

COMMUNICATION SYSTEM FOR THE REMOTE
HYBRID POWER SYSTEM IN RAMEA NEWFOUNDLAND

JUAN FERNANDO ACEVEDO



**COMMUNICATION SYSTEM FOR THE REMOTE HYBRID
POWER SYSTEM IN RAMEA NEWFOUNDLAND**

by

© Juan Fernando Acevedo

A thesis submitted to the School of Graduate Studies in partial fulfillment of the
requirements for the degree of Master of Engineering.

Faculty of Engineering and Applied Science
Memorial University of Newfoundland

May 2011

ABSTRACT

A reliable communication system is essential for the operation of a remote hybrid power system. Such a system is needed to interconnect the wind turbines, diesel generators, and the hydrogen energy storage unit with a centralized supervisory controller and data acquisition system. For the purpose of this research, we have considered the remote wind-diesel-hydrogen hybrid power system currently under development at Ramea, Newfoundland. This thesis illustrates the implementation of a half-duplex collective transmission agreement with low RF transceivers and Power Line Carrier modems which allows the system to have a redundancy network and provide uninterrupted communication between the wind turbines and the main power building. Power line couplers with high pass filters and high frequency amplifiers are also designed and implemented to permit data transmission through high voltage power lines without affecting the performance of the data acquisition system. The research also provides the description of wind turbines parameters being measured at Ramea's remote hybrid power solution.

ACKNOWLEDGMENTS

I would like to thank Dr. Tariq Iqbal for his continuous guidance and support, the National Science and Engineering Research Council (NSERC) Wind Energy Strategic Network and Memorial University of Newfoundland for the financial support for this research. I would also like to thank Newfoundland and Labrador Hydro for providing site access and system data.

TRIBUTE

I would like to dedicate my work to my parents for their constant and unconditional support, to my family and friends for encouraging me in times of weakness.

"The ultimate challenge is in my mind"

TABLE OF CONTENTS

	Page
Abstract.....	ii
Acknowledgments.....	iii
Tribute.....	iv
Table of Contents.....	v
List of Tables.....	viii
List of Figures.....	ix
List of Abbreviations and Symbols.....	x
List of Appendices.....	xii
CHAPTER 1: INTRODUCTION AND LITERATURE REVIEW.....	1
1.1 WIND-DIESEL HYBRID POWER SYSTEMS WORLDWIDE.....	1
1.1.1 Canada's Wind Power Capacity.....	4
1.2 WIND-HYDROGEN-DIESEL (WHD) POWER SYSTEM OF RAMEA, NEWFOUNDLAND.....	6
CHAPTER 2: COMMUNICATION METHODS FOR HYBRID POWER SYSTEMS.....	10
2.1. FIBER OPTIC.....	12

2.1.1 Free Space Optical.....	13
2.2. CONTROLLER AREA NETWORK (CAN) BUS.....	14
2.3. WIRELESS ETHERNET.....	16
2.3.1 Worldwide Interoperability for Microwave Access (WIMAX).....	16
2.4. LOW RF TRANSCEIVERS.....	17
2.5. POWER LINE CARRIER.....	18
CHAPTER 3: COMMUNICATION SYSTEM FOR RAMEA'S HYBRID POWER SYSTEM.....	20
3.1. TRANSMISSION ALGORITHM	20
3.2. COMMUNICATION SYSTEM SETUP	22
3.2.1. DAST's Microcontroller Pin Configuration	23
3.2.2. Serial-to-Ethernet Adaptor (XPORT XP1001000-03).....	24
3.2.3. Inductive Coupling Stage.....	25
3.2.3.1. High Pass Filter (HPF)	26
3.2.3.2. High Frequency Amplifier (HFA).....	28
3.2.3.3. Inductive Coupling Device (ICD)	29
3.3. COMMUNICATION SYSTEM PROTOTYPES	31
3.3.1. Graphic User Interface (GUI)	32
CHAPTER 4. EXPERIMENTAL RESULTS	35

