,2,957
FITEM,2,963
FLST,3,2,4,ORDE,2
FITEM,3,970
FITEM,3,-971
LSBL,P51X,P51X,,KEEP
FLST,2,2,5,ORDE,2
FITEM,2,404
FITEM,2,409
FLST,3,2,4,ORDE,2
FITEM,3,882
FITEM,3,972
ASBL,P51X,P51X,,KEEP
FLST,2,4,4
FITEM,2,971
FITEM,2,964
FITEM,2,956
FITEM,2,870
AL,P51X
FLST,2,4,4
FITEM,2,970
FITEM,2,958
FITEM,2,873
FITEM,2,965
AL,P51X
! Areas On Outside Edge
LSTR, 518, 523
NUMMRG,KP,...
FLST,2,5,4
FITEM,2,954
FITEM,2,957
FITEM,2,962
FITEM,2,873
FITEM,2,972
AL,P51X
! Lip Inside Area
FLST,2,28,5,ORDE,25
FITEM,2,401
FITEM,2,403
FITEM,2,405
FITEM,2,-406
FITEM,2,408
FITEM,2,411
FITEM,2,-412
FITEM,2,414
FITEM,2,-416
FITEM,2,418
FITEM,2,-420
FITEM,2,422
FITEM,2,-424
FITEM,2,426
FITEM,2,-427
FITEM,2,429
FITEM,2,431
FITEM,2,433
FITEM,2,435
FITEM,2,437
FITEM,2,-438
FITEM,2,440
FITEM,2,-441
FITEM,2,446
FITEM,2,449
ASBA,P51X, 450 ! Cutting Ends of Bolsters
FLST,2,25,5,ORDE,19
FITEM,2,413
FITEM,2,417
FITEM,2,421
FITEM,2,425
FITEM,2,439
FITEM,2,461
FITEM,2,-463
FITEM,2,467
FITEM,2,-469
FITEM,2,473
FITEM,2,-475
FITEM,2,479
FITEM,2,-481
FITEM,2,488
FITEM,2,-489
FITEM,2,492
FITEM,2,-493
FITEM,2,495
FITEM,2,-496
ADELE,P51X,,1
FLST,2,3,5,ORDE,3
FITEM,2,402
FITEM,2,458
FITEM,2,-459
ADELE,P51X,,1 ! Deleting Ends of Bolsters
FLST,2,2,4,ORDE,2
FITEM,2,931
FITEM,2,953
LDELE,P51X,,1
LSTR, 515, 517
LSTR, 519, 530
LSTR, 519, 522
LSTR, 527, 535
LSTR, 534, 539
LSTR, 538, 543
LSTR, 542, 547
LSTR, 546, 548 ! Connecting Missing Lines
FLST,2,5,4
FITEM,2,972
FITEM,2,977
FITEM,2,981
FITEM,2,974
FITEM,2,975
AL,P51X
FLST,2,4,4
FITEM,2,987
FITEM,2,1029
FITEM,2,993
FITEM,2,991
AL,P51X
FLST,2,4,4
FITEM,2,998
FITEM,2,1030
FITEM,2,1004
FITEM,2,1002
AL,P51X
FLST,2,4,4
FITEM,2,1009
FITEM,2,1031
FITEM,2,1013
FITEM,2,1015
AL,P51X
FLST,2,4,4
FITEM,2,1020
FITEM,2,1032
FITEM,2,1026
FITEM,2,1024
AL,P51X
FLST,2,4,4
FITEM,2,980
FITEM,2,1041

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FITEM,2,1038		FITEM,2,877	
FITEM,2,1035		FITEM,2,1030	
AL,P51X	! Areas on Ends of Bolsters	FITEM,2,875	
FLST,2,24,4		FITEM,2,1029	
FITEM,2,872		FITEM,2,874	
FITEM,2,871		FITEM,2,983	
FITEM,2,980		FITEM,2,890	
FITEM,2,1038		AL,P51X	! Lip Internal Area
FITEM,2,885		FLST,2,1,5,ORDE,1	
FITEM,2,1024		FITEM,2,417	
FITEM,2,1020		FLST,3,1,5,ORDE,1	
FITEM,2,884		FITEM,3,407	
FITEM,2,1026		ASBA,P51X,P51X,,KEEP	
FITEM,2,1013		! Subtracted Upper Bolster End Area	
FITEM,2,1009		KWPLAN,-1, 535, 533, 480	
FITEM,2,877		WPSTYLE,.....0	
FITEM,2,1015		FLST,2,3,5,ORDE,3	
FITEM,2,1002		FITEM,2,414	
FITEM,2,998		FITEM,2,-415	
FITEM,2,1004		FITEM,2,418	
FITEM,2,875		ASBW,P51X	
FITEM,2,991		KWPAVE, 539	
FITEM,2,987		FLST,2,3,5,ORDE,3	
FITEM,2,993		FITEM,2,419	
FITEM,2,873		FITEM,2,-420	
FITEM,2,975		FITEM,2,423	
FITEM,2,974		ASBW,P51X	
FITEM,2,874		KWPAVE, 543	
AL,P51X	! Lip Inside Area	FLST,2,3,5,ORDE,3	
FLST,2,4,4		FITEM,2,414	
FITEM,2,958		FITEM,2,424	
FITEM,2,961		FITEM,2,426	
FITEM,2,955		ASBW,P51X	
FITEM,2,872		KWPAVE, 547	
AL,P51X		FLST,2,3,5,ORDE,3	
FLST,2,7,4		FITEM,2,419	
FITEM,2,964		FITEM,2,427	
FITEM,2,880		FITEM,2,431	
FITEM,2,876		ASBW,P51X	
FITEM,2,965		WPCSYS,-1,0	! Using WPlane to Cut Lip Areas
FITEM,2,730		LSTR, 547, 493	
FITEM,2,961		LSTR, 543, 486	
FITEM,2,960		LSTR, 539, 483	
AL,P51X		LSTR, 535, 476	
FLST,2,4,4		FLST,2,4,4	
FITEM,2,956		FITEM,2,896	
FITEM,2,952		FITEM,2,926	
FITEM,2,960		FITEM,2,912	
FITEM,2,959		FITEM,2,929	
AL,P51X	! Lip Outer Areas	AL,P51X	
KWPLAN,-1, 527, 467, 535		FLST,2,4,4	
ASBW, 414		FITEM,2,898	
WPSTYLE,.....0	! Cut Outer Area w/ WPlane	FITEM,2,920	
LSTR, 518, 469		FITEM,2,900	
FLST,2,1,4,ORDE,1		FITEM,2,922	
FITEM,2,886		AL,P51X	
FLST,3,1,4,ORDE,1		FLST,2,4,4	
FITEM,3,983		FITEM,2,921	
LSBL,P51X,P51X,,KEEP		FITEM,2,911	
FLST,2,13,4		FITEM,2,905	
FITEM,2,730		FITEM,2,913	
FITEM,2,1041		AL,P51X	
FITEM,2,885		FLST,2,4,4	
FITEM,2,1032		FITEM,2,931	
FITEM,2,884		FITEM,2,899	
FITEM,2,1031		FITEM,2,897	
		FITEM,2,893	

AL,P51X	! Lip Gusset Areas	wpoff,0,0,-700.5+503	
-----		FLST,2,5,5,ORDE,4	
-----	Top Plate Areas	FITEM,2,446	
-----		FITEM,2,451	
FLST,2,4,4		FITEM,2,-453	
FITEM,2,951		FITEM,2,455	
FITEM,2,1039		ASBW,P51X	
FITEM,2,1027		FLST,2,5,4	
FITEM,2,885		FITEM,2,1001	
AL,P51X		FITEM,2,1000	
FLST,2,4,4		FITEM,2,1003	
FITEM,2,1028		FITEM,2,988	
FITEM,2,1016		FITEM,2,990	
FITEM,2,938		AL,P51X	! Outside Bolster Gusset
FITEM,2,884		WPSTYLE,.....,1	
AL,P51X		wpoff,0,0,-1575-503+700.5	
FLST,2,4,4		FLST,2,3,5,ORDE,3	
FITEM,2,936		FITEM,2,463	
FITEM,2,1017		FITEM,2,467	
FITEM,2,877		FITEM,2,-468	
FITEM,2,1005		ASBW,P51X	
AL,P51X		KL,1033,5,,	
FLST,2,4,4		KL,1022,5,,	
FITEM,2,1006		LSTR, 552, 553	
FITEM,2,875		FLST,2,2,4,ORDE,2	
FITEM,2,994		FITEM,2,1022	
FITEM,2,934		FITEM,2,1033	
AL,P51X		FLST,3,1,4,ORDE,1	
FLST,2,4,4		FITEM,3,953	
FITEM,2,995		LSBL,P51X,P51X,, ,KEEP	
FITEM,2,874		FLST,2,4,4	
FITEM,2,963		FITEM,2,957	
FITEM,2,932		FITEM,2,954	
AL,P51X		FITEM,2,953	
-----		FITEM,2,968	
-----	Internal Bolster Gussets	AL,P51X	! 2nd Center Gusset Area
-----		wpoff,0,0,-75.5*20.7	
-----		FLST,2,3,5,ORDE,3	
*AFUN,DEG		FITEM,2,452	
KWPAVE, 398		FITEM,2,-453	
wpro,,9.000000,		FITEM,2,455	
KWPAVE, 508		ASBW,P51X	
wpoff,0,0,-503	! Placing WPlane	KL,1044,5,,	
FLST,2,3,5,ORDE,3		KL,1048,5,,	
FITEM,2,454		LSTR, 559, 558	
FITEM,2,490		FLST,2,2,4,ORDE,2	
FITEM,2,-491		FITEM,2,1044	
ASBW,P51X		FITEM,2,1046	
WPSTYLE,.....,0		FLST,3,1,4,ORDE,1	
KL,943,5,,		FITEM,3,973	
KL,949,5,,		LSBL,P51X,P51X,, ,KEEP	
LSTR, 502, 503		FLST,2,4,4	
FLST,2,2,4,ORDE,2		FITEM,2,973	
FITEM,2,943		FITEM,2,976	
FITEM,2,949		FITEM,2,1039	
FLST,3,1,4,ORDE,1		FITEM,2,1023	
FITEM,3,960		AL,P51X	! 3rd Center Gusset Area
LSBL,P51X,P51X,, ,KEEP		-----	
FLST,2,4,4		-----	Rounded Sections of Bolsters
FITEM,2,978		-----	
FITEM,2,962		WPCSYS,-1,0	
FITEM,2,960		KL,756,34*20.5/3085.14,,	
FITEM,2,942		KWPLAN,-1, 510, 511, 462	
AL,P51X	! 1st Center Gusset Area	FLST,3,1,3,ORDE,1	
WPSTYLE,.....,1		FITEM,3,510	
		KGEN,2,P51X, , , -1000, , ,0	

LARC,510,560,561,60*20.5,	! Creating Arc	FITEM,2,-510	
WPSTYLE,.....0		ASBW,P51X	
FLST,2,1,4,ORDE,1		KWPLAN,-1, 498, 491, 435	
FITEM,2,756		FLST,2,2,5,ORDE,2	
FLST,3,1,4,ORDE,1		FITEM,2,511	
FITEM,3,1044		FITEM,2,-512	
LSBL,P51X,P51X,,KEEP		ASBW,P51X	
FLST,2,5,4		KWPLAN,-1, 497, 490, 431	
FITEM,2,989		FLST,2,2,5,ORDE,2	
FITEM,2,1044		FITEM,2,513	
FITEM,2,1050		FITEM,2,-514	
FITEM,2,760		ASBW,P51X	! Cutting Top Bolster As Required
FITEM,2,864			
AL,P51X	! Creating Area	WPCSYS,-1,0	
		WPSTYLE,.....0	
FLST,3,1,5,ORDE,1		FLST,3,1,5,ORDE,1	
FITEM,3,453		FITEM,3,455	
AGEN,2,P51X,,,-16.5*20.5,, ,0		AGEN,4,P51X,,,-776.6,, ,0	! Copying Rounded Section
FLST,2,2,5,ORDE,2			
FITEM,2,377		FLST,2,6,5,ORDE,6	
FITEM,2,442		FITEM,2,350	
ASBA,P51X, 455		FITEM,2,357	
! Used Copied Area to Cut Top Bolster		FITEM,2,364	
		FITEM,2,466	
FLST,3,1,4,ORDE,1		FITEM,2,472	
FITEM,3,1044		FLST,3,3,5,ORDE,3	
LGEN,2,P51X,,,-16.5*20.5,, ,0		FITEM,3,513	
LSTR, 563, 560		FITEM,3,-514	
FLST,2,1,5,ORDE,1		FITEM,3,517	
FITEM,2,341		ASBA,P51X,P51X,,KEEP	! Dividing Areas
FLST,2,1,5,ORDE,1			
FITEM,2,338		FLST,2,5,4	
FLST,3,1,4,ORDE,1		FITEM,2,1098	
FITEM,3,756		FITEM,2,752	
ASBL,P51X,P51X,,KEEP	! Dividing Areas	FITEM,2,1075	
		FITEM,2,1053	
NUMMRG,KP,...		FITEM,2,1088	
FLST,2,5,4		AL,P51X	
FITEM,2,734		FLST,2,5,4	
FITEM,2,1051		FITEM,2,1070	
FITEM,2,1056		FITEM,2,1087	
FITEM,2,1057		FITEM,2,1060	
FITEM,2,949		FITEM,2,1058	
AL,P51X		FITEM,2,1097	
FLST,2,4,4		AL,P51X	
FITEM,2,734		FLST,2,5,4	
FITEM,2,1044		FITEM,2,1079	
FITEM,2,756		FITEM,2,1092	
FITEM,2,990		FITEM,2,1063	
AL,P51X	! Closing Rounded Section	FITEM,2,1054	
		FITEM,2,1100	
KWPLAN,-1, 480, 473, 419		AL,P51X	
FLST,2,2,5,ORDE,2		FLST,2,5,4	
FITEM,2,501		FITEM,2,1077	
FITEM,2,-502		FITEM,2,1091	
ASBW,P51X		FITEM,2,1061	
KWPLAN,-1, 479, 472, 415		FITEM,2,1066	
FLST,2,2,5,ORDE,2		FITEM,2,1099	
FITEM,2,505		AL,P51X	
FITEM,2,-506		FLST,2,5,4	
ASBW,P51X		FITEM,2,1083	
KWPLAN,-1, 489, 482, 427		FITEM,2,1096	
FLST,2,2,5,ORDE,2		FITEM,2,1064	
FITEM,2,507		FITEM,2,1069	
FITEM,2,-508		FITEM,2,1102	
ASBW,P51X		AL,P51X	
KWPLAN,-1, 488, 481, 423		FLST,2,5,4	
FLST,2,2,5,ORDE,2		FITEM,2,1081	
FITEM,2,509			

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ITEM,2,1101
ITEM,2,1067
ITEM,2,1072
ITEM,2,1095
AL,P51X          ! Filling in Side Areas

|-----
|----- Canopy Brace
|-----

FLST,3,3,4,ORDE,2
ITEM,3,757
ITEM,3,-759
LGEN,2,P51X,,,-(2000-300)*cos(12.5),(2000-
300)*sin(12.5),.0
FLST,3,3,4,ORDE,2
ITEM,3,757
ITEM,3,-759
LGEN,2,P51X,,,-(
(2000+300)*cos(12.5),(2000+300)*sin(12.5),.0
FLST,2,3,5,ORDE,3
ITEM,2,341
ITEM,2,343
ITEM,2,442
FLST,3,6,4,ORDE,6
ITEM,3,535
ITEM,3,725
ITEM,3,763
ITEM,3,777
ITEM,3,784
ITEM,3,787
ASBL,P51X,P51X,,KEEP ! Lower Reinforced Area

KWPLAN,-1, 465, 474, 521
KWPAVE, 395
wpoff,0,0,2000-300
FLST,2,2,5,ORDE,2
ITEM,2,480
ITEM,2,488
ASBW,P51X
wpoff,0,0,600
FLST,2,2,5,ORDE,2
ITEM,2,341
ITEM,2,343
ASBW,P51X
WPCSYS,-1,0          ! Upper Reinforced Area

KL,996,160/600,,
KL,996,(600-160)/600,,
FLST,3,2,3,ORDE,2
ITEM,3,596
ITEM,3,-597
KGEN,2,P51X,,,-92.925,,.0
FLST,3,2,3,ORDE,2
ITEM,3,598
ITEM,3,-599
KGEN,2,P51X,,,-6*25.4,,.0
FLST,2,4,3
ITEM,2,598
ITEM,2,600
ITEM,2,601
ITEM,2,599
A,P51X
FLST,2,1,5,ORDE,1
ITEM,2,531
FLST,3,1,5,ORDE,1
ITEM,3,341
ASBA,P51X,P51X,,KEEP ! Lower End Area

KDISTANCE, 591, 594

KL,1011,160/600.29,,
KL,1011,(600.29-160)/600.29,,
FLST,3,2,3,ORDE,2
ITEM,3,602
ITEM,3,-603
KGEN,2,P51X,,,-92.925,,.0
FLST,3,2,3,ORDE,2
ITEM,3,604
ITEM,3,-605
KGEN,2,P51X,,,-6*25.4,,.0
FLST,2,4,3
ITEM,2,604
ITEM,2,606
ITEM,2,607
ITEM,2,605
A,P51X
FLST,2,1,5,ORDE,1
ITEM,2,541
FLST,3,1,5,ORDE,1
ITEM,3,531
ASBA,P51X,P51X,,KEEP ! Upper End Area

LSTR, 588, 604
LSTR, 605, 599
LSTR, 600, 606
LSTR, 607, 601
FLST,2,4,4
ITEM,2,1124
ITEM,2,1128
ITEM,2,1130
ITEM,2,1129
ITEM,2,1129
AL,P51X
FLST,2,4,4
ITEM,2,1132
ITEM,2,1130
ITEM,2,1046
ITEM,2,1127
AL,P51X
FLST,2,4,4
ITEM,2,711
ITEM,2,1131
ITEM,2,1129
ITEM,2,1125
AL,P51X
FLST,2,4,4
ITEM,2,733
ITEM,2,1126
ITEM,2,1132
ITEM,2,1131
AL,P51X          ! Canopy Brace Areas

|-----
|----- Correcting Mistake in Front Floor/Wall Angle Plate
|-----
! Correction Necessary for correct mesh generation.
! Old Area was not attached to Wall or Floor plates...

ADELE, 379,,1 ! Deleted Area with unbroken sides

LSTR, 447, 405          ! Replaced Missing Edge

FLST,2,15,4
ITEM,2,379
ITEM,2,792
ITEM,2,769
ITEM,2,809
ITEM,2,833
ITEM,2,837
ITEM,2,839
ITEM,2,845

```

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FITEM,2,848
FITEM,2,850
FITEM,2,853
FITEM,2,843
FITEM,2,835
FITEM,2,860
FITEM,2,858
AL,P51X ! Replaced Area using proper line segments

!-----
!----- Adding Missing Gusset in Pivot Structure
!-----

KWPLAN,-1, 180, 183, 178
KWPAVE, 209
FLST,2,3,5,ORDE,3
FITEM,2,33
FITEM,2,129
FITEM,2,140
ASBW,P51X ! Using Workplane to Cut Areas

WPSTYLE,,,,,,,,,0
FLST,2,4,4
FITEM,2,1137
FITEM,2,1133
FITEM,2,1134
FITEM,2,362
AL,P51X ! Creating Gusset Area from Created lines

!-----
!-----Correcting Mistake in 2nd Bolster/Rear Stringer
!-----
!-----
! Correction Necessary for correct mesh generation.
! Old Area was not made up of proper lines to be
! attached to surrounding areas. Caused discontinuous
! mesh.

ADELE, 52
FLST,2,5,4
FITEM,2,151
FITEM,2,173
FITEM,2,155
FITEM,2,139
FITEM,2,156
AL,P51X

!-----
!----- Cleanup
!-----

NUMMRG,ALL,, ! Merging Coincident
Items
NUMCMP,AREA
NUMCMP,LINE
NUMCMP,KP ! Compressing Numbers

FINISH
/EOF

```

❖ Filename: 2_6_round_corners_INPUT

```

!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
!           FEA of 930E Truck Box Structure
!Routine to Add Rounded Bolster Fillets to Geometry
!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!

FINISH

/TITLE,Adding Bolster Fillets

/PREP7
*AFUN,DEG
APLOT
/AUTO, 1
/REP
/USER, 1
/VIEW, 1, 0.909916171862, -0.375169699704,
0.176918785347
/ANG, 1, 179.498910154
/LIG, 1,1,1.000, 0.501901609919, 0.563136024018
, 0.656485028324, 0.000000000000E+00
/ZOOM,1,RECT,0.068021,0.615836,0.967367,0.09853
4

!-----
!----- Forward Bolsters
!-----

FLST,2,2,5,ORDE,2
FITEM,2,189
FITEM,2,201
ADELE,P51X,,1 ! Deleting STR Side Areas

AFILLT,97,100,38, ! First Bolster from Front
AFILLT,114,116,38,
AFILLT,96,101,38,
AFILLT,552,99,38,
AFILLT,551,115,38,
AFILLT,550,98,38, ! 38mm Bolster Fillets
ADELE, 258,,1 ! Deleting End Cap Area
LSTR, 70, 611 ! Creating Line in Middle
FLST,2,4,4
FITEM,2,83
FITEM,2,1136
FITEM,2,253
FITEM,2,1144
AL,P51X
FLST,2,4,4
FITEM,2,124
FITEM,2,83
FITEM,2,85
FITEM,2,1161
AL,P51X ! Creating New End Cap Areas

AFILLT,282,261,38,
AFILLT,274,280,38,
AFILLT,264,268,38,
AFILLT,109,113,38,
AFILLT,86,95,38,
AFILLT,561,93,38,
AFILLT,560,111,38,
AFILLT,559,266,38,
AFILLT,558,278,38,
AFILLT,557,284,38,
FLST,2,3,4
FITEM,2,79
FITEM,2,625
FITEM,2,647

AL,P51X
FLST,2,3,4
FITEM,2,243
FITEM,2,605
FITEM,2,1165
AL,P51X
FLST,2,3,4
FITEM,2,269
FITEM,2,1167
FITEM,2,220
AL,P51X
FLST,2,3,4
FITEM,2,1181
FITEM,2,221
FITEM,2,634
AL,P51X
FLST,3,2,5,ORDE,2
FITEM,3,284
FITEM,3,568
ASBA, 85,P51X
FLST,3,2,5,ORDE,2
FITEM,3,557
FITEM,3,567
ASBA, 88,P51X
ADELE, 258,,1
LSTR, 62, 640
FLST,2,4,4
FITEM,2,1147
FITEM,2,242
FITEM,2,1187
FITEM,2,68
AL,P51X
FLST,2,4,4
FITEM,2,120
FITEM,2,68
FITEM,2,72
FITEM,2,1190
AL,P51X ! Second Bolster

AFILLT,283,260,38,
AFILLT,277,279,38,
AFILLT,265,267,38,
AFILLT,110,112,38,
AFILLT,89,91,38,
AFILLT,572,84,38,
AFILLT,571,108,38,
AFILLT,570,263,38,
AFILLT,568,272,38,
AFILLT,567,281,38,
FLST,2,3,4
FITEM,2,1189
FITEM,2,595
FITEM,2,237
AL,P51X
FLST,2,3,4
FITEM,2,592
FITEM,2,1207
FITEM,2,214
AL,P51X
FLST,2,3,4
FITEM,2,1162
FITEM,2,589
FITEM,2,75
AL,P51X
FLST,2,3,4
FITEM,2,602
FITEM,2,1209

```

FITEM,2,215
 AL,P51X
 FLST,3,2,5,ORDE,2
 FITEM,3,578
 FITEM,3,-579
 ASBA, 44,P51X
 FLST,3,2,5,ORDE,2
 FITEM,3,281
 FITEM,3,567
 ASBA, 87,P51X
 ADELE, 257,,1
 LSTR, 58, 131
 FLST,2,4,4
 FITEM,2,69
 FITEM,2,1210
 FITEM,2,233
 FITEM,2,625
 AL,P51X
 FLST,2,4,4
 FITEM,2,116
 FITEM,2,1213
 FITEM,2,64
 FITEM,2,69
 AL,P51X

I Third Bolster

AFILLT,81,82,38,
 AFILLT,106,107,38,
 AFILLT,80,83,38,
 AFILLT,581,78,38,
 AFILLT,579,105,38,
 AFILLT,578,79,38,
 ADELE, 256,,1
 LSTR, 50, 66
 FLST,2,4,4
 FITEM,2,58
 FITEM,2,1162
 FITEM,2,211
 FITEM,2,602
 AL,P51X
 FLST,2,4,4
 FITEM,2,58
 FITEM,2,112
 FITEM,2,1222
 FITEM,2,54
 AL,P51X

I Fourth Bolster

AFILLT,75,76,38,
 AFILLT,103,104,38,
 AFILLT,74,77,38,
 AFILLT,588,72,38,
 AFILLT,587,102,38,
 AFILLT,586,73,38,
 ADELE, 255,,1
 LSTR, 42, 59
 FLST,2,4,4
 FITEM,2,49
 FITEM,2,1224
 FITEM,2,197
 FITEM,2,647
 AL,P51X
 FLST,2,4,4
 FITEM,2,108
 FITEM,2,1237
 FITEM,2,45
 FITEM,2,49
 AL,P51X

I Fifth Bolster

LSTR, 616, 229
 LSTR, 617, 247
 LSTR, 619, 154

LSTR, 621, 153
 FLST,2,5,4
 FITEM,2,530
 FITEM,2,766
 FITEM,2,791
 FITEM,2,1145
 FITEM,2,187
 AL,P51X
 FLST,2,5,4
 FITEM,2,395
 FITEM,2,724
 FITEM,2,781
 FITEM,2,1139
 FITEM,2,186
 AL,P51X
 FLST,2,4,4
 FITEM,2,244
 FITEM,2,190
 FITEM,2,531
 FITEM,2,186
 AL,P51X
 FLST,2,4,4
 FITEM,2,187
 FITEM,2,638
 FITEM,2,188
 FITEM,2,88
 AL,P51X

I STR Nose Areas

KWPLAN,-1, 148, 70, 617
 KWPAVE, 612
 ASBW, 14
 KWPAVE, 627
 ASBW, 595
 KWPAVE, 630
 ASBW, 14
 KWPAVE, 633
 ASBW, 595
 KWPAVE, 149
 ASBW, 14
 KWPAVE, 639
 ASBW, 595
 KWPAVE, 642
 ASBW, 14
 KWPAVE, 643
 ASBW, 595
 KWPAVE, 71
 ASBW, 14
 KWPAVE, 651
 ASBW, 595
 KWPAVE, 320
 ASBW, 14
 KWPAVE, 327
 ASBW, 595
 KWPAVE, 63
 ASBW, 14
 KWPAVE, 659
 ASBW, 595
 KWPAVE, 126
 ASBW, 14
 KWPAVE, 661
 ASBW, 595
 KWPAVE, 57
 ASBW, 14
 KWPAVE, 667
 ASBW, 595

I Using Cplane to Divide STR Bottom Area

FLST,2,4,3
 FITEM,2,153
 FITEM,2,621

FITEM,2,624			FITEM,2,77		
FITEM,2,36			FITEM,2,1262		
A,P51X			FITEM,2,1294		
FLST,2,4,3			FITEM,2,1246		
FITEM,2,154			AL,P51X		
FITEM,2,619			FLST,2,4,4		
FITEM,2,612			FITEM,2,1243		
FITEM,2,37			FITEM,2,1178		
A,P51X			FITEM,2,1292		
LSTR, 626,	40		FITEM,2,1290		
LSTR, 627,	41		AL,P51X		
FLST,2,4,4			FLST,2,4,4		
FITEM,2,89			FITEM,2,239		
FITEM,2,192			FITEM,2,1289		
FITEM,2,229			FITEM,2,1240		
FITEM,2,1283			FITEM,2,1290		
AL,P51X			AL,P51X		
FLST,2,4,4			FLST,2,4,4		
FITEM,2,200			FITEM,2,1285		
FITEM,2,249			FITEM,2,1289		
FITEM,2,1284			FITEM,2,1235		
FITEM,2,86			FITEM,2,1284		
AL,P51X			AL,P51X		
LSTR, 627,	630		LSTR, 639,	642	
LSTR, 632,	626		LSTR, 644,	638	
FLST,2,4,4			LSTR, 642,	669	
FITEM,2,1159			LSTR, 644,	668	
FITEM,2,65			LSTR, 643,	671	
FITEM,2,626			LSTR, 647,	670	
FITEM,2,1285			LSTR, 71,	673	
AL,P51X			LSTR, 646,	672	
FLST,2,4,4			FLST,2,4,4		
FITEM,2,1153			FITEM,2,1176		
FITEM,2,1286			FITEM,2,78		
FITEM,2,611			FITEM,2,610		
FITEM,2,76			FITEM,2,1296		
AL,P51X			AL,P51X		
LSTR, 632,	44		FLST,2,4,4		
LSTR, 635,	48		FITEM,2,1296		
LSTR, 630,	45		FITEM,2,1293		
LSTR, 633,	49		FITEM,2,1248		
LSTR, 634,	52		FITEM,2,1298		
LSTR, 149,	53		AL,P51X		
LSTR, 115,	638		FLST,2,4,4		
LSTR, 118,	639		FITEM,2,234		
FLST,2,4,4			FITEM,2,1300		
FITEM,2,1286			FITEM,2,1251		
FITEM,2,1263			FITEM,2,1298		
FITEM,2,1234			AL,P51X		
FITEM,2,1267			FLST,2,4,4		
AL,P51X			FITEM,2,82		
FLST,2,4,4			FITEM,2,1191		
FITEM,2,240			FITEM,2,1295		
FITEM,2,1288			FITEM,2,1182		
FITEM,2,1239			AL,P51X		
FITEM,2,1287			FLST,2,4,4		
AL,P51X			FITEM,2,1295		
FLST,2,4,4			FITEM,2,1297		
FITEM,2,1173			FITEM,2,1249		
FITEM,2,1291			FITEM,2,1294		
FITEM,2,1242			AL,P51X		
FITEM,2,1288			FLST,2,4,4		
AL,P51X			FITEM,2,235		
FLST,2,4,4			FITEM,2,1299		
FITEM,2,80			FITEM,2,1252		
FITEM,2,1293			FITEM,2,1297		
FITEM,2,1245			AL,P51X		
FITEM,2,1291			LSTR, 650,	674	
AL,P51X			LSTR, 651,	675	
FLST,2,4,4			LSTR, 650,	69	

LSTR, 651, 320
 LSTR, 320, 677
 LSTR, 69, 676
 LSTR, 327, 679
 LSTR, 678, 655
 FLST,2,4,4
 FITEM,2,1198
 FITEM,2,1300
 FITEM,2,1254
 FITEM,2,1302
 AL,P51X
 FLST,2,4,4
 FITEM,2,1199
 FITEM,2,1299
 FITEM,2,1255
 FITEM,2,1301
 AL,P51X
 FLST,2,4,4
 FITEM,2,1303
 FITEM,2,74
 FITEM,2,1302
 FITEM,2,1257
 AL,P51X
 FLST,2,4,4
 FITEM,2,62
 FITEM,2,1304
 FITEM,2,1258
 FITEM,2,1301
 AL,P51X
 FLST,2,4,4
 FITEM,2,73
 FITEM,2,273
 FITEM,2,1305
 FITEM,2,1201
 AL,P51X
 FLST,2,4,4
 FITEM,2,1305
 FITEM,2,1308
 FITEM,2,1260
 FITEM,2,1303
 AL,P51X
 FLST,2,4,4
 FITEM,2,208
 FITEM,2,1308
 FITEM,2,1263
 FITEM,2,1310
 AL,P51X
 FLST,2,4,4
 FITEM,2,59
 FITEM,2,227
 FITEM,2,1306
 FITEM,2,620
 AL,P51X
 FLST,2,4,4
 FITEM,2,1304
 FITEM,2,1306
 FITEM,2,1307
 FITEM,2,1261
 AL,P51X
 FLST,2,4,4
 FITEM,2,60
 FITEM,2,1309
 FITEM,2,1264
 FITEM,2,1307
 AL,P51X
 LSTR, 63, 681
 LSTR, 654, 680
 LSTR, 659, 683
 LSTR, 658, 682
 LSTR, 659, 126

LSTR, 658, 61
 LSTR, 125, 685
 LSTR, 684, 61
 LSTR, 687, 661
 LSTR, 686, 663
 LSTR, 57, 689
 LSTR, 682, 688
 LSTR, 690, 666
 LSTR, 691, 667
 FLST,2,4,4
 FITEM,2,1310
 FITEM,2,1266
 FITEM,2,1312
 FITEM,2,1211
 AL,P51X
 FLST,2,4,4
 FITEM,2,61
 FITEM,2,1314
 FITEM,2,1269
 FITEM,2,1312
 AL,P51X
 FLST,2,4,4
 FITEM,2,71
 FITEM,2,247
 FITEM,2,1316
 AL,P51X
 FLST,2,4,4
 FITEM,2,1316
 FITEM,2,1318
 FITEM,2,1314
 FITEM,2,1272
 AL,P51X
 FLST,2,4,4
 FITEM,2,194
 FITEM,2,1320
 FITEM,2,1275
 FITEM,2,1318
 AL,P51X
 FLST,2,4,4
 FITEM,2,1228
 FITEM,2,1322
 FITEM,2,1278
 FITEM,2,1320
 AL,P51X
 FLST,2,4,4
 FITEM,2,51
 FITEM,2,1323
 FITEM,2,1281
 FITEM,2,1322
 AL,P51X
 FLST,2,4,4
 FITEM,2,1309
 FITEM,2,1267
 FITEM,2,1311
 FITEM,2,1214
 AL,P51X
 FLST,2,4,4
 FITEM,2,52
 FITEM,2,1313
 FITEM,2,1270
 FITEM,2,1311
 AL,P51X
 FLST,2,4,4
 FITEM,2,55
 FITEM,2,1219
 FITEM,2,1315
 FITEM,2,210
 AL,P51X
 FLST,2,4,4

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FITEM,2,1315
FITEM,2,1317
FITEM,2,1273
FITEM,2,1313
AL,P51X
FLST,2,4,4
FITEM,2,1276
FITEM,2,1319
FITEM,2,50
FITEM,2,1317
AL,P51X
FLST,2,4,4
FITEM,2,1229
FITEM,2,1321
FITEM,2,1279
FITEM,2,1319
AL,P51X
FLST,2,4,4
FITEM,2,43
FITEM,2,1324
FITEM,2,1282
FITEM,2,1321
AL,P51X
FLST,2,5,4
FITEM,2,44
FITEM,2,181
FITEM,2,67
FITEM,2,1231
FITEM,2,1323
AL,P51X
FLST,2,5,4
FITEM,2,53
FITEM,2,21
FITEM,2,46
FITEM,2,196
FITEM,2,1324
AL,P51X      ! Create new STR Side Areas

FLST,2,2,4
FITEM,2,645
FITEM,2,644
AL,P51X
FLST,2,1,5,ORDE,1
FITEM,2,659
VEXT,P51X,,,-500,0,0,,,
FLST,2,2,5,ORDE,2
FITEM,2,627
FITEM,2,630
ASBV,P51X,! Punching hoist pivot holes through STR

!-----
!----- View Commands
!-----

APLOT
/FOC, 1, 728.863089244 , 454.608961372 , -
2964.04580614
/LIG, 1,1,1,000, 0.501901609919 , 0.563136024018
, 0.856485028324 , 0.000000000000E+00
/REPLO
/FOC, 1, 546.253384735 , 414.680522353 , -
2109.53178436
/LIG, 1,1,1,000, 0.501901609919 , 0.563136024018
, 0.856485028324 , 0.000000000000E+00
/REPLO
/VIEW, 1, 0.979085862791 , -0.172403948742 ,
0.108017367776
/ANG, 1, 1, 177.967602415
/LIG, 1,1,1,000, 0.418274067285 , 0.865517664516
, 0.618169105386 , 0.000000000000E+00

/REPLO
/ZOOM,1,RECT,-0.054853,0.502041,1.365910,-
0.134894

!-----
!----- Rear Bolsters
!-----

FLST,2,8,5,ORDE,5
FITEM,2,1
FITEM,2,46
FITEM,2,-50
FITEM,2,52
FITEM,2,65
ADELE,P51X,,1

AFILLT,7,5,38,
AFILLT,70,68,38,
AFILLT,69,67,38,
AFILLT,2,52,38,
AFILLT,66,48,38,
AFILLT,51,47,38,
AFILLT,56,3,38,
AFILLT,57,60,38,
AFILLT,58,59,38,

KWPAVE, 709
ASBW, 54
KWPAVE, 714
ASBW, 58
WPSTYLE,,,,,,0

LDELE,151,,1
LDELE,152,,1
LDELE,153,,1

LSTR, 82, 707
LSTR, 8, 709
LSTR, 96, 705
LSTR, 12, 706
LSTR, 16, 714
LSTR, 700, 77
LSTR, 85, 713
LSTR, 99, 711
LSTR, 711, 698
LSTR, 700, 716
LSTR, 716, 79
LSTR, 79, 718
LSTR, 698, 92
LSTR, 92, 720

FLST,2,5,4
FITEM,2,143
FITEM,2,144
FITEM,2,145
FITEM,2,1328
FITEM,2,151
AL,P51X
FITEM,2,1338
FITEM,2,8
FITEM,2,132
FITEM,2,131
FITEM,2,130
AL,P51X
FLST,2,4,4
FITEM,2,142
FITEM,2,152
FITEM,2,15
FITEM,2,151

```


AL,P51X
 FLST,2,4,4
 FITEM,2,22
 FITEM,2,13
 FITEM,2,136
 FITEM,2,8
 AL,P51X
 FLST,2,4,4
 FITEM,2,1349
 FITEM,2,164
 FITEM,2,147
 FITEM,2,152
 AL,P51X
 FLST,2,4,4
 FITEM,2,1
 FITEM,2,169
 FITEM,2,150
 FITEM,2,164
 AL,P51X
 FLST,2,4,4
 FITEM,2,1351
 FITEM,2,153
 FITEM,2,137
 FITEM,2,13
 AL,P51X
 FLST,2,4,4
 FITEM,2,14
 FITEM,2,160
 FITEM,2,149
 FITEM,2,153
 AL,P51X
 FLST,2,6,4
 FITEM,2,169
 FITEM,2,177
 FITEM,2,154
 FITEM,2,1367
 FITEM,2,1360
 FITEM,2,155
 AL,P51X
 FLST,2,6,4
 FITEM,2,126
 FITEM,2,1363
 FITEM,2,1355
 FITEM,2,2
 FITEM,2,170
 FITEM,2,160
 AL,P51X
 FLST,2,3,4
 FITEM,2,129
 FITEM,2,1368
 FITEM,2,1367
 AL,P51X
 FLST,2,3,4
 FITEM,2,12
 FITEM,2,1366
 FITEM,2,1363
 AL,P51X
 FLST,2,4,4
 FITEM,2,1366
 FITEM,2,1368
 FITEM,2,156
 FITEM,2,1361
 AL,P51X
 FLST,2,5,4
 FITEM,2,129
 FITEM,2,138
 FITEM,2,140
 FITEM,2,141
 FITEM,2,1360
 AL,P51X

FLST,2,5,4
 FITEM,2,12
 FITEM,2,10
 FITEM,2,127
 FITEM,2,128
 FITEM,2,1355
 AL,P51X

FLST,2,2,5,ORDE,2
 FITEM,2,251
 FITEM,2,-252
 ADELE,P51X,,1
 LSTR, 18, 701
 FLST,2,4,4
 FITEM,2,16
 FITEM,2,1353
 FITEM,2,133
 FITEM,2,1337
 AL,P51X
 FLST,2,4,4
 FITEM,2,16
 FITEM,2,18
 FITEM,2,1342
 FITEM,2,96
 AL,P51X
 LSTR, 10, 6
 FLST,2,4,4
 FITEM,2,1354
 FITEM,2,23
 FITEM,2,4
 FITEM,2,20
 AL,P51X
 FLST,2,3,4
 FITEM,2,91
 FITEM,2,7
 FITEM,2,20
 AL,P51X

|-----
----- View Commands

/FOC, 1, 616.287701829 , 133.456951868 , -
 3193.18773912
 /LIG, 1,1,1,000, 0.418274067285 , 0.665517664516
 , 0.618169105386 , 0.000000000000E+00
 /REPLO
 /FOC, 1, 640.064788830 , 123.004270488 , -
 3425.39015066
 /LIG, 1,1,1,000, 0.418274067285 , 0.665517664516
 , 0.618169105386 , 0.000000000000E+00
 /REPLO

|-----
----- Bolsters Near Pivot Structure

FLST,2,3,5,ORDE,3
 FITEM,2,138
 FITEM,2,548
 FITEM,2,-549
 ADELE,P51X,,1
 FLST,2,10,5,ORDE,10
 FITEM,2,8
 FITEM,2,-9
 FITEM,2,12
 FITEM,2,-13
 FITEM,2,18
 FITEM,2,127

FITEM,2,130			FITEM,2,277
FITEM,2,545			FITEM,2,166
FITEM,2,-546			FITEM,2,286
ADELE,P51X,,1			FITEM,2,359
FLST,2,2,5,ORDE,2			AL,P51X
FITEM,2,27			FLST,2,6,4
FITEM,2,117			FITEM,2,313
ADELE,P51X,,1			FITEM,2,32
ADELE, 131,,1			FITEM,2,1375
FLST,2,6,5,ORDE,2			FITEM,2,184
FITEM,2,132			FITEM,2,308
FITEM,2,-137			FITEM,2,31
ADELE,P51X,,1			AL,P51X
FLST,2,2,5,ORDE,2			FLST,2,4,4
FITEM,2,253			FITEM,2,288
FITEM,2,-254			FITEM,2,1378
ADELE,P51X,,1	! Deleting Pivot Areas		FITEM,2,38
			FITEM,2,1372
AFILLT,23,20,38,			AL,P51X
AFILLT,119,19,38,			FLST,2,10,4
AFILLT,120,121,38,			FITEM,2,1333
AFILLT,122,19,38,			FITEM,2,365
AFILLT,10,13,38,			FITEM,2,139
AFILLT,22,8,38,			FITEM,2,32
AFILLT,71,26,38,			FITEM,2,1375
AFILLT,24,21,38,			FITEM,2,184
AFILLT,124,123,38,			FITEM,2,308
AFILLT,125,131,38,			FITEM,2,351
AFILLT,25,130,38,			FITEM,2,288
AFILLT,28,8,38,	! Creating 38mm Fillets		FITEM,2,359
			AL,P51X
LSTR, 34, 101			
LSTR, 26, 207			FLST,2,6,4
FLST,2,4,4			FITEM,2,1373
FITEM,2,39			FITEM,2,280
FITEM,2,1395			FITEM,2,1390
FITEM,2,283			FITEM,2,41
FITEM,2,321			FITEM,2,315
AL,P51X			FITEM,2,33
FLST,2,4,4			AL,P51X
FITEM,2,104			FLST,2,3,4
FITEM,2,1381			FITEM,2,292
FITEM,2,30			FITEM,2,279
FITEM,2,39			FITEM,2,1382
AL,P51X			AL,P51X
FLST,2,4,4			ADELE, 134,,1
FITEM,2,284			LSTR, 739, 162
FITEM,2,24			FLST,2,4,4
FITEM,2,364			FITEM,2,1395
FITEM,2,100			FITEM,2,346
AL,P51X			FITEM,2,297
FLST,2,4,4			FITEM,2,1394
FITEM,2,1379			AL,P51X
FITEM,2,284			FLST,2,10,4
FITEM,2,348			FITEM,2,1390
FITEM,2,276			FITEM,2,280
AL,P51X	! Replacing Bolster End Caps		FITEM,2,312
			FITEM,2,1391
LSTR, 100, 89			FITEM,2,278
LSTR, 89, 104			FITEM,2,297
LSTR, 203, 104			FITEM,2,292
LSTR, 203, 204			FITEM,2,285
LSTR, 204, 162			FITEM,2,315
LSTR, 162, 184			FITEM,2,41
FLST,2,9,4			AL,P51X
FITEM,2,139			FLST,2,9,4
FITEM,2,365			FITEM,2,1373
FITEM,2,1333			FITEM,2,312
FITEM,2,313			FITEM,2,1391
FITEM,2,35			FITEM,2,278

FITEM,2,297		
FITEM,2,296		
FITEM,2,344		
FITEM,2,275		
FITEM,2,34		
AL,P51X		
FLST,2,4,4		
FITEM,2,285		
FITEM,2,291		
FITEM,2,1132		
FITEM,2,1133		
AL,P51X		
FLST,2,4,4		
FITEM,2,290		
FITEM,2,351		
FITEM,2,829		
FITEM,2,1132		
AL,P51X		
FLST,2,9,4		
FITEM,2,359		
FITEM,2,286		
FITEM,2,166		
FITEM,2,139		
FITEM,2,1333		
FITEM,2,365		
FITEM,2,313		
FITEM,2,35		
FITEM,2,277		
AL,P51X		
LSTR, 111,	100	
LSTR, 206,	24	
FLST,2,15,4		
FITEM,2,296		
FITEM,2,291		
FITEM,2,1382		
FITEM,2,279		
FITEM,2,290		
FITEM,2,1372		
FITEM,2,38		
FITEM,2,1378		
FITEM,2,286		
FITEM,2,302		
FITEM,2,335		
FITEM,2,337		
FITEM,2,338		
FITEM,2,334		
FITEM,2,25		
AL,P51X		
FLST,3,1,4,ORDE,1		
FITEM,3,292		
LGEN,2,P51X,--,363,...,1		
LSTR, 209,	9	
LSTR, 13,	201	
LSTR, 9,	204	
LSTR, 13,	162	
FLST,2,4,4		
FITEM,2,360		
FITEM,2,352		
FITEM,2,1386		
FITEM,2,291		
AL,P51X		
FLST,2,4,4		
FITEM,2,349		
FITEM,2,1392		
FITEM,2,292		
FITEM,2,1386		
AL,P51X		
FLST,2,4,4		
FITEM,2,358		
FITEM,2,1392		
FITEM,2,296		
FITEM,2,366		
AL,P51X		
LSTR, 209,	206	
FLST,2,6,4		
FITEM,2,1393		
FITEM,2,354		
FITEM,2,286		
FITEM,2,288		
FITEM,2,290		
FITEM,2,360		
AL,P51X		
FLST,2,6,4		
FITEM,2,289		
FITEM,2,1335		
FITEM,2,176		
FITEM,2,1357		
FITEM,2,26		
FITEM,2,361		
AL,P51X		
FLST,2,6,4		
FITEM,2,294		
FITEM,2,1384		
FITEM,2,42		
FITEM,2,1388		
FITEM,2,36		
FITEM,2,347		
AL,P51X		
FLST,2,11,4		
FITEM,2,311		
FITEM,2,361		
FITEM,2,26		
FITEM,2,1357		
FITEM,2,176		
FITEM,2,1335		
FITEM,2,830		
FITEM,2,1135		
FITEM,2,1393		
FITEM,2,299		
FITEM,2,29		
AL,P51X		
FLST,2,13,4		
FITEM,2,1134		
FITEM,2,352		
FITEM,2,36		
FITEM,2,1388		
FITEM,2,42		
FITEM,2,1384		
FITEM,2,310		
FITEM,2,27		
FITEM,2,333		
FITEM,2,349		
FITEM,2,358		
FITEM,2,347		
FITEM,2,1135		
AL,P51X		
FLST,2,10,4		
FITEM,2,303		
FITEM,2,327		
FITEM,2,331		
FITEM,2,336		
FITEM,2,326		
FITEM,2,28		
FITEM,2,349		
FITEM,2,358		
FITEM,2,352		
FITEM,2,1393		
AL,P51X		

```

LSTR, 111, 109
LSTR, 24, 20
FLST,2,3,4
FITEM,2,1396
FITEM,2,196
FITEM,2,302
AL,P51X
FLST,2,3,4
FITEM,2,303
FITEM,2,1397
FITEM,2,299
AL,P51X
FLST,2,2,5,ORDE,2
FITEM,2,681
FITEM,2,691
AADD,P51X
FLST,2,2,5,ORDE,2
FITEM,2,690
FITEM,2,692
AADD,P51X

```

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|-----|
|-----|
|-----|

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/IFINISH
/ISAVE
/EOF

```

❖ Filename: 2_7_SCL_mods_INPUT

```

!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
!       FEA of 930E Truck Box Structure
!       Routine to Incorporate Syncrude
!       Modifications to Geometry
!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!!
FINISH
/TITLE Incorporating Syncrude's Modifications
/REP7
*AFUN,DEG

```

```

-----
|-----Wear Package on Side Wall
|-----

```

KWPLAN,-1, 218, 30, 236

```

FLST,2,4,5,ORDE,4
FITEM,2,293
FITEM,2,313
FITEM,2,316
FITEM,2,321
ASBW,P51X ! Used WPlane to divide Side Areas
! Wear Package only cover back 1/3rd of Sidewall

```

```

-----
|-----View Commands
|-----
APLOT
(AUTO, 1
/REP
/USER, 1
/VIEW, 1, 0.153749767104, -0.580357600040,
0.799716240420
/ANG, 1, -172.364133592
/LIG, 1,1,1.000,-0.282687364737, 0.461125582318
, 0.841101094489, 0.000000000000E+00
/REPLO
/ZOOM,1,RECT,0.394496,0.585044,0.838009,0.06774
2

```

```

-----
| Flat Plate Between Forward Two Bolsters
| between STR's
|-----

```

```

LSTR, 351, 625
FLST,2,4,4
FITEM,2,668
FITEM,2,663
FITEM,2,1286
FITEM,2,1156
AL,P51X

```

```

-----
|-----Exhaust Plenum
|-----

```

```

KWPLAN,-1, 43, 47, 657
wpoff,0,0,-430
WPSTYLE,,,,,0
FLST,2,17,5,ORDE,17
FITEM,2,74
FITEM,2,80
FITEM,2,83
FITEM,2,89
FITEM,2,91
FITEM,2,103

```

```

FITEM,2,-104
FITEM,2,106
FITEM,2,-107
FITEM,2,110
FITEM,2,112
FITEM,2,159
FITEM,2,161
FITEM,2,-162
FITEM,2,562
FITEM,2,573
FITEM,2,582
ASBW,P51X
ASBW,95

```

! Dividing Bolster Areas

```

FLST,3,2,3,ORDE,2
FITEM,3,752
FITEM,3,-753
KGEN,2,P51X,,,25,,0
LSTR, 755, 754
LSTR, 752, 754
LSTR, 753, 755

```

```

FLST,2,21,4
FITEM,2,199
FITEM,2,236
FITEM,2,1451
FITEM,2,1423
FITEM,2,1449
FITEM,2,1444
FITEM,2,1453
FITEM,2,1412
FITEM,2,1441
FITEM,2,1418
FITEM,2,1448
FITEM,2,1438
FITEM,2,1454
FITEM,2,703
FITEM,2,1435
FITEM,2,1415
FITEM,2,1447
FITEM,2,1432
FITEM,2,1456
FITEM,2,228
FITEM,2,213
AL,P51X

```

! Plenum Side Area

```

LGEN,2,213,,,150,-150,,0
LGEN,2,260,,,280,,,0
LSTR, 754, 757
LSTR, 757, 759
LSTR, 759, 123
LSTR, 758, 756
LSTR, 756, 755
LSTR, 758, 353

```

```

FLST,2,4,4
FITEM,2,213
FITEM,2,260
FITEM,2,1195
FITEM,2,629
AL,P51X
FLST,2,5,4
FITEM,2,228
FITEM,2,629
FITEM,2,1169
FITEM,2,1179
FITEM,2,1455
AL,P51X

```

! Slanted Side Area

! End Area

FLST,2,4,4
FITEM,2,260
FITEM,2,1169
FITEM,2,1189
FITEM,2,592
AL,P51X

! Top Area

KWPLAN,-1, 753, 353, 756

wprot,0,45,0
FLST,2,2,5,ORDE,2
FITEM,2,89
FITEM,2,95
ASBW,P51X
FLST,2,2,5,ORDE,2
FITEM,2,106
FITEM,2,-107
ADELE,P51X,,1
ASBW, 83
ADELE, 89,,1
LSTR, 353, 762
WPSTYLE,,,,,0
FLST,2,5,4
FITEM,2,213
FITEM,2,1217
FITEM,2,1230
FITEM,2,236
FITEM,2,191
AL,P51X
LDELE, 1200,,1

! Created Front Slope

----- Guide Pin Stiffened Region

KWPLAN,-1, 56, 73, 351

wpoff,0,0,-170
FLST,2,2,5,ORDE,2
FITEM,2,165
FITEM,2,293
ASBW,P51X
FLST,2,2,5,ORDE,2
FITEM,2,109
FITEM,2,553
ASBW,P51X
FLST,2,4,4
FITEM,2,1189
FITEM,2,250
FITEM,2,1460
FITEM,2,219
AL,P51X

----- Exhaust Holes Under Plenum

WPSTYLE,,,,,0

KWPLAN,-1, 51, 742, 649

wpoff,150,150,0
PCIRC,100,0,360,
ADELE, 165
FLST,3,2,4,ORDE,2
FITEM,3,603
FITEM,3,1464
LGEN,2,P51X,,75,,0
FLST,2,2,4,ORDE,2
FITEM,2,603
FITEM,2,1464
LDELE,P51X,,1
LSTR, 769, 765

LSTR, 770, 767

FLST,2,6,4
FITEM,2,1466
FITEM,2,1464
FITEM,2,1463
FITEM,2,1156
FITEM,2,603
FITEM,2,1465
AL,P51X
FLST,2,1,5,ORDE,1
FITEM,2,165
VEXT,P51X,,0,0,-1000,...

! Volume used to punch holes

FLST,2,2,5,ORDE,2

FITEM,2,718
FITEM,2,720
ASBV,P51X, 1

! Punching Holes

KWPLAN,-1, 56, 133, 351

wpoff,150,150,0
wpoff,300
PCIRC,100,0,360,
ADELE, 165
FLST,3,2,4,ORDE,2
FITEM,3,1156
FITEM,3,1463
LGEN,2,P51X,,75,,0
FLST,2,2,4,ORDE,2
FITEM,2,1156
FITEM,2,1463
LDELE,P51X,,1
LSTR, 767, 770
LSTR, 769, 765

FLST,2,6,4

FITEM,2,1156

FITEM,2,1466

FITEM,2,1465

FITEM,2,1463

FITEM,2,603

FITEM,2,1464

AL,P51X

ASBA, 112, 165

! Hole under Flat Plate

----- View Commands

APLOT

/AUTO,1

/REP

/USER,1

/VIEW,1,-0.183489902166,-0.610128668722,

0.770762261276

/ANG,1,165.565256178

/LJ,1,1.1,0.00,-0.845654851235,0.254431698830

,0.469182675739,0.000000000000E+00

/REPLO

/ZOOM,1,RECT,0.147238,-0.404082,0.416693,-

0.061224

----- Completely Replaced Rear STR
----- 1 1/8 inch plate straight back

FLST,2,21,5,ORDE,13

FITEM,2,53

FITEM,2,-55

FITEM,2,58

FITEM,2,-59		FITEM,2,50	
FITEM,2,126		FITEM,2,54	
FITEM,2,139		FITEM,2,-55	
FITEM,2,-140		FITEM,2,60	
FITEM,2,660		FITEM,2,67	
FITEM,2,-662		ASBW,P51X	
FITEM,2,665		ASBW, 48	
FITEM,2,-671		KWPAVE, 158	
FITEM,2,674		FLST,2,12,5,ORDE,10	
FITEM,2,-676		FITEM,2,2	
ADELE,P51X,,1		FITEM,2,46	
FLST,2,2,5,ORDE,2		FITEM,2,51	
FITEM,2,672		FITEM,2,66	
FITEM,2,-673		FITEM,2,139	
ADELE,P51X,,1	! Deleting Old STR Areas	FITEM,2,-140	
		FITEM,2,146	
LSTR, 158, 167		FITEM,2,-149	
ASBL,149,8,,KEEP		FITEM,2,154	
FLST,2,3,5,ORDE,3		FITEM,2,165	
FITEM,2,54		ASBW,P51X	! Cutting Areas for New Width
FITEM,2,148			
FITEM,2,203		FLST,2,3,5,ORDE,3	
AADD,P51X		FITEM,2,7	
FLST,2,3,5,ORDE,3		FITEM,2,54	
FITEM,2,1		FITEM,2,57	
FITEM,2,5		ADELE,P51X,,1	
FITEM,2,49		FLST,2,3,4,ORDE,3	
AADD,P51X		FITEM,2,131	
FLST,2,3,5,ORDE,2		FITEM,2,1344	
FITEM,2,68		FITEM,2,1346	
FITEM,2,-70		LCOMB,P51X,,0	
AADD,P51X		FLST,2,3,4,ORDE,3	
FLST,2,3,5,ORDE,3		FITEM,2,130	
FITEM,2,2		FITEM,2,1334	
FITEM,2,48		FITEM,2,1338	
FITEM,2,65		LCOMB,P51X,,0	
AADD,P51X		FLST,2,4,4	
FLST,2,3,5,ORDE,3		FITEM,2,131	
FITEM,2,146		FITEM,2,1347	
FITEM,2,-147		FITEM,2,130	
FITEM,2,154		FITEM,2,132	
AADD,P51X		AL,P51X	
FLST,2,3,5,ORDE,3		FLST,2,3,5,ORDE,3	
FITEM,2,3		FITEM,2,4	
FITEM,2,47		FITEM,2,29	
FITEM,2,57		FITEM,2,52	
AADD,P51X		ADELE,P51X,,1	
FLST,2,3,5,ORDE,3		FLST,2,3,5,ORDE,3	
FITEM,2,627		FITEM,2,55	
FITEM,2,630		FITEM,2,-56	
FITEM,2,659		FITEM,2,64	
AADD,P51X		ADELE,P51X,,1	
FLST,2,3,5,ORDE,3		FLST,2,2,4,ORDE,2	
FITEM,2,29		FITEM,2,1359	
FITEM,2,63		FITEM,2,1362	
FITEM,2,-64		LDELE,P51X,,1	
AADD,P51X		FLST,2,3,4,ORDE,3	
FLST,2,3,5,ORDE,3		FITEM,2,10	
FITEM,2,4		FITEM,2,178	
FITEM,2,62		FITEM,2,1348	
FITEM,2,199		LCOMB,P51X,,0	
AADD,P51X	! Adding Areas (Cleanup)	FLST,2,3,4,ORDE,3	
		FITEM,2,2	
KWPLAN,-1, 167, 175, 723		FITEM,2,171	
FLST,2,11,5,ORDE,10		FITEM,2,177	
FITEM,2,1		LCOMB,P51X,,0	
FITEM,2,-3		FLST,2,3,4,ORDE,3	
FITEM,2,5		FITEM,2,144	
FITEM,2,29		FITEM,2,1340	
FITEM,2,47		FITEM,2,1349	

LCOB,P51X, 0
 FLST,2,3,4,ORDE,3
 FITEM,2,145
 FITEM,2,1351
 FITEM,2,1361
 LCOB,P51X, 0
 FLST,2,4,4
 FITEM,2,13
 FITEM,2,10
 FITEM,2,367
 FITEM,2,2
 AL,P51X
 FLST,2,4,4
 FITEM,2,144
 FITEM,2,145
 FITEM,2,147
 FITEM,2,1325
 AL,P51X

! Repairing Corner Areas

LSTR, 20, 92
 LSTR, 766, 109
 FLST,2,11,4
 FITEM,2,9
 FITEM,2,277
 FITEM,2,1467
 FITEM,2,1365
 FITEM,2,1347
 FITEM,2,1328
 FITEM,2,367
 FITEM,2,1367
 FITEM,2,1358
 FITEM,2,1366
 FITEM,2,1325
 AL,P51X
 FLST,2,11,4
 FITEM,2,1
 FITEM,2,147
 FITEM,2,6
 FITEM,2,141
 FITEM,2,150
 FITEM,2,13
 FITEM,2,153
 FITEM,2,132
 FITEM,2,152
 FITEM,2,155
 FITEM,2,29
 AL,P51X
 FLST,2,4,4
 FITEM,2,353
 FITEM,2,1
 FITEM,2,145
 FITEM,2,9
 AL,P51X
 FLST,2,5,4

! Creating New STR Areas

FITEM,2,163
 FITEM,2,1366
 FITEM,2,1325
 FITEM,2,170
 FITEM,2,1368
 AL,P51X
 FLST,2,5,4
 FITEM,2,6
 FITEM,2,147
 FITEM,2,154
 FITEM,2,128
 FITEM,2,138
 AL,P51X ! Stiffeners inside Rear Angle Bolster

FLST,2,3,4,ORDE,3

FITEM,2,157
 FITEM,2,162
 FITEM,2,1470
 LCOB,P51X, 0
 FLST,2,3,4,ORDE,3
 FITEM,2,158
 FITEM,2,165
 FITEM,2,1472
 LCOB,P51X, 0
 FLST,2,3,4,ORDE,3
 FITEM,2,156
 FITEM,2,168
 FITEM,2,1471
 LCOB,P51X, 0 ! Cleanup

KWPLAN,-1, 84, 11, 8
 FLST,2,3,5,ORDE,3
 FITEM,2,29
 FITEM,2,46
 FITEM,2,51
 ASBW,P51X
 KWPAVE, 12
 FLST,2,3,5,ORDE,3
 FITEM,2,56
 FITEM,2,66
 FITEM,2,139
 ASBW,P51X
 KWPAVE, 82
 FLST,2,3,5,ORDE,3
 FITEM,2,140
 FITEM,2,146
 FITEM,2,-147
 ASBW,P51X
 KWPAVE, 79
 FLST,2,3,5,ORDE,3
 FITEM,2,148
 FITEM,2,-149
 FITEM,2,154
 ASBW,P51X ! Using CPlane to Divide STR Areas

FLST,2,3,4,ORDE,3
 FITEM,2,159
 FITEM,2,179
 FITEM,2,1468
 LCOB,P51X, 0

 !----- Areas for 1" Fishplating

KL,155,0,3, ,
 KWPAVE, 81
 FLST,2,2,5,ORDE,2
 FITEM,2,667
 FITEM,2,-668
 ASBW,P51X ! Divided Rear STR Areas

KL,71,5, ,
 KWPAVE, 709
 FLST,2,4,5,ORDE,4
 FITEM,2,645
 FITEM,2,-646
 FITEM,2,652
 FITEM,2,-653
 ASBW,P51X
 WPSTYLE,0

! Divided Areas between 5th and 6th Bolsters

FINISH
 /EOF |-----

❖ *Filename: 3_1_assignprop_floor_INPUT*

```
!@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
!      FEA of 930E Truck Box Structure
!      Thickness and Mat Prop Assignment Routine
!      Floor Structure
!@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
FINISH
FINISH
/TITLE,Assigning Floor Thicknesses and Material
Properties
```

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/PREP7
*AFUN,DEG
```

```
-----
----- Pivot Structure
-----
```

```
CM,_Y,AREA
ASEL,,,33
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT,1,5,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! Gusset Above Cutout - 5mm
```

```
FLST,5,2,5,ORDE,2
FITEM,5,11
FITEM,5,118
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT,1,90,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! Reinforced Section - 90mm total
```

```
FLST,5,8,5,ORDE,7
FITEM,5,137
FITEM,5,549
FITEM,5,679
FITEM,5,-681
FITEM,5,688
FITEM,5,-689
FITEM,5,693
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT,1,63,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! Sides - 1.5" thick+ 1" FishPlating
```

```
FLST,5,8,5,ORDE,8
FITEM,5,138
FITEM,5,253
FITEM,5,-254
FITEM,5,545
FITEM,5,-546
FITEM,5,548
FITEM,5,686
FITEM,5,-687
```

```
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT,1,38,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! Inner Pieces of Side Walls - 1.5"
```

```
FLST,5,2,5,ORDE,2
FITEM,5,141
FITEM,5,-142
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT,1,19,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! Front Narrowing Section - 3/4"
```

```
FLST,5,7,5,ORDE,5
FITEM,5,129
FITEM,5,143
FITEM,5,-144
FITEM,5,682
FITEM,5,-685
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT,1,16,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! Bottom Plates - 5/8"
```

```
-----
----- Rear Stringer Structure
-----
```

```
FLST,5,15,5,ORDE,14
FITEM,5,29
FITEM,5,546
FITEM,5,51
FITEM,5,55
FITEM,5,-57
FITEM,5,64
FITEM,5,66
FITEM,5,139
FITEM,5,-140
FITEM,5,146
FITEM,5,-147
FITEM,5,154
FITEM,5,165
FITEM,5,669
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT,1,29,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! Side Areas 1 1/8"
```

FLST,5,2,5,ORDE,2
 FITEM,5,148
 FITEM,5,-149
 CM,_Y,AREA
 ASEL,,,P51X
 CM,_Y1,AREA
 CMSEL,S,_Y
 CMSEL,S,_Y1
 AATT,1,54,1,0
 CMSEL,S,_Y
 CMDELE,_Y
 CMDELE,_Y1 ! Side Areas - 1 1/8" w/ 1" FishPlate

FLST,5,2,5,ORDE,2
 FITEM,5,52
 FITEM,5,54
 CM,_Y,AREA
 ASEL,,,P51X
 CM,_Y1,AREA
 CMSEL,S,_Y
 CMSEL,S,_Y1
 AATT,1,5,1,0
 CMSEL,S,_Y
 CMDELE,_Y
 CMDELE,_Y1 ! Gusset Plates inside Rear Angle - 5mm

 Front Stringer Structure

FLST,5,19,5,ORDE,3
 FITEM,5,14
 FITEM,5,596
 FITEM,5,-613
 CM,_Y,AREA
 ASEL,,,P51X
 CM,_Y1,AREA
 CMSEL,S,_Y
 CMSEL,S,_Y1
 AATT,1,25,1,0
 CMSEL,S,_Y
 CMDELE,_Y
 CMDELE,_Y1 ! Bottom Plate - 1"

FLST,5,12,5,ORDE,8
 FITEM,5,647
 FITEM,5,-649
 FITEM,5,654
 FITEM,5,-658
 FITEM,5,668
 FITEM,5,671
 FITEM,5,674
 FITEM,5,-675
 CM,_Y,AREA
 ASEL,,,P51X
 CM,_Y1,AREA
 CMSEL,S,_Y
 CMSEL,S,_Y1
 AATT,1,44,1,0
 CMSEL,S,_Y
 CMDELE,_Y
 CMDELE,_Y1 ! 3/4" SidePlate w/ 1" FishPlate

FLST,5,46,5,ORDE,20
 FITEM,5,183
 FITEM,5,363
 FITEM,5,-365
 FITEM,5,586

FITEM,5,592
 FITEM,5,-595
 FITEM,5,614
 FITEM,5,-626
 FITEM,5,628
 FITEM,5,-629
 FITEM,5,631
 FITEM,5,-644
 FITEM,5,650
 FITEM,5,-651
 FITEM,5,663
 FITEM,5,-664
 FITEM,5,667
 FITEM,5,670
 FITEM,5,672
 FITEM,5,-673
 CM,_Y,AREA
 ASEL,,,P51X
 CM,_Y1,AREA
 CMSEL,S,_Y
 CMSEL,S,_Y1
 AATT,1,19,1,0
 CMSEL,S,_Y
 CMDELE,_Y
 CMDELE,_Y1 ! 3/4" SidePlate

 Bolsters and Back Angle Bolster

FLST,5,14,5,ORDE,14
 FITEM,5,1
 FITEM,5,5
 FITEM,5,7
 FITEM,5,48
 FITEM,5,-49
 FITEM,5,65
 FITEM,5,112
 FITEM,5,203
 FITEM,5,562
 FITEM,5,630
 FITEM,5,660
 FITEM,5,666
 FITEM,5,677
 FITEM,5,-678
 CM,_Y,AREA
 ASEL,,,P51X
 CM,_Y1,AREA
 CMSEL,S,_Y
 CMSEL,S,_Y1
 AATT,1,16,1,0
 CMSEL,S,_Y
 CMDELE,_Y
 CMDELE,_Y1 ! Rear Bolster (Angle) - 5/8"

FLST,5,17,5,ORDE,16
 FITEM,5,2
 FITEM,5,4
 FITEM,5,47
 FITEM,5,50
 FITEM,5,58
 FITEM,5,60
 FITEM,5,63
 FITEM,5,68
 FITEM,5,-70
 FITEM,5,199
 FITEM,5,251
 FITEM,5,-252
 FITEM,5,553
 FITEM,5,627

FITEM,5,659		FITEM,5,-591	
FITEM,5,661		FITEM,5,706	
CM_YAREA		FITEM,5,-707	
ASEL,,,P51X		FITEM,5,714	
CM_Y1AREA		FITEM,5,-715	
CMSSEL,S,Y		FITEM,5,728	
CMSSEL,S,Y1		FITEM,5,-729	
AATT,1,9,1,0		CM_YAREA	
CMSSEL,S,Y		ASEL,,,P51X	
CMDELE,Y		CM_Y1AREA	
CMDELE,Y1 ! 2nd Bolster from Back - 9mm		CMSSEL,S,Y	
		CMSSEL,S,Y1	
FLST,5,17,5,ORDE,14		AATT,1,9,1,0	
FITEM,5,9		CMSSEL,S,Y	
FITEM,5,-10		CMDELE,Y	
FITEM,5,12		CMDELE,Y1 ! 5th Bolster (2 Ahead Pivot) - 9mm	
FITEM,5,-13			
FITEM,5,18		FLST,5,22,5,ORDE,20	
FITEM,5,-20		FITEM,5,78	
FITEM,5,23		FITEM,5,-79	
FITEM,5,27		FITEM,5,81	
FITEM,5,117		FITEM,5,-82	
FITEM,5,119		FITEM,5,105	
FITEM,5,-122		FITEM,5,256	
FITEM,5,127		FITEM,5,281	
FITEM,5,135		FITEM,5,313	
FITEM,5,-136		FITEM,5,316	
CM_YAREA		FITEM,5,567	
ASEL,,,P51X		FITEM,5,579	
CM_Y1AREA		FITEM,5,581	
CMSSEL,S,Y		FITEM,5,583	
CMSSEL,S,Y1		FITEM,5,-584	
AATT,1,9,1,0		FITEM,5,708	
CMSSEL,S,Y		FITEM,5,-710	
CMDELE,Y		FITEM,5,716	
CMDELE,Y1 ! 3rd Bolster (Near Pivot) - 9mm		FITEM,5,-717	
		FITEM,5,725	
FLST,5,17,5,ORDE,12		FITEM,5,-727	
FITEM,5,8		CM_YAREA	
FITEM,5,21		ASEL,,,P51X	
FITEM,5,-22		CM_Y1AREA	
FITEM,5,24		CMSSEL,S,Y	
FITEM,5,-26		CMSSEL,S,Y1	
FITEM,5,28		AATT,1,9,1,0	
FITEM,5,71		CMSSEL,S,Y	
FITEM,5,123		CMDELE,Y	
FITEM,5,-125		CMDELE,Y1 ! 6th Bolster - 9mm	
FITEM,5,128			
FITEM,5,130		FLST,5,32,5,ORDE,27	
FITEM,5,-134		FITEM,5,84	
CM_YAREA		FITEM,5,87	
ASEL,,,P51X		FITEM,5,108	
CM_Y1AREA		FITEM,5,257	
CMSSEL,S,Y		FITEM,5,260	
CMSSEL,S,Y1		FITEM,5,263	
AATT,1,9,1,0		FITEM,5,265	
CMSSEL,S,Y		FITEM,5,267	
CMDELE,Y		FITEM,5,272	
CMDELE,Y1 ! 4th Bolster (1 Ahead of Pivot) - 9mm		FITEM,5,277	
		FITEM,5,279	
FLST,5,20,5,ORDE,16		FITEM,5,283	
FITEM,5,72		FITEM,5,-284	
FITEM,5,-73		FITEM,5,321	
FITEM,5,75		FITEM,5,557	
FITEM,5,-77		FITEM,5,568	
FITEM,5,102		FITEM,5,570	
FITEM,5,255		FITEM,5,-572	
FITEM,5,578		FITEM,5,574	
FITEM,5,585		FITEM,5,-577	
FITEM,5,587		FITEM,5,701	

FITEM,5,711
 FITEM,5,-713
 FITEM,5,719
 FITEM,5,722
 FITEM,5,-724
 FITEM,5,732
 CM_YAREA
 ASEL,,,P51X
 CM_Y1,AREA
 CMSEL,S,Y
 CMSEL,S,Y1
 AATT, 1, 9, 1, 0
 CMSEL,S,Y
 CMDELE,_Y
 CMDELE,_Y1 ! 7th Bolster (Near Hoist) - 9mm

FLST,5,30,5,ORDE,26
 FITEM,5,74
 FITEM,5,80
 FITEM,5,86
 FITEM,5,88
 FITEM,5,93
 FITEM,5,111
 FITEM,5,113
 FITEM,5,161
 FITEM,5,258
 FITEM,5,261
 FITEM,5,264
 FITEM,5,266
 FITEM,5,268
 FITEM,5,274
 FITEM,5,278
 FITEM,5,280
 FITEM,5,282
 FITEM,5,293
 FITEM,5,550
 FITEM,5,556
 FITEM,5,558
 FITEM,5,-561
 FITEM,5,563
 FITEM,5,-566
 FITEM,5,721
 FITEM,5,733
 CM_YAREA
 ASEL,,,P51X
 CM_Y1,AREA
 CMSEL,S,Y
 CMSEL,S,Y1
 AATT, 1, 9, 1, 0
 CMSEL,S,Y
 CMDELE,_Y
 CMDELE,_Y1 ! 8th Bolster (Near Hoist) - 9mm

FLST,5,18,5,ORDE,13
 FITEM,5,96
 FITEM,5,-101
 FITEM,5,114
 FITEM,5,-116
 FITEM,5,159
 FITEM,5,162
 FITEM,5,189
 FITEM,5,201
 FITEM,5,259
 FITEM,5,551
 FITEM,5,-552
 FITEM,5,554
 FITEM,5,-555
 CM_YAREA
 ASEL,,,P51X
 CM_Y1,AREA

CMSEL,S,_Y
 CMSEL,S,_Y1
 AATT, 1, 9, 1, 0
 CMSEL,S,_Y
 CMDELE,_Y
 CMDELE,_Y1 ! Last Bolster (Front) - 9mm

|-----
----- Floor Plate

FLST,5,54,5,ORDE,43
 FITEM,5,3
 FITEM,5,34
 FITEM,5,-37
 FITEM,5,39
 FITEM,5,-43
 FITEM,5,45
 FITEM,5,53
 FITEM,5,59
 FITEM,5,62
 FITEM,5,67
 FITEM,5,89
 FITEM,5,106
 FITEM,5,126
 FITEM,5,150
 FITEM,5,-153
 FITEM,5,155
 FITEM,5,-157
 FITEM,5,185
 FITEM,5,191
 FITEM,5,193
 FITEM,5,-194
 FITEM,5,204
 FITEM,5,262
 FITEM,5,269
 FITEM,5,-271
 FITEM,5,273
 FITEM,5,275
 FITEM,5,-276
 FITEM,5,285
 FITEM,5,-286
 FITEM,5,343
 FITEM,5,349
 FITEM,5,-350
 FITEM,5,544
 FITEM,5,547
 FITEM,5,573
 FITEM,5,582
 FITEM,5,662
 FITEM,5,665
 FITEM,5,699
 FITEM,5,-700
 FITEM,5,702
 FITEM,5,-705
 CM_YAREA
 ASEL,,,P51X
 CM_Y1,AREA
 CMSEL,S,_Y
 CMSEL,S,_Y1
 AATT, 1, 29, 1, 0
 CMSEL,S,_Y
 CMDELE,_Y
 CMDELE,_Y1
 ! Floor Plate - 5/8" x 1/2" Wear Pkg. = 28.575mm

FLST,5,4,5,ORDE,4
 FITEM,5,342
 FITEM,5,356
 FITEM,5,-357

FITEM,5,377
 CM_YAREA
 ASEL,,,P51X
 CM_Y1,AREA
 CMSEL,S_Y
 CMSEL,S_Y1
 AATT, 1, 16, 1, 0
 CMSEL,S_Y
 CMDELE,_Y
 CMDELE,_Y1
 ! Front Angle Plate and Floor Plate Under - 5/8"

 |-----
----- Holst Pivot

FLST,5,4,5,ORDE,4
 FITEM,5,44
 FITEM,5,85
 FITEM,5,569
 FITEM,5,580
 CM_YAREA
 ASEL,,,P51X
 CM_Y1,AREA
 CMSEL,S_Y
 CMSEL,S_Y1
 AATT, 1, 9, 1, 0
 CMSEL,S_Y
 CMDELE,_Y
 CMDELE,_Y1 ! Gussets inside Bolsters - 9mm

FLST,5,2,5,ORDE,2
 FITEM,5,287
 FITEM,5,288
 CM_YAREA
 ASEL,,,P51X
 CM_Y1,AREA
 CMSEL,S_Y
 CMSEL,S_Y1
 AATT, 1, 38, 1, 0
 CMSEL,S_Y
 CMDELE,_Y
 CMDELE,_Y1 ! Pivot Side Plates - 1.5"

 |-----
----- Wall Corner Section

FLST,5,17,5,ORDE,3
 FITEM,5,30
 FITEM,5,167
 FITEM,5,182
 CM_YAREA
 ASEL,,,P51X
 CM_Y1,AREA
 CMSEL,S_Y
 CMSEL,S_Y1
 AATT, 1, 5, 1, 0
 CMSEL,S_Y
 CMDELE,_Y
 CMDELE,_Y1 ! Gussets inside Corner Stringer - 5mm

FLST,5,57,5,ORDE,27
 FITEM,5,6
 FITEM,5,16
 FITEM,5,31
 FITEM,5,38
 FITEM,5,92
 FITEM,5,94
 FITEM,5,158

FITEM,5,160
 FITEM,5,163
 FITEM,5,164
 FITEM,5,166
 FITEM,5,184
 FITEM,5,186
 FITEM,5,188
 FITEM,5,190
 FITEM,5,192
 FITEM,5,195
 FITEM,5,-198
 FITEM,5,200
 FITEM,5,202
 FITEM,5,218
 FITEM,5,-238
 FITEM,5,240
 FITEM,5,-250
 FITEM,5,296
 FITEM,5,305
 FITEM,5,-306
 CM_YAREA
 ASEL,,,P51X
 CM_Y1,AREA
 CMSEL,S_Y
 CMSEL,S_Y1
 AATT, 1, 5, 1, 0
 CMSEL,S_Y
 CMDELE,_Y
 CMDELE,_Y1 ! Corner Stringer Outside Plate - 5mm

FLST,5,13,5,ORDE,4
 FITEM,5,207
 FITEM,5,-217
 FITEM,5,376
 FITEM,5,378
 CM_YAREA
 ASEL,,,P51X
 CM_Y1,AREA
 CMSEL,S_Y
 CMSEL,S_Y1
 AATT, 1, 12, 1, 0
 CMSEL,S_Y
 CMDELE,_Y
 CMDELE,_Y1
 ! Corner Plate (Not same as Side Wall) - 12mm

FLST,5,6,5,ORDE,6
 FITEM,5,32
 FITEM,5,61
 FITEM,5,90
 FITEM,5,145
 FITEM,5,205
 FITEM,5,-206
 CM_YAREA
 ASEL,,,P51X
 CM_Y1,AREA
 CMSEL,S_Y
 CMSEL,S_Y1
 AATT, 1, 25, 1, 0
 CMSEL,S_Y
 CMDELE,_Y
 CMDELE,_Y1

! Corner Plate - 12mm + 1/2" Wear Package

 |-----
----- Exhaust Plenum

FLST,5,5,5,ORDE,5
 FITEM,5,83

```

FITEM,5,91
FITEM,5,95
FITEM,5,103
FITEM,5,-104
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 3, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1

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|-----|
|----- Guide Pin Stiffened Region -----|
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```

FLST,5,2,5,ORDE,2
FITEM,5,107
FITEM,5,109
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 16, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! 5/8" Plate

```

```

CM,_Y,AREA
ASEL,,, 110
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 9, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! 9mm Plate Between
Bolsters

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FINISH
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❖ *Filename: 3_2_assignprop_wall_INPUT*

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!@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
!      FEA of 930E Truck Box Structure
!      Thickness and Mat Prop Assignment Routine
!      Side Structure
!@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@

```

FINISH
FINISH

/TITLE,Assigning Wall Thicknesses and Material
Properties

/PREP7
*AFUN,DEG

```

|-----|
|-----| Wall Structure
|-----|

```

FLST,5,6,5,ORDE,6

FITEM,5,289
FITEM,5,317
FITEM,5,691
FITEM,5,694
FITEM,5,697
FITEM,5,-698

CM,_Y,AREA

ASEL,,,P51X

CM,_Y1,AREA

CMSSEL,S,_Y

CMSSEL,S,_Y1

AATT, 1, 8, 1, 0

CMSSEL,S,_Y

CMDELE,_Y

CMDELE,_Y1 ! Side Sheet - 8mm

FLST,5,6,5,ORDE,6

FITEM,5,239
FITEM,5,301
FITEM,5,690
FITEM,5,692
FITEM,5,695
FITEM,5,-696

CM,_Y,AREA

ASEL,,,P51X

CM,_Y1,AREA

CMSSEL,S,_Y

CMSSEL,S,_Y1

AATT, 1, 21, 1, 0

CMSSEL,S,_Y

CMDELE,_Y

CMDELE,_Y1 ! Side Sheet - 8mm +1/2" Wear Pkg.

FLST,5,23,5,ORDE,14

FITEM,5,290
FITEM,5,-292
FITEM,5,294
FITEM,5,-295
FITEM,5,297
FITEM,5,-300
FITEM,5,302
FITEM,5,-304
FITEM,5,307
FITEM,5,-312
FITEM,5,314
FITEM,5,-315

FITEM,5,318
FITEM,5,-320
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSSEL,S,_Y
CMSSEL,S,_Y1
AATT, 1, 9, 1, 0
CMSSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! All Wall Bolsters - 9mm

FLST,5,4,5,ORDE,2

FITEM,5,322
FITEM,5,-325
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSSEL,S,_Y
CMSSEL,S,_Y1

AATT, 1, 9, 1, 0

CMSSEL,S,_Y

CMDELE,_Y

CMDELE,_Y1 ! SideBoards - 3/8" ~ 9mm

```

|-----|
|-----|
|-----|

```

FINISH
/EOF

❖ *Filename: 3_3_assignprop_front_INPUT*

```
!@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
!      FEA of 930E Truck Box Structure
!      Thickness and Mat Prop Assignment Routine
!      Front Structure
!@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
FINISH
```

/TITLE Assigning Front Thicknesses and Material Properties

/PREP7
*AFUN,DEG

```
!-----
!----- Top Beam
!-----
```

FLST,5,31,5,ORDE,20

```
FITEM,5,340
FITEM,5,344
FITEM,5,351
FITEM,5,358
FITEM,5,368
FITEM,5,371
FITEM,5,398
FITEM,5,408
FITEM,5,426
FITEM,5,428
FITEM,5,430
FITEM,5,432
FITEM,5,434
FITEM,5,441
FITEM,5,443
FITEM,5,496
FITEM,5,498
FITEM,5,-510
FITEM,5,513
FITEM,5,-514
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 9, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1
```

! Top Beam - 9mm

```
!-----
!----- Bolsters
!-----
```

FLST,5,34,5,ORDE,20

```
FITEM,5,337
FITEM,5,-338
FITEM,5,345
FITEM,5,-347
FITEM,5,352
FITEM,5,-354
FITEM,5,359
FITEM,5,-361
FITEM,5,363
FITEM,5,-367
FITEM,5,369
FITEM,5,-370
FITEM,5,372
FITEM,5,-375
```

```
FITEM,5,516
FITEM,5,-521
FITEM,5,528
FITEM,5,531
```

```
FITEM,5,-534
FITEM,5,536
CM,_Y,AREA
```

ASEL,,,P51X

CM,_Y1,AREA

CMSEL,S,_Y

CMSEL,S,_Y1

AATT, 1, 9, 1, 0

CMSEL,S,_Y

CMDELE,_Y

CMDELE,_Y1 ! All Front Bolsters - 9mm

CM,_Y,AREA

ASEL,,, 15

CM,_Y1,AREA

CMSEL,S,_Y

CMSEL,S,_Y1

AATT, 1, 9, 1, 0

CMSEL,S,_Y

CMDELE,_Y

CMDELE,_Y1

```
!-----
!----- Front Sheet
!-----
```

FLST,5,32,5,ORDE,7

FITEM,5,17

FITEM,5,187

FITEM,5,326

FITEM,5,-335

FITEM,5,379

FITEM,5,-397

FITEM,5,442

CM,_Y,AREA

ASEL,,,P51X

CM,_Y1,AREA

CMSEL,S,_Y

CMSEL,S,_Y1

AATT, 1, 9, 1, 0

CMSEL,S,_Y

CMDELE,_Y

CMDELE,_Y1 ! Front Sheet - 9mm No Wear Pkg.

```
!-----
!-----
!-----
```

FINISH

/EOF

❖ Filename: 3_4_assignprop_canopy_INPUT

```

@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
!      FEA of 930E Truck Box Structure
!      Thickness and Mat Prop Assignment Routine
!      Canopy Structure
!@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
FINISH

```

/TITLE, Assigning Canopy Thickness and Material Properties

/PREP7
*AFUN,DEG

```

|-----|
|-----| Bolsters
|-----|

```

FLST,5,42,5,ORDE,27

```

FITEM,5,409
FITEM,5,440
FITEM,5,444
FITEM,5,447
FITEM,5,449
FITEM,5,450
FITEM,5,452
FITEM,5,457
FITEM,5,459
FITEM,5,463
FITEM,5,465
FITEM,5,469
FITEM,5,471
FITEM,5,473
FITEM,5,476
FITEM,5,479
FITEM,5,481
FITEM,5,486
FITEM,5,489
FITEM,5,491
FITEM,5,493
FITEM,5,495
FITEM,5,497
FITEM,5,522
FITEM,5,527
FITEM,5,537
FITEM,5,538
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT,1,5,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1

```

! Top and Bottom Bolsters - 5mm
! Incl. Internal Stiffeners

```

|-----|
|-----| Canopy Sheet
|-----|

```

FLST,5,21,5,ORDE,17

```

FITEM,5,415
FITEM,5,423
FITEM,5,427
FITEM,5,433
FITEM,5,435
FITEM,5,437

```

```

FITEM,5,439
FITEM,5,448
FITEM,5,454
FITEM,5,456
FITEM,5,472
FITEM,5,477
FITEM,5,482
FITEM,5,485
FITEM,5,487
FITEM,5,488
FITEM,5,492
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT,1,5,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1

```

! Canopy Sheet - 5mm Mat #1

```

|-----|
|-----| Rounded Fillet Sections
|-----|

```

FLST,5,12,5,ORDE,12

```

FITEM,5,336
FITEM,5,348
FITEM,5,355
FITEM,5,362
FITEM,5,451
FITEM,5,453
FITEM,5,458
FITEM,5,464
FITEM,5,470
FITEM,5,511
FITEM,5,512
FITEM,5,515
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT,1,5,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1

```

! Rounded Fillets and Side Plates - 5mm

```

|-----|
|-----| Eye Brow
|-----|

```

FLST,5,28,5,ORDE,13

```

FITEM,5,399
FITEM,5,407
FITEM,5,410
FITEM,5,414
FITEM,5,416
FITEM,5,422
FITEM,5,424
FITEM,5,425
FITEM,5,429
FITEM,5,431
FITEM,5,436
FITEM,5,445
FITEM,5,446
CM,_Y,AREA

```

```

ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT,1,5,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1
! All Plates - 5mm
! Incl. Gussets

```

```

|-----|
|-----| Canopy Braces
|-----|

```

```

FLST,5,4,5,ORDE,3
FITEM,5,539
FITEM,5,541
FITEM,5,543
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT,1,8,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1
! Square Tubing - 8mm

```

```

FLST,5,3,5,ORDE,3
FITEM,5,478
FITEM,5,529
FITEM,5,540
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT,1,18,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1
! Upper Reinforced Section - 5mm + 1/2" (17.7mm)

```

```

FLST,5,4,5,ORDE,4
FITEM,5,339
FITEM,5,341
FITEM,5,530
FITEM,5,535
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT,1,22,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1
! Lower Reinforced Section - 9mm + 1/2" (21.7mm)

```

```

|-----|
|-----|
|-----|

```

```

FINISH
/EOF

```

❖ Filename: 3_5_add_guidepin_INPUT

```
!@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
!      FEA of 830E Truck Box Structure
!      Routine to Incorporate Syncrude
!      Modifications to Geometry
!@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
```

FINISH

/TITLE,Incorporating Syncrude's Modifications

/PREP7

*AFUN,DEG

```
-----
|----- View Commands
|-----
```

```
APLOT
/AUTO, 1
/REP
/USER, 1
/VIEW, 1, 0.153749767104, -0.580357600040,
0.799716240420
/ANG, 1, -172.364133592
/LIG, 1,1,1.000, -0.282687364737, 0.461125582318
, 0.841101094489, 0.000000000000E+00
/REPLO
/ZOOM,1,RECT,0.394496,0.585044,0.838009,0.06774
2
```

```
-----
|----- Dividing Exhaust Plenum Side Area
|-----
```

```
KWPAVE, 744
LSBW, 1202
KWPAVE, 750
LSBW, 55
KWPAVE, 97
LSBW, 1202
KWPAVE, 748
LSBW, 55
KWPAVE, 33
LSBW, 1202
KWPAVE, 746
LSBW, 55
ADELE, 95,,1
WPSTYLE,,,,,0
```

```
LSTR, 744, 782
FLST,2,5,4
FITEM,2,55
FITEM,2,71
FITEM,2,213
FITEM,2,199
FITEM,2,1451
AL,P51X
LSTR, 750, 783
FLST,2,6,4
FITEM,2,1423
FITEM,2,55
FITEM,2,1272
FITEM,2,1483
FITEM,2,1444
FITEM,2,1449
AL,P51X
LSTR, 97, 784
FLST,2,4,4
```

```
FITEM,2,1453
FITEM,2,1273
FITEM,2,1483
FITEM,2,1484
AL,P51X
LSTR, 748, 785
FLST,2,8,4
FITEM,2,1441
FITEM,2,1412
FITEM,2,1484
FITEM,2,1315
FITEM,2,1485
FITEM,2,1438
FITEM,2,1448
FITEM,2,1418
AL,P51X
LSTR, 33, 786
FLST,2,4,4
FITEM,2,1486
FITEM,2,1485
FITEM,2,1316
FITEM,2,1454
AL,P51X
LSTR, 746, 787
FLST,2,8,4
FITEM,2,1487
FITEM,2,1478
FITEM,2,1486
FITEM,2,703
FITEM,2,1435
FITEM,2,1415
FITEM,2,1447
FITEM,2,1432
AL,P51X
FLST,2,4,4
FITEM,2,1487
FITEM,2,1202
FITEM,2,1456
FITEM,2,228
AL,P51X
```

```
FLST,5,7,5,ORDE,7
FITEM,5,95
FITEM,5,645
FITEM,5,-646
FITEM,5,652
FITEM,5,-653
FITEM,5,676
FITEM,5,718
CM,_YAREA
ASEL,,,P51X
CM,_Y1AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 3, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1
```

```
-----
|----- Creating Guide Pin Geometry
|-----
```

NUMSTR,AREA,750,! Start New Area Numbers at 750

```
KWPLAN,-1, 755, 56, 351
KWPAVE, 756
```

```

ASBW, 107
ASBW, 109
wpoff,0,0,250-80
FLST,2,2,5,ORDE,2
FITEM,2,750
FITEM,2,753
ASBW,P51X          ! Cutting Existing Areas

LSTR, 788, 756
LSTR, 792, 790
FLST,2,3,4
FITEM,2,1189
FITEM,2,1490
FITEM,2,668
AL,P51X
FLST,2,3,4
FITEM,2,1488
FITEM,2,1498
FITEM,2,1494
AL,P51X          ! Gussets Under pin

LSTR, 788, 756
LSTR, 792, 790
FLST,2,3,4
FITEM,2,1189
FITEM,2,1490
FITEM,2,668
AL,P51X
FLST,2,3,4
FITEM,2,1488
FITEM,2,1498
FITEM,2,1494
AL,P51X
FLST,3,1,3,ORDE,1
FITEM,3,791
KGEN,2,P51X,,0,-90,-250,-250*sin(9),0
FLST,3,1,3,ORDE,1
FITEM,3,793
KGEN,2,P51X,,0,-150,-150*sin(9),0
FLST,3,1,3,ORDE,1
FITEM,3,794
KGEN,2,P51X,,0,-130,-130*sin(9),0
FLST,3,3,3,ORDE,2
FITEM,3,793
FITEM,3,-795
KGEN,2,P51X,,0,170*sin(9),-170,0
LSTR, 795, 798
LSTR, 794, 797
LSTR, 793, 796
FLST,3,1,4,ORDE,1
FITEM,3,1501
LGEN,2,P51X,,0,0,0,0 ! guide pin lines

LSTR, 794, 795
LSTR, 797, 798
LSTR, 796, 800
LSTR, 793, 799
LSTR, 791, 793
LSTR, 789, 796
LSTR, 792, 799
LSTR, 800, 788
LSTR, 800, 798
LSTR, 799, 795
LSTR, 793, 794
LSTR, 796, 797
FLST,2,4,4
FITEM,2,1490
FITEM,2,1508
FITEM,2,1510
FITEM,2,1505

AL,P51X
FLST,2,4,4
FITEM,2,1498
FITEM,2,1507
FITEM,2,1509
FITEM,2,1506
AL,P51X
FLST,2,4,4
FITEM,2,1506
FITEM,2,1512
FITEM,2,1503
FITEM,2,1513
AL,P51X
FLST,2,4,4
FITEM,2,1496
FITEM,2,1501
FITEM,2,1508
FITEM,2,1507
AL,P51X
FLST,2,4,4
FITEM,2,1501
FITEM,2,1514
FITEM,2,1513
FITEM,2,1500
AL,P51X
FLST,2,4,4
FITEM,2,1500
FITEM,2,1503
FITEM,2,1504
FITEM,2,1489
AL,P51X

!-----
!----- Updating Material Thickness Specs
!-----

FLST,5,6,5,ORDE,4
FITEM,5,751
FITEM,5,-752
FITEM,5,754
FITEM,5,-757
CM,_YAREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 16, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1          ! 5/8" Plate

FLST,5,2,5,ORDE,2
FITEM,5,750
FITEM,5,753
CM,_YAREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 9, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1          ! 9mm
GussetsPlate

```

```

FLST,5,7,5,ORDE,2
FITEM,5,758
FITEM,5,-764
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT,1,16,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! 5/8" Plate - Guide Material

```

```

-----
----- Dividing Forward STR for New BC
-----

```

```

NUMSTR,KP,1000,
NUMSTR,LINE,2000,
NUMSTR,AREA,1000,
! Start New Area Numbers at 1000

```

```

KWPLAN,-1,63,327,681

```

```

KL,1274,5,

```

```

KWPAVE,1000

```

```

FLST,2,16,5,ORDE,2
FITEM,2,596
FITEM,2,-611
ASBW,P51X

```

```

FLST,5,32,5,ORDE,2
FITEM,5,1000
FITEM,5,-1031
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT,1,25,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! Restoring 1" Plate
Thickness

```

```

-----
-----
-----

```

```

FINISH
/EOF

```

❖ Filename: 4_1_FEA_manual_mesh_INPUT

```

@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
! FEA of 930E Truck Box Structure
! Manual Meshing Routine
! @@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@

```

/TITLE,Meshing Model Geometry

```

-----
|                                     |
|----- View Settings                |
|-----

```

```

ERASE
LPLOT
WPSTYLE,.....0
/VIEW,1,1,1,1
/ANG,1
/REP,FAST
/AUTO,1
/REP
/USER,1
/VIEW,1,0.857837457633,-0.313003209901,-
0.407607515722
/ANG,1,-12.1890301189
/IG,1,1,1,000,0.935109786654,-0.251682781996
,-0.249450324014,0.000000000000E+00
/REPO

```

```

-----
|                                     |
|----- Manual Mesh Sizing          |
|-----

```

/PREP7

```

-----
|                                     |
|----- Bolster Stringer Joint Lines
|-----

```

```

FLST,5,4,4,ORDE,4
FITEM,5,150
FITEM,5,152
FITEM,5,1365
FITEM,5,1367
CM,_Y,LINE
LSEL,.,.,P51X
CM,_Y1,LINE
CMSEL,_,Y
LESIZE,_Y1,.,8,10,
CMDEL,_,Y
CMDEL,_,Y1 ! Div's Down Bolster Side Edges
! 2nd Bolster

```

```

FLST,5,10,4,ORDE,10
FITEM,5,285
FITEM,5,308
FITEM,5,313
FITEM,5,315
FITEM,5,347
FITEM,5,351
FITEM,5,361
FITEM,5,1335
FITEM,5,1373
FITEM,5,1384
CM,_Y,LINE
LSEL,.,.,P51X
CM,_Y1,LINE
CMSEL,_,Y
!LESIZE,_Y1,.,15,1/10,

```

```

LESIZE,_Y1,.,8,1/10,
CMDEL,_,Y ! Div's Down Bolster Side Edges
CMDEL,_,Y1 ! Pivot Region
FLST,5,2,4,ORDE,2
FITEM,5,351
FITEM,5,1384
CM,_Y1,LINE
LSEL,.,.,P51X
*GET,_z1,LINE,,COUNT
*SET,_z2,0
*DO,_z5,1,_z1
*SET,_z2,LSNEXT(_z2)
*GET,_z3,LINE,_z2,ATTR,NDIV
*GET,_z4,LINE,_z2,ATTR,SPAC
*IF,_z3,GT,0,THEN
*IF,_z4,NE,0,THEN
LESIZE,_z2,.,_z3,1/_z4
*ENDIF
*ENDIF
*ENDDO
CMSEL,S,_Y1
CMDELE,_,Y1 ! Flip Bias on Some Lines

```