4.1. COST – BENEFIT ASSESSMENT	37
4.1.1. Benefits.....	38
CHAPTER 5: CONCLUSIONS AND RECOMMENDATIONS	40
5.1. FUTURE WORK	43
BIBLIOGRAPHY AND REFERENCES	45
APPENDICES	55

LIST OF TABLES

	Page
Table 1.1. Isolated power system categories.....	2
Table 1.2. List of Some Wind-Diesel Hybrid Power Systems.....	3
Table 1.3. Canada's current wind farm capacity.....	5
Table 2.1. Wind Turbine's analog and digital recorded data and sampling time.....	11
Table 3.1. DAST's Microcontroller PIC16F873A Pin Configuration.....	24
Table 4.1. Hardware Cost.....	37
Table 4.2. Load Consumption.....	43

LIST OF FIGURES

	Page
Figure 1.1. Current Ramea WHD Power System.....	6
Figure 1.2. Six (6) 65kW Wind Turbines.....	7
Figure 1.3. Three (3) 100kW Wind Turbines.....	8
Figure 2.1. Optical Fiber Cable.....	12
Figure 2.2. Hill between the DAS and MPCB	14
Figure 2.3. Classic CAN connection diagram	15
Figure 3.1. DAST Transmission Flow Chart	21
Figure 3.2. Communication System Diagram	22
Figure 3.3. Data Acquisition System Transmitter Prototype Setup	23
Figure 3.4. High Pass Filter	26
Figure 3.5. 1 st Sample of Data Signal	27
Figure 3.6. 2 nd Sample of Data Signal	28
Figure 3.7. High Frequency Amplifier	29
Figure 3.8. Inductive Coupling Device Diagram	30
Figure 3.9. Inverted HPF	31
Figure 3.10. Communication System Prototypes	32
Figure 3.11. Graphic User Interface	33
Figure 4.1. Microcontroller's Algorithm XPORT initialization + Buffer	36
Figure 4.2. ICD & HPF+HFA Signal	37

LIST OF ABBREVIATIONS AND SYMBOLS

AC:	Alternate Current
BPL:	Broadband over PowerLines
CAN:	Controller Area Network
DAS:	Data Acquisition System
DAST:	Data Acquisition System Transmitter
DSL:	Digital Subscriber Line
EMF:	ElectroMagnetic Field
FHSS:	Frequency Hopping Spread Spectrum
FSK:	Frequency Shifting Keying
FSO:	Free Space Optical
GUI:	Graphic User Interface
HFA:	High Frequency Amplifier
HPF:	High Pass Filter
ICD:	Inductive Coupling Device
ISM:	Industrial Scientific Medical
ISO:	International Organization for Standardization
LAN:	Local Area Network
MIMO:	Multiple Input Multiple Output
MPCB:	Main Power Control Building
MPCBR:	Main Power Control Building Receiver

PLC:	Power Line Carrier
RC:	Resistor Condenser
RF:	Radio Frequency
SCADA:	Supervisory Control And Data Acquisition
TCP/IP:	Transmission Control Protocol/Internet Protocol
USART:	Universal Synchronous/Asynchronous Receiver/Transmitter
USB:	Universal Serial Bus
UTP:	Unshielded Twisted Pair
WHD:	Wind Hydrogen Diesel
Wi-Fi:	Wireless Fidelity
WIMAX:	Worldwide Interoperability for Microwave Access

LIST OF APPENDICES

	Page
APPENDIX A. Ramea Wind-Hydrogen-Diesel Project, Realistic Point Count	
EMS Group – St. John's	55
APPENDIX B. Microcontroller (DAS) source code	67
APPENDIX C. Graphic User Interface source code	70
APPENDIX D. Components' datasheets used for this project	73
APPENDIX E. Data Acquisition System Transmitter Schematic	85

CHAPTER 1: INTRODUCTION AND LITERATURE REVIEW

Isolated power systems on rural communities have been diesel dependent for decades not only to maintain residents' power demands but because of topography challenges they are unable to connect to main power grids. Nevertheless, fossil fuels' continuous cost growth and carbon emissions have made rural power plants shifted from diesel to a combination of renewable energy technology and diesel engines. Having evolved into hybrid power systems, energy grid's control system demands a constant and reliable communication not only to monitor and control selected carbon free sources of energy but to maintain a balanced distribution on power demand.

1.1 WIND-DIESEL HYBRID POWER SYSTEMS WORLDWIDE

Renewable energy systems can be a sustainable energy source guaranteeing reliability, sustainability, and affordability, but because of their natural characteristics they often have an intermittent energy source which requires complex techniques for optimal utilization. As a counter measure to potential power outages, hybrid power systems provide a higher level of stability with a combination of several carbon-free energy sources like wind or solar and non-renewable sources like diesel or natural gas. Remote power system categories are shown in Table 1.1.

Table 1.1. Isolated power system categories [1]

Installed Power (MW)	Category
<0.001	Micro System
0.001 – 0.1	Village Power System
0.1 – 10	Island Power System
>10	Large Interconnected System

Implementation of these hybrid systems has spread worldwide, countries like Australia, Canada, China, Greece, Norway, UK, USA and others, are increasingly growing their hybrid solutions in order to address global challenges such as carbon emission crisis, fuel flexibility, power efficiency, and economic growth among others. T. Ackerman [1] analyzes the history of hybrid power systems, their categories depending on power capacity, and illustrates a list of hybrid power systems installed in Sal, Cape Verde; Mindelo, Cape Verde; Dachen Island, China; Kythnos, Greece; Lemnos, Greece.

Table 1.2 shows a selection of some wind-diesel solutions installed around the globe, the technical data was retrieved from several references such as Meridian Energy [2], a report containing technical information about Ross Island, Antarctica hybrid energy system. S. Bennett [3] shows a chronological expose of Ross Island's (Antarctica) Wind Energy project progress report up to Dec 2009. The Renewable Energy Alaska Project reports [4]-[5] illustrate technical data about hybrid power projects in Summit station (Greenland), Kotzebue Alaska (USA), Guantanamo (Cuba), Ross Island (Antarctica), St. Paul Alaska (USA), Coral Bay (Australia). The National Renewable Energy Laboratory

[6] presents power capacity information and wind penetration data of the hybrid power system in Mawson, Antarctica. J. Zimmerman [7] and D. Clarke's [8] research has information about isolated renewable energy/diesel systems installed in Bremer Bay, Cocos Island, Denham, Esperance, Hopetoun, Graciosa, Flores, Rottneest, and Ross Island in Australia. P. Lundsager et al. [9] reports technical information about hybrid power systems installed in: Sal and Mindelo (Cape Verde), La Desirade (Guadeloupe), Marsabit (Kenya), Cape Clear Island and Rathlin Island (Ireland), Froya (Norway).