```

FLST,5,20,4,ORDE,20
FITEM,5,196
FITEM,5,210
FITEM,5,227
FITEM,5,247
FITEM,5,273
FITEM,5,610
FITEM,5,611
FITEM,5,620
FITEM,5,626
FITEM,5,1139
FITEM,5,1145
FITEM,5,1153
FITEM,5,1159
FITEM,5,1176
FITEM,5,1182
FITEM,5,1191
FITEM,5,1201
FITEM,5,1216
FITEM,5,1219
FITEM,5,1231
CM,_Y,LINE
LSEL,.,.,P51X
CM,_Y1,LINE
CMSEL,_,Y
LESIZE,_Y1,.,8,1/10,
!LESIZE,_Y1,.,15,1/10,
CMDEL,_,Y
CMDELE,_,Y1 ! Div's Down Forward Bolster Side Edges

```

```

FLST,5,2,4,ORDE,2
FITEM,5,247
FITEM,5,273
CM,_Y1,LINE
LSEL,.,.,P51X
*GET,_z1,LINE,,COUNT
*SET,_z2,0
*DO,_z5,1,_z1
*SET,_z2,LSNEXT(_z2)
*GET,_z3,LINE,_z2,ATTR,NDIV
*GET,_z4,LINE,_z2,ATTR,SPAC
*IF,_z3,GT,0,THEN
*IF,_z4,NE,0,THEN

```

```

LESIZE_z2,,,z3,1/_z4
*ENDIF
*ENDIF
*ENDDO
CMSEL,S,_Y1
CMDELE,_Y1 ! Flip Bias on Some Lines

FLST,5,2,4,ORDE,2
FITEM,5,153
FITEM,5,1328
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,,,7,-6,
!LESIZE,_Y1,,,10,-5,
! Div's Small Near Bolster Corners
CMDEL,_Y ! Larger in Center (2nd Bolster)
CMDEL,_Y1

FLST,5,9,4,ORDE,9
FITEM,5,297
FITEM,5,359
FITEM,5,1155
FITEM,5,1178
FITEM,5,1199
FITEM,5,1214
FITEM,5,1229
FITEM,5,1375
FITEM,5,1390
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,,,15,-7,
!LESIZE,_Y1,,,17,-7,
! Div's Small Near Bolster Corners
CMDEL,_Y ! Larger in Center (Bolster Bottom Outside)
CMDEL,_Y1

FLST,5,7,4,ORDE,7
FITEM,5,1149
FITEM,5,1173
FITEM,5,1198
FITEM,5,1211
FITEM,5,1228
FITEM,5,1357
FITEM,5,1388
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,,,15,-7,
!LESIZE,_Y1,,,20,-7,
! Div's Small Near Bolster Corners
CMDEL,_Y ! Larger in Center (Bolster Bottom Inside)
CMDEL,_Y1

FLST,5,2,4,ORDE,2
FITEM,5,147
FITEM,5,1325
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,,,2,1,
CMDEL,_Y
CMDEL,_Y1
! Div's on Rounded Corners (1st Rear Bolster)

FLST,5,4,4,ORDE,4
FITEM,5,13
FITEM,5,132
FITEM,5,367
FITEM,5,1347
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,,,5,1,
CMDEL,_Y
CMDEL,_Y1 ! Div's on Rounded Corners (2nd Bolster)

FLST,5,18,4,ORDE,17
FITEM,5,32
FITEM,5,38
FITEM,5,41
FITEM,5,43
FITEM,5,50
FITEM,5,52
FITEM,5,60
FITEM,5,62
FITEM,5,77
FITEM,5,86
FITEM,5,88
FITEM,5,139
FITEM,5,184
FITEM,5,235
FITEM,5,239
FITEM,5,278
FITEM,5,-280
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,,,10,1,
!LESIZE,_Y1,,,10,1,
CMDEL,_Y
CMDEL,_Y1 ! Div's on Rounded Corners (Outside)

FLST,5,14,4,ORDE,14
FITEM,5,26
FITEM,5,36
FITEM,5,42
FITEM,5,51
FITEM,5,61
FITEM,5,74
FITEM,5,80
FITEM,5,89
FITEM,5,176
FITEM,5,194
FITEM,5,208
FITEM,5,234
FITEM,5,240
FITEM,5,244
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,,,10,1,
!LESIZE,_Y1,,,10,1,
CMDEL,_Y
CMDEL,_Y1 ! Div's on Rounded Corners (Inside)

FLST,2,2,4,ORDE,2
FITEM,2,365
FITEM,2,1333
LCOMB,P51X,0
FLST,5,2,4,ORDE,2
FITEM,5,365

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FITEM,5,1378
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,,10,1,
CMDEL,_Y
CMDEL,_Y1
FLST,5,14,ORDE,1
FITEM,5,1382
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,,1,1,
CMDEL,_Y
CMDEL,_Y1
FLST,2,2,4,ORDE,2
FITEM,2,312
FITEM,2,1391
LCOMB,P51X,,0
FLST,5,1,4,ORDE,1
FITEM,5,312
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,,7,1,
CMDEL,_Y
CMDEL,_Y1      ! Sizing a Few Misc. Lines

|-----
|----- Bolster Lines Inside Stringer Box
|-----

FLST,2,3,4,ORDE,3
FITEM,2,160
FITEM,2,174
FITEM,2,1469
LCOMB,P51X,,0
FLST,5,2,4,ORDE,2
FITEM,5,159
FITEM,5,160
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,,4,1,
CMDEL,_Y
CMDEL,_Y1      ! Inside Bolster (Top) (2nd Bolster)

FLST,5,14,4,ORDE,14
FITEM,5,37
FITEM,5,255
FITEM,5,257
FITEM,5,259
FITEM,5,261
FITEM,5,263
FITEM,5,265
FITEM,5,267
FITEM,5,270
FITEM,5,271
FITEM,5,274
FITEM,5,301
FITEM,5,307
FITEM,5,319
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,,4,1,
CMDEL,_Y
CMDEL,_Y1      ! Inside Bolster (Top) (Rest of Bolsters)

FLST,5,4,4,ORDE,4
FITEM,5,2
FITEM,5,10
FITEM,5,130
FITEM,5,131
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,,7,-5,
!LESIZE,_Y1,,10,-10,
! Div's Small Near Bolster Corners
CMDEL,_Y      ! Larger in Center (Inside Bolster Bottom)
CMDEL,_Y1      ! (2nd Bolster)

FLST,5,28,4,ORDE,28
FITEM,5,218
FITEM,5,251
FITEM,5,252
FITEM,5,254
FITEM,5,269
FITEM,5,305
FITEM,5,314
FITEM,5,320
FITEM,5,350
FITEM,5,362
FITEM,5,589
FITEM,5,648
FITEM,5,1141
FITEM,5,1151
FITEM,5,1157
FITEM,5,1168
FITEM,5,1174
FITEM,5,1180
FITEM,5,1192
FITEM,5,1197
FITEM,5,1203
FITEM,5,1209
FITEM,5,1218
FITEM,5,1227
FITEM,5,1233
FITEM,5,1374
FITEM,5,1376
FITEM,5,1383
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,,7,-5,
!LESIZE,_Y1,,10,-10,
! Div's Small Near Bolster Corners
CMDEL,_Y      ! Larger in Center (Inside Bolster Bottom)
CMDEL,_Y1      ! (Rest of Bolsters)

|-----
|----- Bolster Lines Between Two Stringers
|-----

FLST,5,2,4,ORDE,2
FITEM,5,126
FITEM,5,137
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,,7,1/3,

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!LESIZE_Y1,,10,1/3,
CMDEL_Y      ! Bolster Div's Inside Stringer (Top)
CMDEL_Y1     ! (1st Bolster)

FLST,5,2,4,ORDE,2
FITEM,5,140
FITEM,5,151
CM_Y,LINE
LSEL,,,P51X
CM_Y1,LINE
CMSEL,_Y
LESIZE_Y1,,7,1/3,
!LESIZE_Y1,,10,1/3,
CMDEL_Y      ! Bolster Div's Inside Stringer (Top)
CMDEL_Y1     ! (2nd Bolster)

FLST,5,4,4,ORDE,4
FITEM,5,316
FITEM,5,317
FITEM,5,323
FITEM,5,324
CM_Y,LINE
LSEL,,,P51X
CM_Y1,LINE
CMSEL,_Y
LESIZE_Y1,,10,1/3,
!LESIZE_Y1,,10,1/3,
CMDEL_Y      ! Bolster Div's Inside Stringer (Top)
CMDEL_Y1     ! 3rd and 4th Bolsters

FLST,5,1,4,ORDE,1
FITEM,5,185
CM_Y,LINE
LSEL,,,P51X
CM_Y1,LINE
CMSEL,_Y
LESIZE_Y1,,10,1/3,
!LESIZE_Y1,,10,1/3,
CMDEL_Y
CMDEL_Y1

FLST,5,1,4,ORDE,1
FITEM,5,127
FITEM,5,148
FITEM,5,149
CM_Y,LINE
LSEL,,,P51X
CM_Y1,LINE
CMSEL,_Y
LESIZE_Y1,,7,3/1,
!LESIZE_Y1,,10,3/1,
CMDEL_Y      ! Bolster Div's Inside Stringer (Bottom)
CMDEL_Y1     ! (1st Bolster)

FLST,5,1,4,ORDE,1
FITEM,5,127
CM_Y1,LINE
LSEL,,,P51X
*GET,_z1,LINE,_COUNT
*SET,_z2,0
*DO,_z5,1,_z1
*SET,_z2,LSNEXT(_z2)
*GET,_z3,LINE,_z2,ATTR,NDIV
*GET,_z4,LINE,_z2,ATTR,SPAC
*IF,_z3,GT,0,THEN
*IF,_z4,NE,0,THEN
LESIZE,_z2,,_z3,1/_z4
*ENDIF
*ENDIF
*ENDDO
CMSEL,S,_Y1
CMDELE,_Y1

FLST,5,4,4,ORDE,4
FITEM,5,135
FITEM,5,136
FITEM,5,142
FITEM,5,143
CM_Y,LINE

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LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,,,7,3/1,
!LESIZE,_Y1,,,10,3/1,
! Bolster Div's Inside Stringer (Bottom)
CMDEL,_Y
CMDEL,_Y1

FLST,5,8,4,ORDE,8
FITEM,5,295
FITEM,5,304
FITEM,5,309
FITEM,5,355
FITEM,5,1369
FITEM,5,1371
FITEM,5,1385
FITEM,5,1387
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,,,10,1/3,
!LESIZE,_Y1,,,15,1/3,
! Bolster Div's Inside Stringer (Bottom)
CMDEL,_Y
CMDEL,_Y1
FLST,5,3,4,ORDE,3
FITEM,5,355
FITEM,5,1369
FITEM,5,1385
CM,_Y1,LINE
LSEL,,,P51X
*GET,_z1,LINE,,COUNT
*SET,_z2,0
*DO,_z5,1,_z1
*SET,_z2,LSNEXT(_z2)
*GET,_z3,LINE,_z2,ATTR,NDIV
*GET,_z4,LINE,_z2,ATTR,SPAC
*IF,_z3,GT,0,THEN
*IF,_z4,NE,0,THEN
LESIZE,_z2,,,z3,1/_z4
*ENDIF
*ENDIF
*ENDDO
CMSEL,S,_Y1
CMDELE,_Y1

FLST,5,1,4,ORDE,1
FITEM,5,1232
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,,,10,1/3,
!LESIZE,_Y1,,,15,1/3,
CMDEL,_Y
CMDEL,_Y1
FLST,5,13,4,ORDE,13
FITEM,5,205
FITEM,5,1408
FITEM,5,-1409
FITEM,5,1419
FITEM,5,-1420
FITEM,5,1430
FITEM,5,-1431
FITEM,5,1436
FITEM,5,-1437
FITEM,5,1442
FITEM,5,-1443

FITEM,5,1452
FITEM,5,1457
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,,,4,2,
!LESIZE,_Y1,,,7,2,
CMDEL,_Y
CMDEL,_Y1
FLST,5,2,4,ORDE,2
FITEM,5,1419
FITEM,5,-1420
CM,_Y1,LINE
LSEL,,,P51X
*GET,_z1,LINE,,COUNT
*SET,_z2,0
*DO,_z5,1,_z1
*SET,_z2,LSNEXT(_z2)
*GET,_z3,LINE,_z2,ATTR,NDIV
*GET,_z4,LINE,_z2,ATTR,SPAC
*IF,_z3,GT,0,THEN
*IF,_z4,NE,0,THEN
LESIZE,_z2,,,z3,1/_z4
*ENDIF
*ENDIF
*ENDDO
CMSEL,S,_Y1
CMDELE,_Y1
FLST,5,2,4,ORDE,2
FITEM,5,1408
FITEM,5,-1409
CM,_Y1,LINE
LSEL,,,P51X
*GET,_z1,LINE,,COUNT
*SET,_z2,0
*DO,_z5,1,_z1
*SET,_z2,LSNEXT(_z2)
*GET,_z3,LINE,_z2,ATTR,NDIV
*GET,_z4,LINE,_z2,ATTR,SPAC
*IF,_z3,GT,0,THEN
*IF,_z4,NE,0,THEN
LESIZE,_z2,,,z3,1/_z4
*ENDIF
*ENDIF
*ENDDO
CMSEL,S,_Y1
CMDELE,_Y1
FLST,5,13,4,ORDE,13
FITEM,5,191
FITEM,5,686
FITEM,5,700
FITEM,5,1410
FITEM,5,-1411
FITEM,5,1433
FITEM,5,-1434
FITEM,5,1439
FITEM,5,-1440
FITEM,5,1445
FITEM,5,-1446
FITEM,5,1450
FITEM,5,1455
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,,,6,2,
!LESIZE,_Y1,,,8,2,
CMDEL,_Y
CMDEL,_Y1

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FLST,5,9,4,ORDE,9
FITEM,5,191
FITEM,5,1433
FITEM,5,-1434
FITEM,5,-1439
FITEM,5,-1440
FITEM,5,1445
FITEM,5,-1446
FITEM,5,1450
FITEM,5,1455
CM,_Y1,LINE
LSEL,, ,P51X
*GET,_z1,LINE,COUNT
*SET,_z2,0
*DO,_z5,1,_z1
*SET,_z2,LSNEXT(_z2)
*GET,_z3,LINE,_z2,ATTR,NDIV
*GET,_z4,LINE,_z2,ATTR,SPAC
*IF,_z3,GT,0,THEN
*IF,_z4,NE,0,THEN
LESIZE,_z2,,, _z3,1/_z4
*ENDIF
*ENDIF
*ENDDO
CMSEL,S,_Y1
CMDELE,_Y1
FLST,5,13,4,ORDE,13
FITEM,5,191
FITEM,5,686
FITEM,5,700
FITEM,5,1410
FITEM,5,-1411
FITEM,5,1433
FITEM,5,-1434
FITEM,5,1439
FITEM,5,-1440
FITEM,5,1445
FITEM,5,-1446
FITEM,5,1450
FITEM,5,1455
CM,_Y,LINE
LSEL,, ,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,, ,6,2
!LESIZE,_Y1,, ,8,2,
CMDEL,_Y
CMDEL,_Y1
FLST,5,9,4,ORDE,9
FITEM,5,191
FITEM,5,1433
FITEM,5,-1434
FITEM,5,1439
FITEM,5,-1440
FITEM,5,1445
FITEM,5,-1446
FITEM,5,1450
FITEM,5,1455
CM,_Y1,LINE
LSEL,, ,P51X
*GET,_z1,LINE,COUNT
*SET,_z2,0
*DO,_z5,1,_z1
*SET,_z2,LSNEXT(_z2)
*GET,_z3,LINE,_z2,ATTR,NDIV
*GET,_z4,LINE,_z2,ATTR,SPAC
*IF,_z3,GT,0,THEN
*IF,_z4,NE,0,THEN
LESIZE,_z2,,, _z3,1/_z4
*ENDIF
*ENDIF
*ENDDO
CMSEL,S,_Y1
CMDELE,_Y1
FLST,5,2,4,ORDE,2
FITEM,5,1458
FITEM,5,-1459
CM,_Y,LINE
LSEL,, ,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,, ,1,1,
CMDEL,_Y
CMDEL,_Y1
FLST,5,2,4,ORDE,2
FITEM,5,1461
FITEM,5,-1462
CM,_Y,LINE
LSEL,, ,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,, ,8,3,
!LESIZE,_Y1,, ,13,3,
CMDEL,_Y
! Bolster Div's inside Stringer (Bottom)
CMDEL,_Y1
! (Forward Bolsters)

!-----
!----- Bolster Lines Outside of Stringers
!-----

FLST,5,3,4,ORDE,3
FITEM,5,164
FITEM,5,169
FITEM,5,370
CM,_Y,LINE
LSEL,, ,P51X
CM,_Y1,LINE

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CMSEL,,Y
LESIZE,_Y1,,.15,1/2,
CMDEL,_Y
CMDEL,_Y1

! Div's Bottom of Bolster
! Rear (1st) Bolster

FLST,5,4,4,ORDE,4
FITEM,5,649
FITEM,5,1143
FITEM,5,1146
FITEM,5,1160
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,_Y
FLST,5,4,4,ORDE,4
FITEM,5,368
FITEM,5,-369
FITEM,5,1327
FITEM,5,1355
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,,.20,1/5,
!LESIZE,_Y1,,.30,1/5,
CMDEL,_Y
CMDEL,_Y1

! Div's Bottom of Bolster
! 2nd Bolster

FLST,5,20,4,ORDE,20
FITEM,5,256
FITEM,5,262
FITEM,5,318
FITEM,5,345
FITEM,5,-346
FITEM,5,356
FITEM,5,363
FITEM,5,587
FITEM,5,595
FITEM,5,621
FITEM,5,649
FITEM,5,1143
FITEM,5,1146
FITEM,5,1160
FITEM,5,1220
FITEM,5,-1221
FITEM,5,1236
FITEM,5,1377
FITEM,5,1380
FITEM,5,1394
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,,.30,1/5,
!LESIZE,_Y1,,.35,1/5,
CMDEL,_Y
CMDEL,_Y1
FLST,5,2,4,ORDE,2
FITEM,5,256
FITEM,5,262
CM,_Y1,LINE
LSEL,,,P51X
*GET,_z1,LINE,COUNT
*SET,_z2,0
*DO,_z5,1,_z1
*SET,_z2,LSNEXT(_z2)
*GET,_z3,LINE,_z2,ATTR,NDIV
*GET,_z4,LINE,_z2,ATTR,SPAC
*IF,_z3,GT,0,THEN
*IF,_z4,NE,0,THEN

LESIZE,_z2,,_z3,1/_z4
*ENDIF
*ENDIF
*ENDDO
CMSEL,S,_Y1
CMDELE,_Y1

! Bottom Bolster Divisions in Bolsters
! w/ Hoist Pivot Stiffeners

FLST,5,8,4,ORDE,8
FITEM,5,264
FITEM,5,266
FITEM,5,1164
FITEM,5,1170
FITEM,5,1181
FITEM,5,1183
FITEM,5,1193
FITEM,5,1206
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,,.5,1,
!LESIZE,_Y1,,.6,1,

! Bolster Segment Between Hoist Pivot / Str

CMDEL,_Y
CMDEL,_Y1
FLST,5,8,4,ORDE,8
FITEM,5,593
FITEM,5,600
FITEM,5,608
FITEM,5,646
FITEM,5,1163
FITEM,5,1166
FITEM,5,-1167
FITEM,5,1208
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,,.5,1,
!LESIZE,_Y1,,.6,1,

! Bolster Segment Inside Hoist Pivot

CMDEL,_Y
CMDEL,_Y1
FLST,5,8,4,ORDE,8
FITEM,5,605
FITEM,5,634
FITEM,5,1140
FITEM,5,1158
FITEM,5,1185
FITEM,5,1188
FITEM,5,1194
FITEM,5,1212
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,,.30-5-5,1/5,
!LESIZE,_Y1,,.35-12,1/5,

! Bolster Lines Outside Hoist Pivot

CMDEL,_Y
CMDEL,_Y1
FLST,5,3,4,ORDE,3
FITEM,5,1185
FITEM,5,1188
FITEM,5,1194
CM,_Y1,LINE
LSEL,,,P51X
*GET,_z1,LINE,COUNT

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*SET,_z2,0
*DO,_z5,1,_z1
*SET,_z2,LSNEXT(_z2)
*GET,_z3,LINE,_z2,ATTR,NDIV
*GET,_z4,LINE,_z2,ATTR,SPAC
*IF,_z3,GT,0,THEN
*IF,_z4,NE,0,THEN
LESIZE,_z2,,,_z3,1/_z4
*ENDIF
*ENDIF
*ENDDO
CMSEL,S,_Y1
CMDEL,_Y1

FLST,5,2,4,ORDE,2
FITEM,5,11
FITEM,5,146
CM,_Y,LINE
LSEL,,,_P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,, ,15,2/1,
CMDEL,_Y
CMDEL,_Y1

FLST,5,2,4,ORDE,2
FITEM,5,1360
FITEM,5,1363
CM,_Y,LINE
LSEL,,,_P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,, ,20,1/5,
! Div's Top of Bolster
! Rear (1st) Bolster
CMDEL,_Y
CMDEL,_Y1

FLST,5,10,4,ORDE,10
FITEM,5,189
FITEM,5,195
FITEM,5,203
FITEM,5,209
FITEM,5,217
FITEM,5,287
FITEM,5,293
FITEM,5,298
FITEM,5,376
FITEM,5,534
CM,_Y,LINE
LSEL,,,_P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,, ,30,5,
! Div's Top of Bolster
! Except Hoist Bolsters
! Top Bolster Divisions in Bolsters w/
! Hoist Pivot Stiffeners
CMDEL,_Y
CMDEL,_Y1

FLST,5,4,4,ORDE,4
FITEM,5,597
FITEM,5,598
FITEM,5,601
FITEM,5,604
CM,_Y,LINE
LSEL,,,_P51X
CM,_Y1,LINE
CMSEL,,_Y

LESIZE,_Y1,, ,5,1,
! Bolster Segment Between Hoist Pivot / Str
! Bolster Segment Inside Hoist Pivot
CMDEL,_Y
CMDEL,_Y1
FLST,5,4,4,ORDE,4
FITEM,5,612
FITEM,5,613
FITEM,5,615
FITEM,5,617
CM,_Y,LINE
LSEL,,,_P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,, ,30-5-5,1/5,
LESIZE,_Y1,, ,35-12,1/5,
! Bolster Lines Outside Hoist Pivot
CMDEL,_Y
CMDEL,_Y1

!-----
!----- Front Stringer Section
!-----

FLST,2,2,4,ORDE,2
FITEM,2,48
FITEM,2,57
LDELE,P51X,, ,1
FLST,5,38,4,ORDE,14
FITEM,5,188
FITEM,5,190
FITEM,5,192
FITEM,5,200
FITEM,5,1283
FITEM,5,1284
FITEM,5,1287
FITEM,5,1294
FITEM,5,1297
FITEM,5,1304
FITEM,5,1307
FITEM,5,1314
FITEM,5,1317
FITEM,5,1324
CM,_Y,LINE
LSEL,,,_P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,, ,7,7,
! Lines Below Bolster Corners
! Lines Below Bolster Corners
CMDEL,_Y
CMDEL,_Y1
FLST,5,8,4,ORDE,7
FITEM,5,1293
FITEM,5,1294
FITEM,5,1310

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FITEM,5,1318
FITEM,5,-1320
FITEM,5,1323
FITEM,5,-1324
CM,_Y1,LINE
LSEL,,,P51X
*GET,_z1,LINE,COUNT
*SET,_z2,0
*DO,_z5,1,_z1
*SET,_z2,LSNEXT(_z2)
*GET,_z3,LINE,_z2,ATTR,NDIV
*GET,_z4,LINE,_z2,ATTR,SPAC
*IF,_z3,GT,0,THEN
*IF,_z4,NE,0,THEN
LESIZE,_z2,,_z3,1/_z4
*ENDIF
*ENDIF
*ENDDO
CMSEL,S,_Y1
CMDELE,_Y1

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|-----|
|-----| Exhaust Plenum Section
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FLST,5,10,4,ORDE,10
FITEM,5,1202
FITEM,5,1273
FITEM,5,1315
FITEM,5,-1316
FITEM,5,1415
FITEM,5,1418
FITEM,5,1453
FITEM,5,-1454
FITEM,5,1456
FITEM,5,1478
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,,,5,1,
CMDEL,_Y
CMDEL,_Y1

```

```

FLST,5,5,4,ORDE,5
FITEM,5,703
FITEM,5,1412
FITEM,5,1432
FITEM,5,1438
FITEM,5,1444
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,,,2,1,
CMDEL,_Y
CMDEL,_Y1

```

```

|-----|
|-----|
|-----| Automatic Meshing
|-----|

```

```

|-----|
|-----| Mesher Options
|-----|
MOPT,AMESH,DEFA
MOPT,QMESH,DEFA
MOPT,VMESH,DEFA
MOPT,TIMP,1
MOPT,PYRA,ON

```

```

MOPT,SPLIT,2 ! Split Quads on WARNING
MSHKEY,0
MSHMID,0
MSHPATTERN,0
KEYW,ACCEPT,0
MSHA,0,2D
MSHA,1,3D

```

```

|-----|
|-----| Pivot Structure
|-----|

```

```

SMRTSIZE,1 ! Fine Mesh Setting

```

```

FLST,5,2,5,ORDE,2
FITEM,5,11
FITEM,5,118
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,,_Y
CMDEL,,_Y1
CMDEL,,_Y2

```

```

! Meshing Reinforced Section

```

```

MSHKEY,0
FLST,5,44,5,ORDE,28
FITEM,5,11
FITEM,5,18
FITEM,5,-20
FITEM,5,26
FITEM,5,33
FITEM,5,36
FITEM,5,53
FITEM,5,71
FITEM,5,118
FITEM,5,121
FITEM,5,-122
FITEM,5,125
FITEM,5,129
FITEM,5,131
FITEM,5,133
FITEM,5,137
FITEM,5,-138
FITEM,5,141
FITEM,5,-144
FITEM,5,152
FITEM,5,157
FITEM,5,253
FITEM,5,-254
FITEM,5,544
FITEM,5,-549
FITEM,5,679
FITEM,5,-689
FITEM,5,693
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y2
CMDEL,,_Y
CMDEL,,_Y1
CMDEL,,_Y2

```

```

! Meshing Rest of Pivot Structure

```

```

|-----|
|-----| Rear Stringer Structure
|-----|

```

SMRTSIZE,1 ! Fine Mesh Setting

MSHKEY,0
 FLST,5,19,5,ORDE,15
 FITEM,5,29
 FITEM,5,46
 FITEM,5,51
 FITEM,5,-52
 FITEM,5,54
 FITEM,5,-57
 FITEM,5,64
 FITEM,5,66
 FITEM,5,139
 FITEM,5,-140
 FITEM,5,146
 FITEM,5,-149
 FITEM,5,154
 FITEM,5,165
 FITEM,5,669
 CM,_Y,AREA
 ASEL,,,P51X
 CM,_Y1,AREA
 CHKMISH,'AREA'
 CMSEL,S,_Y
 AMESH,_Y1
 CMDEL,_Y
 CMDEL,_Y1
 CMDEL,_Y2

 !----- Front Stringer Structure
 !-----

SMRTSIZE,3 ! Fine Mesh Setting

MSHKEY,0
 FLST,5,97,5,ORDE,30
 FITEM,5,14
 FITEM,5,-15
 FITEM,5,37
 FITEM,5,39
 FITEM,5,41
 FITEM,5,43
 FITEM,5,183
 FITEM,5,342
 FITEM,5,349
 FITEM,5,586
 FITEM,5,592
 FITEM,5,-595
 FITEM,5,612
 FITEM,5,-626
 FITEM,5,628
 FITEM,5,-629
 FITEM,5,631
 FITEM,5,-644
 FITEM,5,647
 FITEM,5,-651
 FITEM,5,654
 FITEM,5,-658
 FITEM,5,663
 FITEM,5,-664
 FITEM,5,667
 FITEM,5,-668
 FITEM,5,670
 FITEM,5,-675
 FITEM,5,1000
 FITEM,5,-1031
 CM,_Y,AREA

ASEL,,,P51X
 CM,_Y1,AREA
 CHKMISH,'AREA'
 CMSEL,S,_Y
 AMESH,_Y1
 CMDEL,_Y
 CMDEL,_Y1
 CMDEL,_Y2

 !----- All Bolster Areas incl. Inside Stringer
 !-----

SMRTSIZE,6 ! Mesh Setting

MSHKEY,0 ! Rear Bolster (Angle)
 FLST,5,14,5,ORDE,14
 FITEM,5,1
 FITEM,5,5
 FITEM,5,7
 FITEM,5,48
 FITEM,5,-49
 FITEM,5,65
 FITEM,5,112
 FITEM,5,203
 FITEM,5,562
 FITEM,5,630
 FITEM,5,660
 FITEM,5,666
 FITEM,5,677
 FITEM,5,-678
 CM,_Y,AREA
 ASEL,,,P51X
 CM,_Y1,AREA
 CHKMISH,'AREA'
 CMSEL,S,_Y
 AMESH,_Y1
 CMDEL,_Y
 CMDEL,_Y1
 CMDEL,_Y2

SMRTSIZE,1

MSHKEY,0 ! 2nd Bolster from Back
 FLST,5,17,5,ORDE,16
 FITEM,5,2
 FITEM,5,4
 FITEM,5,47
 FITEM,5,50
 FITEM,5,58
 FITEM,5,60
 FITEM,5,63
 FITEM,5,68
 FITEM,5,-70
 FITEM,5,199
 FITEM,5,251
 FITEM,5,-252
 FITEM,5,553
 FITEM,5,627
 FITEM,5,659
 FITEM,5,661
 CM,_Y,AREA
 ASEL,,,P51X
 CM,_Y1,AREA
 CHKMISH,'AREA'
 CMSEL,S,_Y
 AMESH,_Y1
 CMDEL,_Y
 CMDEL,_Y1
 CMDEL,_Y2

```

MSHKEY,0
FLST,5,24,5,ORDE,19
FITEM,5,8
FITEM,5,-10
FITEM,5,12
FITEM,5,-13
FITEM,5,21
FITEM,5,-25
FITEM,5,27
FITEM,5,-28
FITEM,5,117
FITEM,5,119
FITEM,5,-120
FITEM,5,123
FITEM,5,-124
FITEM,5,127
FITEM,5,-128
FITEM,5,130
FITEM,5,132
FITEM,5,134
FITEM,5,-136
CM,_Y,AREA
ASEL,...,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1      ! Two Bolsters in Pivot Region
CMDEL,_Y2      ! Areas Inside Pivot Meshed Previously

```

```

MSHKEY,0
FLST,5,20,5,ORDE,16
FITEM,5,72
FITEM,5,73
FITEM,5,75
FITEM,5,-77
FITEM,5,102
FITEM,5,255
FITEM,5,578
FITEM,5,585
FITEM,5,587
FITEM,5,-591
FITEM,5,706
FITEM,5,-707
FITEM,5,714
FITEM,5,-715
FITEM,5,728
FITEM,5,-729
CM,_Y,AREA
ASEL,...,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2

```

! 5th Bolster

```

MSHKEY,0
FLST,5,22,5,ORDE,20
FITEM,5,78
FITEM,5,-79
FITEM,5,81
FITEM,5,-82
FITEM,5,105
FITEM,5,256
FITEM,5,281
FITEM,5,313

```

```

FITEM,5,316
FITEM,5,567
FITEM,5,579
FITEM,5,581
FITEM,5,583
FITEM,5,-584
FITEM,5,708
FITEM,5,-710
FITEM,5,716
FITEM,5,-717
FITEM,5,725
FITEM,5,-727
CM,_Y,AREA
ASEL,...,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2

```

! 6th Bolster

```

MSHKEY,0
FLST,5,32,5,ORDE,27
FITEM,5,84
FITEM,5,87
FITEM,5,108
FITEM,5,257
FITEM,5,260
FITEM,5,263
FITEM,5,265
FITEM,5,267
FITEM,5,272
FITEM,5,277
FITEM,5,279
FITEM,5,283
FITEM,5,-284
FITEM,5,321
FITEM,5,557
FITEM,5,568
FITEM,5,570
FITEM,5,-572
FITEM,5,574
FITEM,5,-577
FITEM,5,701
FITEM,5,711
FITEM,5,-713
FITEM,5,719
FITEM,5,722
FITEM,5,-724
FITEM,5,732
CM,_Y,AREA
ASEL,...,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2

```

! 7th Bolster

```

FLST,5,4,4,ORDE,3
FITEM,5,603
FITEM,5,1464
FITEM,5,-1466
CM,_Y,LINE
LSEL,...,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,...,4,1,

```


! Sizing lines in Exhaust Hole (8th bolster)

```
CMDEL_Y
CMDEL_Y1

MSHKEY,0
FLST,5,30,5,ORDE,26
FITEM,5,74
FITEM,5,80
FITEM,5,86
FITEM,5,88
FITEM,5,93
FITEM,5,111
FITEM,5,113
FITEM,5,161
FITEM,5,258
FITEM,5,261
FITEM,5,264
FITEM,5,266
FITEM,5,268
FITEM,5,274
FITEM,5,278
FITEM,5,280
FITEM,5,282
FITEM,5,293
FITEM,5,550
FITEM,5,556
FITEM,5,558
FITEM,5,-561
FITEM,5,563
FITEM,5,-566
FITEM,5,721
FITEM,5,733
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2
```

! 8th Bolster

```
MSHKEY,0
FLST,5,18,5,ORDE,13
FITEM,5,96
FITEM,5,-101
FITEM,5,114
FITEM,5,-116
FITEM,5,159
FITEM,5,162
FITEM,5,189
FITEM,5,201
FITEM,5,259
FITEM,5,551
FITEM,5,-552
FITEM,5,554
FITEM,5,-555
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2
```

! Front (9th) Bolster

```
!-----
!----- Wall Corner Section
!-----
```

SMRTSIZE,6

! Mesh Setting

```
MSHAPE,1,2D
CM,_Y,AREA
ASEL,,, 197
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2
CM,_Y,AREA
ASEL,,, 158
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2
CM,_Y,AREA
ASEL,,, 160
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2
CM,_Y,AREA
ASEL,,, 163
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2
CM,_Y,AREA
ASEL,,, 164
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2
CM,_Y,AREA
ASEL,,, 166
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2
CM,_Y,AREA
ASEL,,, 225
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2
Exhaust Hole Regions
```

! Triangular Mesh on

MSHAPE,0,2D

FLST,5,95,5,ORDE,36

FITEM,5,6

FITEM,5,16

FITEM,5,30

FITEM,5,-32

FITEM,5,38

FITEM,5,61

FITEM,5,90

FITEM,5,92

FITEM,5,94

FITEM,5,145

FITEM,5,158

FITEM,5,160

FITEM,5,163

FITEM,5,-164

FITEM,5,166

FITEM,5,-182

FITEM,5,184

FITEM,5,186

FITEM,5,188

FITEM,5,190

FITEM,5,192

FITEM,5,195

FITEM,5,-198

FITEM,5,200

FITEM,5,202

FITEM,5,205

FITEM,5,-238

FITEM,5,240

FITEM,5,-250

FITEM,5,296

FITEM,5,305

FITEM,5,-306

FITEM,5,334

FITEM,5,-335

FITEM,5,376

FITEM,5,378

CM,_Y,AREA

ASEL,,,P51X

CM,_Y1,AREA

CHKMSH,'AREA'

CMSEL,S,_Y

AMESH,_Y2

CMDEL,_Y

CMDEL,_Y1

CMDEL,_Y2 ! Quad Mesh on Rest of Corner Areas

----- Canopy Support Beam

SMRTSIZE,6

! Mesh Setting

FLST,5,34,5,ORDE,22

FITEM,5,326

FITEM,5,-327

FITEM,5,340

FITEM,5,344

FITEM,5,351

FITEM,5,398

FITEM,5,368

FITEM,5,371

FITEM,5,398

FITEM,5,408

FITEM,5,426

FITEM,5,428

FITEM,5,430

FITEM,5,432

FITEM,5,434

FITEM,5,441

FITEM,5,-443

FITEM,5,496

FITEM,5,498

FITEM,5,-510

FITEM,5,513

FITEM,5,-514

CM,_Y,AREA

ASEL,,,P51X

CM,_Y1,AREA

CHKMSH,'AREA'

CMSEL,S,_Y

AMESH,_Y1

CMDEL,_Y

CMDEL,_Y1

CMDEL,_Y2

! Meshing Box Beam

FLST,5,8,4,ORDE,8

FITEM,5,732

FITEM,5,1042

FITEM,5,1068

FITEM,5,1073

FITEM,5,1075

FITEM,5,1077

FITEM,5,1079

FITEM,5,1081

CM,_Y,LINE

LSEL,,,P51X

CM,_Y1,LINE

CMSEL,,,Y

LESIZE,_Y1,,,10,1,

! 10 Div's on Fillet Lines

CMDEL,_Y

CMDEL,_Y1

FLST,5,4,5,ORDE,4

FITEM,5,453

FITEM,5,511

FITEM,5,-512

FITEM,5,515

CM,_Y,AREA

ASEL,,,P51X

CM,_Y1,AREA

CHKMSH,'AREA'

CMSEL,S,_Y

AMESH,_Y1

CMDEL,_Y

CMDEL,_Y1

CMDEL,_Y2

! Meshing Rounded Fillet Areas

/UI,MESH,OFF

FLST,5,8,5,ORDE,8

FITEM,5,336

FITEM,5,348

FITEM,5,355

FITEM,5,362

FITEM,5,451

FITEM,5,458

FITEM,5,464

FITEM,5,470

CM,_Y,AREA

ASEL,,,P51X

CM,_Y1,AREA

CHKMSH,'AREA'

CMSEL,S,_Y

AMESH,_Y1

CMDEL,_Y

CMDEL,_Y1

CMDEL,_Y2

! Meshing Fillet Side Areas

/UI,MESH,OFF

FLST,5,67,5,ORDE,40

FITEM,5,289
 FITEM,5,291
 FITEM,5,326
 FITEM,5,-329
 FITEM,5,336
 FITEM,5,340
 FITEM,5,344
 FITEM,5,348
 FITEM,5,351
 FITEM,5,355
 FITEM,5,358
 FITEM,5,362
 FITEM,5,368
 FITEM,5,371
 FITEM,5,375
 FITEM,5,398
 FITEM,5,408
 FITEM,5,426
 FITEM,5,428
 FITEM,5,430
 FITEM,5,432
 FITEM,5,434
 FITEM,5,441
 FITEM,5,-444
 FITEM,5,451
 FITEM,5,-453
 FITEM,5,457
 FITEM,5,-460
 FITEM,5,464
 FITEM,5,467
 FITEM,5,470
 FITEM,5,-473
 FITEM,5,477
 FITEM,5,496
 FITEM,5,498
 FITEM,5,-515
 FITEM,5,517
 FITEM,5,519
 FITEM,5,521
 FITEM,5,-524
 CM,_Y,AREA
 ASEL,...,P51X
 CM,_Y1,AREA
 CHKMSH,'AREA'
 CMSEL,S,_Y
 AMESH,_Y2
 CMDEL,_Y
 CMDEL,_Y1
 CMDEL,_Y2 ! Meshing Rest of Canopy Support

 ----- Eyebrow of Canopy

SMRTSIZE,10 ! Mesh Setting

FLST,5,35,5,ORDE,14
 FITEM,5,399
 FITEM,5,-407
 FITEM,5,410
 FITEM,5,-425
 FITEM,5,427
 FITEM,5,429
 FITEM,5,431
 FITEM,5,433
 FITEM,5,435
 FITEM,5,-436
 FITEM,5,445
 FITEM,5,-446
 FITEM,5,454

FITEM,5,-455
 CM,_Y,AREA
 ASEL,...,P51X
 CM,_Y1,AREA
 CHKMSH,'AREA'
 CMSEL,S,_Y
 AMESH,_Y1
 CMDEL,_Y
 CMDEL,_Y1
 CMDEL,_Y2

 ----- Front / Floor Corner

SMRTSIZE,6 ! Mesh Setting

MSHKEY,0
 FLST,5,40,5,ORDE,34
 FITEM,5,15
 FITEM,5,-17
 FITEM,5,31
 FITEM,5,183
 FITEM,5,-184
 FITEM,5,334
 FITEM,5,-335
 FITEM,5,337
 FITEM,5,-338
 FITEM,5,342
 FITEM,5,-343
 FITEM,5,345
 FITEM,5,349
 FITEM,5,-350
 FITEM,5,352
 FITEM,5,356
 FITEM,5,-357
 FITEM,5,359
 FITEM,5,363
 FITEM,5,-365
 FITEM,5,370
 FITEM,5,376
 FITEM,5,-380
 FITEM,5,382
 FITEM,5,-383
 FITEM,5,385
 FITEM,5,-386
 FITEM,5,389
 FITEM,5,393
 FITEM,5,-394
 FITEM,5,533
 FITEM,5,586
 FITEM,5,592
 FITEM,5,-594
 CM,_Y,AREA
 ASEL,...,P51X
 CM,_Y1,AREA
 CHKMSH,'AREA'
 CMSEL,S,_Y
 AMESH,_Y2
 CMDEL,_Y
 CMDEL,_Y1
 CMDEL,_Y2

 ----- Floor Plate Areas

SMRTSIZE,3 ! Mesh Setting

MSHKEY,0

FLST,5,57,5,ORDE,46

FITEM,5,3
FITEM,5,34
FITEM,5,-37
FITEM,5,39
FITEM,5,-43
FITEM,5,45
FITEM,5,53
FITEM,5,59
FITEM,5,62
FITEM,5,67
FITEM,5,89
FITEM,5,106
FITEM,5,126
FITEM,5,150
FITEM,5,-153
FITEM,5,155
FITEM,5,-157
FITEM,5,185
FITEM,5,191
FITEM,5,193
FITEM,5,-194
FITEM,5,204
FITEM,5,262
FITEM,5,269
FITEM,5,-271
FITEM,5,273
FITEM,5,275
FITEM,5,-276
FITEM,5,285
FITEM,5,-286
FITEM,5,342
FITEM,5,-343
FITEM,5,349
FITEM,5,-350
FITEM,5,356
FITEM,5,-357
FITEM,5,544
FITEM,5,547
FITEM,5,573
FITEM,5,582
FITEM,5,662
FITEM,5,665
FITEM,5,699
FITEM,5,-700
FITEM,5,702
FITEM,5,-705
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y2
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2

----- Side Wall Areas

SMRTSIZE,7 ! Mesh Setting

MSHKEY,0
FLST,5,39,5,ORDE,19
FITEM,5,239
FITEM,5,289
FITEM,5,-292
FITEM,5,294
FITEM,5,-295

FITEM,5,297
FITEM,5,-304
FITEM,5,307
FITEM,5,-312
FITEM,5,314
FITEM,5,-315
FITEM,5,317
FITEM,5,-320
FITEM,5,322
FITEM,5,-325
FITEM,5,690
FITEM,5,-692
FITEM,5,694
FITEM,5,-698
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y2
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2

----- Canopy Brace

SMRTSIZE,7 ! Mesh Setting

MSHKEY,0
FLST,5,11,5,ORDE,8
FITEM,5,339
FITEM,5,341
FITEM,5,478
FITEM,5,529
FITEM,5,-530
FITEM,5,535
FITEM,5,539
FITEM,5,-543
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
ACLEAR,_Y1
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2

----- Front Wall Areas

SMRTSIZE,6 ! Mesh Setting

MSHKEY,0
FLST,5,126,5,ORDE,39
FITEM,5,15
FITEM,5,-17
FITEM,5,31
FITEM,5,183
FITEM,5,-184
FITEM,5,187
FITEM,5,289
FITEM,5,291
FITEM,5,326
FITEM,5,-342
FITEM,5,344

FITEM,5,-348
 FITEM,5,351
 FITEM,5,-398
 FITEM,5,408
 FITEM,5,426
 FITEM,5,428
 FITEM,5,430
 FITEM,5,432
 FITEM,5,434
 FITEM,5,441
 FITEM,5,-443
 FITEM,5,451
 FITEM,5,458
 FITEM,5,464
 FITEM,5,470
 FITEM,5,496
 FITEM,5,498
 FITEM,5,-510
 FITEM,5,513
 FITEM,5,-514
 FITEM,5,516
 FITEM,5,-521
 FITEM,5,528
 FITEM,5,530
 FITEM,5,-536
 FITEM,5,586
 FITEM,5,592
 FITEM,5,-594
 CM,_Y,AREA
 ASEL,...,P51X
 CM,_Y1,AREA
 CHKMSH,'AREA'
 CMSEL,S,_Y
 AMESH,_Y2
 CMDEL,_Y
 CMDEL,_Y1
 CMDEL,_Y2

|-----
----- Rest of Canopy

SMRTSIZE,7

| Mesh Setting

MSHKEY,0
 FLST,5,157,5,ORDE,25
 FITEM,5,289
 FITEM,5,-292
 FITEM,5,326
 FITEM,5,-330
 FITEM,5,336
 FITEM,5,340
 FITEM,5,344
 FITEM,5,348
 FITEM,5,351
 FITEM,5,355
 FITEM,5,358
 FITEM,5,362
 FITEM,5,368
 FITEM,5,371
 FITEM,5,375
 FITEM,5,398
 FITEM,5,-515
 FITEM,5,517
 FITEM,5,519
 FITEM,5,521
 FITEM,5,-527
 FITEM,5,529
 FITEM,5,532
 FITEM,5,536

FITEM,5,-543
 CM,_Y,AREA
 ASEL,...,P51X
 CM,_Y1,AREA
 CHKMSH,'AREA'
 CMSEL,S,_Y
 AMESH,_Y2
 CMDEL,_Y
 CMDEL,_Y1
 CMDEL,_Y2

|-----
----- Exhaust Plenum

SMRTSIZE,1

MSHKEY,0
 FLST,5,7,5,ORDE,7
 FITEM,5,95
 FITEM,5,645
 FITEM,5,-646
 FITEM,5,652
 FITEM,5,-653
 FITEM,5,676
 FITEM,5,718
 CM,_Y,AREA
 ASEL,...,P51X
 CM,_Y1,AREA
 CHKMSH,'AREA'
 CMSEL,S,_Y
 AMESH,_Y1
 CMDEL,_Y
 CMDEL,_Y1
 CMDEL,_Y2

SMRTSIZE,6

MSHKEY,0
 FLST,5,4,5,ORDE,4
 FITEM,5,83
 FITEM,5,91
 FITEM,5,103
 FITEM,5,-104
 CM,_Y,AREA
 ASEL,...,P51X
 CM,_Y1,AREA
 CHKMSH,'AREA'
 CMSEL,S,_Y
 AMESH,_Y1
 CMDEL,_Y
 CMDEL,_Y1
 CMDEL,_Y2

|-----
----- Rest of Structure

SMRTSIZE,7

| Mesh Setting

MSHKEY,0
 FLST,5,743,5,ORDE,11
 FITEM,5,1
 FITEM,5,-106
 FITEM,5,108
 FITEM,5,110
 FITEM,5,-719
 FITEM,5,721
 FITEM,5,-729
 FITEM,5,732

```

FITEM,5,-733
FITEM,5,750
FITEM,5,-764
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CHKMSH,AREA
CMSEL,S,_Y
AMESH,_Y2
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2

```

```

|-----
|----- Refining Mesh on 5th Bolster
|-----

```

```

ALLSEL,ALL
FLST,5,18,5,ORDE,14
FITEM,5,72
FITEM,5,75
FITEM,5,-77
FITEM,5,102
FITEM,5,578
FITEM,5,585
FITEM,5,587
FITEM,5,-591
FITEM,5,706
FITEM,5,-707
FITEM,5,714
FITEM,5,-715
FITEM,5,728
FITEM,5,-729
ASEL,R,,,P51X
CM,Bolster,AREA

```

```

ALLSEL,ALL      ! Created Bolster Component
                  ! Note : No refinement

```

```

|-----
|----- Reversing Area Normals as Required
|-----

```

```

FLST,5,11,5,ORDE,11
FITEM,5,187
FITEM,5,317
FITEM,5,323
FITEM,5,381
FITEM,5,387
FITEM,5,390
FITEM,5,392
FITEM,5,395
FITEM,5,442
FITEM,5,690
FITEM,5,694
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMDEL,_Y
AREVERSE,_Y1,0
CMDEL,_Y1

```

```

! Reversed Some Area Normals Inside Box

```

```

FLST,5,7,5,ORDE,6
FITEM,5,409
FITEM,5,437
FITEM,5,-439
FITEM,5,448
FITEM,5,456
FITEM,5,483

```

```

CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMDEL,_Y
AREVERSE,_Y1,0
CMDEL,_Y1

```

```

! Reversed Some Area Normals on Canopy

```

```

FLST,5,11,5,ORDE,11
FITEM,5,97
FITEM,5,-98
FITEM,5,101
FITEM,5,114
FITEM,5,189
FITEM,5,201
FITEM,5,259
FITEM,5,551
FITEM,5,-552
FITEM,5,614
FITEM,5,626
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMDEL,_Y
AREVERSE,_Y1,0
CMDEL,_Y1
FLST,5,14,5,ORDE,12
FITEM,5,74
FITEM,5,80
FITEM,5,161
FITEM,5,258
FITEM,5,261
FITEM,5,264
FITEM,5,274
FITEM,5,293
FITEM,5,550
FITEM,5,556
FITEM,5,558
FITEM,5,-561
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMDEL,_Y
AREVERSE,_Y1,0
CMDEL,_Y1
FLST,5,14,5,ORDE,11
FITEM,5,87
FITEM,5,321
FITEM,5,557
FITEM,5,568
FITEM,5,570
FITEM,5,-572
FITEM,5,574
FITEM,5,-577
FITEM,5,701
FITEM,5,711
FITEM,5,724
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMDEL,_Y
AREVERSE,_Y1,0
CMDEL,_Y1
FLST,5,10,5,ORDE,10
FITEM,5,79

```