Table 1.2. List of Some Wind-Diesel Hybrid Power Systems

Country or Region	Site	Diesel Power (MW)	Wind Power (MW)	Avg. Load (MW)	Commissioned	Inst. Wind Penetration
Antarctica	Mawson	0.48	0.6	0.53	2002	34% (avg)
Antarctica	Ross Island	3	0.99	1.75	2010	20%
Australia	Bremer Bay	1.25	0.6		2005	>80%
Australia	Cocos Island	1.28	0.08		2005	15% (avg)
Australia	Coral Bay	2.24	0.825		2007	>90%
Australia	Denham	1.6	1.2		1998	>50%
Australia	Esperance	14.5	5.6		2003	>22%
Australia	Hopetoun	2.56	1.2		2004	>90%
Australia	Graciosa	3.2	0.8			60% (avg)
Australia	Flores	4	0.6			>50%
Australia	Rottneest	1.3	0.6		2006	37% (avg)
Canada	Rainco	2.78	0.69	0.7	2004	10% (avg)
Cape Verde	Sal	2.82	0.6	0.56		14% (avg)
Cape Verde	Mindelo	11.2	0.9	1.9		14% (avg)
China	Dachen Island	10.44	0.185			15% (avg)
Cuba	Guantanamo	22.8	3.8	12.5	2005	25%
Greece	Kythnos Island	2.774	0.315			
Greece	Lemnos Island	10.4	1.14			
Greenland	Summit	0.2	0.06			16%
Guadeloupe	La Desirade	0.88	0.14			49%
Kenya	Marsabit	0.3	0.15			46% (avg)
Norway	Froya	0.95	0.955			100%
Ireland	Cape Clear Island	0.072	0.06			70%

Country or Region	Site	Diesel Power (MW)	Wind Power (MW)	Avg. Load (MW)	Commissioned	Inst. Wind Penetration
Ireland	Rathlin Island	0.26	0.99			100%
USA	St. Paul, Alaska	0.3	0.22	0.12	1999	68.5% (avg)
USA	Kotzebue, Alaska	11	1.14	1.37		50%

1.1.1 Canada's Wind Power Capacity

Although Canada has made a remarkable effort on expanding its national wind power capacity as seen in Table 1.3, there has been little progress with hybrid power systems development. According to J. Macgillivray [10] and the news reports [11]-[13] the Toktoyaktuk Wind-Diesel project will save 88,000 liters of diesel per year and will offset 247 tones of emissions year long.

According to the research done by T. M. Weis and A. Ilincu in 2007 [14] there have been several low-penetration wind-diesel systems installed across remote Canadian communities like Big Trout Lake (ON), Cambridge Bay (Nunavut), Ellesmere Island (Nunavut), Fort Severn (ON), Igloodik (NT), Iqaluit (Nunavut), Kasabonika Lake (ON), Kugluktuk (Nunavut), Kuujuaq (PQ), Omingmaktok (NT), Sachs Harbour (NT), Rankin Inlet (Nunavut) and Winisk (ON), but only Cambridge Bay and Kuujuaq hybrid power systems where operational for 8 years, the rest had a maximum life span of 2 years.

Other initiatives like PEI's Energy Corporation [15] or B. Saulnier and R. Gagnon [16] are new Canadian developments on hybrid power systems. Projects like Nalcor Energy "Wind-Hydrogen-Diesel (WHD) Power System" in Ramen NL, Northern Wind

Tuktoyaktuk's project, PEI Wind-Hydrogen Village and Quaqtaq's studies are some of the major research contributions to the few Canadian national efforts to provide rural communities with efficient and cleaner sources of energy in order to reduce carbon emissions as a counter measure to global warming and fossil fuel economic challenges.

Technical data from Table 1.3 was retrieved from the Canadian Wind Energy Association (CANWEA) [17] [18] studies; the reports show graphs and tables explaining province's wind installed capacity and the Canadian wind energy projects with a signed power purchase agreement and/or already under construction/construction plan in place as of Aug. 24, 2010.

Table 1.3. Canada's current wind farm capacity

Province	Installed Capacity (MW)	Planned /Under Construction (MW)
Alberta	884	1039.6
British Columbia	103.5	711.2
Manitoba	194	138
New Brunswick	249	163.5
Newfoundland and Labrador	54.7	
Nova Scotia	214	185.55
Ontario	1,447	4032.1
Prince Edward Island	164	10
Quebec	663	2361
Saskatchewan	171.2	54.75
Yukon	0.81	
TOTAL	4055.21	8695.7

1.2 WIND-HYDROGEN-DIESEL (WHD) POWER SYSTEM OF RAMEA, NEWFOUNDLAND

Located six (6) kilometers South-West of Newfoundland, Ramea is an island community of 600 residents, its Hybrid Power System, shown in Figure 1.1, has a 2.775MW diesel plant consisting of three 925kW diesel generators and six 65kW wind turbines located North-West of the island added to the system by Frontier Power Systems (<http://www.frontierpower.com>).

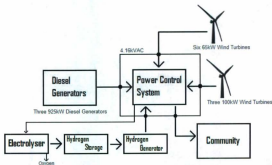


Figure 1.1. Current Ramea WHD Power System

According to "Ramea Wind-Hydrogen Diesel Project" 2007 progress report done by Newfoundland Hydro (<http://www.nh.nl.ca/>) (a Nalcor Energy company), the development of the hybrid power project was undertaken by Nalcor Energy

(<http://www.nalcorenergy.com>), they upgraded it in 2009 with three new 100kW wind turbines sited north of the Island and a Hydrogen facility currently under development [19]. Their power infrastructure combines wind, hydrogen, and diesel generators in order to reduce the isolated community dependence on diesel and replace it with energy generation from a renewable resource.



Figure 1.2. Six (6) 65kW Wind Turbines

In September of 2004, Newfoundland Hydro began purchasing wind energy from Frontier Power's wind turbines (WindMatic WM15S, see Figure 1.2) which can have a combined wind penetration of 10% and offsets approximately 750 tonnes of emissions annually. The new three 100kW wind turbines installed by Nalcor Energy were positioned 130m, 200m, and 270m (see Figure 1.3) from the Main Power Control Building (MPCB). Nalcor Energy's winter 2010 "Ramea Report" mentions that the new wind turbines were commissioned in December 2009 and generated energy on the Ramea grid for the first time on May 8, 2010 [20].



Figure 1.3. Three (3) 100kW Wind Turbines

With Frontier Power's wind turbines Data Acquisition System (DAS) located 1.6km of the Main Power Control Building, the only remote connection currently installed is a wireless link between the DAS and the MPCB by the use of two Cirronet HN-210D transceivers. Unfortunately they are constantly having communication failures, especially during winter season. According to the HN-210 datasheet, its functional frequency is 2.4GHz ISM band which allows them to operate in the free-license electromagnetic spectrum [21]. The problem relies in transmitting under hazardous weather conditions like snow storms, rain, hail, or a combination of all three, limiting remote supervision and control; a 2.4GHz transmission is vulnerable to atmospheric attenuation. A reliable and low cost communication solution must be engineered in order to have a trustworthy control of Ramea's Hybrid Power System.

A communication system prototype for the remote WHD hybrid power system currently under development at Ramea, Newfoundland is presented in this document which motivation and focal points involve a cost-effective solution to maintain reliable and uninterrupted data transmission throughout the power grid, no modification on current

power infrastructure, a combination of different communication methods working in sync for superior transmission stability, and comparison of commonly preferred techniques which will highlight the advantages and usefulness of this project. The proposed system is based on hybrid transmission between a wireless connection and data communication through existing power lines.

In chapter 2, hybrid power systems' communication methods are evaluated in order to have a broad analysis of the engineering involve in this thesis. In chapters 3 and 4, system prototype features and advantages are introduced, engineering design is explain in detail, and finally lab results and cost-effective solutions are studied for evaluation purposes. Conclusions and recommendations are discussed in chapter 5 for possible future development of the project.

CHAPTER 2: COMMUNICATION METHODS FOR HYBRID POWER SYSTEMS

Hybrid power solutions are always demanding trustworthy communications between renewable and non-renewable power systems to facilitate supervision and control of carbon free sources of energy and maintain a balanced distribution on power demand. In order to accomplish a constant and reliable communication link, numerous technologies need to be evaluated based on performance under any weather condition, transmission security, dedicated physical layer dependence, cost-effective solution, bandwidth capabilities, among others. The study will focus on technologies like Fiber Optic, FSO, CAN Bus, Wi-Fi, WIMAX, Low RF links, and PLC.