```

FITEM.5,313
FITEM.5,316
FITEM.5,567
FITEM.5,579
FITEM.5,581
FITEM.5,583
FITEM.5,-584
FITEM.5,708
FITEM.5,727
CM_YAREA
ASEL,,,P51X
CM_Y1AREA
CMSEL,S,Y
CMDEL,Y
AREVERSE,_Y1,0
CMDEL,_Y1
FLST,5,8,5,ORDE,5
FITEM.5,73
FITEM.5,77
FITEM.5,585
FITEM.5,587
FITEM.5,-591
CM_YAREA
ASEL,,,P51X
CM_Y1AREA
CMSEL,S,Y
CMDEL,_Y
AREVERSE,_Y1,0
CMDEL,_Y1
FLST,5,11,5,ORDE,9
FITEM.5,8
FITEM.5,21
FITEM.5,24
FITEM.5,26
FITEM.5,123
FITEM.5,125
FITEM.5,128
FITEM.5,130
FITEM.5,-133
CM_YAREA
ASEL,,,P51X
CM_Y1AREA
CMSEL,S,Y
CMDEL,_Y
AREVERSE,_Y1,0
CMDEL,_Y1
FLST,5,10,5,ORDE,8
FITEM.5,12
FITEM.5,-13
FITEM.5,18
FITEM.5,-20
FITEM.5,27
FITEM.5,117
FITEM.5,120
FITEM.5,-122
CM_YAREA
ASEL,,,P51X
CM_Y1AREA
CMSEL,S,Y
CMDEL,_Y
AREVERSE,_Y1,0
CMDEL,_Y1
FLST,5,12,5,ORDE,12
FITEM.5,4
FITEM.5,7
FITEM.5,48
FITEM.5,-49
FITEM.5,58
FITEM.5,60
FITEM.5,68

FITEM.5,251
FITEM.5,553
FITEM.5,562
FITEM.5,627
FITEM.5,660
CM_YAREA
ASEL,,,P51X
CM_Y1AREA
CMSEL,S,Y
CMDEL,_Y
AREVERSE,_Y1,0
CMDEL,_Y1      ! Reversed Normals on Bolsters

FLST,5,19,5,ORDE,19
FITEM.5,11
FITEM.5,51
FITEM.5,64
FITEM.5,137
FITEM.5,139
FITEM.5,149
FITEM.5,165
FITEM.5,549
FITEM.5,625
FITEM.5,631
FITEM.5,-632
FITEM.5,636
FITEM.5,642
FITEM.5,651
FITEM.5,656
FITEM.5,658
FITEM.5,669
FITEM.5,672
FITEM.5,674
CM_YAREA
ASEL,,,P51X
CM_Y1AREA
CMSEL,S,Y
CMDEL,_Y
AREVERSE,_Y1,0
CMDEL,_Y1
FLST,5,20,5,ORDE,20
FITEM.5,29
FITEM.5,56
FITEM.5,-57
FITEM.5,140
FITEM.5,142
FITEM.5,148
FITEM.5,154
FITEM.5,364
FITEM.5,592
FITEM.5,618
FITEM.5,-619
FITEM.5,621
FITEM.5,628
FITEM.5,633
FITEM.5,637
FITEM.5,648
FITEM.5,663
FITEM.5,668
FITEM.5,670
FITEM.5,688
CM_YAREA
ASEL,,,P51X
CM_Y1AREA
CMSEL,S,Y
CMDEL,_Y
AREVERSE,_Y1,0
CMDEL,_Y1
CM_YAREA
ASEL,,, 623

```

```

CM,_Y1,AREA
CMSEL,S,_Y
CMDEL,_Y
AREVERSE,_Y1,0
CMDEL,_Y1
! Reversed Some Normals on STR's

```

```

|-----|
|----- Correction -----|
|-----|

```

```

! Removing STR Area and Elements from the Inside of
! small Bolsters in the hinge pivot structure...

```

```

FLST,2,2,5,ORDE,2
FITEM,2,686
FITEM,2,-687
ACLEAR,P51X ! Clearing Meshed Areas

```

```

FLST,2,2,5,ORDE,2
FITEM,2,686
FITEM,2,-687
ADELE,P51X ! Deleting Areas only

```

```

FINISH
FINISH

```

```

*SET,nodes,ndimg(0,12)
*SET,elems,elimg(0,12)
*SET,sol_time,(((3e-
8)*(nodes**2))+0.0005*nodes+0.022)/60

```

```

/EOF

```

```

|-----|
|-----|

```


❖ Filename: 4_3_FEA_support_INPUT

```

@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
!      FEA of 930E Truck Box Structure
!      Support BC's Routine
!@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
FINISH
FINISH

/PREP7
*AFUN,RAD

DOFSEL,S,UY
DCUM,ADD,1,,0, ! Set DOF Accumulation to ADD
DOFSEL,ALL

*SET,displspe,(UyPin-UyNose)/(-3490-(-7730))
! Slope of Uy along Z
*SET,intecept,UyPin-displspe*(-3490)

!-----
!----- Hinge Support Conditions
!-----

*IF,hingetyp,EQ,1,THEN

    FLST,5,4,4,ORDE,4
    FITEM,5,325
    FITEM,5,330
    FITEM,5,339
    FITEM,5,342
    LSEL,S,,,P51X
    NSLL,S,1
    *GET,count,NODE,0,COUNT
    *GET,Nindex,NODE,0,NUM,MIN
    *DO,index,0,count+10,1
        /GOPR ! Resume Print to Output
        *GET,Zloc,NODE,Nindex,LOC,Z
    D,Nindex,UY,(displspe*(Zloc)+intecept)
    *GET,Next,NODE,Nindex,NXTH
    *IF,Next,EQ,0,EXIT
    *SET,Nindex,Next
    /NOPR ! Suspend Print to Output
*ENDDO
ALLSEL,ALL ! Bearing Force on Top of Pin

!FLST,2,4,4,ORDE,4
!FITEM,2,325
!FITEM,2,330
!FITEM,2,339
!FITEM,2,342
!DL,P51X,,UY,UyPin
! Bearing Force on Top of Pin

FLST,2,4,4,ORDE,4
FITEM,2,325
FITEM,2,328
FITEM,2,339
FITEM,2,-340
DL,P51X,,UZ,
! Preventing Forward Movement

*ELSEIF,hingetyp,EQ,2,THEN

    *IF,CE_DONE,NE,1,THEN

        N,70000,601*(984-601)/2,-.197*(-
364+197)/2,-3490,...
        KNODE,0, 70000

FLST,2,3,3
FITEM,2,194
FITEM,2,1018
FITEM,2,189
A,P51X

TYPE, 1
MAT, 1
REAL, 9
ESYS, 0
SECNUM,

KL,2050,5,,
KL,2051,5,,
KL,2052,5,,
FLST,3,3,3,ORDE,2
FITEM,3,1019
FITEM,3,-1021
NKPT,0,P51X
FLST,2,8,1
FITEM,2,17
FITEM,2,70000
FITEM,2,5
FITEM,2,5
FITEM,2,70001
FITEM,2,70002
FITEM,2,5
FITEM,2,70003
E,P51X
! Creating Element In Hinge (for CERIG)

FLST,2,21,1
FITEM,2,70000
FITEM,2,17
FITEM,2,240
FITEM,2,241
FITEM,2,242
FITEM,2,243
FITEM,2,244
FITEM,2,245
FITEM,2,246
FITEM,2,247
FITEM,2,248
FITEM,2,249
FITEM,2,250
FITEM,2,251
FITEM,2,252
FITEM,2,253
FITEM,2,254
FITEM,2,255
FITEM,2,256
FITEM,2,257
FITEM,2,258
FITEM,2,18
CERIG,P51X,,ALL,... ! Outside Top-Rear

FLST,2,21,1
FITEM,2,70000
FITEM,2,17
FITEM,2,315
FITEM,2,314
FITEM,2,313
FITEM,2,312
FITEM,2,311
FITEM,2,310
FITEM,2,309
FITEM,2,308

```

FITEM,2,307
 FITEM,2,306
 FITEM,2,305
 FITEM,2,304
 FITEM,2,303
 FITEM,2,302
 FITEM,2,301
 FITEM,2,300
 FITEM,2,299
 FITEM,2,298
 FITEM,2,297
 FITEM,2,20
 CERIG,P51X, ,ALL, , , ! Outside Top-Front

FLST,2,21,1
 FITEM,2,70000
 FITEM,2,18
 FITEM,2,259
 FITEM,2,260
 FITEM,2,261
 FITEM,2,262
 FITEM,2,263
 FITEM,2,264
 FITEM,2,265
 FITEM,2,266
 FITEM,2,267
 FITEM,2,268
 FITEM,2,269
 FITEM,2,270
 FITEM,2,271
 FITEM,2,272
 FITEM,2,273
 FITEM,2,274
 FITEM,2,275
 FITEM,2,276
 FITEM,2,277
 !FITEM,2,19
 CERIG,P51X, ,ALL, , ,
 ! Outside Bottom-Rear

FLST,2,21,1
 FITEM,2,70000
 FITEM,2,19
 FITEM,2,278
 FITEM,2,279
 FITEM,2,280
 FITEM,2,281
 FITEM,2,282
 FITEM,2,283
 FITEM,2,284
 FITEM,2,285
 FITEM,2,286
 FITEM,2,287
 FITEM,2,288
 FITEM,2,289
 FITEM,2,290
 FITEM,2,291
 FITEM,2,292
 FITEM,2,293
 FITEM,2,294
 FITEM,2,295
 FITEM,2,296
 !FITEM,2,20
 CERIG,P51X, ,ALL, , ,
 ! Outside Bottom-Front

FLST,2,21,1
 FITEM,2,70000
 FITEM,2,6
 FITEM,2,61

FITEM,2,60
 FITEM,2,59
 FITEM,2,58
 FITEM,2,57
 FITEM,2,56
 FITEM,2,55
 FITEM,2,54
 FITEM,2,53
 FITEM,2,52
 FITEM,2,51
 FITEM,2,50
 FITEM,2,49
 FITEM,2,48
 FITEM,2,47
 FITEM,2,46
 FITEM,2,45
 FITEM,2,44
 FITEM,2,43
 !FITEM,2,5
 CERIG,P51X, ,ALL, , , ! Inside Top-Rear

FLST,2,21,1
 FITEM,2,70000
 !FITEM,2,11
 FITEM,2,111
 FITEM,2,112
 FITEM,2,113
 FITEM,2,114
 FITEM,2,115
 FITEM,2,116
 FITEM,2,117
 FITEM,2,118
 FITEM,2,119
 FITEM,2,120
 FITEM,2,121
 FITEM,2,122
 FITEM,2,123
 FITEM,2,124
 FITEM,2,125
 FITEM,2,126
 FITEM,2,127
 FITEM,2,128
 FITEM,2,129
 FITEM,2,5
 CERIG,P51X, ,ALL, , , ! Inside Top-Front

FLST,2,21,1
 FITEM,2,70000
 FITEM,2,10
 FITEM,2,91
 FITEM,2,90
 FITEM,2,89
 FITEM,2,88
 FITEM,2,87
 FITEM,2,86
 FITEM,2,85
 FITEM,2,84
 FITEM,2,83
 FITEM,2,82
 FITEM,2,81
 FITEM,2,80
 FITEM,2,79
 FITEM,2,78
 FITEM,2,77
 FITEM,2,76
 FITEM,2,75
 FITEM,2,74
 FITEM,2,73
 !FITEM,2,6
 CERIG,P51X, ,ALL, , , ! Inside Bottom-Rear

```

FLST,2,21,1
FITEM,2,70000
FITEM,2,11
FITEM,2,110
FITEM,2,109
FITEM,2,108
FITEM,2,107
FITEM,2,106
FITEM,2,105
FITEM,2,104
FITEM,2,103
FITEM,2,102
FITEM,2,101
FITEM,2,100
FITEM,2,99
FITEM,2,98
FITEM,2,97
FITEM,2,96
FITEM,2,95
FITEM,2,94
FITEM,2,93
FITEM,2,92
FITEM,2,10
CERIG,P51X,,ALL,,...! Inside Bottom-Front

*SET,CE_DONE,1

*ENDIF

D,70000,UY,((dispslpe*(-3490))+intcept)
D,70000,UZ,0
D,70000,ROTY,0
D,70000,ROTZ,0

*ENDIF

=====
|----- Stringer (STR) Support Conditions
|=====

*IF,STRtype,EQ,1,THEN
  FLST,2,32,5,ORDE,2
  FITEM,2,1000
  FITEM,2,-1031
  DA,P51X,UY,UyNose
  ! Distributed STR Support
*ELSEIF,STRtype,EQ,2,THEN
  FLST,5,16,4,ORDE,16
  FITEM,5,2002
  FITEM,5,2006
  FITEM,5,2009
  FITEM,5,2012
  FITEM,5,2015
  FITEM,5,2018
  FITEM,5,2021
  FITEM,5,2024
  FITEM,5,2027
  FITEM,5,2030
  FITEM,5,2033
  FITEM,5,2036
  FITEM,5,2039
  FITEM,5,2042
  FITEM,5,2046
  FITEM,5,2049
  LSEL,S,,P51X
  ! Selecting STR CenterLines
  NSLL,S,1! Selecting nodes attached to Lines

*GET,count,NODE,0,COUNT

*GET,Nindex,NODE,0,NUM,MIN
*DO,index,0,count+10,1
  !GOPR ! Resume Print to Output
  *GET,Zloc,NODE,Nindex,LOC,Z

D,Nindex,UY,(dispslpe*(Zloc)+intcept)
*GET,Next,NODE,Nindex,NXTH
*IF,Next,EQ,0,EXIT
*SET,Nindex,Next
!NOPR ! Suspend Print to Output

*ENDDO
ALLSEL,ALL
*ELSEIF,STRtype,EQ,3,THEN

FINISH
/PREP7

*IF,Rub_DONE,NE,1,THEN
  ! Material #2
  UIMP,2,EX,,.207000/100,
  ! Modulus in N/mm*2
  ! 1/100th of Steel
  UIMP,2,DENS,,.0.00000786,
  ! Density in kg/mm*3
  UIMP,2,ALPX,...
  UIMP,2,REFT,...
  UIMP,2,NUXY,...
  UIMP,2,PRXY,...,0.3,
  UIMP,2,GXY,...
  UIMP,2,MU,...
  UIMP,2,DAMP,...

  MAT, 2

  ET,2,SOLID95
  KEYOPT,2,5,0
  KEYOPT,2,6,0
  KEYOPT,2,11,0
  EXTOPT,ESIZE,1,1,
  EXTOPT,ACLEAR,0
  FLST,2,32,5,ORDE,2
  FITEM,2,1000
  FITEM,2,-1031
  VEXT,P51X,,.0,-25,4,0,...
  ESLV,S

*SET,Rub_DONE,1

*ENDIF

ALLSEL,ALL
ALLSEL,BELOW,VOLU

CSYS,0 ! Active CS is Global Cartesian
NSEL,S,LOC,Y,-465.5,-465.3

*GET,count,NODE,0,COUNT
  ! Frame Disp. BC's
*GET,Nindex,NODE,0,NUM,MIN
*DO,index,0,count+10,1
  !GOPR ! Resume Print to Output
  *GET,Zloc,NODE,Nindex,LOC,Z

D,Nindex,UY,(dispslpe*(Zloc)+intcept)
*GET,Next,NODE,Nindex,NXTH
*IF,Next,EQ,0,EXIT
*SET,Nindex,Next
!NOPR ! Suspend Print to Output

*ENDDO

```

```

*IF,Shim,EQ,1,THEN
! Adding Shim Displacements
! Shim Values From Optimum Slope...
! *SET,deltamax,4.5
! *SET,shimslope,deltamax/(7730-
3490)

! *SET,shimintc,deltamax*7730/(7730-3490)
! *SET,shim_1,0.324976415
! *SET,shim_2,0.974929245
! *SET,shim_3,1.62488208
! *SET,shim_4,2.2748349
! *SET,shim_5,2.92478774

! Trial Shim Values
! *SET,shim_1,0.0
! *SET,shim_2,1.5
! *SET,shim_3,2.0
! *SET,shim_4,2.5
! *SET,shim_5,3.0

! Trial Shim Values
*SET,shim_1,Amt_Shim
*SET,shim_2,Amt_Shim
*SET,shim_3,Amt_Shim
*SET,shim_4,Amt_Shim
*SET,shim_5,Amt_Shim

! Shim Displacement Routine
*GET,count,NODE,0,COUNT
*GET,Nindex,NODE,0,NUM,MIN
*DO,index,0,count+10,1
    *GET,Zloc,NODE,Nindex,LOC,Z
    !D,Nindex,U,Y,(shimslope)*(Zloc)+shi
mintc)

    *IF,Zloc,GE,-5280.4,THEN
        D,Nindex,U,Y,shim_5
    *ELSEIF,Zloc,GE,-5892.8,THEN
        D,Nindex,U,Y,shim_4
    *ELSEIF,Zloc,GE,-6505.2,THEN
        D,Nindex,U,Y,shim_3
    *ELSEIF,Zloc,GE,-7117.6,THEN
        D,Nindex,U,Y,shim_2
    *ELSE
        D,Nindex,U,Y,shim_1
    *ENDIF
    *GET,Next,NODE,Nindex,NXTH
    *IF,Next,EQ,0,EXIT
    *SET,Nindex,Next
*ENDDO

*ENDIF

ALLSEL,ALL

*ENDIF

!-----
!----- Guide Pin Conditions
!-----

FLST,2,1.5,ORDE,1
FITEM,2,763
/GO
DAP,P51X,UX,0 ! Ux=0 on Guide Pin

!-----
!----- Nose Load Cell
!-----

```

```

*IF,Loadcell,EQ,1,THEN
*IF,Rub_DONE,EQ,1,THEN
*IF,Ldc_DONE,NE,1,THEN

!-----
! Start Making Load Cell #1
!-----

FLST,2,2.5,ORDE,2
FITEM,2,593
FITEM,2,595
ACLEAR,P51X
FLST,2,2.5,ORDE,2
FITEM,2,593
FITEM,2,595
ADELE,P51X,,1
! Clearing and Deleting Side Areas

KW/PLAN,-1, 153, 154, 1023
wpoff,0.0,-25.4*3
! Using CPlane to Cut Nose..

FLST,2,2.6,ORDE,2
FITEM,2,1
FITEM,2,-2
VCLEAR,P51X
FLST,2,2.5,ORDE,2
FITEM,2,1000
FITEM,2,-1001
ACLEAR,P51X
VCLEAR, 3
ACLEAR, 1002
ACLEAR, 183
VCLEAR, 4
! Clearing Mesh to Operate on Geom

VSWB, 1 ! Cutting Volume

FLST,3,2.3,ORDE,2
FITEM,3,153
FITEM,3,1075
KGEN,2,P51X,, ,25.4*3,, ,0 ! Copy KP's

LSTR, 1075, 1080
LSTR, 153, 1079
LSTR, 1079, 1080 ! Box End Lines
LSTR, 1079, 616
LSTR, 1080, 621
FLST,2,4,4
FITEM,2,2202
FITEM,2,2053
FITEM,2,531
FITEM,2,186
AL,P51X
FLST,2,4,4
FITEM,2,244
FITEM,2,2202
FITEM,2,2055
FITEM,2,2203
AL,P51X
FLST,2,5,4
FITEM,2,2203
FITEM,2,1149
FITEM,2,2002
FITEM,2,2198
FITEM,2,192
AL,P51X
FLST,2,4,4
FITEM,2,2002
FITEM,2,2055

```

```

FITEM,2,2053
FITEM,2,2190
AL,P51X      ! Patching Up Areas

K,0,-440,-0.7731464844E+04,
K,0,-440,-0.7655253802E+04,
K,0,-363.8,-0.7731464844E+04,
K,0,-363.8,-0.7655253802E+04,

LSTR,1063,1084
LSTR,1064,1082
LSTR,1062,1081
LSTR,1061,1083
LSTR,1063,1079
LSTR,1060,1084
LSTR,1062,1075
LSTR,153,1081
FLST,2,4,4
FITEM,2,2209
FITEM,2,2208
FITEM,2,2204
FITEM,2,2055
AL,P51X
FLST,2,4,4
FITEM,2,2211
FITEM,2,2053
FITEM,2,2207
FITEM,2,2208
AL,P51X
FLST,2,4,4
FITEM,2,2211
FITEM,2,2210
FITEM,2,2206
FITEM,2,2190
AL,P51X
FLST,2,4,4
FITEM,2,2209
FITEM,2,2210
FITEM,2,2205
FITEM,2,2002
AL,P51X      ! Creating Square Pipe Areas

FLST,5,4,5,ORDE,4
FITEM,5,1000
FITEM,5,1033
FITEM,5,-1034
FITEM,5,1036
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1      ! STR Side Areas
AATT,1,19,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1
FLST,5,5,5,ORDE,4
FITEM,5,1001
FITEM,5,-1003
FITEM,5,1149
FITEM,5,1154
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1      ! STR Bottom Areas
AATT,1,25,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1

```

```

R,2,1.875,.,.,.,. ! Define Pipe Thickness

FLST,5,4,5,ORDE,2
FITEM,5,1158
FITEM,5,-1161
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1      ! Pipe Thickness
AATT,1,2,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1

FLST,5,4,4,ORDE,4
FITEM,5,2002
FITEM,5,2053
FITEM,5,2056
FITEM,5,2190
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,,Y
LESIZE,_Y1,,.4,1,
CMDELE,_Y
CMDELE,_Y1
FLST,5,4,4,ORDE,2
FITEM,5,2208
FITEM,5,-2211
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,,Y
LESIZE,_Y1,,.10,1, ! Pipe Lsize Commands
CMDELE,_Y
CMDELE,_Y1

APLOT

MSHKEY,0
FLST,5,9,5,ORDE,8
FITEM,5,183
FITEM,5,1000
FITEM,5,-1002
FITEM,5,1033
FITEM,5,-1034
FITEM,5,1036
FITEM,5,1149
FITEM,5,1154
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDELE,_Y
CMDELE,_Y1
CMDELE,_Y2 ! Re-Meshing Cleared Areas

FLST,5,4,4,ORDE,2
FITEM,5,2204
FITEM,5,-2207
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,,Y
LESIZE,_Y1,,.4,1,
CMDELE,_Y

```

```

CMDEL,_Y1
MSHKEY,0
MSHAPE,1,3d
MSHKEY,0
FLST,5,4,5,ORDE,2
FITEM,5,1158
FITEM,5,-1161
CM,_Y,AREA
ASEL,...,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2      ! Meshing Pipe Areas

EXTOPT,ESIZE,1,1,
EXTOPT,ACLEAR,0
VSWEEP,33,1149,1150
VSWEEP,2,1001,1038
VSWEEP,4,1003,1046
VSWEEP,3,1002,1042
VSWEEP,34,1154,1155
                ! Re-Meshing Volumes

-----
! Start Making Load Cell #2
-----

ACLEAR, 592      ! Clearing STR Area

FLST,3,4,4,ORDE,2
                ! Copying Load Cell End Lines
FITEM,3,2204
FITEM,3,-2207
LGEN,2,P51X,...,363.8-25.4,-74.746198-
25.4,.0

FLST,3,1,3,ORDE,1
FITEM,3,1087
KGEN,2,P51X,...,800,...,0
LSTR, 1089, 1087
FLST,2,4,4,ORDE,2
FITEM,2,2212
FITEM,2,-2215
ADRAG,P51X,..., 2216
                ! Dragging Load Cell Areas

KWPLAN,-1, 145, 110, 616
ADELE, 592,...,1 ! Deleting STR Area
FLST,2,4,5,ORDE,2
FITEM,2,1162
FITEM,2,-1165
ASBW,P51X
                ! Cutting Load Cell with Work Plane

FLST,2,4,5,ORDE,2
FITEM,2,1170
FITEM,2,-1173
ADELE,P51X,...,1
LDELE, 2216,...,1
                ! Deleting Ends of Load Cell

LSTR, 145, 1095
LSTR, 1094, 110
LSTR, 1097, 229
LSTR, 1096, 616

FLST,2,4,4

FITEM,2,2216
FITEM,2,2229
FITEM,2,1139
FITEM,2,2219
AL,P51X
FLST,2,4,4
FITEM,2,2217
FITEM,2,395
FITEM,2,2218
FITEM,2,2232
AL,P51X
FLST,2,5,4
FITEM,2,781
FITEM,2,724
FITEM,2,2216
FITEM,2,2227
FITEM,2,2217
AL,P51X
FLST,2,4,4
FITEM,2,2229
FITEM,2,2227
FITEM,2,2232
FITEM,2,2231
AL,P51X
FLST,2,4,4
FITEM,2,2231
FITEM,2,186
FITEM,2,2218
FITEM,2,2219
AL,P51X ! New Areas for STR Sidewall

FLST,5,5,5,ORDE,3
FITEM,5,1162
FITEM,5,-1165
FITEM,5,1170
CM,_Y,AREA
ASEL,...,P51X
CM,_Y1,AREA
CMSEL,S,_Y1
AATT, 1, 19, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! STR Sidewall Thickness

FLST,5,4,5,ORDE,2
FITEM,5,1166
FITEM,5,-1169
CM,_Y,AREA
ASEL,...,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 2, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! Load Cell Thickness

FLST,5,4,4,ORDE,4
FITEM,5,2227
FITEM,5,2229
FITEM,5,2231
FITEM,5,-2232
CM,_Y,LINE
LSEL,...,P51X
CM,_Y1,LINE
CMSEL,S,_Y1
LESIZE,ALL,...,4,1,1
CMSEL,S,_Y
CMDELE,_Y

```

```

CMDELE,_Y1
FLST,2,4,5,ORDE,2
FITEM,2,1166
FITEM,2,-1169
ACLEAR,P51X
FLST,5,4,4,ORDE,4
FITEM,5,2225
FITEM,5,-2226
FITEM,5,2228
FITEM,5,2230
CM,_Y,LINE
LSEL,...,P51X
CM,_Y1,LINE
CMSEL,S,_Y1
LESIZE,ALL,...,10,1,1
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1      ! LSize for Load Cell #2

MSHKEY,0
FLST,5,4,5,ORDE,2
FITEM,5,1166
FITEM,5,-1169
CM,_Y,AREA
ASEL,...,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDELE,_Y
CMDEL,_Y1
CMDEL,_Y2 ! Meshing Load Cell Areas

MSHKEY,0
FLST,5,4,5,ORDE,3
FITEM,5,1162
FITEM,5,-1164
FITEM,5,1170
CM,_Y,AREA
ASEL,...,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDELE,_Y
CMDEL,_Y1
CMDEL,_Y2 ! Re-Meshing STR Sidewall

!FLST,2,2,5,ORDE,2
!FITEM,2,1161
!FITEM,2,1167
!ACLEAR,P51X
! Clearing Mesh on Load Cell Areas
! Making into Channel Sections...
! Very Low Torsional Stiffness...

-----
! Start Making Load Cell #3
-----

ACLEAR, 621
! Clearing and Deleting STR Area for 3rd LC
ADELE, 621,...,1

FLST,3,4,5,ORDE,2
! Copying LC Areas Over...
FITEM,3,1158
FITEM,3,-1161
FLST,3,4,5,ORDE,2
FITEM,3,1158

FITEM,3,-1161
AGEN,2,P51X,...,15,854.464844+67.1,...,0

FLST,2,4,5,ORDE,2
FITEM,2,1171
FITEM,2,-1174
ACLEAR,P51X
! Clearing FE Mesh on LC Areas

FLST,3,3,8
FITEM,3,718.981990107,-294.6,-
6672.40301715
FITEM,3,724.27996329,-298.2,-
6877.4345793
FITEM,3,718.888997891,-436.6,-
6668.8042184
WPLANE,-1,P51X
FLST,2,4,5,ORDE,2
FITEM,2,1171
FITEM,2,-1174
ASBW,P51X
! Using WPlane to Cut LC Areas

FLST,2,4,5,ORDE,4
FITEM,2,1176
FITEM,2,1178
FITEM,2,1180
FITEM,2,1182
ADELE,P51X,...,1 ! Deleting End Areas

LSTR, 1104, 52
LSTR, 1101, 634
LSTR, 1103, 48
LSTR, 635, 1102
FLST,2,4,4
FITEM,2,2220
FITEM,2,2249
FITEM,2,2223
FITEM,2,1242
AL,P51X
FLST,2,4,4
FITEM,2,1291
FITEM,2,2220
FITEM,2,2251
FITEM,2,2222
AL,P51X
FLST,2,4,4
FITEM,2,2222
FITEM,2,2242
FITEM,2,2224
FITEM,2,1173
AL,P51X
FLST,2,4,4
FITEM,2,2246
FITEM,2,2224
FITEM,2,1288
FITEM,2,2223
AL,P51X
FLST,2,4,4
FITEM,2,2242
FITEM,2,2246
FITEM,2,2249
FITEM,2,2251
AL,P51X ! Re-creating STR side area

FLST,5,5,5,ORDE,3
FITEM,5,1171
FITEM,5,-1174
FITEM,5,1176
CM,_Y,AREA

```

```

ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 19, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1
FLST,5,4,5,ORDE,4
FITEM,5,1175
FITEM,5,1177
FITEM,5,1179
FITEM,5,1181
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 2, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! STR and LC Thicknesses...

```

```

FLST,5,4,4,ORDE,4
FITEM,5,2240
FITEM,5,2241
FITEM,5,2245
FITEM,5,2248
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,,,10,1,
CMDEL,_Y
CMDEL,_Y1
FLST,5,4,4,ORDE,4
FITEM,5,2242
FITEM,5,2246
FITEM,5,2249
FITEM,5,2251
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,S,_Y1
LESIZE,ALL,,,4,1,1
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1
MSHKEY,0
FLST,5,4,5,ORDE,4
FITEM,5,1175
FITEM,5,1177
FITEM,5,1179
FITEM,5,1181
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2 ! Meshing LC Areas

```

```

FLST,5,1,4,ORDE,1
FITEM,5,2224
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,_Y

```

```

LESIZE,_Y1,,,4,1,
CMDEL,_Y
CMDEL,_Y1
MSHKEY,0
CM,_Y,AREA
ASEL,,, 1173
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2
MSHKEY,0
FLST,5,4,5,ORDE,4
FITEM,5,1171
FITEM,5,1172
FITEM,5,1174
FITEM,5,1176
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2 ! Meshing STR Side Areas

```

```

-----
! Start Making Load Cell #4
-----

```

```

FLST,3,4,5,ORDE,4
FITEM,3,1175
FITEM,3,1177
FITEM,3,1179
FITEM,3,1181
AGEN,2,P51X,,,40,3699.9,,0

```

```

FLST,2,4,5,ORDE,4
FITEM,2,1178
FITEM,2,1180
FITEM,2,1182
FITEM,2,1183
ACLEAR,P51X
ACLEAR, 681 ! Clearing Meshed Areas

```

```

ADELE, 681,,1 ! Delete Pivot Area

```

```

KWPLAN,-1, 24, 201, 209
FLST,2,4,5,ORDE,4
FITEM,2,1178
FITEM,2,1180
FITEM,2,1182
FITEM,2,1183
ASBW,P51X

```

```

! Using WPlane to Cut LC Areas

```

```

FLST,2,4,5,ORDE,4
FITEM,2,1185
FITEM,2,1187
FITEM,2,1189
FITEM,2,1191
ADELE,P51X,,,1 ! Deleting End Areas

```

```

LSTR, 1109, 206
LSTR, 24, 20
LSTR, 24, 1111

```



```

LSTR, 199, 1110
FLST,2,6,4
FITEM,2,2237
FITEM,2,299
FITEM,2,2234
FITEM,2,2267
FITEM,2,2265
FITEM,2,2239
AL,P51X
FLST,2,4,4
FITEM,2,2258
FITEM,2,2262
FITEM,2,2265
FITEM,2,2267
AL,P51X
FLST,2,5,4
FITEM,2,2239
FITEM,2,2262
FITEM,2,2243
FITEM,2,331
FITEM,2,327
AL,P51X
FLST,2,10,4
FITEM,2,358
FITEM,2,349
FITEM,2,352
FITEM,2,28
FITEM,2,336
FITEM,2,326
FITEM,2,2243
FITEM,2,2258
FITEM,2,2234
FITEM,2,1393
AL,P51X      ! Re-Creating Pivot STR Areas

FLST,5,4,5,ORDE,4
FITEM,5,1178
FITEM,5,1180
FITEM,5,1182
FITEM,5,-1183
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 63, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1
FLST,5,4,5,ORDE,4
FITEM,5,1184
FITEM,5,1186
FITEM,5,1188
FITEM,5,1190
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 2, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1      ! Shell Thicknesses

FLST,5,4,4,ORDE,4
FITEM,5,2256
FITEM,5,-2257
FITEM,5,2261
FITEM,5,2264
CM,_Y,LINE

LSEL,,,P51X
CM,_Y1,LINE
CMSEL,S,_Y
LESIZE,_Y1,,,10,1
CMDELE,_Y
CMDELE,_Y1
FLST,5,4,4,ORDE,4
FITEM,5,2258
FITEM,5,2262
FITEM,5,2265
FITEM,5,2267
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,S,_Y
LESIZE,_Y1,,,4,1
CMDELE,_Y
CMDELE,_Y1      ! LC LSizeing..

MSHKEY,0
FLST,5,8,5,ORDE,7
FITEM,5,1178
FITEM,5,1180
FITEM,5,1182
FITEM,5,-1184
FITEM,5,1186
FITEM,5,1188
FITEM,5,1190
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDELE,_Y
CMDELE,_Y1
CMDELE,_Y2
! Re-Meshing Pivot Areas and Load Cell

*SET,Ldc_DONE,1
! Purpose: Do not re-build Load cells...

*ENDIF      ! Ldc_DONE
*ENDIF      ! Rub_Done
*ENDIF      ! Loadcell

=====
=====

*SET,dispslpe
*SET,intocept
*SET,count
*SET,Nindex
*SET,index
*SET,Zloc
*SET,Next      ! Deleting Parameters
*SET,deltamax
*SET,shimslope
*SET,shimintc

FINISH
FINISH

/EOF !=====
=====

```

❖ *Filename: 4_4_FEA_load_algorithm_INPUT*

```

!@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
!      FEA of 930E Truck Box Structure
!      Oilsand Pressure Load Algorithm
!@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@

FINISH

/TITLE,Oilsand Load Application Algorithm

*SET,Ka,0.5           ! Rankine Active Pressure Coefficient
*SET,tors,308.5       ! Payload (Short Tons)
*SET,density,1.6       ! Density (Metric tonnes / m^3)
*SET,G,9.81           ! Gravity (9.81 m/sec^2)

*SET,XPeak,0          ! X Location of Peak
*SET,ZPeak,2450       ! Z Location of Peak

*SET,mass,0.9071847*tons ! Mass (Metric Tonnes)
*SET,rho,1000*density  ! Density (kg/m^3)

/REP7
ALLSEL,ALL
SFADELE,ALL,1,ALL
SFADELE,ALL,2,ALL
SFADELE,ALL,3,ALL
SFADELE,ALL,4,ALL
SFADELE,ALL,5,ALL
SFADELE,ALL,6,ALL      ! Clearing All Pressures

*AFUN,DEG
LOCAL,99,0,0,0,-8105,0,9,0
                ! Rotated Co-ordinate System
CSYS,99          ! Changing Active CS to Rotated CS

SFGRAD,PRES,,X,,
                ! Making Sure NO Pressure Gradients
SFGRAD,PRES,,Y,,
SFGRAD,PRES,,Z,,

FINISH

*DIM,TRACKER,ARRAY,10000,1,1,
*DIM,FR_INT,TABLE,2000,1,1,Xloc,height,
*DIM,FL_INT,TABLE,2000,1,1,Xloc,height,

aplot
/VIEW,1,,1,1,1
/ANG,1
/REP,FAST
/AUTO,1
/REP
/USER,1
/VIEW,1,-0.573647192861,0.458489757215,0.678760665221
/ANG,1,3.44081229588
/REPLO

/!NERR,0,10000, ! Error Message Suppression

|-----|
|-----|
|      Calling Proper Component Section      |
|-----|
|-----|

FINISH

! Half Model Components Section
/INPUT,4_4_FEA_algorithm_comp_INPUT,/home/dw11589/930E_Full_half,

```

```
! Combined Full Model Components Section
/INPUT,4_4_FEA_algorithm_comp_INPUT,,/home/dw11589/930E_Full,,comb,
```

```
! Slice Components Section
/INPUT,4_4_FEA_algorithm_comp_INPUT,,/home/dw11589/930E_Full,,slice,
```

```
-----
!
! Applying Load to Front Wall
!
-----
```

```
*GET,numcomp,COMP,0,NCOMP
*IF,numcomp,GT,3,THEN
```

```
/PREP7
```

```
ALLSEL,ALL
CMSEL,S,Front ! Select Comp = Front
ALLSEL,BELOW,AREA
! Selecting Elements Below Selected Areas
```

```
INDEX = 0
*DO,Xloc,0.4200,100 ! Front Wall Intercept Calculations
  *DO,Zloc,-2000,0.50
    *IF,jumpout,EQ,1,CYCLE
    *SET,surf,((22.229*mass/density+1024)*(1-(Xloc-XPeak)/4854)**2)*(1-(Zloc-ZPeak)/6671)**2)
    *SET,wall,(-2.53865*Zloc)
    *IF,surf,LT,wall,CYCLE ! Finding height up wall
    *IF,surf,GE,wall,THEN ! (topsurf / wall intercept)
      *SET,height,(-2.53865*Zloc)
      *SET,jumpout,1
    *ENDIF
    *IF,Zloc,LT,-1277.666,THEN
      *SET,height,3243.544
    *ENDIF
  *ENDDO
  *SET,jumpout,0
  INDEX = INDEX+1
  FR_INT(INDEX,0,1) = Xloc
  FR_INT(INDEX,1,1) = height
*ENDDO
```

```
! Speeding Up Do Loop
```

```
*GET,count,ELEM,0,COUNT
*GET,Eindex,ELEM,0,NUM,MIN
```

```
*DO,I,0,count+10,1
  !IF,elmirq(I,1),EQ,-1,CYCLE ! Skip if Element is Not Selected
  *GET,Xcent,ELEM,Eindex,CENT,X ! Calling Centroid Locations
  *GET,Ycent,ELEM,Eindex,CENT,Y
  *GET,Zcent,ELEM,Eindex,CENT,Z

  ! Pressure Calculations
  *SET,topsurf,((22.229*mass/density+1024)*(1-(Xcent-XPeak)/4854)**2)*(1-(Zcent-ZPeak)/6671)**2)
  *SET,column,(topsurf-Ycent)
  *IF,column,GT,0,THEN
    *SET,vertpres,rho*G*(1/(1000**3))*column
  *ELSE
    *SET,vertpres,0 ! Preventing Negative Pressure
  *ENDIF
  height = FR_INT(Xcent) ! Height = F(Xlocation)
  *IF,column,GT,0,THEN
    *SET,basepres,Ka*rho*G*(1/(1000**3))*height
    *SET,horzpres,(basepres*(1-Ycent/height))
  *ELSE
    *SET,horzpres,0 ! Preventing Negative Pressure
  *ENDIF
```

```

! Pressure Combination
*SET,pressure,(vertpres*0.366501226)+(horzpres*0.930417568)
*IF,pressure*10e6,GE,0,THEN
    SFE,Eindex,1,PRES,,,-pressure,, ! Apply Pressure to Elem i
*ENDIF

!/GOPR ! Resume Print to Output
*SET,Elemleft,(Elemleft-1) ! Number of Elements Left
!/NOPR ! Suspend Print to Output

*GET,Next,ELEM,Eindex,NXTH
*IF,Next,EQ,0,EXIT
*SET,Eindex,Next

*enddo
FINISH
*ENDIF

-----
!
! Applying Load to Floor
!
-----

/REP7

ALLSEL,ALL
CMSEL,S,Floor ! Select Comp = Floor
ALLSEL,BELOW,AREA ! Selecting Elements Below Selected Areas

INDEX = 0
*DO,Xloc,0,4200,100 ! Front Wall Intercept Calculations
    *DO,Zloc,3000,8500,100
        *IF,jumpout,EQ,1,CYCLE
            *SET,surf,((22.229*mass/density+1024)*(1-((Xloc-XPeak)/4854)**2)*(1-((Zloc-ZPeak)/6671)**2))
            *SET,floor,(0.158384*Zloc)
            *IF,surf,GT,floor,CYCLE ! Finding height up floor
            *IF,surf,LE,wall,THEN ! (topsurf / wall intercept)
                *SET,height,(0.158384*Zloc)
                *SET,jumpout,1
            *ENDIF
            *IF,Zloc,GT,8005.214,THEN
                *SET,height,1267.901
                *SET,jumpout,1
            *ENDIF
        *ENDDO
        *SET,jumpout,0
        INDEX = INDEX+1
        FL_INT(INDEX,0,1) = Xloc
        FL_INT(INDEX,1,1) = height
    *ENDDO ! Speeding Up Do Loop

*GET,count,ELEM,0,COUNT
*GET,Eindex,ELEM,0,NUM,MIN

*DO,i,0,count+10,1
    *IF,elmqr(i,1),EQ,-1,CYCLE ! Skip if Element is Not Selected
    *GET,Xcent,ELEM,Eindex,CENT,X ! Calling Centroid Locations
    *GET,Ycent,ELEM,Eindex,CENT,Y
    *GET,Zcent,ELEM,Eindex,CENT,Z

    ! Pressure Calculations
    *SET,topsurf,((22.229*mass/density+1024)*(1-((Xcent-XPeak)/4854)**2)*(1-((Zcent-ZPeak)/6671)**2))
    *SET,column,(topsurf-Ycent)
    *IF,column,GT,0,THEN
        *SET,vertpres,rho*G*(1/(1000**3))*column
    *ELSE
        *SET,vertpres,0 ! Preventing Negative Pressure
    *ENDIF
    height = FL_INT(Xcent) ! Height = F(Xlocation)

```

```

*IF,column,GT,0,THEN
    *SET,basepres,Ka*rho*G*(1/(1000**3))*height
    *SET,horzpres,(basepres*(1-Ycent/height))
*ELSE
    *SET,horzpres,0 ! Preventing Negative Pressure
*ENDIF

! Pressure Combination
*SET,pressure,(vertpres*0.98768834)+(horzpres*0.156434465)
*IF,pressure*10e6,GE,0,THEN
    SFE,Eindex,1,PRES,,-pressure,, ! Apply Pressure to Elem i
*ENDIF

!/GOPR ! Resume Print to Output
*SET,Elemlft,(Elemlft-1) ! Number of Elements Left
!/NOPR ! Suspend Print to Output

*GET,Next,ELEM,Eindex,NXTH
*IF,Next,EQ,0,EXIT
*SET,Eindex,Next

*enddo
FINISH

-----
!
! Applying Load to Side Wall
!
-----

/PREP7

ALLSEL,ALL
CMSEL,S,Side ! Select Comp = Side
ALLSEL,BELOW,AREA ! Selecting Elements Below Selected Areas

! Speeding Up Do Loop
*GET,count,ELEM,0,COUNT
*GET,Eindex,ELEM,0,NUM,MIN

*DO,i,0,count+10,1
    !IF,elmigr(i,1),EQ,-1,CYCLE ! Skip if Element is Not Selected

    *GET,Xcent,ELEM,Eindex,CENT,X ! Calling Centroid Locations
    *GET,Ycent,ELEM,Eindex,CENT,Y
    *GET,Zcent,ELEM,Eindex,CENT,Z

    *SET,height,((22.229*mass/density+1024)*(1-((Xcent-XPeak)/4854)**2)*(1-((Zcent-ZPeak)/6671)**2))
    *SET,column,(height-Ycent) ! Vertical Pressure Calculations
    *IF,column*10e3,GT,0,THEN
        *SET,basepres,Ka*rho*G*(1/(1000**3))*height
        *SET,horzpres,(basepres*(1-Ycent/height))
    *ELSE
        *SET,horzpres,0 ! Preventing Negative Pressure
    *ENDIF

    ! Pressure Combination
    *SET,pressure,horzpres
    *IF,pressure*10e6,GE,0,THEN
        SFE,Eindex,1,PRES,,-pressure,, ! Apply Pressure to Elem i
    *ENDIF

    !/GOPR ! Resume Print to Output
    *SET,Elemlft,(Elemlft-1) ! Number of Elements Left
    !/NOPR ! Suspend Print to Output

    *GET,Next,ELEM,Eindex,NXTH
    *IF,Next,EQ,0,EXIT
    *SET,Eindex,Next

*enddo
FINISH

```

Applying Load to Side Angle Pieces

/PREP7

ALLSEL,ALL
 CMSEL,S,Angle_S ! Select Comp = Side Angle
 ALLSEL,BELOW,AREA ! Selecting Elements Below Selected Areas

! Speeding Up Do Loop

*GET,count,ELEM,0,COUNT
 *GET,Eindex,ELEM,0,NUM,MIN

*DO,i,0,count+10,1

! IF,elmiqr(i,1),EQ,-1,CYCLE ! Skip if Element is Not Selected

*GET,Xcent,ELEM,Eindex,CENT,X ! Calling Centroid Locations
 *GET,Ycent,ELEM,Eindex,CENT,Y
 *GET,Zcent,ELEM,Eindex,CENT,Z

*SET,topsurf,((22.229*mass/density+1024)*(1-((Xcent-XPeak)/4854)**2)*(1-((Zcent-ZPeak)/6671)**2))

*SET,column,(topsurf-Ycent) ! Vertical Pressure Calculations

*IF,column,GT,0,THEN
 *SET,vertpres,rho*G*(1/(1000**3))*column

*ELSE
 *SET,vertpres,0 ! Preventing Negative Pressure
 *ENDIF

*IF,column,GT,0,THEN ! Horizontal Approximation
 *SET,horzpres,Ka*rho*G*(1/(1000**3))*column

*ELSE
 *SET,horzpres,0 ! Preventing Negative Pressure
 *ENDIF

! Pressure Combination

*SET,presure,(vertpres*0.707106781)+(horzpres*0.707106781)/ 45 deg

*IF,presure*10e6,GE,0,THEN
 SFE,Eindex,1,PRES,,-presure,, ! Apply Pressure to Elem i

*ENDIF

! /GOPR ! Resume Print to Output
 *SET,Elemlft,(Elemlft-1) ! Number of Elements Left
 ! /NOPR ! Suspend Print to Output

*GET,Next,ELEM,Eindex,NXTH
 *IF,Next,EQ,0,EXIT
 *SET,Eindex,Next

*enddo

FINISH

Applying Load to Front Angle Pieces

*GET,numcomp,COMP,0,NCOMP
 *IF,numcomp,GT,3,THEN

/PREP7

ALLSEL,ALL
CMSEL,S,Angle_F
ALLSEL,BELOW,AREA

! Select Comp = Front Angle
! Selecting Elements Below Selected Areas

! Speeding Up Do Loop

*GET,count,ELEM,0,COUNT
*GET,Eindex,ELEM,0,NUM,MIN

*DO,i,0,count+10,1

! *IF,elmigr(i,1),EQ,-1,CYCLE ! Skip if Element is Not Selected

*GET,Xcent,ELEM,Eindex,CENT,X ! Calling Centroid Locations
*GET,Ycent,ELEM,Eindex,CENT,Y
*GET,Zcent,ELEM,Eindex,CENT,Z

*SET,topsurf,((22.229*mass/density+1024)*(1-((Xcent-XPeak)/4854)**2))*(1-((Zcent-ZPeak)/6671)**2))

*SET,column,(topsurf-Ycent) ! Vertical Pressure Calculations

*IF,column,GT,0,THEN
*SET,vertpres,rho*G*(1/(1000**3))*column

*ELSE
*SET,vertpres,0 ! Preventing Negative Pressure

*ENDIF
*IF,column,GT,0,THEN ! Horizontal Approximation
*SET,horzpres,Ka*rho*G*(1/(1000**3))*column

*ELSE
*SET,horzpres,0 ! Preventing Negative Pressure

*ENDIF
! Pressure Combination
*SET,pressure,(vertpres*0.8660254)+(horzpres*0.5) ! 60 deg

*IF,pressure*10e6,GE,0,THEN
SFE,Eindex,1,PRES,,pressure,, ! Apply Pressure to Elem i

*ENDIF

! /GOPR ! Resume Print to Output
*SET,Elemlft,(Elemleft-1) ! Number of Elements Left
! /NOPR ! Suspend Print to Output

*GET,Next,ELEM,Eindex,NXTH
*IF,Next,EQ,0,EXIT
*SET,Eindex,Next

*enddo

FINISH

*ENDIF

ALLSEL,ALL

! Deleting Parameters and Display Commands

! Display Commands (Not Needed)

EPLT
/VIEW,1,1,1,1
/ANG,1