Table 2.1 shows a sample of analog & digital parameters measured to run proper diagnostics on wind turbine performance, statistical analysis, historical data record, updates on weather changes, remote control, dynamic warnings, and other features needed for the hybrid power system's Supervisory Control And Data Acquisition (SCADA). A suitable and reliable physical layer of communication is indeed needed for un-interrupted remote recording of these parameters, A. L. Pereira in 2000 studied methods like Parallel ports, Universal Serial Bus (USB), and Ethernet LAN for "Modular supervisory controller for hybrid power systems" [22]. R. Sebastian, M. Castro, E. Sancristobal, F. Yeves, J. Peire, and J. Quesada in 2002 proposed in their research "Approaching hybrid wind-diesel systems and Controller Area Network" a CAN Bus as a

suitable implementation for hybrid wind-diesel systems [23]. Ramea's power system communication network relies on Fiber Optic and RF wireless transceivers, but there is no mention (wireless communication excluded) of a non invasive technique that does not require modifying the infrastructure such as Power Line Carrier or PLC which can be adjusted to meet this requirement.

Table 2.1 was sampled from Newfoundland Hydro's "Ramea Wind-Hydrogen-Diesel Project, Realistic Point Count for EMS Group – St. John's" report. They provided the hard copy in February 2009 so please refer to Appendix A for full scanned table content.

Table 2.1. Wind Turbine's analog and digital recorded data and sampling time

WindMatic WM155	Unit	Point Type	Scan Rate
Inverter Power	kW	Analog	10s
Rotor Speed	RPM	Analog	10s
Inst. Wind Speed	m/s	Analog	10s
One Min.Avg Wind Speed	m/s	Analog	10s
Ten Min.Avg Wind Speed	m/s	Analog	10s
Hours Online		Analog	10s
Cumulative Energy Production	kWh	Analog	10s
Breaker Status	Open/ Closed	Digital	10s
Permission to Operate	Yes/No	Digital	10s

2.1. FIBER OPTIC

In recent years, Fiber Optic has become more appropriate for high speed data communication. The use of optic light pulses through the fiber lines instead of electronic pulses makes it unaffected to electromagnetic interferences, and with proper thermoplastic over-coating insulation it can be suitable to transmit under extreme weather conditions as mentioned in 1994 by H. Kirkham et al. [24]. Figure 2.1 below (retrieved from Home Theater Accessories Resource commercial webpage "How Optical Cable Works" [26]) shows the composition of an optical cable, Mary Bellis' article on "The birth of fiber optics" explains that a Fiber optic cables are optic wires inside an outer insulation that transmit digital information using light waves traveling by internal reflection over longer distances than any other high speed wired form of communication [25].



Figure 2.1. Optical Fiber Cable

Fiber optic networks can handle high speed data transmissions (up to several Gigabytes) and has been used for the communication network of the new three (3) 100kW wind turbines at Ramea. Even do the current fiber optic cables connecting these wind turbines to the MPCB allow them to reach Gbps transmissions, Table 2.1 above shows that the parameter scan rate does not require high bandwidth capability. Inconveniences like elevated costs and installation makes fiber optic not suitable for Ramea's hybrid power system. According to Newfoundland Hydro, CAN\$19,380.00 was the estimated cost for only the fiber optic cables and considering expanding this network to the 65kW wind turbines' DAS will not fulfill the low budget aspiration of this project.

2.1.1 Free Space Optical

Emulating a Fiber Optic communication in a wireless environment could be another approach. A. Akbulut, H. Gokhan Ilk, F. Ari in 2005 mention in their study "Design, Availability and Reliability Analysis on an Experimental Outdoor FSO/RF Communication System", that a Free Space Optical (FSO) technology can provide a 155Mbps full duplex connection, but the FSO devices have to be carefully installed in specific locations as they need a "Line-of-sight alignment", and data transmission is very susceptible when exposed to poor weather conditions [27]. This option is also not suitable for Ramea because of its low performance during poor weather conditions and since line of site transmission is not possible due to a hill between wind turbines' DAS and the diesel plant (Figure 2.2).