```

/REP,FAST
/AUTO,1
/REP
/USER,1
/VIEW,1,0.736873689155,-0.272748618737,0.618567180837
/ANG,1,1.56201349016
/LIG,1,1,1.000,0.333241232397,-0.895070804294,0.296308177969,0.000000000000E+00
/REPLO
/PSF,PRES,NORM,2
/PBF,DEFA,1
/PSYMB,CS,0
/PSYMB,NDIR,0
/PSYMB,ESYS,0
/PSYMB,LDIR,0
/PSYMB,ECON,0
/PSYMB,XNODE,0
/PSYMB,DOT,1
/PSYMB,PCONV,
/PSYMB,LAYR,0
!*
/PBC,ALL,1
/VSCALE,1,6,0
/REPLOT
/REP
!*

```

! Deleting Parameters

```

TRACKER=
FR_INT=
FL_INT=
surf=
Xloc=
Zloc=
wall=
height=
jumpout=
lowelem=
highelem=
Xcent=
Ycent=
Zcent=
topsurf=
column=
vertpres=
height=
basepres=
horzpres=
pressure=
Elemleft=

CMDELE,ANGLE_F
CMDELE,ANGLE_S
CMDELE,FLOOR
CMDELE,FRONT
CMDELE,SIDE

```

! Deleting Components

```

CSYS,0

```

! Returning to the Global Cartesian
! Co-ordinate System

```

/EOF

```

! End of File Marker

❖ Filename: 4_4_FEA_algorithm_comp_INPUT

```

!@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
! FEA of 930E Truck Box Structure
! Oil and Pressure Load Algorithm
! Select Components Subroutine
!@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@

!-----
!-----
!      Creating Body Half Model
!      Floor, Front, and Side Components
!-----
!-----
:half

FINISH
/PREP7

ALLSEL,ALL

FLST,5,54,5,ORDE,43
FITEM,5,3
FITEM,5,34
FITEM,5,-37
FITEM,5,39
FITEM,5,-43
FITEM,5,45
FITEM,5,53
FITEM,5,59
FITEM,5,62
FITEM,5,67
FITEM,5,89
FITEM,5,106
FITEM,5,126
FITEM,5,150
FITEM,5,-153
FITEM,5,155
FITEM,5,-157
FITEM,5,185
FITEM,5,191
FITEM,5,193
FITEM,5,-194
FITEM,5,204
FITEM,5,262
FITEM,5,269
FITEM,5,-271
FITEM,5,273
FITEM,5,275
FITEM,5,-276
FITEM,5,285
FITEM,5,-286
FITEM,5,343
FITEM,5,349
FITEM,5,-350
FITEM,5,544
FITEM,5,547
FITEM,5,573
FITEM,5,582
FITEM,5,662
FITEM,5,665
FITEM,5,699
FITEM,5,-700
FITEM,5,702
FITEM,5,-705
ASEL,S,,P51X      ! Selecting Floor Areas

CM,floor,AREA      ! Storing Areas as Component
ALLSEL,BELOW,AREA

! Selecting Elements Below Selected Areas
*SET,Elemleft,elemigr(0,13)      ! Element Counter

ALLSEL,ALL

FLST,5,12,5,ORDE,10
FITEM,5,187
FITEM,5,381
FITEM,5,384
FITEM,5,387
FITEM,5,-388
FITEM,5,390
FITEM,5,-392
FITEM,5,395
FITEM,5,-397
FITEM,5,442
ASEL,S,,P51X      ! Selecting Front Wall Areas

CM,Front,AREA      ! Storing Areas as Component
ALLSEL,BELOW,AREA

! Selecting Elements Below Selected Areas
*SET,Elemleft,(Elemleft+elemigr(0,13))      ! Element Counter

ALLSEL,ALL

FLST,5,13,5,ORDE,9
FITEM,5,239
FITEM,5,289
FITEM,5,301
FITEM,5,317
FITEM,5,323
FITEM,5,690
FITEM,5,-692
FITEM,5,694
FITEM,5,-698
ASEL,S,,P51X

CM,Side,AREA      ! Storing Areas as Component
ALLSEL,BELOW,AREA

! Selecting Elements Below Selected Areas
*SET,Elemleft,(Elemleft+elemigr(0,13))      ! Element Counter

ALLSEL,ALL

ASEL,S,,,377

CM,Angle_F,AREA      ! Storing Areas as Component
ALLSEL,BELOW,AREA

! Selecting Elements Below Selected Areas
*SET,Elemleft,(Elemleft+elemigr(0,13))      ! Element Counter

FLST,5,18,5,ORDE,7
FITEM,5,32
FITEM,5,61
FITEM,5,90
FITEM,5,145
FITEM,5,205
FITEM,5,-217
FITEM,5,378
ASEL,S,,P51X

CM,Angle_S,AREA      ! Storing Areas as Component
ALLSEL,BELOW,AREA

! Selecting Elements Below Selected Areas

```

```
*SET,Elemleft,(Elemleft+elmigr(0,13))
! Element Counter
```

```
ALLSEL,ALL
```

```
FINISH
```

```
/EOF ! End of File Marker
```

```
-----
!
! Creating Body Slice Model
! Floor, Front, and Side Components
!
!-----
```

```
:slice
```

```
FINISH
/PRP7
```

```
ALLSEL,ALL
FLST,5,7,5,ORDE,7
FITEM,5,191
FITEM,5,229
FITEM,5,323
FITEM,5,325
FITEM,5,551
FITEM,5,553
FITEM,5,555
ASEL,S,,P51X ! Selecting Floor Areas
```

```
CM,floor,AREA ! Storing Areas as Component
ALLSEL,BELOW,AREA
! Selecting Elements Below Selected Areas
*SET,Elemleft,elmigr(0,13) ! Element Counter
```

```
ALLSEL,ALL
```

```
FLST,5,5,5,ORDE,5
FITEM,5,597
FITEM,5,601
FITEM,5,603
FITEM,5,605
FITEM,5,610
ASEL,S,,P51X
```

```
CM,Side,AREA ! Storing Areas as Component
ALLSEL,BELOW,AREA
! Selecting Elements Below Selected Areas
*SET,Elemleft,(Elemleft+elmigr(0,13))
! Element Counter
```

```
FLST,5,3,3,ORDE,3
FITEM,5,211
FITEM,5,557
FITEM,5,585
ASEL,S,,P51X
```

```
CM,Angle_S,AREA ! Storing Areas as Component
ALLSEL,BELOW,AREA
! Selecting Elements Below Selected Areas
*SET,Elemleft,(Elemleft+elmigr(0,13))
! Element Counter
```

```
ALLSEL,ALL
FINISH
```

```
/EOF ! End of File Marker
```

```
-----
!
! Creating Combined Frame and Body Full Model
! Floor, Front, and Side Components
!
!-----
```

```
:comb
```

```
FINISH
/PRP7
```

```
ALLSEL,ALL
```

```
FLST,5,108,5,ORDE,86
FITEM,5,283
FITEM,5,314
FITEM,5,-317
FITEM,5,319
FITEM,5,-323
FITEM,5,325
FITEM,5,333
FITEM,5,339
FITEM,5,342
FITEM,5,347
FITEM,5,369
FITEM,5,386
FITEM,5,406
FITEM,5,430
FITEM,5,-433
FITEM,5,435
FITEM,5,-437
FITEM,5,465
FITEM,5,471
FITEM,5,473
FITEM,5,-474
FITEM,5,484
FITEM,5,542
FITEM,5,549
FITEM,5,-551
FITEM,5,553
FITEM,5,555
FITEM,5,-556
FITEM,5,565
FITEM,5,-566
FITEM,5,623
FITEM,5,629
FITEM,5,-630
FITEM,5,624
FITEM,5,627
FITEM,5,653
FITEM,5,662
FITEM,5,942
FITEM,5,945
FITEM,5,979
FITEM,5,-980
FITEM,5,982
FITEM,5,-985
FITEM,5,1314
FITEM,5,1345
FITEM,5,-1348
FITEM,5,1350
FITEM,5,-1354
FITEM,5,1356
FITEM,5,1364
FITEM,5,1370
FITEM,5,1373
FITEM,5,1378
FITEM,5,1400
```

```

FITEM,5,1417
FITEM,5,1435
FITEM,5,1459
FITEM,5,-1462
FITEM,5,1464
FITEM,5,-1466
FITEM,5,1494
FITEM,5,1500
FITEM,5,1502
FITEM,5,-1503
FITEM,5,1513
FITEM,5,1571
FITEM,5,1578
FITEM,5,-1580
FITEM,5,1582
FITEM,5,1584
FITEM,5,-1585
FITEM,5,1594
FITEM,5,-1595
FITEM,5,1652
FITEM,5,1658
FITEM,5,-1659
FITEM,5,1853
FITEM,5,1856
FITEM,5,1882
FITEM,5,1891
FITEM,5,1955
FITEM,5,1958
FITEM,5,1990
FITEM,5,-1991
FITEM,5,1993
FITEM,5,-1996
ASEL,S,,P51X          ! Selecting Floor Areas

CM,floor,AREA          ! Storing Areas as Component
ALLSEL,BELOW,AREA
! Selecting Elements Below Selected Areas
*SET,Elemleft,elmigr(0,13) ! Element Counter

ALLSEL,ALL

FLST,5,24,5,ORDE,20
FITEM,5,467
FITEM,5,661
FITEM,5,664
FITEM,5,667
FITEM,5,-668
FITEM,5,670
FITEM,5,-672
FITEM,5,675
FITEM,5,-677
FITEM,5,722
FITEM,5,1496
FITEM,5,1690
FITEM,5,1693
FITEM,5,1696
FITEM,5,-1697
FITEM,5,1699
FITEM,5,-1701
FITEM,5,1704
FITEM,5,-1706
FITEM,5,1751
ASEL,S,,P51X          ! Selecting Front Wall Areas

CM,Front,AREA          ! Storing Areas as Component
ALLSEL,BELOW,AREA
! Selecting Elements Below Selected Areas
*SET,Elemleft,(Elemleft+elmigr(0,13))
! Element Counter

ALLSEL,ALL

FLST,5,26,5,ORDE,18
FITEM,5,519
FITEM,5,569
FITEM,5,581
FITEM,5,597
FITEM,5,603
FITEM,5,970
FITEM,5,-972
FITEM,5,974
FITEM,5,-978
FITEM,5,1548
FITEM,5,1598
FITEM,5,1610
FITEM,5,1626
FITEM,5,1632
FITEM,5,1981
FITEM,5,-1983
FITEM,5,1985
FITEM,5,-1989
ASEL,S,,P51X          ! Selecting Side Wall Areas

CM,Side,AREA          ! Storing Areas as Component
ALLSEL,BELOW,AREA
! Selecting Elements Below Selected Areas
*SET,Elemleft,(Elemleft+elmigr(0,13))
! Element Counter

ALLSEL,ALL

FLST,5,2,5,ORDE,2
FITEM,5,657
FITEM,5,1686
ASEL,S,,P51X

CM,Angle_F,AREA ! Storing Areas as Component
ALLSEL,BELOW,AREA
! Selecting Elements Below Selected Areas
*SET,Elemleft,(Elemleft+elmigr(0,13))
! Element Counter

FLST,5,36,5,ORDE,14
FITEM,5,312
FITEM,5,341
FITEM,5,370
FITEM,5,425
FITEM,5,485
FITEM,5,-497
FITEM,5,658
FITEM,5,1343
FITEM,5,1372
FITEM,5,1401
FITEM,5,1454
FITEM,5,1514
FITEM,5,-1526
FITEM,5,1687
ASEL,S,,P51X

CM,Angle_S,AREA ! Storing Areas as Component
ALLSEL,BELOW,AREA
! Selecting Elements Below Selected Areas
*SET,Elemleft,(Elemleft+elmigr(0,13))
! Element Counter

ALLSEL,ALL
FINISH

/EOF          ! End of File Marker

```

❖ Filename: 4_5_FEA_symm_INPUT

```

@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
!           FEA of 930E Truck Box Structure
!           Symmetry BC's Routine
@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
FINISH                                           FITEM,2,236

/TITLE,Applying Symmetry Boundary Conditions    FITEM,2,238
                                                FITEM,2,246
*AFUN,DEG                                       FITEM,2,258
                                                FITEM,2,268
                                                FITEM,2,281
                                                FITEM,2,300
                                                FITEM,2,306
                                                FITEM,2,322
                                                FITEM,2,357
                                                FITEM,2,377
                                                FITEM,2,594
                                                FITEM,2,606
                                                FITEM,2,727
                                                FITEM,2,-728
                                                FITEM,2,733
                                                FITEM,2,780
                                                FITEM,2,810
                                                FITEM,2,814
                                                FITEM,2,-817
                                                FITEM,2,855
                                                FITEM,2,859
                                                FITEM,2,869
                                                FITEM,2,885
                                                FITEM,2,-886
                                                FITEM,2,938
                                                FITEM,2,943
                                                FITEM,2,-944
                                                FITEM,2,946
                                                FITEM,2,950
                                                FITEM,2,952
                                                FITEM,2,-953
                                                FITEM,2,957
                                                FITEM,2,960
                                                FITEM,2,-961
                                                FITEM,2,974
                                                FITEM,2,982
                                                FITEM,2,1020
                                                FITEM,2,1023
                                                FITEM,2,1032
                                                FITEM,2,-1033
                                                FITEM,2,1038
                                                FITEM,2,1041
                                                FITEM,2,1045
                                                FITEM,2,1137
                                                FITEM,2,1150
                                                FITEM,2,1152
                                                FITEM,2,1172
                                                FITEM,2,1175
                                                FITEM,2,1179
                                                FITEM,2,1196
                                                FITEM,2,1207
                                                FITEM,2,1225
                                                FITEM,2,-1226
                                                FITEM,2,1326
                                                FITEM,2,1343
                                                FITEM,2,1350
                                                FITEM,2,1364
                                                FITEM,2,1370
                                                FITEM,2,1389
                                                FITEM,2,1489
                                                FITEM,2,1491
                                                FITEM,2,1497
                                                FITEM,2,1499
                                                FITEM,2,1509
                                                FITEM,2,-1512
                                                DL,P51X, ,UX,0

ERASE                                           FITEM,2,236
APLOT                                           FITEM,2,238
WPSTYLE,.....,0                               FITEM,2,246
/AUTO, 1                                       FITEM,2,258
/REP                                           FITEM,2,268
/USER, 1                                       FITEM,2,281
/VIEW, 1, 0.868057538878 , -0.230609820303 , - FITEM,2,300
0.439653522647                                FITEM,2,306
/ANG, 1, -7.45986669049                       FITEM,2,322
/REPLO                                         FITEM,2,357

                                                FITEM,2,377
                                                FITEM,2,594
                                                FITEM,2,606
                                                FITEM,2,727
                                                FITEM,2,-728
                                                FITEM,2,733
                                                FITEM,2,780
                                                FITEM,2,810
                                                FITEM,2,814
                                                FITEM,2,-817
                                                FITEM,2,855
                                                FITEM,2,859
                                                FITEM,2,869
                                                FITEM,2,885
                                                FITEM,2,-886
                                                FITEM,2,938
                                                FITEM,2,943
                                                FITEM,2,-944
                                                FITEM,2,946
                                                FITEM,2,950
                                                FITEM,2,952
                                                FITEM,2,-953
                                                FITEM,2,957
                                                FITEM,2,960
                                                FITEM,2,-961
                                                FITEM,2,974
                                                FITEM,2,982
                                                FITEM,2,1020
                                                FITEM,2,1023
                                                FITEM,2,1032
                                                FITEM,2,-1033
                                                FITEM,2,1038
                                                FITEM,2,1041
                                                FITEM,2,1045
                                                FITEM,2,1137
                                                FITEM,2,1150
                                                FITEM,2,1152
                                                FITEM,2,1172
                                                FITEM,2,1175
                                                FITEM,2,1179
                                                FITEM,2,1196
                                                FITEM,2,1207
                                                FITEM,2,1225
                                                FITEM,2,-1226
                                                FITEM,2,1326
                                                FITEM,2,1343
                                                FITEM,2,1350
                                                FITEM,2,1364
                                                FITEM,2,1370
                                                FITEM,2,1389
                                                FITEM,2,1489
                                                FITEM,2,1491
                                                FITEM,2,1497
                                                FITEM,2,1499
                                                FITEM,2,1509
                                                FITEM,2,-1512
                                                DL,P51X, ,UX,0

                                                FITEM,2,1512
                                                FITEM,2,224
                                                FITEM,2,230

```

FLST,2,106,4,ORDE,102

FITEM,2,5
FITEM,2,17
FITEM,2,40
FITEM,2,47
FITEM,2,56
FITEM,2,66
FITEM,2,70
FITEM,2,81
FITEM,2,90
FITEM,2,93
FITEM,2,95
FITEM,2,97
FITEM,2,99
FITEM,2,101
FITEM,2,103
FITEM,2,105
FITEM,2,107
FITEM,2,109
FITEM,2,111
FITEM,2,113
FITEM,2,115
FITEM,2,117
FITEM,2,119
FITEM,2,121
FITEM,2,123
FITEM,2,125
FITEM,2,134
FITEM,2,172
FITEM,2,175
FITEM,2,183
FITEM,2,193
FITEM,2,198
FITEM,2,207
FITEM,2,212
FITEM,2,224
FITEM,2,230
FITEM,2,236
FITEM,2,238
FITEM,2,246
FITEM,2,258
FITEM,2,268
FITEM,2,281
FITEM,2,300
FITEM,2,306
FITEM,2,322
FITEM,2,357
FITEM,2,377
FITEM,2,594
FITEM,2,606
FITEM,2,727
FITEM,2,-728
FITEM,2,733
FITEM,2,780
FITEM,2,810
FITEM,2,814
FITEM,2,-817
FITEM,2,855
FITEM,2,859
FITEM,2,869
FITEM,2,885
FITEM,2,-886
FITEM,2,938
FITEM,2,943
FITEM,2,-944
FITEM,2,946
FITEM,2,950
FITEM,2,952
FITEM,2,-953

FITEM,2,957
FITEM,2,960
FITEM,2,-961
FITEM,2,974
FITEM,2,982
FITEM,2,1020
FITEM,2,1023
FITEM,2,1032
FITEM,2,-1033
FITEM,2,1038
FITEM,2,1041
FITEM,2,1045
FITEM,2,1137
FITEM,2,1150
FITEM,2,1152
FITEM,2,1172
FITEM,2,1175
FITEM,2,1179
FITEM,2,1196
FITEM,2,1207
FITEM,2,1225
FITEM,2,-1226
FITEM,2,1326
FITEM,2,1343
FITEM,2,1350
FITEM,2,1364
FITEM,2,1370
FITEM,2,1389
FITEM,2,1489
FITEM,2,1491
FITEM,2,1497
FITEM,2,1499
FITEM,2,1509
FITEM,2,-1512
DL,P51X,,ROTY,0

FLST,2,106,4,ORDE,102

FITEM,2,5
FITEM,2,17
FITEM,2,40
FITEM,2,47
FITEM,2,56
FITEM,2,66
FITEM,2,70
FITEM,2,81
FITEM,2,90
FITEM,2,93
FITEM,2,95
FITEM,2,97
FITEM,2,99
FITEM,2,101
FITEM,2,103
FITEM,2,105
FITEM,2,107
FITEM,2,109
FITEM,2,111
FITEM,2,113
FITEM,2,115
FITEM,2,117
FITEM,2,119
FITEM,2,121
FITEM,2,123
FITEM,2,125
FITEM,2,134
FITEM,2,172
FITEM,2,175
FITEM,2,183
FITEM,2,193
FITEM,2,198
FITEM,2,207

FITEM,2,212
 FITEM,2,224
 FITEM,2,230
 FITEM,2,236
 FITEM,2,238
 FITEM,2,246
 FITEM,2,258
 FITEM,2,268
 FITEM,2,281
 FITEM,2,300
 FITEM,2,306
 FITEM,2,322
 FITEM,2,357
 FITEM,2,377
 FITEM,2,594
 FITEM,2,606
 FITEM,2,727
 FITEM,2,-728
 FITEM,2,733
 FITEM,2,780
 FITEM,2,810
 FITEM,2,814
 FITEM,2,-817
 FITEM,2,855
 FITEM,2,859
 FITEM,2,869
 FITEM,2,885
 FITEM,2,-886
 FITEM,2,938
 FITEM,2,943
 FITEM,2,-944
 FITEM,2,946
 FITEM,2,950
 FITEM,2,952
 FITEM,2,-953
 FITEM,2,957
 FITEM,2,960
 FITEM,2,-961
 FITEM,2,974
 FITEM,2,982
 FITEM,2,1020
 FITEM,2,1023
 FITEM,2,1032
 FITEM,2,-1033
 FITEM,2,1038
 FITEM,2,1041
 FITEM,2,1045
 FITEM,2,1137
 FITEM,2,1150
 FITEM,2,1152
 FITEM,2,1172
 FITEM,2,1175
 FITEM,2,1179
 FITEM,2,1196
 FITEM,2,1207
 FITEM,2,1225
 FITEM,2,-1226
 FITEM,2,1326
 FITEM,2,1343
 FITEM,2,1350
 FITEM,2,1364
 FITEM,2,1370
 FITEM,2,1389
 FITEM,2,1489
 FITEM,2,1491
 FITEM,2,1497
 FITEM,2,1499
 FITEM,2,1509
 FITEM,2,-1512
 DL,P51X, ROTZ,0

-----Symmetry Conditions on Load Cell

*IF,Loadcell,EQ,1,THEN

FLST,2,16,4,ORDE,12
 FITEM,2,2204
 FITEM,2,-2207
 FITEM,2,2212
 FITEM,2,-2215
 FITEM,2,2221
 FITEM,2,2233
 FITEM,2,2235
 FITEM,2,-2236
 FITEM,2,2238
 FITEM,2,2244
 FITEM,2,2250
 FITEM,2,2254
 DL,P51X, ,UX,0

FLST,2,16,4,ORDE,12
 FITEM,2,2204
 FITEM,2,-2207
 FITEM,2,2212
 FITEM,2,-2215
 FITEM,2,2221
 FITEM,2,2233
 FITEM,2,2235
 FITEM,2,-2236
 FITEM,2,2238
 FITEM,2,2244
 FITEM,2,2250
 FITEM,2,2254
 DL,P51X, ,ROTY,0

FLST,2,16,4,ORDE,12
 FITEM,2,2204
 FITEM,2,-2207
 FITEM,2,2212
 FITEM,2,-2215
 FITEM,2,2221
 FITEM,2,2233
 FITEM,2,2235
 FITEM,2,-2236
 FITEM,2,2238
 FITEM,2,2244
 FITEM,2,2250
 FITEM,2,2254
 DL,P51X, ,ROTZ,0

*ENDIF

FINISH
 FINISH
 /EOF

❖ Filename: 4_6_FEA_antisymm_INPUT

```

@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
| FEA of 930E Truck Box Structure
| Anti-symmetry Frame BC's Routine
| @@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
FINISH

/TITLE Applying Anti-symmetry Boundary Conditions

/REP7
*AFUN,DEG

|-----
|----- View Settings
|-----

ERASE
APLOT
WPSTYLE,.....,0
/AUTO, 1
/REP
/USER, 1
/VIEW, 1, 0.868057538878 , -0.230609820303 , -
0.439653522647
/ANG, 1, -7.45986669049
/REPO

|-----
|----- Anti-Symmetry Conditions
|-----

FLST,2,106,4,ORDE,102
FITEM,2,5
FITEM,2,17
FITEM,2,40
FITEM,2,47
FITEM,2,56
FITEM,2,66
FITEM,2,70
FITEM,2,81
FITEM,2,90
FITEM,2,93
FITEM,2,95
FITEM,2,97
FITEM,2,99
FITEM,2,101
FITEM,2,103
FITEM,2,105
FITEM,2,107
FITEM,2,109
FITEM,2,111
FITEM,2,113
FITEM,2,115
FITEM,2,117
FITEM,2,119
FITEM,2,121
FITEM,2,123
FITEM,2,125
FITEM,2,134
FITEM,2,172
FITEM,2,175
FITEM,2,183
FITEM,2,193
FITEM,2,198
FITEM,2,207
FITEM,2,212
FITEM,2,224
FITEM,2,230

FITEM,2,236
FITEM,2,238
FITEM,2,246
FITEM,2,258
FITEM,2,268
FITEM,2,281
FITEM,2,300
FITEM,2,306
FITEM,2,322
FITEM,2,357
FITEM,2,377
FITEM,2,594
FITEM,2,606
FITEM,2,727
FITEM,2,-728
FITEM,2,733
FITEM,2,780
FITEM,2,810
FITEM,2,814
FITEM,2,-817
FITEM,2,855
FITEM,2,859
FITEM,2,869
FITEM,2,885
FITEM,2,-886
FITEM,2,938
FITEM,2,943
FITEM,2,-944
FITEM,2,946
FITEM,2,950
FITEM,2,952
FITEM,2,-953
FITEM,2,957
FITEM,2,960
FITEM,2,-961
FITEM,2,974
FITEM,2,982
FITEM,2,1020
FITEM,2,1023
FITEM,2,1032
FITEM,2,-1033
FITEM,2,1038
FITEM,2,1041
FITEM,2,1045
FITEM,2,1137
FITEM,2,1150
FITEM,2,1152
FITEM,2,1172
FITEM,2,1175
FITEM,2,1179
FITEM,2,1196
FITEM,2,1267
FITEM,2,1225
FITEM,2,-1226
FITEM,2,1326
FITEM,2,1343
FITEM,2,1350
FITEM,2,1364
FITEM,2,1370
FITEM,2,1389
FITEM,2,1489
FITEM,2,1491
FITEM,2,1497
FITEM,2,1499
FITEM,2,1509
FITEM,2,-1512
DL,P51X, ,ROTX,0

```

FLST,2,106,4,ORDE,102

FITEM,2,5
FITEM,2,17
FITEM,2,40
FITEM,2,47
FITEM,2,56
FITEM,2,66
FITEM,2,70
FITEM,2,81
FITEM,2,90
FITEM,2,93
FITEM,2,95
FITEM,2,97
FITEM,2,99
FITEM,2,101
FITEM,2,103
FITEM,2,105
FITEM,2,107
FITEM,2,109
FITEM,2,111
FITEM,2,113
FITEM,2,115
FITEM,2,117
FITEM,2,119
FITEM,2,121
FITEM,2,123
FITEM,2,125
FITEM,2,134
FITEM,2,172
FITEM,2,175
FITEM,2,183
FITEM,2,193
FITEM,2,198
FITEM,2,207
FITEM,2,212
FITEM,2,224
FITEM,2,230
FITEM,2,236
FITEM,2,238
FITEM,2,246
FITEM,2,258
FITEM,2,268
FITEM,2,281
FITEM,2,300
FITEM,2,306
FITEM,2,322
FITEM,2,357
FITEM,2,377
FITEM,2,594
FITEM,2,606
FITEM,2,727
FITEM,2,-728
FITEM,2,733
FITEM,2,780
FITEM,2,810
FITEM,2,814
FITEM,2,-817
FITEM,2,855
FITEM,2,859
FITEM,2,869
FITEM,2,885
FITEM,2,-886
FITEM,2,938
FITEM,2,943
FITEM,2,-944
FITEM,2,946
FITEM,2,950
FITEM,2,952
FITEM,2,-953

FITEM,2,957
FITEM,2,960
FITEM,2,-961
FITEM,2,974
FITEM,2,982
FITEM,2,1020
FITEM,2,1023
FITEM,2,1032
FITEM,2,-1033
FITEM,2,1038
FITEM,2,1041
FITEM,2,1045
FITEM,2,1137
FITEM,2,1150
FITEM,2,1152
FITEM,2,1172
FITEM,2,1175
FITEM,2,1179
FITEM,2,1196
FITEM,2,1207
FITEM,2,1225
FITEM,2,-1226
FITEM,2,1326
FITEM,2,1343
FITEM,2,1350
FITEM,2,1364
FITEM,2,1370
FITEM,2,1389
FITEM,2,1489
FITEM,2,1481
FITEM,2,1497
FITEM,2,1499
FITEM,2,1509
FITEM,2,-1512
DLP51X,,UY,0

FLST,2,106,4,ORDE,102

FITEM,2,5
FITEM,2,17
FITEM,2,40
FITEM,2,47
FITEM,2,56
FITEM,2,66
FITEM,2,70
FITEM,2,81
FITEM,2,90
FITEM,2,93
FITEM,2,95
FITEM,2,97
FITEM,2,99
FITEM,2,101
FITEM,2,103
FITEM,2,105
FITEM,2,107
FITEM,2,109
FITEM,2,111
FITEM,2,113
FITEM,2,115
FITEM,2,117
FITEM,2,119
FITEM,2,121
FITEM,2,123
FITEM,2,125
FITEM,2,134
FITEM,2,172
FITEM,2,175
FITEM,2,183
FITEM,2,193
FITEM,2,198
FITEM,2,207

FITEM,2,212
 FITEM,2,224
 FITEM,2,230
 FITEM,2,236
 FITEM,2,238
 FITEM,2,246
 FITEM,2,258
 FITEM,2,281
 FITEM,2,300
 FITEM,2,306
 FITEM,2,322
 FITEM,2,357
 FITEM,2,377
 FITEM,2,594
 FITEM,2,606
 FITEM,2,727
 FITEM,2,-728
 FITEM,2,733
 FITEM,2,780
 FITEM,2,810
 FITEM,2,814
 FITEM,2,-817
 FITEM,2,855
 FITEM,2,859
 FITEM,2,869
 FITEM,2,885
 FITEM,2,-886
 FITEM,2,938
 FITEM,2,943
 FITEM,2,-944
 FITEM,2,946
 FITEM,2,950
 FITEM,2,962
 FITEM,2,-953
 FITEM,2,957
 FITEM,2,960
 FITEM,2,-961
 FITEM,2,974
 FITEM,2,982
 FITEM,2,1020
 FITEM,2,1023
 FITEM,2,1032
 FITEM,2,-1033
 FITEM,2,1038
 FITEM,2,1041
 FITEM,2,1045
 FITEM,2,1137
 FITEM,2,1150
 FITEM,2,1152
 FITEM,2,1172
 FITEM,2,1175
 FITEM,2,1179
 FITEM,2,1196
 FITEM,2,1207
 FITEM,2,1225
 FITEM,2,-1226
 FITEM,2,1326
 FITEM,2,1343
 FITEM,2,1350
 FITEM,2,1364
 FITEM,2,1370
 FITEM,2,1389
 FITEM,2,1489
 FITEM,2,1491
 FITEM,2,1497
 FITEM,2,1499
 FITEM,2,1509
 FITEM,2,-1512
 DL,P51X,UZ,0

 Anti-Symmetry Conditions on Load Cell

*IF,Loadcell,EQ,1,THEN

FLST,2,16,4,ORDE,12
 FITEM,2,2204
 FITEM,2,-2207
 FITEM,2,2212
 FITEM,2,-2215
 FITEM,2,2221
 FITEM,2,2233
 FITEM,2,2235
 FITEM,2,-2236
 FITEM,2,2238
 FITEM,2,2244
 FITEM,2,2250
 FITEM,2,2254
 DL,P51X,ROT,0

FLST,2,16,4,ORDE,12
 FITEM,2,2204
 FITEM,2,-2207
 FITEM,2,2212
 FITEM,2,-2215
 FITEM,2,2221
 FITEM,2,2233
 FITEM,2,2235
 FITEM,2,-2236
 FITEM,2,2238
 FITEM,2,2244
 FITEM,2,2250
 FITEM,2,2254
 DL,P51X,U,0

FLST,2,16,4,ORDE,12
 FITEM,2,2204
 FITEM,2,-2207
 FITEM,2,2212
 FITEM,2,-2215
 FITEM,2,2221
 FITEM,2,2233
 FITEM,2,2235
 FITEM,2,-2236
 FITEM,2,2238
 FITEM,2,2244
 FITEM,2,2250
 FITEM,2,2254
 DL,P51X,UZ,0

*ENDIF

FINISH
 /EOF

❖ Filename: 5_1_post_StressPath_INPUT

```

!@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
!      FEA of 930E Truck Box Structure
!      Bolster Stress Plot
!@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@

```

```

FINISH
/CLEAR

```

```

|----- Reading Database and Results Files
|-----

```

```

RESUME,July_18_4Loadcells.db,
/GRAPHICS,FULL

```

```

/POST1
INRES,
FILE,July_18_4Loadcells,rst,

```

```

SET,1,LAST,1,      ! Load Step #,Last
Substep, Scale=1

```

```

/EOF

```

```

LCDEF,1,1,,
LCDEF,2,2,,
LCDEF,3,3,,
LCDEF,4,4,,
LCASE,1,
LCOPER,ADD,4,,
/TITLE,LOAD CASE 5: Twist + Ore Load
LCWRITE,5,,
SET,1,LAST,-1,
LCOPER,ADD,4,,
/TITLE,LOAD CASE 6: Inverted Twist + Ore Load
LCWRITE,6,,
LCASE,2,
LCOPER,ADD,4,,
/TITLE,LOAD CASE 7: Uniform Frame Displacement +
Ore Load
LCWRITE,7,,
SET,2,LAST,-1,
LCOPER,ADD,4,,
/TITLE,LOAD CASE 8: Inverted Uniform Frame
Displacement + Ore Load
LCWRITE,8,,
LCASE,5,
LCOPER,SUB,2,,
/TITLE,LOAD CASE 9: Twist + OreLoad - Uniform...
Uypin=0 UyNose=-2.0
LCWRITE,9,,
LCASE,6,
LCOPER,ADD,2,,
/TITLE,LOAD CASE 10: Inverted Twist + OreLoad +
Uniform... Uypin=0 UyNose=+2.0
LCWRITE,10,,

```

```

|-----
! Rotating Co-ordinate System to Match Bolster Plate
|-----

```

```

CSKP,11,0,119,60,39,1,1,
      ! Rotating Co-ordinate System to
RSYS,11      ! align w/ Bottom of Bolster

```

```

|-----

```

```

|----- Selecting Which Bolster to Study
|-----

```

```

ALLSEL,ALL

```

```

FLST,5,16,5,ORDE,14
FITEM,5,96
FITEM,5,-97
FITEM,5,99
FITEM,5,-101
FITEM,5,114
FITEM,5,-116
FITEM,5,159
FITEM,5,162
FITEM,5,189
FITEM,5,201
FITEM,5,551
FITEM,5,-552
FITEM,5,554
FITEM,5,-555
ASEL,R,,P51X
CM,Bolster1,AREA

```

```

ALLSEL,ALL

```

```

FLST,5,28,5,ORDE,24
FITEM,5,74
FITEM,5,80
FITEM,5,86
FITEM,5,93
FITEM,5,111
FITEM,5,113
FITEM,5,161
FITEM,5,261
FITEM,5,264
FITEM,5,266
FITEM,5,268
FITEM,5,274
FITEM,5,278
FITEM,5,280
FITEM,5,282
FITEM,5,293
FITEM,5,550
FITEM,5,556
FITEM,5,558
FITEM,5,-561
FITEM,5,563
FITEM,5,-566
FITEM,5,721
FITEM,5,731
FITEM,5,733
ASEL,R,,P51X
CM,Bolster2,AREA

```

```

ALLSEL,ALL

```

```

FLST,5,30,5,ORDE,25
FITEM,5,84
FITEM,5,108
FITEM,5,260
FITEM,5,263
FITEM,5,265
FITEM,5,267
FITEM,5,272
FITEM,5,277
FITEM,5,279
FITEM,5,283
FITEM,5,-284

```

FITEM,5,321
 FITEM,5,557
 FITEM,5,568
 FITEM,5,570
 FITEM,5,-572
 FITEM,5,574
 FITEM,5,-577
 FITEM,5,701
 FITEM,5,711
 FITEM,5,-713
 FITEM,5,719
 FITEM,5,722
 FITEM,5,-724
 FITEM,5,732
 ASEL,R,,P51X
 CM,Bolster3,AREA

ALLSEL,ALL

FLST,5,20,5,ORDE,18
 FITEM,5,78
 FITEM,5,81
 FITEM,5,-82
 FITEM,5,105
 FITEM,5,281
 FITEM,5,313
 FITEM,5,316
 FITEM,5,567
 FITEM,5,579
 FITEM,5,581
 FITEM,5,583
 FITEM,5,-584
 FITEM,5,708
 FITEM,5,-710
 FITEM,5,716
 FITEM,5,-717
 FITEM,5,725
 FITEM,5,-727
 ASEL,R,,P51X
 CM,Bolster4,AREA

ALLSEL,ALL

FLST,5,18,5,ORDE,14
 FITEM,5,72
 FITEM,5,75
 FITEM,5,-77
 FITEM,5,102
 FITEM,5,578
 FITEM,5,585
 FITEM,5,587
 FITEM,5,-591
 FITEM,5,706
 FITEM,5,-707
 FITEM,5,714
 FITEM,5,-715
 FITEM,5,728
 FITEM,5,-729
 ASEL,R,,P51X
 CM,Bolster5,AREA

ALLSEL,ALL

FLST,5,15,5,ORDE,10
 FITEM,5,21
 FITEM,5,-22
 FITEM,5,24
 FITEM,5,-26
 FITEM,5,71
 FITEM,5,123

FITEM,5,-125
 FITEM,5,128
 FITEM,5,130
 FITEM,5,-134
 ASEL,R,,P51X
 CM,Bolster6,AREA

ALLSEL,ALL

FLST,5,15,5,ORDE,12
 FITEM,5,9
 FITEM,5,-10
 FITEM,5,12
 FITEM,5,-13
 FITEM,5,18
 FITEM,5,-20
 FITEM,5,23
 FITEM,5,27
 FITEM,5,117
 FITEM,5,119
 FITEM,5,-122
 FITEM,5,127
 ASEL,R,,P51X
 CM,Bolster7,AREA

ALLSEL,ALL

FLST,5,15,5,ORDE,14
 FITEM,5,2
 FITEM,5,4
 FITEM,5,47
 FITEM,5,50
 FITEM,5,58
 FITEM,5,60
 FITEM,5,63
 FITEM,5,68
 FITEM,5,-70
 FITEM,5,199
 FITEM,5,553
 FITEM,5,627
 FITEM,5,659
 FITEM,5,661
 ASEL,R,,P51X
 CM,Bolster8,AREA

ALLSEL,ALL

FLST,5,12,5,ORDE,12
 FITEM,5,1
 FITEM,5,5
 FITEM,5,7
 FITEM,5,48
 FITEM,5,-49
 FITEM,5,65
 FITEM,5,112
 FITEM,5,203
 FITEM,5,562
 FITEM,5,630
 FITEM,5,660
 FITEM,5,666
 ASEL,R,,P51X
 CM,Bolster9,AREA

ALLSEL,ALL

CMSEL,S,Bolster1
 CMSEL,A,Bolster2
 CMSEL,A,Bolster3
 CMSEL,A,Bolster4
 CMSEL,A,Bolster5

! Front Bolster

```

CMSEL,A,Bolster6
CMSEL,A,Bolster7
CMSEL,A,Bolster8
CMSEL,A,Bolster9          ! Rear Bolster

ALLSEL,BELOW,AREA

!-----
!-----
APLOT
/AUTO,1
/REP
AVPRIN,0,0,

:quick

!LCASE,10
SET,1,LAST,-5,

SHELL,TOP
AVPRIN,0,0,
ETABLE,SXTOP,S,X
SHELL,bot
AVPRIN,0,0,
ETABLE,SBOT,S,X
SADD,SEC_BEND,SXTOP,SBOT,1,-1,0,

PLETAB,SEC_BEND,AVG

/EOF
!-----
!-----
!----- Defining Path Locations
!-----

!here
!PADEL,ALL          ! Delete All Paths
!LCASE,1,          ! Read Load Case

PATH,Bolster,2,30,200,          ! Defining Path
! 2 path points, 30 Data sets, 200 Data Points

IPPATH,2,0,3840,-115,-4400-(4670-4400)Y2,0,
IPPATH,1,0,0,-340,-4400-(4670-4400)Y2,0,
!/TITLE,Path Functions Down Centerline of Fifth Bolster

!FLST,2,2,1
!FITEM,2,42488
!FITEM,2,38822
!PPATH,P51X,1
!PDEF,STAT
!/TITLE,Path Functions Down Center of Fifth Bolster
Fillet

IPPATH,2,0,3840,-115,-7440-(7690-7440)Y2,0,
IPPATH,1,0,0,-340,-7500-(7690-7500)Y2,0,
!/TITLE,Path Functions Down Centerline of FRONT
Bolster

!FLST,2,2,1
!FITEM,2,43399
!FITEM,2,42420
!PPATH,P51X,1
!PDEF,STAT
!/TITLE,Path Functions Down Center of FRONT Bolster
Fillet

IPPATH,2,0,1030,-440+100,-7730,0,

```

```

IPPATH,1,0,943,-440+100,-4240,0,
!/TITLE,Path Functions Along Outside of STR

!-----
!----- Mapping Results to Bolster
!-----

PATH,Bolster

PDEF,STAT
AVPRIN,0,0,

SHELL,MID
! Read Results from Middle of Shell Element
PDEF,MidX,S,X,AVG
IPDEF,MidY,S,Y,AVG
IPDEF,MidZ,S,Y,AVG
IPDEF,EPELxMID,EPEL,X,AVG
IPDEF,EPELyMID,EPEL,Y,AVG
IPDEF,EPELzMID,EPEL,Z,AVG

SHELL,BOT
! Read Results from Bottom of Shell Element
PDEF,BotX,S,X,AVG
IPDEF,BotY,S,Y,AVG
IPDEF,EPELxBOT,EPEL,X,AVG

SHELL,TOP ! Read Results from Top of Shell Element
PDEF,TopX,S,X,AVG
IPDEF,TopY,S,Y,NOAVG
IPDEF,EPELxTOP,EPEL,X,AVG

SHELL          ! Resume Top Shell Results

RSYS,0 ! Restoring Results to Global Cartesian
CSYS,0
DSYS,0

!-----
!----- Plotting Results on Graph
!-----

!X/RANGE,450,1350          ! X Range

! Plot Variable Settings
IPLPATH,MidX
IPLPATH,MidX,MidY,MidZ
PLPATH,TopX,BotX,MidX
IPLPATH,MidX,MidY,MidZ
IPLPATH,TopY,BotY,MidY
IPLPATH,EPELxMID,EPELyMID,EPELzMID
IPLPATH,EPELxBOT,EPELxTOP,EPELxMID

!-----
!-----
!-----

/EOF

```

❖ Filename: 5_6_post_RubberReaction_INPUT

```

!@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
!      FEA of 930E Truck Box Structure
!      Rubber Pad Representation
!      Reaction Force Collection Routine
!@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@

```

```

FINISH
/CLEAR
/!NERR,0,,      ! Warning Suppression

```

```

|-----
|      Selecting Rubber Pad Bottom Nodes
|-----
:here

```

```

|----- Reading Database and Results Files
|-----
RESUME,June_25_Shim.db
/GRAPHICS,FULL

```

```

ALLSEL,ALL
ALLSEL,BELOW,VOLU

```

```

/POST1
/INRES,
/FILE,June_25_Shim,rst,
SET,1,LAST,1,,      ! Base Load Step

```

```

|-----
|      Selecting Rubber Pad Volumes
|-----

```

```

ALLSEL,ALL
ALLSEL,BELOW,VOLU

```

```

/ESSEL,S,MAT,,2
/EPLLOT
/AUTO,1
/REP
/USER,1
/VIEW,1,0.475551822770,0.322430127329,*,*
0.818467639465
/ANG,1,6.72302175464
/LIG,1,1,1.000,0.812507096498,-0.550668422625
,-0.191302133977,0.000000000000E+00
/REPLO

```

```

/ZOOM,1,RECT,1.187651,-0.473591,0.626680,-
0.021810
*SET,_ZF,1
/AVPRIN,0,0,
/*
/EFACE,_ZF
/PLNSOL,U,Y,0,1
/*
/DSCALE,1,1.0
/REPLOT
/*

```

```

/EOF

```

INSEL,S,LOC,Y,-465.5,-465.3 ! Selecting Bottom

Nodes

NSEL,R,LOC,Y,-440.5,-439.5 ! Selecting Top Nodes

```
*GET,count,NODE,0,COUNT
*GET,Nindex,NODE,0,NUM,MIN
*DIM,REACTION,ARRAY,count,5,1
*DO,index,1,count+10,1
  /GOPR                      ! Resume Print to Output
  !*GET,Rforce,NODE,Nindex,RF,FY
  *GET,StressY,NODE,Nindex,S,Y
  ! Element Nodal Stress
  REACTION(index,1,1)=index
  REACTION(index,2,1)=Nindex
  REACTION(index,3,1)=NZ(Nindex)
  REACTION(index,4,1)=NX(Nindex)
  !REACTION(index,5,1)=Rforce
  REACTION(index,5,1)=StressY
  *GET,Next,NODE,Nindex,NXTH
  *IF,Next,EQ,0,EXIT
  *SET,Nindex,Next
/NOPR                      ! Suspend Print to Output
*ENDDO
!*CFOPEN,Reaction_Rubber_Top,
*CFOPEN,Reaction_Rubber_SY_Top,
*VWRITE,REACTION(1,1),REACTION(1,2),REACTION
(1,3),REACTION(1,4),REACTION(1,5),...
(' Index ',F4.0,' Node ',F6.0,' Zloc',F10.2,'
Xloc',F10.2,' SY',F12.2)
*CFCLOSE
count=
Nindex=
index=
Rforce=
Next=
REACTION=
```

ALLSEL,ALL

/EOF

```
!-----
!-----
!-----
```

❖ Filename: 5_7_post_LoadCells_INPUT

```

@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
|          FEA of 930E Truck Box Structure
|          Load Cell Study Algorithm...
@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@@
FINISH
/CLear
/INERR,0,,          ! Warning Supression

|----- Reading Database and Results Files
|-----

RESUME,July_18_4Loadcells.db,
/GRAPHICS,FULL

/POST1
INRES,
FILE,July_18_4Loadcells.rst

SET,1,Last,1,          ! Load Step #,Last
Substep, Scale=1

|----- Creating Load Cell Component Areas
|-----

ALLSEL,ALL
FLST,5,4,5,ORDE,4
FITEM,5,1184
FITEM,5,1186
FITEM,5,1188
FITEM,5,1190
ASEL,S,,P51X
CM,Loadcel4,AREA

ALLSEL,ALL
FLST,5,4,5,ORDE,4
FITEM,5,1175
FITEM,5,1177
FITEM,5,1179
FITEM,5,1181
ASEL,S,,P51X
CM,Loadcel3,AREA

ALLSEL,ALL
FLST,5,4,5,ORDE,2
FITEM,5,1158
FITEM,5,-1161
ASEL,S,,P51X
CM,Loadcel2,AREA

ALLSEL,ALL
FLST,5,4,5,ORDE,2
FITEM,5,1166
FITEM,5,-1169
ASEL,S,,P51X
CM,Loadcel1,AREA

ALLSEL,ALL

/CMSEL,S,Loadcel1
/CMSEL,S,Loadcel2
/CMSEL,S,Loadcel3
/CMSEL,S,Loadcel4

ALLSEL,BELOW,AREA
/EOF

```

```

|----- Combining Load Sets.
|-----

LCDEF,1,1,,
LCDEF,2,2,,
LCDEF,3,3,,
LCDEF,4,4,,
LCASE,1,
LCOPER,ADD,4,,
/TITLE,LOAD CASE 5: Twist + Ore Load
LCWRITE,5,,/
SET,1,Last,-1,
LCOPER,ADD,4,,
/TITLE,LOAD CASE 6: Inverted Twist + Ore Load
LCWRITE,6,,/
LCASE,2,
LCOPER,ADD,4,,
/TITLE,LOAD CASE 7: Uniform Frame Displacement +
Ore Load
LCWRITE,7,,/
SET,2,Last,-1,
LCOPER,ADD,4,,
/TITLE,LOAD CASE 8: Inverted Uniform Frame
Displacement + Ore Load
LCWRITE,8,,/
LCASE,5
LCOPER,SUB,2,,
/TITLE,LOAD CASE 9: Twist + OreLoad - Uniform...
Uypin=0 UyNose=-2.0
LCWRITE,9,,/
LCASE,6
LCOPER,ADD,2,,
/TITLE,LOAD CASE 10: Inverted Twist + OreLoad +
Uniform... Uypin=0 UyNose=+2.0
LCWRITE,10,,/

```

❖ *Filename: 6_1_submodel_Main_INPUT*

```

=====
!
!      Sub-model of Bolster-Stringer Intersection
!
=====

----- Sub-Model Creation -----

/INPUT,6_2_submodel_geom_INPUT,...,0      ! Creating Sub-model Solid Geometry
SAVE                                       ! Saving sub_geom.db
/EOF

:mesh
FINISH
FINISH
/CLEAR
RESUME,sub_geom.db
/INPUT,6_3_submodel_mesh_INPUT,...,0      ! Meshing with Solid Elements
SAVE                                       ! Saving sub_mesh.db
/EOF

----- Shell to Solid Results Transfer -----

:tran
FINISH
FINISH
/CLEAR
RESUME,sub_mesh.db
/INPUT,6_4_submodel_tran_INPUT,...,0      ! Results Transfer Routine
!SAVE                                       ! Saving sub_modl.db
/EOF

! (load sets??)
! Solve

```


❖ Filename: 6_2_submodel_geom_INPUT

```

*****
***** Sub-model Geometry Creation Routine *****
*****
***** Cropping Geometry to Sub-model Region *****
*****

FINISH
FINISH
/CLEAR
RESUME geom.db
/TITLE Building Sub-Model Geometry
/FILNAME,sub_geom

/PREP7

KWPLAN,-1, 175, 19, 723
KL,1357,0.5,,
KL,1335,0.5,,
KWPAVE, 1018 ! Moving Work Plane

FLST,2,5,5,ORDE,5
FITEM,2,120
FITEM,2,122
FITEM,2,685
FITEM,2,-686
FITEM,2,688
ASBW,P51X ! Cutting Areas

KWPAVE, 1019 ! Moving Work Plane

FLST,2,2,5,ORDE,2
FITEM,2,19
FITEM,2,117
ASBW,P51X ! Cutting Areas

KWPLAN,-1, 1018, 727, 726
KWPAVE, 1019 ! Moving Work Plane

ASBW, 1038 ! Cutting Area

FLST,5,9,5,ORDE,9
FITEM,5,119
FITEM,5,121
FITEM,5,1035
FITEM,5,-1036
FITEM,5,1039
FITEM,5,-1040
FITEM,5,1043
FITEM,5,1045
FITEM,5,1047
ASEL,S,,P51X ! Selecting Areas

ALLSEL,BELOW,AREA

FLST,3,1,4,ORDE,1 ! STR Lower Edge Lines
FITEM,3,2071
LGEN,2,P51X,,,-38*(33.3/109),-38*(103.8/109),.0
FLST,3,1,4,ORDE,1
FITEM,3,2059
LGEN,2,P51X,,,-38,,.0
KWPLAN,-1, 1021, 727, 1029
LARC,1032,1030,727,38+38,

FLST,5,3,5,ORDE,3
FITEM,5,1039
FITEM,5,-1040
FITEM,5,1047
ASEL,U,,P51X
ASEL,INVE ! Inverting Selection

FLST,2,761,5,ORDE,29
FITEM,2,1
FITEM,2,-18
FITEM,2,20
FITEM,2,-106
FITEM,2,108
FITEM,2,110
FITEM,2,-116
FITEM,2,118
FITEM,2,123
FITEM,2,-595
FITEM,2,612
FITEM,2,-684
FITEM,2,687
FITEM,2,689
FITEM,2,-719
FITEM,2,721
FITEM,2,-729
FITEM,2,732
FITEM,2,-733
FITEM,2,750
FITEM,2,-764
FITEM,2,1000
FITEM,2,-1034
FITEM,2,1037
FITEM,2,1039
FITEM,2,-1042
FITEM,2,1044
FITEM,2,1046
FITEM,2,-1047
ADELE,P51X,,.1 ! Deleting Unselected Areas

ALLSEL,ALL
FLST,2,20,4,ORDE,5
FITEM,2,48
FITEM,2,57
FITEM,2,428
FITEM,2,-444
FITEM,2,1502
LDELE,P51X,,.1 ! Deleting Unneeded Lines

FLST,3,1,4,ORDE,1 ! STR Upper Edge Lines
FITEM,3,2071
LGEN,2,P51X,,.38*(33.3/109),38*(103.8/109),.0
FLST,3,1,3,ORDE,1
FITEM,3,1018
KGEN,2,P51X,,.38,,.0
LSTR, 1003, 1001

LSTR, 1003, 1018
LSTR, 1018, 1033
LSTR, 1001, 727
LSTR, 1001, 177
LSTR, 1002, 1019
LSTR, 1019, 1031
LSTR, 177, 1030
LSTR, 727, 1032 ! Creating Lines for STR Areas

NUMMRG,KP,... ! Merging Coincident Keypoints

```

FLST,2,4,4
 FITEM,2,2002
 FITEM,2,2059
 FITEM,2,2004
 FITEM,2,2001
 AL,P51X
 FLST,2,3,4
 FITEM,2,176
 FITEM,2,2005
 FITEM,2,2004
 AL,P51X
 FLST,2,4,4
 FITEM,2,2000
 FITEM,2,2005
 FITEM,2,2071
 FITEM,2,2006
 AL,P51X
 FLST,2,4,4
 FITEM,2,2007
 FITEM,2,2071
 FITEM,2,2062
 FITEM,2,2008
 AL,P51X
 FLST,2,4,4
 FITEM,2,176
 FITEM,2,2008
 FITEM,2,2079
 FITEM,2,2009
 AL,P51X
 FLST,2,4,4
 FITEM,2,2009
 FITEM,2,2059
 FITEM,2,2003
 FITEM,2,2078
 AL,P51X

! STR Areas

wpcff,0,0,-383/2
 FLST,2,3,5,ORDE,3
 FITEM,2,119
 FITEM,2,1035
 FITEM,2,1045
 ASBW,P51X
 wpcff,0,0,383
 FLST,2,3,5,ORDE,3
 FITEM,2,121
 FITEM,2,1036
 FITEM,2,1043
 ASBW,P51X

! Cutting Bolster Areas Along Box Width

FLST,2,6,5,ORDE,6
 FITEM,2,1007
 FITEM,2,-1008
 FITEM,2,1011
 FITEM,2,1013
 FITEM,2,1015
 FITEM,2,-1016
 ADELE,P51X,,1

----- Creating Volume Geometry -----

KWPLAN,-1, 1007, 1019, 1004
 wpcff,0,0,4.5
 ASBW, 1003
 wpcff,0,0,-9
 ASBW, 1002
 KWPLAN,-1, 1010, 1018, 1009
 wpcff,0,0,4.5

ASBW, 1005
 wpcff,0,0,-9
 ASBW, 1000
 KWPLAN,-1, 1018, 727, 1003
 LARC,1014,1020,1001,38+4.5,
 LARC,1012,1016,1001,38+4.5,
 FLST,2,1,5,ORDE,1
 FITEM,2,1001
 FLST,3,1,4,ORDE,1
 FITEM,3,2002
 ASBL,P51X,P51X,,KEEP
 FLST,2,1,5,ORDE,1
 FITEM,2,1004
 FLST,3,1,4,ORDE,1
 FITEM,3,2004
 ASBL,P51X,P51X,,KEEP

! Dividing STR Areas for Bolster Thickness

FLST,2,6,5,ORDE,6
 FITEM,2,1001
 FITEM,2,-1002
 FITEM,2,1008
 FITEM,2,1011
 FITEM,2,1015
 FITEM,2,-1016
 VDRAG,P51X,,,,, 2019
 FLST,2,6,5,ORDE,6
 FITEM,2,1001
 FITEM,2,-1002
 FITEM,2,1008
 FITEM,2,1011
 FITEM,2,1015
 FITEM,2,-1016
 VDRAG,P51X,,,,, 2027

! Extruding Bolster Volumes

NUMMRG,KP...
 ! Merging Coincident KP's Lines, Areas and Volumes

KWPLAN,-1, 1021, 1020, 1003
 wpcff,0,0,(1+1.5)*25.4/2
 FLST,2,6,6,ORDE,2
 FITEM,2,7
 FITEM,2,-12
 VSW,P51X
 wpcff,0,0,-(1+1.5)*25.4
 FLST,2,6,6,ORDE,2
 FITEM,2,1
 FITEM,2,-6
 VSW,P51X
 ! Using WPlane to Cut Bolster Volumes for STR
 Thickness.

FLST,2,3,5,ORDE,3
 FITEM,2,1000
 FITEM,2,1003
 FITEM,2,1005
 VDRAG,P51X,,,,, 2143
 FLST,2,3,5,ORDE,3
 FITEM,2,1000
 FITEM,2,1003
 FITEM,2,1005
 VDRAG,P51X,,,,, 2111
 FLST,2,3,5,ORDE,3
 FITEM,2,1007
 FITEM,2,1013
 FITEM,2,1018
 VDRAG,P51X,,,,, 2096
 FLST,2,3,5,ORDE,3
 FITEM,2,1007

FITEM,2,1013
FITEM,2,1018
VDRAG,P51X,..... 2070 ! Extruding STR Volumes

NUMMRG,KP,...
! Merging Coincident KP's Lines, Areas and Volumes

----- Creating Weld Geometry

KWPLAN,-1, 1048, 1049, 1053

wpcff,0,0,8.5
FLST,2,2,6,ORDE,2

FITEM,2,3

FITEM,2,6

VSbw,P51X

KWPAVE, 1042

wpcff,0,0,-8.5

FLST,2,2,6,ORDE,2

FITEM,2,32

FITEM,2,35

VSbw,P51X

KWPLAN,-1, 1050, 1047, 1051

wpcff,0,0,8.5

FLST,2,2,6,ORDE,2

FITEM,2,2

FITEM,2,5

VSbw,P51X

KWPAVE, 1045

wpcff,0,0,-8.5

FLST,2,2,6,ORDE,2

FITEM,2,31

FITEM,2,34

VSbw,P51X

! Using CPlane to Cut STR Volumes for Weld..

KWPLAN,-1, 1074, 1096, 1073

LARC,1096,1073,1074,0.2500372547E+02,

LARC,1088,1066,1001,25.00372547,

LARC,1092,1068,1067,25.00372547,

FLST,2,4,4

FITEM,2,2179

FITEM,2,2013

FITEM,2,2014

FITEM,2,2228

AL,P51X

FLST,2,4,4

FITEM,2,2181

FITEM,2,2014

FITEM,2,2141

FITEM,2,2207

AL,P51X

FLST,2,2,6,ORDE,2

FITEM,2,1

FITEM,2,4

FLST,3,2,5,ORDE,2

FITEM,3,1007

FITEM,3,1130

VSBA,P51X,P51X ! Cutting STR Pie Shaped Volumes

KDISTANCE, 1074, 1102

LARC,1102,1084,1074,0.5100372640E+02,

LARC,1098,1077,1001,51.0037264,

LARC,1100,1080,1067,51.0037264,

FLST,2,4,4

FITEM,2,2205

FITEM,2,2186

FITEM,2,2199

FITEM,2,2237

AL,P51X

FLST,2,4,4

FITEM,2,2165

FITEM,2,2199

FITEM,2,2204

FITEM,2,2168

AL,P51X

FLST,2,2,6,ORDE,2

FITEM,2,33

FITEM,2,36

FLST,3,2,5,ORDE,2

FITEM,3,1000

FITEM,3,1019

VSBA,P51X,P51X

! Cutting STR Cresent Shaped Volumes

KWPLAN,-1, 1094, 1093, 1078

wpcff,0,0,8.5

FLST,2,6,6,ORDE,2

FITEM,2,19

FITEM,2,-24

VSbw,P51X

KWPAVE, 1086

wpcff,0,0,-8.5

FLST,2,6,6,ORDE,2

FITEM,2,25

FITEM,2,-30

VSbw,P51X

! Using WPlane to Cut Bolster Volumes for Weld

LSTR, 1075, 1114

LSTR, 1073, 1115

LSTR, 1096, 1113

FLST,2,3,4

FITEM,2,2182

FITEM,2,2287

FITEM,2,2149

AL,P51X

FLST,2,3,4

FITEM,2,2286

FITEM,2,2150

FITEM,2,2178

AL,P51X

FLST,2,3,4

FITEM,2,2151

FITEM,2,2232

FITEM,2,2284

AL,P51X

FLST,2,4,4

FITEM,2,2274

FITEM,2,2149

FITEM,2,2188

FITEM,2,2150

AL,P51X

FLST,2,4,4

FITEM,2,2150

FITEM,2,2013

FITEM,2,2275

FITEM,2,2151

AL,P51X

FLST,2,5,5,ORDE,5

FITEM,2,1106

FITEM,2,-1107

FITEM,2,1109

FITEM,2,1154

FITEM,2,1226

VA,P51X

FLST,2,5,5,ORDE,5

FITEM,2,1107

FITEM,2,-1108

```

FITEM,2,1110
FITEM,2,1147
FITEM,2,1229
VA,P51X
LSTR, 1097, 1112
FLST,2,3,4
FITEM,2,2152
FITEM,2,2233
FITEM,2,2285
AL,P51X
FLST,2,4,4
FITEM,2,2269
FITEM,2,2152
FITEM,2,2231
FITEM,2,2151
AL,P51X
FLST,2,5,5,ORDE,5
FITEM,2,1108
FITEM,2,1111
FITEM,2,-1112
FITEM,2,1177
FITEM,2,1223
VA,P51X
! Top Outside Weld

LSTR, 1109, 1087
LSTR, 1106, 1084
FLST,2,3,4
FITEM,2,2206
FITEM,2,2280
FITEM,2,2153
AL,P51X
FLST,2,3,4
FITEM,2,2154
FITEM,2,2200
FITEM,2,2279
AL,P51X
FLST,2,4,4
FITEM,2,2213
FITEM,2,2258
FITEM,2,2154
FITEM,2,2153
AL,P51X
FLST,2,5,5,ORDE,4
FITEM,2,1113
FITEM,2,-1115
FITEM,2,1161
FITEM,2,1218
VA,P51X
LSTR, 1107, 1102
LSTR, 1111, 1103
FLST,2,3,4
FITEM,2,2278
FITEM,2,2236
FITEM,2,2155
AL,P51X
FLST,2,3,4
FITEM,2,2238
FITEM,2,2156
FITEM,2,2282
AL,P51X
FLST,2,4,4
FITEM,2,2155
FITEM,2,2240
FITEM,2,2156
FITEM,2,2264
AL,P51X
FLST,2,5,5,ORDE,4
FITEM,2,1116
FITEM,2,-1118
FITEM,2,1179

FITEM,2,1220
VA,P51X
FLST,2,4,4
FITEM,2,2154
FITEM,2,2155
FITEM,2,2253
FITEM,2,2186
AL,P51X
FLST,2,5,5,ORDE,5
FITEM,2,1114
FITEM,2,1116
FITEM,2,1119
FITEM,2,1188
FITEM,2,1214
VA,P51X
! Bottom Outside Weld

KWPLAN,-1, 1033, 1032, 1003
CSYS,4
FLST,3,6,6,ORDE,2
FITEM,3,25
FITEM,3,-30
VSymm,Z,P51X,,,0,0
! Reflecting Weld Volumes to Inside

NUMMRG,KP,...
! Merging Coincident KP's Lines, Areas and Volumes

VPLOT
FINISH
FINISH
|-----|
|-----|
|-----|

```

❖ Filename: 6_3_submodel_mesh_INPUT

```

=====
|                                     Sub-model Meshing Routine
=====

/TITLE,Meshing Sub-model Volume with Solid
Elements
/FILNAME,sub_mesh
/PRER7

KWPAVE, 1106
wpoff,0,0,20
ALLSEL,ALL
FLST,2,6,6,ORDE,4
FITEM,2,33
FITEM,2,36
FITEM,2,51
FITEM,2,-54
VSBW,P51X      ! Cutting Bolster Volumes
                ! To Help With Meshing

|-----
|----- Selecting Corner Piece Only
|-----

FLST,5,24,6,ORDE,22
FITEM,5,1
FITEM,5,4
FITEM,5,7
FITEM,5,12
FITEM,5,-13
FITEM,5,18
FITEM,5,-19
FITEM,5,24
FITEM,5,26
FITEM,5,30
FITEM,5,-31
FITEM,5,33
FITEM,5,-34
FITEM,5,47
FITEM,5,-50
FITEM,5,54
FITEM,5,-55
FITEM,5,60
FITEM,5,-61
FITEM,5,66
FITEM,5,68
FITEM,5,72
VSEL,,P51X
FLST,5,4,6,ORDE,4
FITEM,5,19
FITEM,5,24
FITEM,5,33
FITEM,5,54
VSEL,U,,P51X
ALLSEL,BELOW,VOLU

|-----
|----- Meshing Corner Piece Only
|-----

! LSize Intersection Region
FLST,5,2,4,ORDE,2
FITEM,5,2251
FITEM,5,2273
CM,_Y,LINE

LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,,.5,1,! Weld Toe Through Thickness
CMDEL,,_Y
CMDEL,,_Y1
FLST,5,3,4,ORDE,3
FITEM,5,2277
FITEM,5,2279
FITEM,5,2286
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,,.5,0.5,! Weld Depth
CMDEL,,_Y
CMDEL,,_Y1
FLST,5,4,4,ORDE,4
FITEM,5,2005
FITEM,5,2036
FITEM,5,2055
FITEM,5,2113
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,,.2,1,! Bolster Thickness
CMDEL,,_Y
CMDEL,,_Y1
FLST,5,3,4,ORDE,3
FITEM,5,2039
FITEM,5,2050
FITEM,5,2110
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,,.8,0.5,! STR Thickness
CMDEL,,_Y
CMDEL,,_Y1
FLST,5,1,4,ORDE,1
FITEM,5,2150
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,,.5,0.5,! Weld Throat Top
CMDEL,,_Y
CMDEL,,_Y1
FLST,5,1,4,ORDE,1
FITEM,5,2154
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,,.5,2,! Weld Throat Bottom
CMDEL,,_Y
CMDEL,,_Y1
FLST,5,2,4,ORDE,2
FITEM,5,2178
FITEM,5,2200
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,,_Y
LESIZE,_Y1,,.3,1,! Weld Height
CMDEL,,_Y

```

CMDL,_Y1		FITEM,5,2003	
EXTOPT,ESIZE,20,0	! 20 Sweep Divisions	FITEM,5,2136	
EXTOPT,ACLEAR,1	! Clear Source Areas	CM,_Y,LINE	
		LSEL,,,P51X	
ET,2,SOLID95	! Solid 95 Element	CM,_Y1,LINE	
		CMSL,_Y	
		LESIZE,_Y1,,.2,1	! Laize Transition Areas
VSWEEP,18,1078,1074		CMDL,_Y	
VSWEEP,26,1107,1108		CMDL,_Y1	
VSWEEP,60,1227,1224		EXTOPT,ESIZE,20,0	! 20 Sweep Divisions
VSWEEP,13,1048,1052		EXTOPT,ACLEAR,1	! Clear Source Areas
VSWEEP,55,1215,1216		VSWEEP,47,1146,1175	
VSWEEP,30,1114,1116		VSWEEP,1,1126,1123	! Sweeping Transition Areas
	! Sweep Meshing Intersection Region		
		ALLSEL,ALL	
FLST,5,1,4,ORDE,1		-----	
FITEM,5,2190		----- Meshing Bolster Corner Only	
CM,_Y,LINE		-----	
LSEL,,,P51X			
CM,_Y1,LINE		ALLSEL,ALL	
CMSL,_Y		FLST,5,14,6,ORDE,14	
LESIZE,_Y1,,.5,2	! Pie Section Line Sizing	FITEM,5,1	
CMDL,_Y		FITEM,5,4	
CMDL,_Y1		FITEM,5,13	
FLST,5,1,4,ORDE,1		FITEM,5,18	
FITEM,5,2227		FITEM,5,26	
CM,_Y,LINE		FITEM,5,30	
LSEL,,,P51X		FITEM,5,-31	
CM,_Y1,LINE		FITEM,5,47	
CMSL,_Y		FITEM,5,55	
LESIZE,_Y1,,.5,0.5	! Pie Section Line Sizing	FITEM,5,60	
CMDL,_Y		FITEM,5,73	
CMDL,_Y1		FITEM,5,78	
EXTOPT,ESIZE,5,2	! Sweep Divisions, Ratio	FITEM,5,-79	
EXTOPT,ACLEAR,1		FITEM,5,84	
VSWEEP,31,1132,1134	! Sweeping Pie Section	VSEL,S,,P51X	
		ALLSEL,BELOW,VOLU	! Selecting Volumes
FLST,5,1,4,ORDE,1		FLST,5,2,4,ORDE,2	
FITEM,5,2219		FITEM,5,2323	
CM,_Y,LINE		FITEM,5,2350	
LSEL,,,P51X		CM,_Y,LINE	
CM,_Y1,LINE		LSEL,,,P51X	
CMSL,_Y		CM,_Y1,LINE	
LESIZE,_Y1,,.5,2	! Crescent Section Line Sizing	CMSL,_Y	
CMDL,_Y		LESIZE,_Y1,,.2,1	! Outside Thickness Div's, Ratio
CMDL,_Y1		CMDL,_Y	
FLST,5,1,4,ORDE,1		CMDL,_Y1	
FITEM,5,2246		FLST,5,3,4,ORDE,3	
CM,_Y,LINE		FITEM,5,2355	
LSEL,,,P51X		FITEM,5,-2356	
CM,_Y1,LINE		FITEM,5,2365	
CMSL,_Y		CM,_Y,LINE	
LESIZE,_Y1,,.5,0.5	! Crescent Section Line Sizing	LSEL,,,P51X	
CMDL,_Y		CM,_Y1,LINE	
CMDL,_Y1		CMSL,_Y	
FLST,5,1,4,ORDE,1		LESIZE,_Y1,,.10,3	! Transition Div's, Ratio
FITEM,5,2215		CMDL,_Y	
CM,_Y,LINE		CMDL,_Y1	
LSEL,,,P51X		EXTOPT,ESIZE,20,0	! 20 Sweep Divisions
CM,_Y1,LINE		EXTOPT,ACLEAR,1	! Clear Source Areas
CMSL,_Y			
LESIZE,_Y1,,.10,1	! Crescent Section Line Sizing	VSWEEP,84,1301,1298	
CMDL,_Y		VSWEEP,79,1288,1290	
CMDL,_Y1			! Sweeping Bolster Transition Regions
EXTOPT,ESIZE,5,2	! Sweep Divisions, Ratio		
EXTOPT,ACLEAR,1		FLST,5,3,4,ORDE,3	
VSWEEP,4,1190,1189	! Sweeping Crescent Section	FITEM,5,2319	
FLST,5,2,4,ORDE,2			

```

FITEM,5,2322
FITEM,5,2349
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,,20,1/3, ! LSIZE Bolster Outside Length
CMDEL,_Y
CMDEL,_Y1
FLST,5,2,4,ORDE,2
FITEM,5,2073
FITEM,5,2097
CM,_Y,LINE
LSEL,,,P51X
CM,_Y1,LINE
CMSEL,_Y
LESIZE,_Y1,,1,1, ! LSize on Outside Edge
CMDEL,_Y
CMDEL,_Y1

VSWEEP,73,1254,1258
VSWEEP,78,1282,1278
! Sweeping Bolster Outside Volumes

-----
----- Meshing Upper Straight Section Only
-----

ALLSEL,ALL
FLST,5,28,6,ORDE,27
FITEM,5,1
FITEM,5,4
FITEM,5,-5
FITEM,5,13
FITEM,5,15
FITEM,5,-16
FITEM,5,18
FITEM,5,26
FITEM,5,-27
FITEM,5,29
FITEM,5,-31
FITEM,5,43
FITEM,5,-44
FITEM,5,46
FITEM,5,-47
FITEM,5,55
FITEM,5,57
FITEM,5,-58
FITEM,5,60
FITEM,5,73
FITEM,5,75
FITEM,5,-76
FITEM,5,78
FITEM,5,-79
FITEM,5,81
FITEM,5,-82
FITEM,5,84
VSEL,S,,P51X
ALLSEL,BELOW,VOLU ! Selecting Volumes

VSWEEP,46,1186,1184
VSWEEP,5,1123,1125
VSWEEP,15,1052,1070
VSWEEP,16,1074,1075
VSWEEP,44,1175,1176
VSWEEP,43,1171,1172
VSWEEP,29,1116,1117
VSWEEP,57,1216,1221
VSWEEP,58,1224,1225
VSWEEP,27,1108,1111
VSWEEP,81,1290,1295
VSWEEP,82,1298,1297
VSWEEP,75,1258,1274
VSWEEP,76,1278,1277 ! Sweeping Commands

-----
----- Reflecting Mesh to Other Side
-----

EXTOPT,ESIZE,30,3,
EXTOPT,ACLEAR,1 ! Sweep Options

VSWEEP,59,1227,1228
VSWEEP,56,1215,1217
VSWEEP,25,1107,1106
VSWEEP,28,1114,1113
VSWEEP,40,1157,1158
VSWEEP,39,1146,1151
VSWEEP,17,1078,1079

ALLSEL,ALL
FLST,2,36,6,ORDE,17
FITEM,2,2
FITEM,2,-3
FITEM,2,7
FITEM,2,-12

```

```

FITEM,2,19
FITEM,2,-24
FITEM,2,32
FITEM,2,34
FITEM,2,-35
FITEM,2,37
FITEM,2,-38
FITEM,2,41
FITEM,2,45
FITEM,2,48
FITEM,2,-50
FITEM,2,61
FITEM,2,-72
VDELE,P51X,,,1
ADELE, 1006,,,1
FLST,2,4,4,ORDE,4
FITEM,2,2010
FITEM,2,-2011
FITEM,2,2147
FITEM,2,-2148
LDELE,P51X,,,1 ! Deleting OtherSide Volumes, etc.

KWPAVE, 1033
CSYS,4 ! Move CPlane and set active CS to CPlane

FLST,3,42,6,ORDE,17
FITEM,3,1
FITEM,3,4
FITEM,3,-6
FITEM,3,13
FITEM,3,-18
FITEM,3,25
FITEM,3,-31
FITEM,3,39
FITEM,3,-40
FITEM,3,42
FITEM,3,-44
FITEM,3,46
FITEM,3,-47
FITEM,3,55
FITEM,3,-60
FITEM,3,73
FITEM,3,-84
VSymm,Z,P51X,,,0,0 ! Reflect Volumes and Mesh

NSEL,S,LOC,Z,-1,1 ! Selecting Center Nodes
NUMMRG,NODE,,, ! Merging Co-incident Nodes
NUMMRG,KP,,, ! Merging Co-incident KP's, Lines, Areas
ALLSEL,ALL
NUMMRG,KP,,, ! Merging Co-incident KP's, Lines, Areas
NUMCMP,ELEM ! Compressing Element Numbers
NUMCMP,NODE ! Compressing Node Numbers

WPSTYLE,,,,,0 ! Turn Off CPlane Display

! Change Active Co-ordinate System to Global Co-
ordinate System
CSYS,0

FINISH
FINISH

|-----
|-----
|-----

```


❖ Filename: 6_4_submodel_tran_INPUT

```

=====
|                                     |
|      Boundary Condition Transfer Routine      |
|                                     |
=====

/TITLE,Performing Cut Boundary Interpolation
/FILNAME,sub_mod1
/PRER7

NUMOFF,NODE,200000,
! Offset Node Number by 200000

|-----|
|-----| Selecting Cut Boundary Nodes
|-----|

FLST,5,44,5,ORDE,44
FITEM,5,1044
FITEM,5,-1045
FITEM,5,1049
FITEM,5,-1050
FITEM,5,1053
FITEM,5,1056
FITEM,5,-1057
FITEM,5,1061
FITEM,5,1063
FITEM,5,1065
FITEM,5,1070
FITEM,5,1075
FITEM,5,1079
FITEM,5,1083
FITEM,5,1217
FITEM,5,1221
FITEM,5,1225
FITEM,5,1228
FITEM,5,1230
FITEM,5,1233
FITEM,5,1236
FITEM,5,1239
FITEM,5,1267
FITEM,5,1269
FITEM,5,1273
FITEM,5,-1274
FITEM,5,1277
FITEM,5,1281
FITEM,5,1283
FITEM,5,1295
FITEM,5,1297
FITEM,5,1300
FITEM,5,1306
FITEM,5,1308
FITEM,5,1315
FITEM,5,1317
FITEM,5,1320
FITEM,5,1324
ASEL,S,,P51X
FLST,5,16,5,ORDE,16
FITEM,5,1044
FITEM,5,1050
FITEM,5,1056

FITEM,5,1065
FITEM,5,1070
FITEM,5,1075
FITEM,5,1079
FITEM,5,1083
FITEM,5,1217
FITEM,5,1221
FITEM,5,1225
FITEM,5,1228
FITEM,5,1230
FITEM,5,1233
FITEM,5,1236
FITEM,5,1239
ASEL,U,,P51X
NSLA,S,1 ! Selecting Bolster Cut Boundary Areas
NWRITE,sub_bol,NODE,,0 ! Writing sub_bol.node

ALLSEL,ALL
FLST,5,10,5,ORDE,10
FITEM,5,1019
FITEM,5,1039
FITEM,5,1128
FITEM,5,1144
FITEM,5,1149
FITEM,5,1153
FITEM,5,1155
FITEM,5,1165
FITEM,5,1187
FITEM,5,1199
ASEL,S,,P51X ! Selecting Stringer Top and Bottom
! Cut Boundary Areas
NSLA,S,1 ! Selecting Nodes Attached to Areas
NWRITE,sub_str1,NODE,,0 ! Writing sub_str1.node

ALLSEL,ALL
FLST,5,24,5,ORDE,24
FITEM,5,1027
FITEM,5,1034
FITEM,5,1044
FITEM,5,1050
FITEM,5,1056
FITEM,5,1065
FITEM,5,1070
FITEM,5,1075
FITEM,5,1079
FITEM,5,1083
FITEM,5,1125
FITEM,5,1129
FITEM,5,1142
FITEM,5,1151
FITEM,5,1158
FITEM,5,1164
FITEM,5,1167
FITEM,5,1169
FITEM,5,1172
FITEM,5,1176
FITEM,5,1184
FITEM,5,1192
FITEM,5,-1193
FITEM,5,1197
ASEL,S,,P51X ! Selecting Stringer Edges
! Cut Boundary Areas
NSLA,S,1 ! Selecting Nodes Attached to Areas
NWRITE,sub_str2,NODE,,0 ! Writing sub_str2.node

ALLSEL,ALL

```

FINISH

----- Performing Cut Boundary Interpolation

RESUME,May_31_Rubber.db ! Shell Element File

FLST,5,54,5,ORDE,30

FITEM,5,11

FITEM,5,18

FITEM,5,-21

FITEM,5,23

FITEM,5,-24

FITEM,5,26

FITEM,5,-27

FITEM,5,33

FITEM,5,36

FITEM,5,53

FITEM,5,71

FITEM,5,117

FITEM,5,-125

FITEM,5,129

FITEM,5,131

FITEM,5,-133

FITEM,5,137

FITEM,5,-138

FITEM,5,143

FITEM,5,151

FITEM,5,-153

FITEM,5,155

FITEM,5,253

FITEM,5,-254

FITEM,5,544

FITEM,5,-549

FITEM,5,679

FITEM,5,-689

FITEM,5,693

FITEM,5,1032

ASEL,S,,P51X

FLST,5,7,5,ORDE,5

FITEM,5,33

FITEM,5,129

FITEM,5,682

FITEM,5,-685

FITEM,5,1032

ASEL,U,,P51X

ASEL,U,,,143

ALLSEL,BELOW,AREA

! Selecting Required Areas and Elements Only

/POST1

INRES,

FILE,May_31_Rubber.rst, ! Read in Results

SET,FIRST

/TITLE,Performing Cut Boundary Interpolation

FLST,5,6,5,ORDE,4 ! Interpolation on Bolster

FITEM,5,19

FITEM,5,117

FITEM,5,119

FITEM,5,-122

ASEL,R,,P51X

ALLSEL,BELOW,AREA

! Selecting Bolster Elements Only

CBDOF,sub_bol,NODE,,sub_bol,CBDO,,0,,1

ALLSEL,ALL

FLST,5,54,5,ORDE,30

FITEM,5,11

FITEM,5,18

FITEM,5,-21

FITEM,5,23

FITEM,5,-24

FITEM,5,26

FITEM,5,-27

FITEM,5,33

FITEM,5,36

FITEM,5,53

FITEM,5,71

FITEM,5,117

FITEM,5,-125

FITEM,5,129

FITEM,5,131

FITEM,5,-133

FITEM,5,137

FITEM,5,-138

FITEM,5,143

FITEM,5,151

FITEM,5,-153

FITEM,5,155

FITEM,5,253

FITEM,5,-254

FITEM,5,544

FITEM,5,-549

FITEM,5,679

FITEM,5,-689

FITEM,5,693

FITEM,5,1032

ASEL,S,,P51X

FLST,5,7,5,ORDE,5

FITEM,5,33

FITEM,5,129

FITEM,5,682

FITEM,5,-685

FITEM,5,1032

ASEL,U,,P51X

ASEL,U,,,143

ALLSEL,BELOW,AREA

! Selecting Required Areas and Elements Only

FLST,5,3,5,ORDE,3 ! Interpolation on Stringer

FITEM,5,681

FITEM,5,686

FITEM,5,688

ASEL,R,,P51X

ALLSEL,BELOW,AREA

! Selecting STR Elements Only

!CBDOF,sub_str1,NODE,,sub_str1,CBDO,,0,,1

!CBDOF,sub_str2,NODE,,sub_str2,CBDO,,0,,1

CSYS,0 ! Ensuring Active CS of Global CS

CBDOF,,,,,0,,1 ! Interpolation Command

FINISH

RESUME,sub_mesh.db

/PREP7 ! Read in Cut Boundary Constraints

/INPUT,sub_mod1,cdbdo,,1,0

/INPUT,sub_mod1,cdbdo,,CB1,0

FINISH

❖ *Filename: 7 1 frame Main INPUT*

```

=====
! FEA of 930E Frame Displacements
=====
!
!----- Geometry Creation
!-----
!
FINISH
FINISH
/CLEAR,START
/FILNAME,frm_geom
/INPUT,7_2_frame_geom,_INPUT,...,0
! Creating Frame Solid Geometry
/INPUT,7_3_frame_mesh,_INPUT,...,0
! Meshing Geometry
SAVE
! Saving frm_geom.db
/EOF

!----- FEA Loads and Solve
!-----
!
:FEA
FINISH
FINISH
/CLEAR
RESUME,frm_geom.db
/FILNAME,frm_FEA

! Strut pressures
*SET,RRpres,139.5 ! kg/cm^2
*SET,LRpres,92.4 ! kg/cm^2
*SET,RFpres,40.9 ! kg/cm^2
*SET,LFpres,60.9 ! kg/cm^2
/INPUT,7_4_frame_loads,_INPUT,...,0 ! Applying BC's

/SOLU
/TITLE,Load Set 1:
LSWRITE,1,
FINISH

/SOLU
!SOLVE
LSSOLVE,1,1,1, ! Solve Load Steps 1 thru 1, incr 1
FINISH
SAVE
! Saving frm_FEA.db

/DELETE,frm_FEA,emat,
/DELETE,frm_FEA,esav,
/DELETE,frm_FEA,mnir,
/DELETE,frm_FEA,stat,
/DELETE,frm_FEA,tri, ! Cleanup
/DELETE,frm_FEA,log,
/DELETE,frm_FEA,err,
/DELETE,frm_FEA,s01,
/DELETE,frm_FEA,s02,
/DELETE,frm_FEA,s03,
/DELETE,frm_FEA,s04,

/EOF

```

❖ Filename: 7_2_frame_geom_INPUT

```

*****
!
!      930E Frame Geometry Creation Routine
!
*****

/TITLE,930E Frame Geometry

!-----
!----- Setup
!-----

/NOPR
KEYW,PR_SET,1
KEYW,PR_STRUC,1
/GO

/PREP7

ET,1,SHELL93      ! Defining Shell Element Type
KEYOPT,1,4,0
KEYOPT,1,5,0
KEYOPT,1,6,0

!-----
!----- Defining Real Constants
!-----
!R,3,3, , , , , ,      ! 1/8" Exhaust Plenum
!R,5,5, , , , , ,      ! 5mm Thickness
!R,8,8, , , , , ,      ! 8mm Thickness
!R,9,9, , , , , ,      ! 9mm Thickness

!-----
!----- Material Properties
!-----
! 690 MPa Tensile Strength
! 620 Mpa Yield Strength
! Elongation in 50mm - 18%
! Modulus is Unknown
UIMP,1,EX, , ,207000,      ! Modulus in N/mm^2
UIMP,1,DENS, , ,0.00000786,      ! Density in kg/mm^3
UIMP,1,ALPX, , , , , , ,
UIMP,1,REFT, , , , , , ,
UIMP,1,NUXY, , , , , , ,
UIMP,1,PRXY, , , , , , ,3,
UIMP,1,GXY, , , , , , ,
UIMP,1,MU, , , , , , ,
UIMP,1,DAMP, , , , , , ,

!-----
!----- Torsion Tubes and Rear Section
!-----

K, ,0,-280.5-640,-3490-240,
      ! KP at Center of Rear Torsion Tube

wprot,0,0,90
KWPAVE, ,1
PCIRC,300, ,0,360,      ! Rear T-Tube Circle
ADELE, ,1
WPCSYS,1
FLST,3,4,4,ORDE,2
FITEM,3,1
FITEM,3,-4
LGEN,2,P51X, , ,191, , ,0
WPSTYLE, , , ,0
FLST,3,2,3,ORDE,2
FITEM,3,7
FITEM,3,9

KGEN,2,P51X, , ,457, , ,0
LSTR, ,3, ,7
LSTR, ,6, ,2
LSTR, ,9, ,5
LSTR, ,4, ,8
LSTR, ,7, ,10
LSTR, ,9, ,11      ! Lines to Main Rail

WPSTYLE, , , ,1
wprot,0,0,90
KWPAVE, ,1
CSYS,4
K, ,3240,-47,0,
KWPAVE, ,12
PCIRC,535.5/2, ,0,360,      ! Center T-Tube Circle
ADELE, ,1

FLST,3,2,3,ORDE,2
FITEM,3,14
FITEM,3,16
KGEN,2,P51X, , , ,813-104.3281654, ,0
LSTR, ,17, ,14
LSTR, ,18, ,16      ! Lines to Main Rail

CSYS,0
FLST,3,1,3,ORDE,1
FITEM,3,17
KGEN,2,P51X, , , ,460-(535.5/2), ,0
FLST,3,1,3,ORDE,1
FITEM,3,10
KGEN,2,P51X, , , ,113, , ,0
LSTR, ,20, ,19
KWPLAN,-1, ,20, ,19, ,10
CSYS,4      ! Active CS is in Plane of Main Rail

wpoft,-240,-227,0
PCIRC,152/2, ,0,360,
CSYS,4
FLST,3,4,4,ORDE,2
FITEM,3,22
FITEM,3,-25
LGEN,2,P51X, , , ,273.930+25, , ,0
PCIRC,152/2+60, ,0,360,
FLST,3,4,4,ORDE,2
FITEM,3,30
FITEM,3,-33
LGEN,2,P51X, , , ,273.930+25, , ,0
FLST,2,2,5,ORDE,2
FITEM,2,1
FITEM,2,-2
ADELE,P51X      ! Pivot and Rear Strut Pin Holes

LDELE, ,21
KDELE, ,20      ! Deleting Construction Line

CSYS,4
K, ,15*30,227,0,
K, ,735.227,0,
K, ,735.227+864,0,
LSTR, ,20, ,37
LSTR, ,37, ,38
LSTR, ,38, ,34
LSTR, ,20, ,29
LSTR, ,31, ,35      ! Rear Frame Lines

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```

FLST,2.5,4,ORDE,5
FITEM,2,30
FITEM,2,-31
FITEM,2,34
FITEM,2,36
FITEM,2,-37
LDELE,P51X,,1      ! Deleting Un-needed Lines
FLST,2,2,4,ORDE,2
FITEM,2,13
FITEM,2,-14
LDELE,P51X,,1

FLST,2,4,4
FITEM,2,12
FITEM,2,9
FITEM,2,2
FITEM,2,6
AL,P51X
FLST,2,4,4
FITEM,2,3
FITEM,2,12
FITEM,2,7
FITEM,2,11
AL,P51X
FLST,2,4,4
FITEM,2,8
FITEM,2,4
FITEM,2,11
FITEM,2,10
AL,P51X
FLST,2,4,4
FITEM,2,5
FITEM,2,1
FITEM,2,9
FITEM,2,10
AL,P51X      ! Middle Rear T-Tube Areas
CSYS,0      ! Active CS to Global CS

KGEN,2,7,,,-2000,,0
LSTR, 7, 10
FLST,2,4,4,ORDE,2
FITEM,2,5
FITEM,2,-8
ADRAG,P51X,,,,, 13 ! Rear T-Tube B4 Cutting

FLST,2,8,4
FITEM,2,39
FITEM,2,38
FITEM,2,21
FITEM,2,40
FITEM,2,33
FITEM,2,32
FITEM,2,41
FITEM,2,35
AL,P51X      ! Rear Frame Area

FLST,2,4,5,ORDE,2
FITEM,2,5
FITEM,2,-8
FLST,3,1,5,ORDE,1
FITEM,3,9
ASBA,P51X,P51X,,KEEP
FLST,2,4,5,ORDE,2
FITEM,2,14
FITEM,2,-17
ADELE,P51X,,1
LDELE, 13,,1      ! Trimming Rear T-Tube with Rail Side

FLST,2,4,4
FITEM,2,23
FITEM,2,22
FITEM,2,25
FITEM,2,24
AL,P51X
FLST,2,4,4
FITEM,2,29
FITEM,2,28
FITEM,2,27
FITEM,2,26
AL,P51X
FLST,2,4,4
FITEM,2,50
FITEM,2,51
FITEM,2,46
FITEM,2,48
AL,P51X
FLST,3,3,5,ORDE,2
FITEM,3,5
FITEM,3,-7
ASBA, 9,P51X      ! Subtracting Pin Hole Areas

FLST,2,2,4,ORDE,2
FITEM,2,19
FITEM,2,-20
LDELE,P51X,,1
FLST,3,1,3,ORDE,1
FITEM,3,14
KGEN,2,P51X,,,-2000,,0
LSTR, 14, 10
FLST,2,4,4,ORDE,2
FITEM,2,15
FITEM,2,-18
ADRAG,P51X,,,,, 13
FLST,2,4,5,ORDE,3
FITEM,2,5
FITEM,2,-7
FITEM,2,9
ASBW,P51X
FLST,2,4,5,ORDE,3
FITEM,2,14
FITEM,2,19
FITEM,2,-21
ADELE,P51X,,1
LDELE, 13,,1      ! Completing Center T-Tube

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----- Main Rail Side Areas
-----

CSYS,4
FLST,3,1,3,ORDE,1
FITEM,3,38
KGEN,2,P51X,,,-1636-735,,0
FLST,3,1,3,ORDE,1
FITEM,3,10
KGEN,2,P51X,,,-1560,540,,0
LSTR, 38, 10
LSTR, 10, 11
FLST,3,1,3,ORDE,1
FITEM,3,37
KGEN,2,P51X,,,-2310,0,,0
LSTR, 11, 17
LSTR, 17, 37
FLST,2,5,4
FITEM,2,38
FITEM,2,20
FITEM,2,13

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FITEM,2.14		KWPAVE, 49	
FITEM,2.19		wpcff,0,-1065,-2175	
AL,P51X	! Rear Side Plate Area	wprot,0,0.90	
		PCIRC,438/2, ,0.360,	
FLST,3.1,3,ORDE,1		ADELE, 14	! Front Tube Circle
FITEM,3.11			
KGEN,2,P51X, ,540, , ,0		CSYS,4	
FLST,3.1,3,ORDE,1		FLST,3.1,3,ORDE,1	
FITEM,3.17		FITEM,3.49	
KGEN,2,P51X, ,840, , ,0		KGEN,2,P51X, ,2175+1670,-585, ,0	
LSTR, 17, 30		KWPAVE, 55	
LSTR, 30, 18		wprot,9,0.0	
LARC,11,18,36,1045,		CSYS,4	
FLST,2.4.4		CSYS,4	
FITEM,2.58		FLST,3.1,3,ORDE,1	
FITEM,2.59		FITEM,3.55	
FITEM,2.56		KGEN,2,P51X, ,0,-305, ,0	
FITEM,2.52		FLST,3.2,3,ORDE,2	
AL,P51X		FITEM,3.55	
FLST,2.4.4		FITEM,3.-56	
FITEM,2.19		KGEN,2,P51X, ,,-203,0, ,0	
FITEM,2.30		LSTR, 58, 56	
FITEM,2.31		LSTR, 56, 55	
FITEM,2.34		LSTR, 55, 57	
AL,P51X		LSTR, 57, 58	! Bumper Square
ASBA, 7, 6	! Center Side Area		
		LSTR, 49, 52	
FLST,3.1,3,ORDE,1		LSTR, 52, 57	
FITEM,3.38		LSTR, 58, 54	
KGEN,2,P51X, ,5280-735, , ,0		LSTR, 54, 50	
FLST,3.1,3,ORDE,1		FLST,2.2.4,ORDE,2	
FITEM,3.45		FITEM,2.66	
KGEN,2,P51X, ,27*30, , ,0		FITEM,2.-67	
FLST,3.1,3,ORDE,1		FLST,3.2.4,ORDE,2	
FITEM,3.37		FITEM,3.74	
KGEN,2,P51X, ,(219*30)-735, , ,0		FITEM,3.-75	
LSTR, 18, 45		LSBL,P51X,P51X, ,DELETE	
LSTR, 45, 46		LSTR, 50, 60	
LSTR, 46, 47		LSTR, 58, 59	
LSTR, 47, 30		FLST,2.5.4	
FLST,2.5.4		FITEM,2.66	
FITEM,2.31		FITEM,2.77	
FITEM,2.36		FITEM,2.65	
FITEM,2.37		FITEM,2.72	
FITEM,2.42		FITEM,2.61	
FITEM,2.43		AL,P51X	
AL,P51X	! Forward Side Area	FLST,2.5.4	
		FITEM,2.76	
FLST,3.1,3,ORDE,1		FITEM,2.64	
FITEM,3.37		FITEM,2.73	
KGEN,2,P51X, ,5280+1650-735, , ,0		FITEM,2.71	
FLST,3.2,3,ORDE,2		FITEM,2.67	
FITEM,3.37		AL,P51X	! Front Portion of Main Rails
FITEM,3.-38			
KGEN,2,P51X, ,(263*30)-735, , ,0		CSYS,0	
LSTR, 46, 50		KDISTANCE, 57, 16	
LSTR, 50, 49		FLST,3.1,3,ORDE,1	
LSTR, 49, 48		FITEM,3.55	
LSTR, 48, 47		KGEN,2,P51X, ,,-2000, , ,0	
FLST,2.5.4		LSTR, 61, 55	
FITEM,2.42		FLST,2.4.4,ORDE,2	
FITEM,2.63		FITEM,2.68	
FITEM,2.62		FITEM,2.-71	
FITEM,2.61		ADRAG,P51X, , , , 74	
FITEM,2.60		FLST,3.1,3,ORDE,1	
AL,P51X	! Side Area Near Horse Collar	FITEM,3.52	
		KGEN,2,P51X, ,,-2000, , ,0	
WPCSYS,-1.0		LSTR, 52, 66	
DSYS,0		FLST,2.6.4,ORDE,4	
CSYS,0		FITEM,2.64	

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FLST,2,2,4,ORDE,2
FITEM,2,74
FITEM,2,87
LDELE P51X, . . . 1 ! Deleting Construction Line
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FLST,3,2,3,ORDE,2
FITEM,3.58
FITEM,3-.59
KGEN,2,P51X,,190.5,...,0
LSTR, 62, 59
LSTR, 61, 58
FLST,2,6,4,ORDE,4
FITEM,2.64
FITEM,2-.65
FITEM,2.76
FITEM,2-.79
ADRAG,P51X,,,,, 74
FLST,2,3,4,ORDE,3
FITEM,2.67
FITEM,2.71
FITEM,2.73
ADRAG,P51X,,,,, 75
FLST,2,3,4,ORDE,2
FITEM,2.68
FITEM,2-.70
ADRAG,P51X,,,,, 75 1 Front Main Rail

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FITEM.2-31	
FITEM.2-34	
ADRAG.P51X,.....	139
FLST.2.54,ORDE,5	
FITEM.2-13	
FITEM.2-14	
FITEM.2-19	
FITEM.2-20	
FITEM.2-38	
ADRAG.P51X,.....	148
FLST.2.84,ORDE,6	
FITEM.2-21	
FITEM.2-32	
FITEM.2-33	
FITEM.2-35	
FITEM.2-38	
FITEM.2-41	
ADRAG.P51X,.....	156

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FLST,3,1,3,ORDE,1
FITEM,3.44
KGEN,2,P51X,,.305,...,0
LSTR,,115,,44
FLST,2,4,4,ORDE,4
FITEM,2.52
FITEM,2.56
FITEM,2.58
FITEM,2.59
ADRA9,P51X,,,,,181 ! Extrude Center T-Tube

FLST,3,3,3,ORDE,3
FITEM,3.22
FITEM,3.25
FITEM,3.41
KGEN,2,P51X,,.305,...,0
LSTR,,121,,25
LSTR,,122,,41
LSTR,,120,,22
FLST,2,4,4,ORDE,2
FITEM,2.26
FITEM,2.-29
ADRA9,P51X,,,,,190
FLST,2,4,4,ORDE,4
FITEM,2.46
FITEM,2.48
FITEM,2.50
FITEM,2.-51
ADRA9,P51X,,,,,191
FLST,2,4,4,ORDE,2
FITEM,2.22
FITEM,2.-25
ADRA9,P51X,,,,,192
! Extrude Rear Hole Areas

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FLST,2,4,4
FITEM,2,209
FITEM,2,216
FITEM,2,214
FITEM,2,212
AL,P51X
FLST,2,4,4
FITEM,2,200
FITEM,2,198
FITEM,2,196
FITEM,2,193
AL,P51X