Figure 2.2. Hill between the DAS and MPCB

2.2. CONTROLLER AREA NETWORK (CAN) BUS

In 1986, the German company BOSCH developed CAN initially as a communication protocol for automotive applications. Shortly after, it was standardized in the International Organization for Standardization ISO 11898 & 11519 allowing the protocol to be used in a wide variety of networking devices including automotive, naval, medical and industrial applications as mentioned in Renesas Electronics Corporation "Introduction to CAN" study on CAN's outline, protocol, features, and standard specifications [28].

For a small overview of this communication method please refer to Renesas Electronics Corporation's "CAN connection diagram" on Figure 2.3 below, the CAN Controller decides the bus level (Dominant or Recessive) by the potential difference between the

two cables (the "Bus"), connected transmitters send signals to the receiver by altering these levels. If two or more devices transmit at the same time, the CAN Controller will decide which signal pass first depending on their priority status.

Even though the 2002 study of "Approaching hybrid wind-diesel systems and Controller Area Network" mentions some advantages to the usage of a CAN Bus like switching from centralized to distributed control and minimum wiring, this communication method still needs a dedicated physical layer, an antagonistic feature to the un-modified power infrastructure attribute of this research. Additionally, the CAN Bus dependence on clock synchronization is an unnecessary feature that can be avoided with other communication technologies.

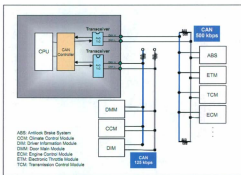


Figure 2.3. Classic CAN connection diagram

2.3. WIRELESS ETHERNET

Since the beginning of the 21st century, wireless networks have been exponentially growing and constantly required for faster Ethernet & Internet access. Cheaper installation expenses and total independency from physical Ethernet ports are the most attractive features in wireless communications.

Low budget commercially available wireless Ethernet modem/routers that uses the IEEE 802.11g or 802.11n standard work in the 2.4, 3.6 and 5 GHz frequency bands and a usual bit rate of 54Mbps (modems that uses IEEE802.11n standard can achieve up to 600Mbps), and its outdoor transmission varies from 100m-420m without compromising their bandwidth capabilities. Intel Corporation's article on "Helping Define 802.11n and other Wireless LAN Standards" states that increasing the throughput can be achieved by using the technology referred to as Multiple-Input-Multiple-Output (MIMO) which utilizes multiple signals from an array of antennas across a designated area [29], but this means a bigger investment to purchase signal repeaters. These modems are discarded for this project due to their dependence on present conditions and their limited outdoor communication range.

2.3.1 Worldwide Interoperability for Microwave Access (WIMAX)

Another possibility could be the use of WIMAX, a wireless telecommunication technology that uses the IEEE 802.16 standard, provides mobile internet access, around 40Mbps bandwidth, and operates under licensed spectrum owned by wireless service

providers. According to Intel Corporation's study on "How WIMAX works", mobile WIMAX base stations over metropolitan size areas can provide wider coverage than Wi-Fi networks (up to two kilometers depending on terrain), and used commonly as a *last mile* wireless broadband replacement for Digital Subscriber Line (DSL) [30]. Nevertheless, the transmission is outside the unlicensed electromagnetic spectrum so there has to be a contract involved with a WIMAX carrier. Therefore, it would be a costly solution for hybrid power systems.

2.4. LOW RF TRANSCEIVERS

Transceiver is a device that has the capability to transmit and receive within the same circuitry. RF Transceiver uses Radio Frequency modules usually for high speed bps transmission, a wireless approach to LANs, but under extremely hazardous weather conditions like snow or hail storms common in Ramea during winter season, wireless transmission frequency band must be in sub-GHz. From Dr. J. Takci's analysis on "Digital Wireless Communication Basics: Overview of basic concepts", it is conceptualized that RF transceivers employing frequencies close to 900MHz makes them perfect to transmit even in extremely bad weather conditions as no attenuation and RF wave scattering is generated by snow or rain drops [31].