FLST,2,4,4		FITEM,2,95	
FITEM,2,204		FITEM,2,97	
FITEM,2,201		FITEM,2,80	
FITEM,2,208		FITEM,2,91	
FITEM,2,206		AL,P51X	
AL,P51X	! Areas to Subtract from Side	FLST,2,6,4	
		FITEM,2,91	
NUMMRG,KP	! Merge KP's, Lines and Areas	FITEM,2,80	
		FITEM,2,83	
FLST,2,8,4		FITEM,2,85	
FITEM,2,165		FITEM,2,87	
FITEM,2,180		FITEM,2,89	
FITEM,2,178		AL,P51X	! Closing Front Section
FITEM,2,176			
FITEM,2,174		LSTR, 87, 64	
FITEM,2,172		LSTR, 92, 66	
FITEM,2,170		FLST,2,4,4	
FITEM,2,164		FITEM,2,72	
AL,P51X		FITEM,2,90	
FLST,3,3,5,ORDE,2		FITEM,2,82	
FITEM,3,85		FITEM,2,126	
FITEM,3,-87		AL,P51X	
ASBA, 60,P51X		FLST,2,4,4	
FLST,2,5,4		FITEM,2,93	
FITEM,2,164		FITEM,2,66	
FITEM,2,155		FITEM,2,135	
FITEM,2,158		FITEM,2,86	
FITEM,2,147		AL,P51X	
FITEM,2,162		FLST,2,2,5,ORDE,2	
AL,P51X		FITEM,2,21	
FLST,2,4,4		FITEM,2,-22	
FITEM,2,187		ADELE,P51X	
FITEM,2,189		LDELE, 84,,1	
FITEM,2,182		ADELE, 89	
FITEM,2,185		FLST,2,2,4,ORDE,2	
AL,P51X		FITEM,2,83	
FLST,2,4,4		FITEM,2,85	
FITEM,2,147		LCOMB,P51X,,0	
FITEM,2,154		FLST,2,4,4	
FITEM,2,137		FITEM,2,134	
FITEM,2,150		FITEM,2,90	
AL,P51X		FITEM,2,93	
FLST,2,1,5,ORDE,1		FITEM,2,83	
FITEM,2,62		AL,P51X	
FLST,3,1,5,ORDE,1		FLST,2,5,4	
FITEM,3,58		FITEM,2,83	
ASBA,P51X,P51X,,KEEP		FITEM,2,87	
FLST,2,5,4		FITEM,2,89	
FITEM,2,137		FITEM,2,91	
FITEM,2,140		FITEM,2,80	
FITEM,2,142		AL,P51X	! Creating Transition Region
FITEM,2,127			
FITEM,2,146			
AL,P51X		!-----	
FLST,2,5,4		!----- Horse Collar Frontal Area	
FITEM,2,136		!-----	
FITEM,2,127			
FITEM,2,130		CSYS,0	
FITEM,2,132		DSYS,0	
FITEM,2,134		WPCSYS,-1,0	
AL,P51X	! Closing Span of Main Rail	KWPAVE, 90	
		wprol,0,9,0	
FLST,2,4,4		wptff,0,0,-355	
FITEM,2,122		FLST,2,4,5,ORDE,4	
FITEM,2,124		FITEM,2,7	
FITEM,2,95		FITEM,2,44	
FITEM,2,99		FITEM,2,46	
AL,P51X		FITEM,2,86	
FLST,2,5,4		ASBW,P51X	! Cutting Main Rail w/ WPlane
FITEM,2,92			
		KWPAVE, 65	

CSYS,4		K, ,323,1102,,	
FLST,5,4,4,ORDE,4		LSTR, 100, 123	
FITEM,5,94		K, 0,575,,	
FITEM,5,98		LSTR, 72, 129	
FITEM,5,133		K, ,-792,1824-293,,	! Top Arcs
FITEM,5,151		LARC, 123,132,129,1824-250,	
LSEL,S, ,P51X		K, ,-792,960+157,,	
ALLSEL,BELOW,LINE		LARC, 129,135,65,960-190,	
FLST,5,94,5,ORDE,9			
FITEM,5,1		WPCSYS,-1,0	
FITEM,5,-6		KWPAVE, 72	
FITEM,5,8		wprot,0,0,90	
FITEM,5,-43		CSYS,0	
FITEM,5,45		WPAVE,0,0,0	
FITEM,5,47		CSYS,4	
FITEM,5,-85		FLST,2,2,4,ORDE,2	
FITEM,5,87		FITEM,2,219	
FITEM,5,-98		FITEM,2,-220	
ASEL,U, ,P51X		LSBW,P51X	
! Selecting Lines only Near Intersection		LDELE, 224, ,1	
		LDELE, 223, ,1	
		WPCSYS,-1,0	
K, ,404,0,		LSTR, 137, 136	
K, ,387,404,0,		NUMMRG,KP	
K, ,387+153,404+157,0,		FLST,2,8,4	
K, ,387+153,-893,0,		FITEM,2,60	
K, ,320,-1102,0,		FITEM,2,218	
K, ,0,-1102,0,		FITEM,2,222	
LSTR, 83, 72		FITEM,2,219	
LSTR, 83, 86		FITEM,2,221	
LSTR, 86, 91		FITEM,2,217	
LSTR, 91, 96		FITEM,2,169	
LSTR, 96, 97		FITEM,2,62	
LSTR, 72, 65		AL,P51X	! Top Collar Area
LSTR, 68, 97			
FLST,2,10,4		ASBA, 86, 46	! Subtracting Circular Cutout
FITEM,2,98			
FITEM,2,159		KWPLAN,-1, 65, 69, 72	
FITEM,2,60		CSYS,4	! Setting WPlane
FITEM,2,62			
FITEM,2,132		K, ,-77,-1102-119,,	
FITEM,2,136		K, ,-77+126,-1102-119-147,,	
FITEM,2,153		LSTR, 97, 132	
FITEM,2,160		LSTR, 132, 135	
FITEM,2,133		LSTR, 135, 96	
FITEM,2,151		FLST,2,4,4	
AL,P51X	! Area Surrounding Main Rail	FITEM,2,153	
		FITEM,2,220	
FLST,3,1,3,ORDE,1		FITEM,2,223	
FITEM,3,86		FITEM,2,224	
KGEND,P51X, ,150,162, ,0		AL,P51X	! Lower Small Area
K, ,46.5*18,575,,			
K, ,46.5*18,-589,,		K, ,-792,-1350-97-293,,	
LSTR, 91, 104		K, ,-792,-1055-119-97-293,,	
LSTR, 104, 101		LARC, 139,132,72,1055-200,	
LSTR, 101, 100		LARC, 138,135,72,1350-200,	
LSTR, ,100, 86		WPCSYS,-1,0	
FLST,2,5,4		wprot,0,0,90	
FITEM,2,161		FLST,2,2,4,ORDE,2	
FITEM,2,132		FITEM,2,225	
FITEM,2,169		FITEM,2,-226	
FITEM,2,168		LSBW,P51X	
FITEM,2,167		FLST,2,2,4,ORDE,2	
AL,P51X	! Outer Widthwise Area	FITEM,2,229	
		FITEM,2,-230	
wpoff,323,760,0		LDELE,P51X, ,1	
PCIRC,305/2, ,0,360,		LSTR, 140, 141	
KWPAVE, 65	! Area for Circular	FLST,2,4,4	
Cutout...		FITEM,2,227	
		FITEM,2,225	

FITEM,2,228		FITEM,2,136
FITEM,2,223		AL,P51X
AL,P51X	! Lower Collar Area	FLST,2,4,4
<hr/>		
	Extruding Horse Collar Frontal Area	FITEM,2,226
<hr/>		
WPSTYLE,.....,0		FITEM,2,161
KWPLAN,-1, 65, 69, 72		FITEM,2,257
CSYS,4		FITEM,2,258
		AL,P51X
FLST,3,4,5,ORDE,4		FLST,2,4,4
FITEM,3,44		FITEM,2,229
FITEM,3,46		FITEM,2,257
FITEM,3,86		FITEM,2,167
FITEM,3,99		FITEM,2,256
AGEN,2,P51X, , , ,355, ,0	! Copying Areas Over	AL,P51X
		FLST,2,4,4
LSTR, 145, 138		FITEM,2,256
LSTR, 72, 152		AL,P51X
LSTR, 137, 154		FLST,2,4,4
LSTR, 136, 155		FITEM,2,255
LSTR, 143, 100		FITEM,2,217
LSTR, 142, 101		FITEM,2,245
LSTR, 104, 139		FITEM,2,266
LSTR, 91, 138		AL,P51X
LSTR, 96, 145		FLST,2,4,4
LSTR(135, 148		FITEM,2,244
LSTR, 141, 150		FITEM,2,221
LSTR, 149, 140		FITEM,2,266
LSTR, 132, 147		FITEM,2,254
LSTR, 97, 146		AL,P51X
LSTR, 153, 129		FLST,2,4,4
LSTR, 156, 123	! Connecting Lines	FITEM,2,253
		FITEM,2,243
FLST,2,4,4		FITEM,2,219
FITEM,2,263		FITEM,2,254
FITEM,2,234		AL,P51X
FITEM,2,264		FLST,2,4,4
FITEM,2,220		FITEM,2,218
AL,P51X		FITEM,2,252
FLST,2,4,4		FITEM,2,241
FITEM,2,227		FITEM,2,265
FITEM,2,263		AL,P51X
FITEM,2,237		FLST,2,4,4
FITEM,2,262		FITEM,2,222
AL,P51X		FITEM,2,242
FLST,2,4,4		FITEM,2,265
FITEM,2,262		FITEM,2,253
FITEM,2,225		AL,P51X
FITEM,2,261		
FITEM,2,238		LSTR, 108, 159
AL,P51X		LSTR, 105, 158
FLST,2,4,4		LSTR, 119, 157
FITEM,2,261		LSTR, 160, 109
FITEM,2,239		FLST,2,4,4
FITEM,2,260		FITEM,2,168
FITEM,2,228		FITEM,2,248
AL,P51X		FITEM,2,267
FLST,2,4,4		FITEM,2,268
FITEM,2,236		AL,P51X
FITEM,2,259		FLST,2,4,4
FITEM,2,224		FITEM,2,205
FITEM,2,260		FITEM,2,250
AL,P51X		FITEM,2,269
FLST,2,4,4		FITEM,2,270
FITEM,2,259		AL,P51X
FITEM,2,251		FLST,2,4,4
FITEM,2,258		FITEM,2,249
		FITEM,2,194
		! Creating Joining Areas

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FITEM,2,270
FITEM,2,267
AL,P51X
FLST,2,4,4
FITEM,2,211
FITEM,2,247
FITEM,2,269
FITEM,2,268
AL,P51X          ! Circular Cutout Pipe

ALLSEL,ALL       ! Selecting Everything

KWPAVE, 149
FLST,2,5,5,ORDE,5
FITEM,2,43
FITEM,2,93
FITEM,2,-94
FITEM,2,97
FITEM,2,-98
ASBW,P51X        ! Cutting Main Rail w/ WPlane

LSTR, 152, 48
LSTR, 161, 146
FLST,2,4,4
FITEM,2,144
FITEM,2,125
FITEM,2,252
FITEM,2,159
AL,P51X
FLST,2,4,4
FITEM,2,273
FITEM,2,160
FITEM,2,254
FITEM,2,143
AL,P51X
FLST,2,10,4
FITEM,2,143
FITEM,2,276
FITEM,2,275
FITEM,2,131
FITEM,2,125
FITEM,2,240
FITEM,2,246
FITEM,2,232
FITEM,2,251
FITEM,2,233
AL,P51X          ! Creating Areas to
                  ! Join with Main Rail

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----- Strut Attachment Areas -----
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KWPLAN,-1, 104, 139, 101
CSYS,4
K,-305,,
K,-305,17*19,,
K,-192,5,17*19,,
K,-192,5,17*19+185+266,,
FLST,3,1,3,ORDE,1
FITEM,3,101
KGEN,2,P51X,,,-192,5,,0
LSTR, 101, 167
LSTR, 167, 166
LSTR, 166, 165
LSTR, 165, 164
LSTR, 164, 163
LSTR, 163, 104
wprot,0,90,0
KWPAVE, 165

FLST,2,3,5,ORDE,3
FITEM,2,44
FITEM,2,100
FITEM,2,111
ASBW,P51X
KWPAVE, 166
FLST,2,3,5,ORDE,3
FITEM,2,130
FITEM,2,132
FITEM,2,-133
ASBW,P51X
LSTR, 167, 100
LSTR, 163, 91
FLST,2,3,4
FITEM,2,291
FITEM,2,161
FITEM,2,283
AL,P51X
LSTR, 169, 165
LSTR, 172, 166
FLST,2,5,4
FITEM,2,283
FITEM,2,285
FITEM,2,293
FITEM,2,282
FITEM,2,281
AL,P51X
FLST,2,4,4
FITEM,2,293
FITEM,2,280
FITEM,2,294
FITEM,2,295
AL,P51X
FLST,2,4,4
FITEM,2,132
FITEM,2,294
FITEM,2,279
FITEM,2,278
AL,P51X
FLST,2,3,4
FITEM,2,278
FITEM,2,168
FITEM,2,290
AL,P51X
LSTR, 174, 166
LSTR, 165, 168
FLST,2,3,4
FITEM,2,302
FITEM,2,296
FITEM,2,294
AL,P51X
FLST,2,3,4
FITEM,2,303
FITEM,2,286
FITEM,2,293
AL,P51X          ! Creating Areas one side

KWPAVE, 173
wprof,-355/2,0,0          ! Moving WPlane

FLST,3,7,5,ORDE,5
FITEM,3,130
FITEM,3,132
FITEM,3,-133
FITEM,3,137
FITEM,3,-140
ARSYM,X,P51X,,,-0,0      ! Reflecting Areas

NUMMRG,KP,...          ! Merging Coincident Items

```

```

FLST,2,2,5,ORDE,2
FITEM,2,106
FITEM,2,115
ADELE,P51X,,1
      ! Deleting Unneeded Areas on Centerline

LSTR, 181, 170
FLST,2,3,4
FITEM,2,305
FITEM,2,309
FITEM,2,321
AL,P51X
FLST,2,2,5,ORDE,2
FITEM,2,106
FITEM,2,147
AADD,P51X
LSTR, 164, 168
FLST,2,3,4
FITEM,2,307
FITEM,2,303
FITEM,2,281
AL,P51X
FLST,2,2,5,ORDE,2
FITEM,2,106
FITEM,2,140
AADD,P51X ! Adding To Fillet Areas on Strut Mounts

WPSTYLE,0
WPCSYS,-1,0
CSYS,0      ! Returning WPlane and Active CS
             ! to Global Cartesian

```

```

/EOF

```

```

! =====
! =====

```

❖ Filename: 7_3_frame_mesh_INPUT

```

*****
|          930E Frame FEA Meshing Routine          |
*****

/TITLE,930E Frame FEA Mesh

|-----|
|----- Defining Material Thicknesses -----|
|-----|

/PREP7

|-----|
|----- Defining Real Constants -----|
|-----|
R,13,12.7,.....,      ! 12.7mm Thickness
R,19,19,.....,         ! 19mm Thickness
R,25,25,.....,         ! 25mm Thickness
R,28,28,.....,         ! 28mm Thickness
R,30,30.5,.....,       ! 30.5mm Thickness
R,32,32,.....,         ! 32mm Thickness
R,33,33,.....,         ! 33mm Thickness
R,36,36,.....,         ! 36mm Thickness
R,38,38,.....,         ! 38mm Thickness
R,41,41,.....,         ! 41mm Thickness
R,42,42,.....,         ! 42mm Thickness
R,45,45,.....,         ! 45mm Thickness
R,46,46,.....,         ! 46mm Thickness
R,51,51,.....,         ! 51mm Thickness
R,127,127,.....,       ! 127mm Thickness

|-----|
|----- Rear Section -----|
|-----|

FLST,5,4,5,ORDE,2
FITEM,5,1
FITEM,5,4
CM,_YAREA
ASEL,,,P51X
CM,_Y1AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 28, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1      ! Inner Rear Torsion-Tube

FLST,5,4,5,ORDE,2
FITEM,5,10
FITEM,5,13
CM,_YAREA
ASEL,,,P51X
CM,_Y1AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 42, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1      ! Outer Rear Torsion Tube
FLST,5,4,5,ORDE,2
FITEM,5,77
FITEM,5,80
CM,_YAREA
ASEL,,,P51X
CM,_Y1AREA
CMSEL,S,_Y

CMSEL,S,_Y1
AATT, 1, 42, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1

FLST,5,7,5,ORDE,3
FITEM,5,61
FITEM,5,63
FITEM,5,68
CM,_YAREA
ASEL,,,P51X
CM,_Y1AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 38, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1      ! Perimeter Areas Rear Section

FLST,5,8,5,ORDE,4
FITEM,5,73
FITEM,5,76
FITEM,5,81
FITEM,5,84
CM,_YAREA
ASEL,,,P51X
CM,_Y1AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 38, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1      ! Pin Hole Inside Areas

|-----|
|----- Center Span -----|
|-----|

FLST,5,8,5,ORDE,7
FITEM,5,48
FITEM,5,49
FITEM,5,51
FITEM,5,53
FITEM,5,55
FITEM,5,57
FITEM,5,59
CM,_YAREA
ASEL,,,P51X
CM,_Y1AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 45, 1, 0
CMSEL,S,_Y

```

CMDELE_Y
CMDELE_Y1 ! Top and Bottom Plate Thickness

FLST,5,2,5,ORDE,2

FITEM,5,43

FITEM,5,125

CM_YAREA

ASEL,,,P51X

CM_Y1AREA

CMSEL,S_Y

CMSEL,S_Y1

AATT, 1, 45, 1, 0

CMSEL,S_Y

CMDELE_Y

CMDELE_Y1

FLST,5,4,5,ORDE,4

FITEM,5,5

FITEM,5,6

FITEM,5,50

FITEM,5,62

CM_YAREA

ASEL,,,P51X

CM_Y1AREA

CMSEL,S_Y

CMSEL,S_Y1

AATT, 1, 25, 1, 0

CMSEL,S_Y

CMDELE_Y1 ! Side Plate Thickness

FLST,5,3,5,ORDE,3

FITEM,5,9

FITEM,5,58

FITEM,5,85

CM_YAREA

ASEL,,,P51X

CM_Y1AREA

CMSEL,S_Y

CMSEL,S_Y1

AATT, 1, 32, 1, 0

CMSEL,S_Y

CMDELE_Y

CMDELE_Y1 ! Casting Side Thickness

FLST,5,8,5,ORDE,4

FITEM,5,15

FITEM,5,18

FITEM,5,69

FITEM,5,72

CM_YAREA

ASEL,,,P51X

CM_Y1AREA

CMSEL,S_Y

CMSEL,S_Y1

AATT, 1, 30, 1, 0

CMSEL,S_Y

CMDELE_Y

CMDELE_Y1 ! Center Torsion Tube

FLST,5,2,5,ORDE,2

FITEM,5,122

FITEM,5,124

CM_YAREA

ASEL,,,P51X

CM_Y1AREA

CMSEL,S_Y

CMSEL,S_Y1

AATT, 1, 33, 1, 0

CMSEL,S_Y

CMDELE_Y

CMDELE_Y1 ! Casting Near Horse Collar

----- Horse Collar

FLST,5,4,5,ORDE,4

FITEM,5,86

FITEM,5,102

FITEM,5,105

FITEM,5,107

CM_YAREA

ASEL,,,P51X

CM_Y1AREA

CMSEL,S_Y

CMSEL,S_Y1

AATT, 1, 33, 1, 0

CMSEL,S_Y

CMDELE_Y

CMDELE_Y1 ! Lower Section

FLST,5,4,5,ORDE,4

FITEM,5,46

FITEM,5,101

FITEM,5,104

FITEM,5,108

CM_YAREA

ASEL,,,P51X

CM_Y1AREA

CMSEL,S_Y

CMSEL,S_Y1

AATT, 1, 41, 1, 0

CMSEL,S_Y

CMDELE_Y

CMDELE_Y1 ! Lower transition Region

FLST,5,4,5,ORDE,4

FITEM,5,7

FITEM,5,97

FITEM,5,98

FITEM,5,109

CM_YAREA

ASEL,,,P51X

CM_Y1AREA

CMSEL,S_Y

CMSEL,S_Y1

AATT, 1, 46, 1, 0

CMSEL,S_Y

CMDELE_Y

CMDELE_Y1 ! Areas Around Main Rail

CM_YAREA

ASEL,,, 93

CM_Y1AREA

CMSEL,S_Y

CMSEL,S_Y1

AATT, 1, 46, 1, 0

CMSEL,S_Y

CMDELE_Y

CMDELE_Y1

FLST,5,4,5,ORDE,4

FITEM,5,113

FITEM,5,114

FITEM,5,116

FITEM,5,117

CM_YAREA

ASEL,,,P51X

CM_Y1AREA

CMSEL,S_Y

CMSEL,S_Y1

AATT, 1, 25, 1, 0

CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! Top Collar Top and Bottom Plates

FLST,5,4,5,ORDE,2
FITEM,5,118
FITEM,5,-121
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 19, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! Circular Cutout Pipe

FLST,5,2,5,ORDE,2
FITEM,5,99
FITEM,5,103
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 33, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! Top Collar Side Plates

FLST,5,13,5,ORDE,10
FITEM,5,44
FITEM,5,100
FITEM,5,110
FITEM,5,-112
FITEM,5,128
FITEM,5,-129
FITEM,5,131
FITEM,5,133
FITEM,5,-136
FITEM,5,143
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 30, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! Areas Near Strut Mount

FLST,5,8,5,ORDE,7
FITEM,5,115
FITEM,5,130
FITEM,5,138
FITEM,5,-139
FITEM,5,141
FITEM,5,145
FITEM,5,-147
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 36, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! Strut Support Fillets

FLST,5,5,5,ORDE,5

FITEM,5,44
FITEM,5,131
FITEM,5,133
FITEM,5,-134
FITEM,5,143
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 38, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! Strut Mount Aoutside Face Areas

FLST,5,2,5,ORDE,2
FITEM,5,137
FITEM,5,144
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 51, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! Top Strut Mount Areas

FLST,5,2,5,ORDE,2
FITEM,5,132
FITEM,5,142
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 127, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! Bottom Strut Mount Areas

----- Front Section -----

FLST,5,4,5,ORDE,4
FITEM,5,92
FITEM,5,94
FITEM,5,96
FITEM,5,126
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 45, 1, 0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! Top and Bottom of Main Rail

FLST,5,2,5,ORDE,2
FITEM,5,123
FITEM,5,127
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT, 1, 33, 1, 0
CMSEL,S,_Y


```

-----
----- Free Meshing
-----

```

```

/VIEW,1,1,1,1
/ANG,1
/AFLOT
/AUTO
/REP,FAST ! View Commands

WPSTYLE,.....,1
MSHKEY,0
FLST,5,163,5,ORDE,2
FITEM,5,1
FITEM,5,-163
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2 ! Free Meshing All Areas

FLST,3,163,5,ORDE,2
FITEM,3,1
FITEM,3,-163
AR,SYM,X,P51X,,,0,0 ! Reflect Model

NUMMRG,ALL,,, ! Merge Coincident Items...

*SET,nodes,ndinqr(0,12)
*SET,elems,elmigr(0,12)
*SET,scl_mins,(((3e-
8)*(nodes**2))+0.0005*nodes+0.022)

/EOF

```

```

-----
-----

```

❖ Filename: 7_4_frame_loads_INPUT

```

=====
| 930E Frame FEA Loading Routine
=====

/TITLE,930E Frame FEA Loading Conditions

/PREP7

! Strut pressures
!*SET,RRpres,139.5 ! kg/cm^2
!*SET,LRpres,92.4 ! kg/cm^2
!*SET,RFpres,40.9 ! kg/cm^2
!*SET,LFPres,60.9 ! kg/cm^2

ET,2,COMBIN14 ! Define Combin14
Element Type
KEYOPT,2,2,0
KEYOPT,2,3,0

R,999,K_Dist,, ! Rubber Support Spring Stiffness
R,1999,K_Hinge,, ! Hinge Pin Spring Stiffness

DOFSEL,S,,FX,FY,FZ,MX,MY,MZ
FCUM,REPL,1,
DOFSEL,ALL ! Replace Force BC's

=====
| Dump Body Rubber Support
=====

*IF,firspas,NE,1,THEN

ALLSEL,ALL
FLST,5,8,5,ORDE,8
FITEM,5,51
FITEM,5,53
FITEM,5,59
FITEM,5,61
FITEM,5,206
FITEM,5,-207
FITEM,5,213
FITEM,5,-214
ASEL,S,,P51X
ALLSEL,BELOW,AREA
NSLA,S,1
NSEL,R,LOC,Z,-4670,-7730
! Selecting Nodes on Main Rail

TYPE, 2
MAT, 1
REAL, 999
ESYS, 0
SECNUM, ! Setting Default Element Attributes

NGEN,2,100000,ALL,,,-5,,1,
! Generating Nodes 5mm
! Below Rubber Support

EINTF,10,
! Define Elements between Co-Incident Nodes

NSEL,R,LOC,Y,-513,-512
D,ALL,,0,,,UY,,,, ! Uy=0 On Top of Springs

ALLSEL,ALL
*ENDIF

=====
| Dump Body Hinge Pins
=====

*IF,firspas,NE,1,THEN

FLST,5,8,5,ORDE,4
FITEM,5,81
FITEM,5,-84
FITEM,5,234
FITEM,5,-237
ASEL,S,,P51X
ALLSEL,BELOW,AREA
NSLA,S,1 ! Selecting Only Hinge Pin Nodes

TYPE, 2
MAT, 1
REAL, 1999
ESYS, 0
SECNUM, ! Setting Default Element Attributes

NGEN,2,100000,ALL,,,-5,,1,
! Generating Nodes 5mm
! Below Hinge Pin Nodes

EINTF,10,
! Define Elements between Co-Incident Nodes

*GET,Nmax,NODE,0,NUM,MAX
D,100000,UY,0,,Nmax,1
*SET,Nmax ! Uy=0 On Top of Springs

ALLSEL,ALL
*ENDIF

=====
| Right Rear Strut Pin
=====

FLST,5,4,5,ORDE,2
FITEM,5,73
FITEM,5,-76
ASEL,S,,P51X
ALLSEL,BELOW,AREA
NSLA,S,1 ! Selecting Right Rear Strut Pin Nodes

! Strut Force in Newtons
*SET,RRfstnut,RRpres*(100**2)/9.81**3.14/4*(0.305**2)

*GET,count,NODE,0,COUNT ! # of Selected Nodes
*SET,fnode,RRfstnut/count ! Newtons/node

F,ALL,FY,fnode ! Applying Force to Nodes
*SET,fnode
*SET,count

ALLSEL,ALL

=====
| Left Rear Strut Pin
=====

FLST,5,4,5,ORDE,2
FITEM,5,226
FITEM,5,-229
ASEL,S,,P51X

```

```
ALLSEL,BELOW,AREA
NSLA,S,1 ! Selecting Left Rear Strut Pin Nodes
```

```
! Strut Force in Newtons
*SET,LRfstnut,LRpres*(100**2)*9.81*3.14/4*(0.305**2)
```

```
*GET,count,NODE,0,COUNT ! # of Selected Nodes
*SET,inode,LRfstnut/count ! Networks/node
```

```
F,ALL,FY,inode ! Applying Force to
Nodes
*SET,fnode
*SET,count
```

```
ALLSEL,ALL
```

```
-----
----- Right Front Strut Mount
-----
```

```
! Strut Force in Newtons
*SET,RFFstnut,RFPres*(100**2)*9.81*3.14/4*(0.400**2)
```

```
KSEL,S,,,177
NSLK,S ! Selecting Point Node
```

```
! Applying Forces to Point Node
*AFUN,DEG
F,ALL,FY,RFFstnut*COS(9)
F,ALL,FZ,RFFstnut*SIN(9)
```

```
ALLSEL,ALL
```

```
-----
----- Left Front Strut Mount
-----
```

```
! Strut Force in Newtons
*SET,LFfstnut,LFPres*(100**2)*9.81*3.14/4*(0.400**2)
```

```
KSEL,S,,,343
NSLK,S ! Selecting Point Node
```

```
! Applying Forces to
Point Node
*AFUN,DEG
F,ALL,FY,LFfstnut*COS(9)
F,ALL,FZ,LFfstnut*SIN(9)
```

```
ALLSEL,ALL
```

```
-----
----- Constraining to Improve Numerical Stability
-----
```

```
*IF,firstpas,NE,1,THEN
```

```
FLST,2,2,3,ORDE,2 ! Ux=0 On Side Keypoints
FITEM,2,84
FITEM,2,110
DK,P51X,,0,,0,UX,,,,,
```

```
FLST,2,2,3,ORDE,2 ! Uz=0 Near Rear Body Pin
FITEM,2,31
FITEM,2,212
DK,P51X,,0,,0,UZ,,,,,
```

```
*ENDIF
```

```
FINISH
```

```
FINISH
```

```
-----
----- Setting Parameters
-----
```

```
*SET,firstpas,1 ! Been through file before...
```

```
*SET,NODES
*SET,ELEMS
```

```
-----
-----
-----
```

❖ Filename: 7_5_frame_post_INPUT

```

*****
*****
|          930E Frame FEA Post Processing Routine
*****
*****

/TITLE,930E Frame FEA Post Processing

|-----
|----- Defining Paths Along Main Rails
|-----

ALLSEL,ALL
FLST,5,8,5,ORDE,8
FITEM,5,51
FITEM,5,53
FITEM,5,59
FITEM,5,61
FITEM,5,206
FITEM,5,-207
FITEM,5,213
FITEM,5,-214
ASEL,S,,P51X      ! Selecting Main Rail Areas
ALLSEL,BELOW,AREA
ESEL,A,TYPE,2

FLST,2,2,1
FITEM,2,5528
FITEM,2,4270
PATH,RPath,2,30,40,
PPATH,P51X,1      ! Path on Right Rail

PDEF,STAT
AVPRIN,0,0,
PDEF,,U,Y,AVG      ! Mapping Results to Path

PAGET,R_Path,TABL  ! Storing Path Items in Array

FLST,2,2,1
FITEM,2,15510
FITEM,2,14252
PATH,LPath,2,30,40,
PPATH,P51X,1      ! Path on Left Rail

PDEF,STAT
AVPRIN,0,0,
PDEF,,U,Y,AVG      ! Mapping Results to Path

PAGET,L_Path,TABL  ! Storing Path Items in Array

|-----
|----- Writing Path Data to Text File
|-----

/EOF

!:txt

!*CFOPEN,XL_Sel_10_R_Path.txt,

!*CFOPEN,XL_H62_D125_R_Path.txt,
!*WRITE,R_Path(1,1),R_Path(1,2),R_Path(1,3),R_Path(1,4),R_Path(1,5),...
(F12.4,F12.1,F12.4,F12.1,F12.4)
!*FCLOS

!*CFOPEN,XL_H62_D125_L_Path.txt,

```

```

*VWRITE,L_Path(1,1),L_Path(1,2),L_Path(1,3),L_Path(1,4),L_Path(1,5),...
(F12.4,F12.1,F12.4,F12.1,F12.4)
*CFCLOS

```

```

|-----
|----- Combining Load Cases to Check Linearity
|-----

```

```

/EOF

```

```

LCDEF,1,1,,
LCDEF,2,2,,
LCDEF,3,3,,
LCDEF,4,4,,
LCDEF,5,5,,
LCASE,1,
LCOPER,ADD,2,,
LCOPER,ADD,3,,
LCOPER,ADD,4,,
/TITLE,Load Case 10: Added Strut Pressures
LCWRITE,10,,/

```

```

|-----
|-----
|-----

```

❖ Filename: 8_1_full_Main_INPUT

```

*****
! Combined 930E Frame and Dump Body FEA Model
*****

----- Call Frame and Body into One Database -----

! *** Had problems with non-similar files on re-runs...
! *** Do not run this group again unless absolutely
! *** necessary

!FINISH
!FINISH
!/CLEAR,START ! Clear and Start New
!RESUME,frm_geom.db ! Call in frame FEA model
!/FILNAM,frame

!/PREP7
!CDWRITE,ALL, ..., ! Archive Frame FEA Model
!FINISH

!FINISH
!/CLEAR,START ! Clear and Start New
!RESUME,mesh.db ! Call in Dump Body FEA

!/PREP7
!AR,SYN,X,ALL, ...,0 ! Reflect Other Half of Model
!NUMMRG,ALL, ... ! Merge Co-incident Items
!CDREAD,ALL,frame.cdb, ... ! Read in Frame FEA Archive
!/FACE,NORMAL ! Display Rendered Areas

!FINISH
!/FILNAM,combined ! Save Combined Database
!SAVE
!/EOF

! *** Had problems with non-similar files are re-runs...
! *** Do not run this group again unless absolutely
! **** necessary

----- Joining Frame and Body At Body Supports -----

join

!FINISH
!FINISH
!/CLEAR,START ! Clear and Start New
!RESUME,combined.db ! Call in Combined Database

!/INPUT,8_2_full_join_INPUT,...,0 ! Join FEA Models

!FINISH
!/FILNAM,joined
!SAVE ! Save Joined Database

!/EOF

----- Applying Ore Load -----

!load

!FINISH
!FINISH
!/CLEAR,START ! Clear and Start New
!RESUME,joined.db ! Call in Database

! Apply Ore Load
!/INPUT,4_4_FEA_load_algorithm_INPUT,,home/dw11
589/930E_Full,1,

!FINISH
!/FILNAM,loaded
!SAVE ! Save Joined Database

!/EOF

----- Creating Strut Support Springs -----

:strut

!FINISH
!FINISH
!/CLEAR,START ! Clear and Start New
!RESUME,loaded.db ! Call in Database

! Set Strut Displacements as Parameters
*SET,displRR,0
*SET,displLR,0
*SET,displRF,0
*SET,displLF,0

!/INPUT,8_3_full_struts_INPUT,...,0 ! Create Strut Springs

!FINISH
!/FILNAM,solvevme
!SAVE ! Save solvevme Database

!/EOF

----- Adjusting Strut Support Displacements -----

:adjust
!FINISH
!FINISH
!/CLEAR,START ! Clear and Start New
!RESUME,solvevme.db ! Call in Database
!FINISH
!/FILNAM,Aug_27

!/INPUT,8_4_full_adjust_INPUT,...,0 ! Adjust Strut Displacements

!SAVE ! Save FILNAM Database

!/EOF

```

❖ *Filename: 8_2_full_join_INPUT*

```

=====
!      Joining Both FEA Models into One...
=====

/REP7

=====
!      Cutting Main Rails for Rubber Pad Support
=====

FLST,2,18,5,ORDE,17
FITEM,2,5
FITEM,2,-6
FITEM,2,9
FITEM,2,50
FITEM,2,-51
FITEM,2,53
FITEM,2,59
FITEM,2,-60
FITEM,2,62
FITEM,2,85
FITEM,2,106
FITEM,2,149
FITEM,2,187
FITEM,2,-189
FITEM,2,195
FITEM,2,197
FITEM,2,220
ACLEAR,P51X
FLST,2,2,5,ORDE,2
FITEM,2,61
FITEM,2,196
ACLEAR,P51X
FLST,2,2,5,ORDE,2
FITEM,2,43
FITEM,2,182
ACLEAR,P51X
! Clearing Mesh on Frame Main Rails

WPCSYS,-1,0
KWPAVE, 2089
! Moving Wplane To End-of-Pad Location

FLST,2,2,5,ORDE,2
FITEM,2,59
FITEM,2,195
ASBW,P51X
KWPAVE, 2171
FLST,2,2,5,ORDE,2
FITEM,2,1000
FITEM,2,1011
ASBW,P51X
KWPAVE, 2170
FLST,2,2,5,ORDE,2
FITEM,2,1015
FITEM,2,-1016
ASBW,P51X
KWPAVE, 2169
FLST,2,2,5,ORDE,2
FITEM,2,1000
FITEM,2,1011
ASBW,P51X
KWPAVE, 2168
FLST,2,2,5,ORDE,2
FITEM,2,1015

FITEM,2,-1016
ASBW,P51X
KWPAVE, 2166
FLST,2,2,5,ORDE,2
FITEM,2,1015
FITEM,2,-1016
ASBW,P51X
KWPAVE, 2165
FLST,2,2,5,ORDE,2
FITEM,2,1000
FITEM,2,1011
ASBW,P51X
KWPAVE, 2164
FLST,2,2,5,ORDE,2
FITEM,2,1015
FITEM,2,-1016
ASBW,P51X
KWPAVE, 2163
FLST,2,2,5,ORDE,2
FITEM,2,1000
FITEM,2,1011
ASBW,P51X
KWPAVE, 2162
FLST,2,2,5,ORDE,2
FITEM,2,53
FITEM,2,189
ASBW,P51X
KWPAVE, 2161
FLST,2,2,5,ORDE,2
FITEM,2,1000
FITEM,2,1050
ASBW,P51X
KWPAVE, 2160
FLST,2,2,5,ORDE,2
FITEM,2,1052
FITEM,2,-1053
ASBW,P51X
KWPAVE, 2159
FLST,2,2,5,ORDE,2
FITEM,2,1000
FITEM,2,1050
ASBW,P51X
KWPAVE, 2158
FLST,2,2,5,ORDE,2
FITEM,2,51
FITEM,2,188
ASBW,P51X
KWPAVE, 2157
FLST,2,2,5,ORDE,2
FITEM,2,1000
FITEM,2,1060
ASBW,P51X
KWPAVE, 1765
FLST,2,2,5,ORDE,2
FITEM,2,1062
FITEM,2,-1063
ASBW,P51X
! Cutting Main Rail Areas At Rubber Locations

FLST,5,40,5,ORDE,9
FITEM,5,1000
FITEM,5,1010

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FITEM,5,-1011
FITEM,5,1014
FITEM,5,-1029
FITEM,5,1045
FITEM,5,-1061
FITEM,5,1064
FITEM,5,-1067
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT,1,45,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1 ! Restoring Area Thicknesses

FLST,5,162,5,ORDE,75
FITEM,5,1
FITEM,5,-6
FITEM,5,8
FITEM,5,-13
FITEM,5,15
FITEM,5,-18
FITEM,5,42
FITEM,5,-43
FITEM,5,45
FITEM,5,47
FITEM,5,-50
FITEM,5,52
FITEM,5,54
FITEM,5,-58
FITEM,5,60
FITEM,5,-65
FITEM,5,69
FITEM,5,-80
FITEM,5,85
FITEM,5,94
FITEM,5,98
FITEM,5,101
FITEM,5,106
FITEM,5,111
FITEM,5,115
FITEM,5,122
FITEM,5,124
FITEM,5,-125
FITEM,5,129
FITEM,5,134
FITEM,5,141
FITEM,5,-143
FITEM,5,148
FITEM,5,-153
FITEM,5,155
FITEM,5,-158
FITEM,5,182
FITEM,5,185
FITEM,5,-187
FITEM,5,190
FITEM,5,-194
FITEM,5,196
FITEM,5,-200
FITEM,5,204
FITEM,5,-215
FITEM,5,220
FITEM,5,229
FITEM,5,233
FITEM,5,236
FITEM,5,245
FITEM,5,249
FITEM,5,256

FITEM,5,258
FITEM,5,-259
FITEM,5,263
FITEM,5,268
FITEM,5,274
FITEM,5,-276
FITEM,5,384
FITEM,5,1000
FITEM,5,1010
FITEM,5,-1011
FITEM,5,1014
FITEM,5,-1029
FITEM,5,1039
FITEM,5,1041
FITEM,5,1043
FITEM,5,-1061
FITEM,5,1064
FITEM,5,-1067
FITEM,5,1415
FITEM,5,2031
FITEM,5,2033
FITEM,5,2035
FITEM,5,-2036
ASEL,S,,,P51X
! Selecting Only Frame Main Rail Areas
ALLSEL,BELOW,AREA

SMRTSIZE,10 ! SmartSize = Coarse

MSHKEY,0
FLST,5,19,5,ORDE,19
FITEM,5,196
FITEM,5,1014
FITEM,5,1016
FITEM,5,1018
FITEM,5,1020
FITEM,5,1022
FITEM,5,1024
FITEM,5,1026
FITEM,5,1028
FITEM,5,1045
FITEM,5,1047
FITEM,5,1049
FITEM,5,1051
FITEM,5,1053
FITEM,5,1055
FITEM,5,1057
FITEM,5,1059
FITEM,5,1061
FITEM,5,1065
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CHKMISH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDELE,_Y1
CMDELE,_Y2
MSHKEY,0
FLST,5,19,5,ORDE,19
FITEM,5,61
FITEM,5,1010
FITEM,5,-1011
FITEM,5,1015
FITEM,5,1017
FITEM,5,1019
FITEM,5,1021
FITEM,5,1023
FITEM,5,1025

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FITEM,5,1027
FITEM,5,1029
FITEM,5,1046
FITEM,5,1048
FITEM,5,1050
FITEM,5,1052
FITEM,5,1054
FITEM,5,1056
FITEM,5,1058
FITEM,5,1064
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2
SMRTSIZE,1 ! SmartSize = Fine
MSHKEY,0
FLST,5,6,5,ORDE,6
FITEM,5,43
FITEM,5,182
FITEM,5,1000
FITEM,5,1060
FITEM,5,1066
FITEM,5,-1067
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2
SMRTSIZE,3 ! SmartSize = Med-Fine
MSHKEY,0
FLST,5,12,5,ORDE,12
FITEM,5,5
FITEM,5,-6
FITEM,5,9
FITEM,5,50
FITEM,5,60
FITEM,5,62
FITEM,5,85
FITEM,5,106
FITEM,5,149
FITEM,5,187
FITEM,5,197
FITEM,5,220
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CHKMSH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2 ! Re-Meshing Frame Main Rail Areas

ALLSEL,ALL

|-----
|----- Creating Rubber Pad Connection
|-----

/PREP7

FLST,5,125,5,ORDE,34
FITEM,5,61
FITEM,5,196
FITEM,5,294
FITEM,5,383
FITEM,5,-384
FITEM,5,423
FITEM,5,-424
FITEM,5,892
FITEM,5,-893
FITEM,5,1000
FITEM,5,1010
FITEM,5,-1011
FITEM,5,1014
FITEM,5,-1029
FITEM,5,1038
FITEM,5,1040
FITEM,5,1042
FITEM,5,1045
FITEM,5,-1061
FITEM,5,1064
FITEM,5,-1067
FITEM,5,1280
FITEM,5,-1311
FITEM,5,1325
FITEM,5,1415
FITEM,5,1452
FITEM,5,-1453
FITEM,5,1905
FITEM,5,-1906
FITEM,5,2030
FITEM,5,2032
FITEM,5,2034
FITEM,5,2037
FITEM,5,-2068
ASEL,S,_P51X
ALLSEL,BELOW,AREA
! Selecting Only Areas Near Rubber pad

LSTR, 2087, 1154
LSTR, 2119, 1158
LSTR, 2090, 1155
LSTR, 2124, 1159
FLST,2,4,4
FITEM,2,2156
FITEM,2,2243
FITEM,2,2242
FITEM,2,4050
ALP51X
FLST,2,4,4
FITEM,2,2155
FITEM,2,2240
FITEM,2,4035
FITEM,2,2239
ALP51X
FLST,2,5,4
FITEM,2,2144
FITEM,2,2242
FITEM,2,3967
FITEM,2,3966
FITEM,2,2239
ALP51X
LSTR, 2121, 1163
LSTR, 2120, 1167
LSTR, 2116, 1162
LSTR, 2115, 1166
LSTR, 2132, 1158
LSTR, 2132, 1162
LSTR, 2131, 1159
LSTR, 2131, 1163

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FLST,2,3,4		
FITEM,2,2243		
FITEM,2,2261		
FITEM,2,4071		
AL,P51X		
FLST,2,3,4		
FITEM,2,2261		
FITEM,2,2162		
FITEM,2,2262		
AL,P51X		
FLST,2,3,4		
FITEM,2,2262		
FITEM,2,4068		
FITEM,2,2255		
AL,P51X		
FLST,2,3,4		
FITEM,2,2240		
FITEM,2,4072		
FITEM,2,2259		
AL,P51X		
FLST,2,3,4		
FITEM,2,2259		
FITEM,2,2161		
FITEM,2,2260		
AL,P51X		
FLST,2,3,4		
FITEM,2,2260		
FITEM,2,4070		
FITEM,2,2257		
AL,P51X		
FLST,2,4,4		
FITEM,2,2168		
FITEM,2,2255		
FITEM,2,2256		
FITEM,2,4042		
AL,P51X		
FLST,2,4,4		
FITEM,2,2167		
FITEM,2,2258		
FITEM,2,4027		
FITEM,2,2257		
AL,P51X		
LSTR, 2114, 1171		
LSTR, 2113, 1175		
LSTR, 2112, 1170		
LSTR, 2111, 1174		
FLST,2,4,4		
FITEM,2,2258		
FITEM,2,4025		
FITEM,2,2265		
FITEM,2,2173		
AL,P51X		
FLST,2,4,4		
FITEM,2,4018		
FITEM,2,2265		
FITEM,2,2266		
FITEM,2,2179		
AL,P51X		
FLST,2,4,4		
FITEM,2,2180		
FITEM,2,2264		
FITEM,2,4023		
FITEM,2,2263		
AL,P51X		
FLST,2,4,4		
FITEM,2,2174		
FITEM,2,4039		
FITEM,2,2256		
FITEM,2,2263		
AL,P51X		
LSTR, 2110, 1179		
LSTR, 2108, 1183		
LSTR, 2109, 1178		
LSTR, 2107, 1182		
FLST,2,4,4		
FITEM,2,2186		
FITEM,2,4020		
FITEM,2,2264		
FITEM,2,2267		
AL,P51X		
FLST,2,4,4		
FITEM,2,2192		
FITEM,2,2268		
FITEM,2,4013		
FITEM,2,2267		
AL,P51X		
FLST,2,4,4		
FITEM,2,2266		
FITEM,2,4016		
FITEM,2,2269		
FITEM,2,2185		
AL,P51X		
FLST,2,4,4		
FITEM,2,4010		
FITEM,2,2270		
FITEM,2,2191		
FITEM,2,2269		
AL,P51X		
LSTR, 2106, 1187		
LSTR, 2105, 1191		
LSTR, 2104, 1186		
LSTR, 2103, 1190		
FLST,2,4,4		
FITEM,2,2198		
FITEM,2,4008		
FITEM,2,2268		
FITEM,2,2271		
AL,P51X		
FLST,2,4,4		
FITEM,2,2271		
FITEM,2,2272		
FITEM,2,4005		
FITEM,2,2204		
AL,P51X		
FLST,2,4,4		
FITEM,2,2270		
FITEM,2,4006		
FITEM,2,2197		
FITEM,2,2273		
AL,P51X		
FLST,2,4,4		
FITEM,2,2273		
FITEM,2,3999		
FITEM,2,2274		
FITEM,2,2203		
AL,P51X		
LSTR, 2099, 1195		
LSTR, 2100, 1199		
LSTR, 2098, 1194		
LSTR, 2097, 1198		
LSTR, 191, 2098		
LSTR, 282, 2099		
FLST,2,4,4		
FITEM,2,2272		
FITEM,2,2199		
FITEM,2,2280		
FITEM,2,4003		
AL,P51X		
FLST,2,3,4		
FITEM,2,2210		

FITEM,2,2280		AL,P51X	
FITEM,2,2275		FLST,2,4,4	
AL,P51X		FITEM,2,2248	
FLST,2,4,4		FITEM,2,2287	
FITEM,2,2220		FITEM,2,3976	
FITEM,2,2276		FITEM,2,2286	
FITEM,2,3988		AL,P51X	
FITEM,2,2275		FLST,2,4,4	
AL,P51X		FITEM,2,3975	
FLST,2,4,4		FITEM,2,2288	
FITEM,2,2278		FITEM,2,2247	
FITEM,2,3986		FITEM,2,2289	
FITEM,2,2219		AL,P51X	
FITEM,2,2277		FLST,2,3,4	
AL,P51X		FITEM,2,2290	
FLST,2,3,4		FITEM,2,2237	
FITEM,2,2279		FITEM,2,2289	
FITEM,2,2209		AL,P51X	
FITEM,2,2277		FLST,2,4,4	
AL,P51X		FITEM,2,3979	
FLST,2,4,4		FITEM,2,2284	
FITEM,2,2279		FITEM,2,2215	
FITEM,2,3996		FITEM,2,2290	
FITEM,2,2187		AL,P51X	
FITEM,2,2274		LSTR, 1764, 1219	
AL,P51X		LSTR, 1763, 1218	
LSTR, 2101, 1203		FLST,2,4,4	
LSTR, 2102, 1207		FITEM,2,2287	
LSTR, 2096, 1202		FITEM,2,3973	
LSTR, 2095, 1206		FITEM,2,2291	
FLST,2,4,4		FITEM,2,2254	
FITEM,2,2276		AL,P51X	
FITEM,2,2226		FLST,2,4,4	
FITEM,2,3990		FITEM,2,3984	
FITEM,2,2281		FITEM,2,2288	
AL,P51X		FITEM,2,2253	
FLST,2,4,4		FITEM,2,2292	
FITEM,2,2278		AL,P51X	
FITEM,2,3983		LSTR, 1765, 1218	
FITEM,2,2225		LSTR, 1765, 1219	
FITEM,2,2283		FLST,2,3,4	
AL,P51X		FITEM,2,3264	
FLST,2,4,4		FITEM,2,2292	
FITEM,2,3992		FITEM,2,2293	
FITEM,2,2281		AL,P51X	
FITEM,2,2232		FLST,2,3,4	
FITEM,2,2282		FITEM,2,2293	
AL,P51X		FITEM,2,2250	
FLST,2,4,4		FITEM,2,2294	
FITEM,2,3982		AL,P51X	
FITEM,2,2284		FLST,2,3,4	
FITEM,2,2231		FITEM,2,3263	
FITEM,2,2283		FITEM,2,2294	
AL,P51X		FITEM,2,2291	
LSTR, 283, 2094		AL,P51X	! Areas for Left Rubber pad
LSTR, 2094, 1211			
LSTR, 1215, 2092		FLST,2,94,5,ORDE,22	
LSTR, 2086, 1214		FITEM,2,1016	
LSTR, 2093, 1210		FITEM,2,1018	
LSTR, 2093, 192		FITEM,2,1020	
FLST,2,4,4		FITEM,2,1022	
FITEM,2,2282		FITEM,2,1024	
FITEM,2,2227		FITEM,2,1026	
FITEM,2,3994		FITEM,2,1028	
FITEM,2,2285		FITEM,2,1045	
AL,P51X		FITEM,2,1047	
FLST,2,3,4		FITEM,2,1049	
FITEM,2,2238		FITEM,2,1051	
FITEM,2,2285		FITEM,2,1053	
FITEM,2,2286		FITEM,2,1055	

FITEM,2,1057
 FITEM,2,1059
 FITEM,2,1061
 FITEM,2,-1063
 FITEM,2,1065
 FITEM,2,1067
 FITEM,2,-1109
 FITEM,2,2037
 FITEM,2,-2068
 VA,P51X

! Left Rubber Pad Volume

LSTR, 1039, 1058
 LSTR, 1037, 1156
 LSTR, 1040, 1069
 LSTR, 1038, 1157
 LSTR, 1157, 1071
 LSTR, 1071, 1161
 LSTR, 1161, 1036
 LSTR, 1034, 1165
 LSTR, 1033, 1164
 LSTR, 1035, 1160
 LSTR, 1160, 1073
 LSTR, 1073, 1156
 FLST,2,5,4
 FITEM,2,2295
 FITEM,2,2139
 FITEM,2,2297
 FITEM,2,2672
 FITEM,2,2669
 AL,P51X
 FLST,2,4,4
 FITEM,2,2153
 FITEM,2,2296
 FITEM,2,1899
 FITEM,2,2295
 AL,P51X
 FLST,2,3,4
 FITEM,2,2306
 FITEM,2,2101
 FITEM,2,2296
 AL,P51X
 FLST,2,3,4
 FITEM,2,2159
 FITEM,2,2306
 FITEM,2,2305
 AL,P51X
 FLST,2,3,4
 FITEM,2,2305
 FITEM,2,2098
 FITEM,2,2304
 AL,P51X
 FLST,2,4,4
 FITEM,2,2165
 FITEM,2,2303
 FITEM,2,1893
 FITEM,2,2304
 AL,P51X
 FLST,2,4,4
 FITEM,2,2154
 FITEM,2,2298
 FITEM,2,2297
 FITEM,2,1900
 AL,P51X
 FLST,2,3,4
 FITEM,2,2299
 FITEM,2,2100
 FITEM,2,2298
 AL,P51X
 FLST,2,3,4
 FITEM,2,2299

FITEM,2,2160
 FITEM,2,2300
 AL,P51X
 FLST,2,3,4
 FITEM,2,2300
 FITEM,2,2096
 FITEM,2,2301
 AL,P51X
 FLST,2,4,4
 FITEM,2,2301
 FITEM,2,2166
 FITEM,2,2302
 FITEM,2,1894
 AL,P51X
 LSTR, 1031, 1168
 LSTR, 1029, 1172
 LSTR, 1032, 1169
 LSTR, 1030, 1173
 FLST,2,4,4
 FITEM,2,2303
 FITEM,2,1890
 FITEM,2,2171
 FITEM,2,2307
 AL,P51X
 FLST,2,4,4
 FITEM,2,2177
 FITEM,2,2307
 FITEM,2,1887
 FITEM,2,2308
 AL,P51X
 FLST,2,4,4
 FITEM,2,2302
 FITEM,2,1891
 FITEM,2,2172
 FITEM,2,2309
 AL,P51X
 FLST,2,4,4
 FITEM,2,2178
 FITEM,2,2310
 FITEM,2,1888
 FITEM,2,2309
 AL,P51X
 LSTR, 1027, 1176
 LSTR, 1025, 1180
 LSTR, 1028, 1177
 LSTR, 1026, 1181
 FLST,2,4,4
 FITEM,2,2183
 FITEM,2,1884
 FITEM,2,2308
 FITEM,2,2311
 AL,P51X
 FLST,2,4,4
 FITEM,2,2311
 FITEM,2,1881
 FITEM,2,2312
 FITEM,2,2189
 AL,P51X
 FLST,2,4,4
 FITEM,2,2313
 FITEM,2,1882
 FITEM,2,2314
 FITEM,2,2190
 AL,P51X
 FLST,2,4,4
 FITEM,2,2310
 FITEM,2,1885
 FITEM,2,2184
 FITEM,2,2313
 AL,P51X

LSTR, 1023, 1184
 LSTR, 1021, 1188
 LSTR, 1024, 1185
 LSTR, 1022, 1189
 FLST,2,4,4
 FITEM,2,2312
 FITEM,2,1878
 FITEM,2,2195
 FITEM,2,2315
 AL,P51X
 FLST,2,4,4
 FITEM,2,2315
 FITEM,2,2316
 FITEM,2,1875
 FITEM,2,2201
 AL,P51X
 FLST,2,4,4
 FITEM,2,2314
 FITEM,2,1879
 FITEM,2,2196
 FITEM,2,2317
 AL,P51X
 FLST,2,4,4
 FITEM,2,2202
 FITEM,2,2318
 FITEM,2,2317
 FITEM,2,1876
 AL,P51X
 LSTR, 17, 468
 LSTR, 468, 1192
 LSTR, 405, 1196
 LSTR, 99, 471
 LSTR, 471, 1193
 LSTR, 406, 1197
 FLST,2,4,4
 FITEM,2,2316
 FITEM,2,2147
 FITEM,2,2319
 FITEM,2,1872
 AL,P51X
 FLST,2,3,4
 FITEM,2,2319
 FITEM,2,2193
 FITEM,2,2320
 AL,P51X
 FLST,2,4,4
 FITEM,2,2217
 FITEM,2,2321
 FITEM,2,1869
 FITEM,2,2320
 AL,P51X
 FLST,2,4,4
 FITEM,2,2318
 FITEM,2,1873
 FITEM,2,2148
 FITEM,2,2322
 AL,P51X
 FLST,2,3,4
 FITEM,2,2205
 FITEM,2,2322
 FITEM,2,2323
 AL,P51X
 FLST,2,4,4
 FITEM,2,2323
 FITEM,2,1870
 FITEM,2,2324
 FITEM,2,2218
 AL,P51X
 LSTR, 401, 1200
 LSTR, 397, 1204

LSTR, 402, 1201
 LSTR, 398, 1205
 FLST,2,4,4
 FITEM,2,2321
 FITEM,2,1866
 FITEM,2,2223
 FITEM,2,2325
 AL,P51X
 FLST,2,4,4
 FITEM,2,2229
 FITEM,2,2326
 FITEM,2,1863
 FITEM,2,2325
 AL,P51X
 FLST,2,4,4
 FITEM,2,2224
 FITEM,2,1867
 FITEM,2,2324
 FITEM,2,2327
 AL,P51X
 FLST,2,4,4
 FITEM,2,1864
 FITEM,2,2327
 FITEM,2,2230
 FITEM,2,2328
 AL,P51X
 LSTR, 30, 393
 LSTR, 393, 1208
 LSTR, 389, 1212
 LSTR, 390, 1213
 LSTR, 394, 1209
 LSTR, 394, 93
 FLST,2,4,4
 FITEM,2,2326
 FITEM,2,2211
 FITEM,2,2329
 FITEM,2,1658
 AL,P51X
 FLST,2,3,4
 FITEM,2,2221
 FITEM,2,2330
 FITEM,2,2329
 AL,P51X
 FLST,2,4,4
 FITEM,2,2245
 FITEM,2,2331
 FITEM,2,853
 FITEM,2,2330
 AL,P51X
 FLST,2,4,4
 FITEM,2,2328
 FITEM,2,2212
 FITEM,2,1859
 FITEM,2,2334
 AL,P51X
 FLST,2,3,4
 FITEM,2,2233
 FITEM,2,2333
 FITEM,2,2334
 AL,P51X
 FLST,2,4,4
 FITEM,2,2246
 FITEM,2,2332
 FITEM,2,873
 FITEM,2,2333
 AL,P51X
 LSTR, 506, 1216
 LSTR, 507, 1217
 LSTR, 1217, 1355
 LSTR, 1355, 1216

```

FLST,2,4,4
FITEM,2,2331
FITEM,2,2251
FITEM,2,2335
FITEM,2,826
AL,P51X
FLST,2,3,4
FITEM,2,2338
FITEM,2,2625
FITEM,2,2335
AL,P51X
FLST,2,3,4
FITEM,2,2234
FITEM,2,2338
FITEM,2,2337
AL,P51X
FLST,2,3,4
FITEM,2,2337
FITEM,2,2628
FITEM,2,2336
AL,P51X
FLST,2,4,4
FITEM,2,2252
FITEM,2,2336
FITEM,2,828
FITEM,2,2332
AL,P51X

```

! Areas for Right Rubber Pad

```

FLST,2,94,5,ORDE,22

```

```

FITEM,2,1011
FITEM,2,1015
FITEM,2,1017
FITEM,2,1019
FITEM,2,1021
FITEM,2,1023
FITEM,2,1025
FITEM,2,1027
FITEM,2,1029
FITEM,2,1046
FITEM,2,1048
FITEM,2,1050
FITEM,2,1052
FITEM,2,1054
FITEM,2,1056
FITEM,2,1058
FITEM,2,1064
FITEM,2,1066
FITEM,2,1110
FITEM,2,-1153
FITEM,2,1280
FITEM,2,-1311
VA,P51X

```

! Right Rubber Pad Volume

```

ALLSEL,ALL

```

```

WPSYLE,.....0

```

```

ET,3,SOLID95

```

! Defining Solid Elements

```

UIMP,3,EX,.,270000/1000, ! Mater #3 = Rubber
UIMP,3,DENS,.,7.86e-06/100,
UIMP,3,ALPX,.,.
UIMP,3,REFT,.,.
UIMP,3,NUXY,.,.
UIMP,3,PRXY,.,0,3,
UIMP,3,GXY,.,.
UIMP,3,MU,.,.
UIMP,3,DAMP,.,.

```

```

VATT, 3, 13, 3, 0

```

! Setting Volume Attributes

```

MSHKEY,0
MSHAPE,1,3d
FLST,5,2,6,ORDE,2
FITEM,5,1
FITEM,5,-2
CM,_Y,VOLU
VSEL,.,.,P51X
CM,_Y1,VOLU
CHKMSH,VOLU*
CMSEL,_,Y
VMESH,_,Y1
CMDEL,_,Y
CMDEL,_,Y1
CMDEL,_,Y2

```

! Meshing Rubber Connection

```

-----
Hinge Pin Connecting Scheme
-----

```

```

ET,4,COMBIN14
KEYOPT,4,2,0
KEYOPT,4,3,0

```

! Element Type 4

! Combination Spring Damper

```

! Chosen because can set spring constant as constant
! Other elements need material, Xsection, etc..

```

```

R,1999,100000,.,. ! 100000 N/mm Spring Constant

```

```

TYPE, 4
MAT, 1
REAL, 1999
ESYS, 0
SECNUM,
TSHAP,LINE

```

! Element type Settings

```

FLST,4,4,1,ORDE,4

```

! Defining Nodes in Centers of Circles

```

FITEM,4,19195
FITEM,4,19207
FITEM,4,87831
FITEM,4,104653
NGEN,2,2000000,P51X,.,.,-167/2,.,1,
FLST,4,4,1,ORDE,4
FITEM,4,1121
FITEM,4,5091
FITEM,4,10716
FITEM,4,14686
NGEN,2,2000000,P51X,.,.,-152/2,.,1,

```

```

FLST,5,81,1,ORDE,5

```

! Right-Hinge Body Outer-Side Wagon Wheel

```

FITEM,5,19207
FITEM,5,-19210
FITEM,5,19430
FITEM,5,-19505
FITEM,5,2019207
NSEL,R,.,P51X
*GET,count,NODE,0,COUNT
*GET,Nindex,NODE,0,NUM,MIN
*GET,Nmaster,NODE,0,NUM,MAX
*DO,index,0,count+10,1
E,Nindex,Nmaster
*GET,Next,NODE,Nindex,NXTH
*IF,Next,EQ,Nmaster,EXIT
*SET,Nindex,Next

```

```

*ENDDO

```

```

ALLSEL,ALL,NODE

```

! Select All Nodes

! Right-Hinge Body Inner-Side Wagon Wheel

```

FLST,5,81,1,ORDE,9
FITEM,5,19195

```

```

FITEM,5,-19196
FITEM,5,19200
FITEM,5,-19201
FITEM,5,19233
FITEM,5,-19251
FITEM,5,19263
FITEM,5,-19319
FITEM,5,2019195
NSEL,R,,P51X
*GET,count,NODE,0,COUNT
*GET,Nindex,NODE,0,NUM,MIN
*GET,Nmaster,NODE,0,NUM,MAX
*DO,index,0,count+10,1
    E,Nindex,Nmaster
    *GET,Next,NODE,Nindex,NXTH
    *IF,Next,EQ,Nmaster,EXIT
    *SET,Nindex,Next
*ENDDO
ALLSEL,ALL,NODE      ! Select All Nodes

```

```

! Right-Hinge Frame Outer-Side Wagon Wheel
FLST,5,25,1,ORDE,3
FITEM,5,5078
FITEM,5,-5101
FITEM,5,2005091
NSEL,R,,P51X
*GET,count,NODE,0,COUNT
*GET,Nindex,NODE,0,NUM,MIN
*GET,Nmaster,NODE,0,NUM,MAX
*DO,index,0,count+10,1
    E,Nindex,Nmaster
    *GET,Next,NODE,Nindex,NXTH
    *IF,Next,EQ,Nmaster,EXIT
    *SET,Nindex,Next
*ENDDO
ALLSEL,ALL,NODE      ! Select All Nodes

```

```

! Right-Hinge Frame Inner-Side Wagon Wheel
FLST,5,25,1,ORDE,3
FITEM,5,1120
FITEM,5,-1143
FITEM,5,2001121
NSEL,R,,P51X
*GET,count,NODE,0,COUNT
*GET,Nindex,NODE,0,NUM,MIN
*GET,Nmaster,NODE,0,NUM,MAX
*DO,index,0,count+10,1
    E,Nindex,Nmaster
    *GET,Next,NODE,Nindex,NXTH
    *IF,Next,EQ,Nmaster,EXIT
    *SET,Nindex,Next
*ENDDO
ALLSEL,ALL,NODE      ! Select All Nodes

```

```

! Left-Hinge Body Outer-Side Wagon Wheel
FLST,5,81,1,ORDE,3
FITEM,5,87810
FITEM,5,-87889
FITEM,5,2087831
NSEL,R,,P51X
*GET,count,NODE,0,COUNT
*GET,Nindex,NODE,0,NUM,MIN
*GET,Nmaster,NODE,0,NUM,MAX
*DO,index,0,count+10,1
    E,Nindex,Nmaster
    *GET,Next,NODE,Nindex,NXTH
    *IF,Next,EQ,Nmaster,EXIT
    *SET,Nindex,Next

```

```

*ENDDO
ALLSEL,ALL,NODE      ! Select All Nodes

! Left-Hinge Body Inner-Side Wagon Wheel
FLST,5,81,1,ORDE,3
FITEM,5,104632
FITEM,5,-104711
FITEM,5,2104653
NSEL,R,,P51X
*GET,count,NODE,0,COUNT
*GET,Nindex,NODE,0,NUM,MIN
*GET,Nmaster,NODE,0,NUM,MAX
*DO,index,0,count+10,1
    E,Nindex,Nmaster
    *GET,Next,NODE,Nindex,NXTH
    *IF,Next,EQ,Nmaster,EXIT
    *SET,Nindex,Next
*ENDDO
ALLSEL,ALL,NODE      ! Select All Nodes

```

```

! Left-Hinge Frame Outer-Side Wagon Wheel
FLST,5,25,1,ORDE,3
FITEM,5,14673
FITEM,5,-14696
FITEM,5,2014686
NSEL,R,,P51X
*GET,count,NODE,0,COUNT
*GET,Nindex,NODE,0,NUM,MIN
*GET,Nmaster,NODE,0,NUM,MAX
*DO,index,0,count+10,1
    E,Nindex,Nmaster
    *GET,Next,NODE,Nindex,NXTH
    *IF,Next,EQ,Nmaster,EXIT
    *SET,Nindex,Next
*ENDDO
ALLSEL,ALL,NODE      ! Select All Nodes

```

```

! Left-Hinge Frame Inner-Side Wagon Wheel
FLST,5,25,1,ORDE,3
FITEM,5,10715
FITEM,5,-10738
FITEM,5,2010716
NSEL,R,,P51X
*GET,count,NODE,0,COUNT
*GET,Nindex,NODE,0,NUM,MIN
*GET,Nmaster,NODE,0,NUM,MAX
*DO,index,0,count+10,1
    E,Nindex,Nmaster
    *GET,Next,NODE,Nindex,NXTH
    *IF,Next,EQ,Nmaster,EXIT
    *SET,Nindex,Next
*ENDDO
ALLSEL,ALL,NODE      ! Select All Nodes

```

```

! Couple all but ROTX on Center Nodes of
! Wagon Wheels to Closest Center Nodes
! Right Outer
CP,1,UX,2005091,2019207
CP,2,UY,2005091,2019207
CP,3,UZ,2005091,2019207
CP,4,ROTX,2005091,2019207
CP,5,ROTZ,2005091,2019207
! Right Inner
CP,6,UX,2001121,2019195
CP,7,UY,2001121,2019195
CP,8,UZ,2001121,2019195
CP,9,ROTX,2001121,2019195
CP,10,ROTZ,2001121,2019195
! Left Outer

```

CP,11,UX,2087831,2014686
CP,12,UY,2087831,2014686
CP,13,UZ,2087831,2014686
CP,14,ROTY,2087831,2014686
CP,15,ROTZ,2087831,2014686

! Left Inner

CP,16,UX,2104653,2010716
CP,17,UY,2104653,2010716
CP,18,UZ,2104653,2010716
CP,19,ROTY,2104653,2010716
CP,20,ROTZ,2104653,2010716

*SET,count ! Deleting Parameters

*SET,Nindex

*SET,Nmaster

*SET,index

*SET,Next

ALLSEL,ALL

FINISH

/EOF

❖ Filename: 8_3_full_struts_INPUT

```

*****
|          Creating Strut Supports...          |
*****

/PREP7

|----- Rear Strut Rigid Regions -----|
|
FLST,5,8,5,ORDE,4
FITEM,5,73
FITEM,5,-76
FITEM,5,208
FITEM,5,-211
ASEL,R,,P51X
ALLSEL,BELOW,AREA

FLST,3,2,3,ORDE,2
! Copy KP's to Center of Strut Pins
FITEM,3,28
FITEM,3,292
KGEN,2,P51X,,.305/2,-.152/2,,.0

LSTR, 292, 1221
LSTR, 1221, 221
LSTR, 28, 1220
LSTR, 1220, 126
FLST,2,3,4
FITEM,2,2339
FITEM,2,507
FITEM,2,2340
AL,P51X
FLST,2,3,4
FITEM,2,2342
FITEM,2,199
FITEM,2,2341
AL,P51X
! Creating Triangle Areas

FLST,5,2,5,ORDE,2
FITEM,5,1154
FITEM,5,-1155
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CMSEL,S,_Y
CMSEL,S,_Y1
AATT,1,13,1,0
CMSEL,S,_Y
CMDELE,_Y
CMDELE,_Y1
MSHKEY,0
FLST,5,2,5,ORDE,2
FITEM,5,1154
FITEM,5,-1155
CM,_Y,AREA
ASEL,,,P51X
CM,_Y1,AREA
CHKMESH,'AREA'
CMSEL,S,_Y
AMESH,_Y1
CMDEL,_Y
CMDEL,_Y1
CMDEL,_Y2 ! Mesh Triangles to "use" center Nodes

FLST,2,362,1,ORDE,11
FITEM,2,2104655
FITEM,2,1144
FITEM,2,-1167
FITEM,2,5030
FITEM,2,-5053
FITEM,2,6307
FITEM,2,-6570
FITEM,2,2104678
FITEM,2,-2104699
FITEM,2,2104727
FITEM,2,-2104753
CERIG,P51X,,ALL,,, ! Right Rear Rigid Region

FLST,2,362,1,ORDE,11
FITEM,2,2104654
FITEM,2,10739
FITEM,2,-10762
FITEM,2,14625
FITEM,2,-14648
FITEM,2,15902
FITEM,2,-16165
FITEM,2,2104656
FITEM,2,-2104677
FITEM,2,2104700
FITEM,2,-2104726
CERIG,P51X,,ALL,,, ! Left Rear Rigid Region

|----- Rear Strut Springs -----|
|
ALLSEL,ALL

R,2999,10000,, ! 10000 N/mm Reduced
Spring Constant

FLST,4,2,1,ORDE,2
! Copy Nodes down from Rear Strut
FITEM,4,2104654 !L
FITEM,4,2104655 !R
NGEN,2,1000000,P51X,,,-1500-850,,1,
! Rigid Region Master Nodes

TYPE, 4
MAT, 1
REAL, 2999
ESYS, 0
SECNUM,
TSHAP,LINE
! Element type Settings

FLST,2,2,1
FITEM,2,2104654
FITEM,2,3104654
E,P51X
! Left Rear Strut Spring

FLST,2,2,1
FITEM,2,2104655
FITEM,2,3104655
E,P51X
! Right Rear Strut Spring

! Left Rear Strut Displacement
D,3104654,,ALL,,,
D,3104654,,dispLR,,,UY,,,,

! Right Rear Strut Displacement
D,3104655,,ALL,,,
D,3104655,,dispRR,,,UY,,,,

```



```

-----
----- Front Strut Rigid Regions
-----

```

FLST,5,10,5,ORDE,10

FITEM,5,131

FITEM,5,132

FITEM,5,137

FITEM,5,142

FITEM,5,144

FITEM,5,265

FITEM,5,266

FITEM,5,271

FITEM,5,275

FITEM,5,277

ASEL,S,,P51X

ALLSEL,BELOW,AREA

FLST,3,2,3,ORDE,2

! Creating KP for Front Strut Moment Arms

FITEM,3,104

FITEM,3,139

KGEM,2,P51X,,.56*25.4,,.0

FLST,3,2,3,ORDE,2

FITEM,3,341

FITEM,3,342

KGEM,2,P51X,,.56*25.4,,.0

LSTR, 341, 1224

LSTR, 1224, 1225

LSTR, 1225, 342

LSTR, 139, 1223

LSTR, 1223, 1222

LSTR, 1222, 104 ! Lines for Moment Arms

KL,2344,5,,

KWPAVE, 1226

FLST,2,2,4,ORDE,2

FITEM,2,2344

FITEM,2,2347

LSBW,P51X

WPSTYLE,0 ! Cut Outer Most Line w/ WPlane
! to ensure node in center of edge

FLST,2,5,4

FITEM,2,2351

FITEM,2,2352

FITEM,2,2345

FITEM,2,578

FITEM,2,2343

AL,P51X

FLST,2,5,4

FITEM,2,2346

FITEM,2,257

FITEM,2,2348

FITEM,2,2349

FITEM,2,2350

AL,P51X ! Creating Areas

FLST,5,2,5,ORDE,2

FITEM,5,1156

FITEM,5,1157

CM,_Y,AREA

ASEL,,P51X

CM,_Y1,AREA

CMSEL,S,_Y

CMSEL,S,_Y1

AATT, 1, 13, 1, 0

CMSEL,S,_Y

CMDELE,_Y

CMDELE,_Y1 ! Setting Element Attributes

SMRTSIZE,1 ! Smartsizes Setting

MSHKEY,0

FLST,5,2,5,ORDE,2

FITEM,5,1156

FITEM,5,1157

CM,_Y,AREA

ASEL,,P51X

CM,_Y1,AREA

CHKMSH,AREA

CMSEL,S,_Y

AMESH,_Y1

CMDELE,_Y

CMDELE,_Y1

CMDELE,_Y2 ! Meshing Moment Arms

FLST,5,2,5,ORDE,2

FITEM,5,131

FITEM,5,265

ASEL,U,,P51X

FLST,2,314,1,ORDE,39

FITEM,2,3104660

FITEM,2,4277

FITEM,2,4286

FITEM,2,4294

FITEM,2,4301

FITEM,2,7781

FITEM,2,8384

FITEM,2,8390

FITEM,2,8393

FITEM,2,8408

FITEM,2,8535

FITEM,2,8539

FITEM,2,8547

FITEM,2,8551

FITEM,2,9090

FITEM,2,9094

FITEM,2,9109

FITEM,2,9113

FITEM,2,9128

FITEM,2,9136

FITEM,2,9138

FITEM,2,9184

FITEM,2,9225

FITEM,2,9237

FITEM,2,9239

FITEM,2,9377

FITEM,2,9400

FITEM,2,9424

FITEM,2,9427

FITEM,2,9444

FITEM,2,9472

FITEM,2,9520

FITEM,2,9543

FITEM,2,3104658

FITEM,2,3104659

FITEM,2,3104724

FITEM,2,3104791

FITEM,2,3104866

FITEM,2,3104933

CERIG,P51X,ALL,,

! Right Front Strut Rigid Region

FLST,2,314,1,ORDE,42

FITEM,2,3104661

```

FITEM,2,13872
FITEM,2,-13881
FITEM,2,13889
FITEM,2,-13896
FITEM,2,17376
FITEM,2,17379
FITEM,2,17985
FITEM,2,-17988
FITEM,2,18003
FITEM,2,18130
FITEM,2,-18134
FITEM,2,18142
FITEM,2,-18146
FITEM,2,18685
FITEM,2,-18689
FITEM,2,18704
FITEM,2,-18708
FITEM,2,18723
FITEM,2,18731
FITEM,2,-18733
FITEM,2,18779
FITEM,2,-18820
FITEM,2,18832
FITEM,2,-18834
FITEM,2,18972
FITEM,2,-18995
FITEM,2,19019
FITEM,2,19027
FITEM,2,-19029
FITEM,2,19039
FITEM,2,-19064
FITEM,2,19076
FITEM,2,-19078
FITEM,2,19115
FITEM,2,-19138
FITEM,2,3104656
FITEM,2,-3104657
FITEM,2,3104662
FITEM,2,-3104723
FITEM,2,3104792
FITEM,2,-3104865
CERIG,P51X,,ALL,,,
! Left Front Strut Rigid Region

|-----
|----- Front Strut Spring Elements
|-----

ALLSEL,ALL

*AFUN,DEG

! Rigid Region Master Nodes
! Copy Nodes down from Rear Strut

FLST,4,2,1,ORDE,2
FITEM,4,3104661,IL
FITEM,4,3104660,IR
NGEN,2,1000000,P51X,,,,-2500*COS(9),-
2500*SIN(9),1,

TYPE, 4
MAT, 1
REAL, 2999
ESYS, 0
SECNUM,
TSHAP,LINE ! Element type Settings

FLST,2,2,1
FITEM,2,3104660
E,P51X

! Right Front Strut Spring

FLST,2,2,1
FITEM,2,3104661
FITEM,2,4104661
E,P51X

! Left Front Strut Spring

! Left Front Strut Displacement
D,4104661,ALL,
D,4104661,,disPLF*COS(9),,,,UY,
D,4104661,,disPLF*SIN(9),,,,UZ,

! Right Front Strut Displacement
D,4104660,ALL,
D,4104660,,disPRF*COS(9),,,,UY,
D,4104660,,disPRF*SIN(9),,,,UZ,

LPLOT

|-----
|----- Additional Restraints to Improve Stability
|-----

FLST,2,2,3,ORDE,2
FITEM,2,36
FITEM,2,227
DK,P51X,,0,,0,UZ,
! Uz=0 on Two Center Torsion Tube KPs

FLST,2,2,3,ORDE,2
FITEM,2,5
FITEM,2,16
/GO
DK,P51X,,0,,0,UX,
! Ux=0 on Rear and Center Torsion
! Tube Centerline KPs

FINISH

|-----
|-----
|-----

```

❖ Filename: 8_4_full_adjust_INPUT

```

*****
! Combined 930E Frame and Dump Body FEA Model
*****

FINISH
/ISOLU          ! Set Strut Displacements

-----
/TITLE,Load Set 1: Ore Load Only
-----

*SET,fmtdiff,0          ! Newtons
*SET,reardiff,0         ! Newtons

*SET,displF,(fmtdiff/2)/100000
*SET,disprF,-(fmtdiff/2)/100000
*SET,displr,(reardiff/2)/100000
*SET,disprR,-(reardiff/2)/100000

          ! Left Front Strut Displacement
D,4104661,...,ALL,...
D,4104661,,displF*cos(9),,,UY,...,
D,4104661,,displF*sin(9),,,UZ,...,
          ! Right Front Strut Displacement
D,4104660,...,ALL,...
D,4104660,,disprF*cos(9),,,UY,...,
D,4104660,,disprF*sin(9),,,UZ,...,
          ! Left Rear Strut Displacement
D,3104654,...,ALL,...
D,3104654,,displr,,UY,...,
          ! Right Rear Strut Displacement
D,3104655,...,ALL,...
D,3104655,,disprR,,UY,...,

LSWRITE,1,
SFEDELE,ALL,ALL,PRES

-----
/TITLE,Load Set 2: Rack Front Difference Only
-----

*SET,fmtdiff,271155     ! Newtons
*SET,reardiff,0         ! Newtons

*SET,displF,(fmtdiff/2)/100000
*SET,disprF,-(fmtdiff/2)/100000
*SET,displr,(reardiff/2)/100000
*SET,disprR,-(reardiff/2)/100000

          ! Left Front Strut Displacement
D,4104661,...,ALL,...
D,4104661,,displF*cos(9),,,UY,...,
D,4104661,,displF*sin(9),,,UZ,...,
          ! Right Front Strut Displacement
D,4104660,...,ALL,...
D,4104660,,disprF*cos(9),,,UY,...,
D,4104660,,disprF*sin(9),,,UZ,...,
          ! Left Rear Strut Displacement
D,3104654,...,ALL,...
D,3104654,,displr,,UY,...,
          ! Right Rear Strut Displacement
D,3104655,...,ALL,...
D,3104655,,disprR,,UY,...,

LSWRITE,2,

-----
/TITLE,Load Set 3: Rack Rear Difference Only
-----

*SET,fmtdiff,0          ! Newtons
*SET,reardiff,-326134   ! Newtons

*SET,displF,(fmtdiff/2)/100000
*SET,disprF,-(fmtdiff/2)/100000
*SET,displr,(reardiff/2)/100000
*SET,disprR,-(reardiff/2)/100000

          ! Left Front Strut Displacement
D,4104661,...,ALL,...
D,4104661,,displF*cos(9),,,UY,...,
D,4104661,,displF*sin(9),,,UZ,...,
          ! Right Front Strut Displacement
D,4104660,...,ALL,...
D,4104660,,disprF*cos(9),,,UY,...,
D,4104660,,disprF*sin(9),,,UZ,...,
          ! Left Rear Strut Displacement
D,3104654,...,ALL,...
D,3104654,,displr,,UY,...,
          ! Right Rear Strut Displacement
D,3104655,...,ALL,...
D,3104655,,disprR,,UY,...,

LSWRITE,3,

-----
/TITLE,Load Set 4: Lean to One side Only
-----

*SET,fmtdiff            ! Newtons
*SET,reardiff           ! Newtons

*SET,displF,5
*SET,disprF,-5
*SET,displr,5
*SET,disprR,-5

          ! Left Front Strut Displacement
D,4104661,...,ALL,...
D,4104661,,displF*cos(9),,,UY,...,
D,4104661,,displF*sin(9),,,UZ,...,
          ! Right Front Strut Displacement
D,4104660,...,ALL,...
D,4104660,,disprF*cos(9),,,UY,...,
D,4104660,,disprF*sin(9),,,UZ,...,
          ! Left Rear Strut Displacement
D,3104654,...,ALL,...
D,3104654,,displr,,UY,...,
          ! Right Rear Strut Displacement
D,3104655,...,ALL,...
D,3104655,,disprR,,UY,...,

LSWRITE,4,
FINISH

/EOF
-----

```

❖ *Filename: 8 5 full post INPUT*

```

=====
! Combined 930E Frame and Dump Body FEA Model
! Post Processing Routine...
=====
=====
!----- Read in Results File
=====
RESUME,Aug_24,db,
!/GRAPHICS,FULL
=====
/POST1
INRES,
FILE,Aug_24,rst,
=====
ISET,1,LAST,1, ! Load Step #,Last
Substep, Scale=1
=====
!----- Combining Load Cases to Check Linearity
=====
ISET,2,LAST,5/1,355755,
!LWRITE,1, , , ,
ISET,3,LAST,5/1,63067,
!LWRITE,2, , , ,
!LCOPER,ADD,1, , ,
!/TITLE,LOAD CASE 3: Combined Results
!LWRITE,3, , , ,
!LCDEF,4,4, , ! Frame FEA Load Case Operations
=====
/EOF
=====
!----- Selecting Which Bolster to Study
=====
ALLSEL,ALL
=====
FLST,5,382,5,ORDE,153
FITEM,5,281
FITEM,5,-282
FITEM,5,284
FITEM,5,-285
FITEM,5,287
FITEM,5,-290
FITEM,5,292
FITEM,5,-293
FITEM,5,298
FITEM,5,-308
FITEM,5,324
FITEM,5,327
FITEM,5,-330
FITEM,5,338
FITEM,5,340
FITEM,5,343
FITEM,5,345
FITEM,5,348
FITEM,5,-362
FITEM,5,364
FITEM,5,-368
FITEM,5,373
FITEM,5,376
FITEM,5,-382
FITEM,5,385
FITEM,5,388
FITEM,5,391
FITEM,5,-397
FITEM,5,399
FITEM,5,-405
FITEM,5,407
FITEM,5,-408
FITEM,5,410
FITEM,5,-416
FITEM,5,439
FITEM,5,441
FITEM,5,-442
FITEM,5,469
FITEM,5,479
FITEM,5,481
FITEM,5,483
FITEM,5,531
FITEM,5,-532
FITEM,5,535
FITEM,5,-541
FITEM,5,543
FITEM,5,-548
FITEM,5,552
FITEM,5,554
FITEM,5,557
FITEM,5,-564
FITEM,5,573
FITEM,5,593
FITEM,5,596
FITEM,5,601
FITEM,5,830
FITEM,5,-852
FITEM,5,854
FITEM,5,-861
FITEM,5,863
FITEM,5,-865
FITEM,5,867
FITEM,5,-871
FITEM,5,907
FITEM,5,910
FITEM,5,939
FITEM,5,-941
FITEM,5,946
FITEM,5,957
FITEM,5,-958
FITEM,5,981
FITEM,5,986
FITEM,5,-997
FITEM,5,999
FITEM,5,1001
FITEM,5,-1009
FITEM,5,1012
FITEM,5,-1013
FITEM,5,1312
FITEM,5,-1313
FITEM,5,1315
FITEM,5,-1316
FITEM,5,1318
FITEM,5,-1321
FITEM,5,1323
FITEM,5,-1324
FITEM,5,1329
FITEM,5,-1339
FITEM,5,1355
FITEM,5,1358
FITEM,5,-136

```

FITEM,5,1369	FITEM,5,439
FITEM,5,1371	FITEM,5,442
FITEM,5,1374	FITEM,5,469
FITEM,5,1376	FITEM,5,481
FITEM,5,1379	FITEM,5,539
FITEM,5,-1393	FITEM,5,831
FITEM,5,-1395	FITEM,5,-832
FITEM,5,-1399	FITEM,5,834
FITEM,5,1404	FITEM,5,-835
FITEM,5,1407	FITEM,5,1407
FITEM,5,-1413	FITEM,5,-1412
FITEM,5,1416	FITEM,5,1423
FITEM,5,1418	FITEM,5,-1425
FITEM,5,1420	FITEM,5,1468
FITEM,5,-1426	FITEM,5,1471
FITEM,5,1428	FITEM,5,1498
FITEM,5,-1434	FITEM,5,1510
FITEM,5,1436	FITEM,5,1568
FITEM,5,-1437	FITEM,5,1860
FITEM,5,1439	FITEM,5,-1861
FITEM,5,-1445	FITEM,5,1863
FITEM,5,1468	FITEM,5,-1864
FITEM,5,1470	ASEL,R,,P51X
FITEM,5,-1471	CM,Bolster1,AREA
FITEM,5,1498	
FITEM,5,1508	
FITEM,5,1510	CMSSEL,S,ALL_BOL
FITEM,5,1512	
FITEM,5,1560	FLST,5,64,5,ORDE,56
FITEM,5,-1561	FITEM,5,354
FITEM,5,1564	FITEM,5,360
FITEM,5,-1570	FITEM,5,365
FITEM,5,1572	FITEM,5,-366
FITEM,5,-1577	FITEM,5,368
FITEM,5,1581	FITEM,5,373
FITEM,5,1583	FITEM,5,391
FITEM,5,1586	FITEM,5,393
FITEM,5,-1593	FITEM,5,441
FITEM,5,1602	FITEM,5,538
FITEM,5,1622	FITEM,5,541
FITEM,5,1625	FITEM,5,544
FITEM,5,1630	FITEM,5,546
FITEM,5,1859	FITEM,5,548
FITEM,5,-1881	FITEM,5,554
FITEM,5,1883	FITEM,5,558
FITEM,5,-1890	FITEM,5,560
FITEM,5,1892	FITEM,5,562
FITEM,5,-1894	FITEM,5,573
FITEM,5,1896	FITEM,5,830
FITEM,5,-1900	FITEM,5,836
FITEM,5,1920	FITEM,5,838
FITEM,5,1923	FITEM,5,-841
FITEM,5,1952	FITEM,5,843
FITEM,5,-1954	FITEM,5,-846
FITEM,5,1959	FITEM,5,849
FITEM,5,1970	FITEM,5,1001
FITEM,5,-1971	FITEM,5,1013
FITEM,5,1992	FITEM,5,1385
FITEM,5,1997	FITEM,5,1391
FITEM,5,-2008	FITEM,5,1396
FITEM,5,2010	FITEM,5,-1397
FITEM,5,-2021	FITEM,5,1399
ASEL,R,,P51X	FITEM,5,1404
CM,ALL_BOL,AREA	FITEM,5,1420
	FITEM,5,1422
	FITEM,5,1470
	FITEM,5,1567
FLST,5,36,5,ORDE,26	FITEM,5,1570
FITEM,5,376	FITEM,5,1573
FITEM,5,-381	FITEM,5,1575
FITEM,5,394	FITEM,5,1577
FITEM,5,-396	

! All Bolsters

FITEM,5,1583
 FITEM,5,1587
 FITEM,5,1589
 FITEM,5,1591
 FITEM,5,1602
 FITEM,5,1859
 FITEM,5,1865
 FITEM,5,1867
 FITEM,5,-1870
 FITEM,5,1872
 FITEM,5,-1875
 FITEM,5,1878
 FITEM,5,2011
 FITEM,5,2021
 ASEL,R,,P51X
 CM,Bolster2,AREA

 CMSEL,S,ALL,_BOL

 FLST,5,68,5,ORDE,58
 FITEM,5,324
 FITEM,5,364
 FITEM,5,367
 FITEM,5,388
 FITEM,5,537
 FITEM,5,540
 FITEM,5,543
 FITEM,5,545
 FITEM,5,547
 FITEM,5,552
 FITEM,5,557
 FITEM,5,559
 FITEM,5,563
 FITEM,5,-564
 FITEM,5,601
 FITEM,5,837
 FITEM,5,848
 FITEM,5,850
 FITEM,5,-852
 FITEM,5,854
 FITEM,5,-857
 FITEM,5,860
 FITEM,5,981
 FITEM,5,991
 FITEM,5,-993
 FITEM,5,999
 FITEM,5,1002
 FITEM,5,-1004
 FITEM,5,1012
 FITEM,5,1355
 FITEM,5,1395
 FITEM,5,1398
 FITEM,5,1418
 FITEM,5,1566
 FITEM,5,1569
 FITEM,5,1572
 FITEM,5,1574
 FITEM,5,1576
 FITEM,5,1581
 FITEM,5,1586
 FITEM,5,1588
 FITEM,5,1592
 FITEM,5,-1593
 FITEM,5,1630
 FITEM,5,1866
 FITEM,5,1877
 FITEM,5,1879
 FITEM,5,-1881
 FITEM,5,1883
 FITEM,5,-1886

FITEM,5,1889
 FITEM,5,1992
 FITEM,5,2002
 FITEM,5,-2004
 FITEM,5,2010
 FITEM,5,2012
 FITEM,5,-2014
 FITEM,5,2020
 ASEL,R,,P51X
 CM,Bolster3,AREA

 CMSEL,S,ALL,_BOL

 FLST,5,44,5,ORDE,40
 FITEM,5,358
 FITEM,5,-359
 FITEM,5,361
 FITEM,5,-362
 FITEM,5,385
 FITEM,5,536
 FITEM,5,561
 FITEM,5,593
 FITEM,5,596
 FITEM,5,847
 FITEM,5,859
 FITEM,5,861
 FITEM,5,863
 FITEM,5,-864
 FITEM,5,988
 FITEM,5,-990
 FITEM,5,996
 FITEM,5,-997
 FITEM,5,1005
 FITEM,5,-1007
 FITEM,5,1389
 FITEM,5,-1390
 FITEM,5,1392
 FITEM,5,-1393
 FITEM,5,1416
 FITEM,5,1565
 FITEM,5,1590
 FITEM,5,1622
 FITEM,5,1625
 FITEM,5,1876
 FITEM,5,1888
 FITEM,5,1890
 FITEM,5,1892
 FITEM,5,-1893
 FITEM,5,1999
 FITEM,5,-2001
 FITEM,5,2007
 FITEM,5,-2008
 FITEM,5,2015
 FITEM,5,-2017
 ASEL,R,,P51X
 CM,Bolster4,AREA

 CMSEL,S,ALL,_BOL

 FLST,5,40,5,ORDE,32
 FITEM,5,352
 FITEM,5,-353
 FITEM,5,355
 FITEM,5,-357
 FITEM,5,382
 FITEM,5,535
 FITEM,5,858
 FITEM,5,865
 FITEM,5,867
 FITEM,5,-871

FITEM,5,986
 FITEM,5,987
 FITEM,5,994
 FITEM,5,995
 FITEM,5,1006
 FITEM,5,1009
 FITEM,5,1383
 FITEM,5,1384
 FITEM,5,1386
 FITEM,5,1388
 FITEM,5,1413
 FITEM,5,1564
 FITEM,5,1887
 FITEM,5,1894
 FITEM,5,1896
 FITEM,5,1900
 FITEM,5,1997
 FITEM,5,1998
 FITEM,5,2005
 FITEM,5,2006
 FITEM,5,2018
 FITEM,5,2019
 ASEL,R,,P51X
 CM,Bolster5,AREA

 CMSEL,S,ALL,BOL

 FLST,5,34,5,ORDE,24
 FITEM,5,288
 FITEM,5,301
 FITEM,5,302
 FITEM,5,304
 FITEM,5,306
 FITEM,5,308
 FITEM,5,351
 FITEM,5,403
 FITEM,5,405
 FITEM,5,408
 FITEM,5,410
 FITEM,5,414
 FITEM,5,1319
 FITEM,5,1332
 FITEM,5,1333
 FITEM,5,1335
 FITEM,5,1337
 FITEM,5,1339
 FITEM,5,1382
 FITEM,5,1432
 FITEM,5,1434
 FITEM,5,1437
 FITEM,5,1439
 FITEM,5,1443
 ASEL,R,,P51X
 CM,Bolster6,AREA

 CMSEL,S,ALL,BOL

 FLST,5,34,5,ORDE,28
 FITEM,5,289
 FITEM,5,290
 FITEM,5,292
 FITEM,5,293
 FITEM,5,298
 FITEM,5,300
 FITEM,5,303
 FITEM,5,307
 FITEM,5,397
 FITEM,5,399
 FITEM,5,402
 FITEM,5,407

FITEM,5,415
 FITEM,5,416
 FITEM,5,1320
 FITEM,5,1321
 FITEM,5,1323
 FITEM,5,1324
 FITEM,5,1329
 FITEM,5,1331
 FITEM,5,1334
 FITEM,5,1338
 FITEM,5,1425
 FITEM,5,1428
 FITEM,5,1431
 FITEM,5,1436
 FITEM,5,1444
 FITEM,5,1445
 ASEL,R,,P51X
 CM,Bolster7,AREA

 CMSEL,S,ALL,BOL

 FLST,5,34,5,ORDE,32
 FITEM,5,282
 FITEM,5,284
 FITEM,5,327
 FITEM,5,330
 FITEM,5,338
 FITEM,5,340
 FITEM,5,343
 FITEM,5,348
 FITEM,5,350
 FITEM,5,479
 FITEM,5,531
 FITEM,5,532
 FITEM,5,833
 FITEM,5,907
 FITEM,5,939
 FITEM,5,941
 FITEM,5,1313
 FITEM,5,1315
 FITEM,5,1358
 FITEM,5,1361
 FITEM,5,1369
 FITEM,5,1371
 FITEM,5,1374
 FITEM,5,1379
 FITEM,5,1381
 FITEM,5,1508
 FITEM,5,1560
 FITEM,5,1561
 FITEM,5,1862
 FITEM,5,1920
 FITEM,5,1952
 FITEM,5,1954
 ASEL,R,,P51X
 CM,Bolster8,AREA

 CMSEL,S,ALL,BOL

 FLST,5,26,5,ORDE,28
 FITEM,5,281
 FITEM,5,285
 FITEM,5,287
 FITEM,5,328
 FITEM,5,329
 FITEM,5,345
 FITEM,5,392
 FITEM,5,483
 FITEM,5,842
 FITEM,5,910

```

FITEM,5,940
FITEM,5,946
FITEM,5,957
FITEM,5,-958
FITEM,5,1312
FITEM,5,1316
FITEM,5,1318
FITEM,5,1359
FITEM,5,-1360
FITEM,5,1376
FITEM,5,1421
FITEM,5,1512
FITEM,5,1871
FITEM,5,1923
FITEM,5,1953
FITEM,5,1959
FITEM,5,1970
FITEM,5,-1971
ASEL,R,,P51X
CM,Bolster9,AREA

ALLSEL,ALL

CMSEL,S,Bolster1      ! Front Bolster
CMSEL,A,Bolster2
CMSEL,A,Bolster3
CMSEL,A,Bolster4
CMSEL,A,Bolster5
CMSEL,A,Bolster6
CMSEL,A,Bolster7
CMSEL,A,Bolster8
CMSEL,A,Bolster9      ! Rear Bolster

ALLSEL,BELOW,AREA

!-----
!----- Plotting Bending Stresses
!-----

/POST1

SHELL,TOP
AVPRIN,0,0
ETABLE,SXTOP,S,X
SHELL,BOT
AVPRIN,0,0
ETABLE,SBOT,S,X
SADD,SEC_BEND,SXTOP,SBOT,1,-1,0,

! /TITLE, Bending Stresses
PLETAB,SEC_BEND,AVG

!-----
!----- Defining Paths Along Main Rails
!-----

:;test
!LCASE,3
!SET,4,1,2,1,

ALLSEL,ALL
FLST,5,36,5,ORDE,8
FITEM,5,1011
FITEM,5,1015
FITEM,5,-1029
FITEM,5,1045
FITEM,5,-1059
FITEM,5,1061
FITEM,5,1064
FITEM,5,-1067

ASEL,R,,P51X      ! Selecting Main Rail Areas
ALLSEL,BELOW,AREA

FLST,2,2,1
FITEM,2,151976
FITEM,2,153615
PATH,LPath,2,30,40,
PPATH,P51X,1      ! Path on Left Rail

PDEF,STAT
AVPRIN,0,0
PDEF,,U,Y,AVG      ! Mapping Results to Path

PAGET,L_Path,TABL      ! Storing Path Items in Array

FLST,2,2,1
FITEM,2,152758
FITEM,2,153550
PATH,RPath,2,30,40,
PPATH,P51X,1      ! Path on Right Rail

PDEF,STAT
AVPRIN,0,0
PDEF,,U,Y,AVG      ! Mapping Results to Path

PAGET,R_Path,TABL      ! Storing Path Items in Array

!-----
!----- Writing Path Data to Text File
!-----

! /EOF
! :;test

*CFOPEN,XL_couple_R_Path.txt,
**WRITE,R_Path(1,1),R_Path(1,2),R_Path(1,3),R_Path(1,4),R_Path(1,5),...
(F12.4,F12.1,F12.4,F12.1,F12.4)
**CFCLOSE

*CFOPEN,XL_couple_L_Path.txt,
**WRITE,L_Path(1,1),L_Path(1,2),L_Path(1,3),L_Path(1,4),L_Path(1,5),...
(F12.4,F12.1,F12.4,F12.1,F12.4)
**CFCLOSE

! /EOF

!-----

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