Even though the bit rate is lower than the Wireless Ethernet modems, they are very appropriate for Ramea's communication system as we could transmit data packages at low speed (57.6kbps) without affecting DAS performance. This data transfer rate can sustain Ramea's current wind farm remote supervision and control.

2.5. POWER LINE CARRIER

Power Line Carrier (PLC) or Power Line Communication technology incorporates high frequency signals traveling throughout power networks to dedicated PLC receivers distributed among the same complex. Using electric power transmission conductors as communication media will achieve a bidirectional data communication saving resources without installing new dedicated cabling. Applications for this technology include D. D. Bois, Energy Business "Broadband over Powerlines (BPL) in a Nutshell", which provides on-site users with high speed internet access through regular power outlets [32], and "Home Automation" [33] technology that allows house residents to control lights & appliances remotely using PLC modules such as: NETGEAR [34], X10 [35], LonWorks [36], INSTEON [37], EHS (European Home Systems) [38], KNX PL 110 [39], among others.

Above applications focus on domestic use (commonly 120-240VAC power lines) but to successfully transmit data through high voltage cabling (>1kVAC), without damaging microcontrollers or other low voltage devices, there has to be a proper installation of stage circuitry such as: Dedicated PLC modems connected to microcontrollers, a coupling and filtering stage between the modems and high voltage carriers, and a final synchronization process with the high voltage signal. The purpose is to have a bilateral communication between the DAS and the MPCB without modifying the power system infrastructure currently in place at Ramea.

In order to achieve a constant transmission, a redundant communication network can be accomplished if PLC operates as primary link and low RF transceivers as backup. Using PLC as primary is based on continuous presence of the power line cable, it is usually available the 24h of any giving day as it is permanently connected from DAS to the MPCB but if a miscommunication occurs then the wireless link will become enabled for data transmission. By implementing PLC and low RF transceivers we can achieve a reliable low cost communication system for control and data acquisition of Ramea's hybrid power system.

The rationale to opt for PLC & Low RF transceivers instead of the others is based on the previous analysis of above technologies. PLC & Low RF have economically feasible modems, accurate transmission capabilities under any weather condition, embedded wireless transmission encryption, no dedicated physical layer, redundant communication capabilities as a hybrid comm. system, the capability for future expansion to more than a pair of modules with the same type of modems, and bandwidth capabilities necessary for Ramea's WHD power system. Details of proposed communication system are provided in the next two chapters.

CHAPTER 3: COMMUNICATION SYSTEM FOR RAMEA'S HYBRID POWER SYSTEM

The communication system design is based primarily on transmission continuity and reliability, that is why the DAS-MPCB network will have two different types of technologies, the PLC system will be setup as primary and wireless link as backup. Low budget Netgear XE102 PLC modems can accomplish a safe communication with a modified coupling stage that will allow a safe link to the existing high voltage carrier (4.16kVAC). This modems use TCP/IP protocol and has LAN compatibility matching the necessary requirements for a remote access and network management from Newfoundland Hydro's control centre in St. John's, NL.

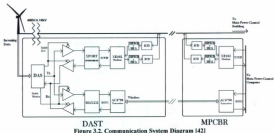
For the wireless link, LaridTech AC4790 transceivers are suitable for Ramea's atypical weather. Its datasheet stipulates a functional frequency variance between 902-928 MHz, a serial interface, enhanced interference rejection, an enabled co-located system operation with increased output power and data integrity [40]. Preliminary field testing demonstrated that successful transmission can be achieved at a maximum distance of 2.01km under optimal (no rain, hail or snow) weather conditions and no line of sight.

3.1. TRANSMISSION ALGORITHM

Figure 3.1 shows the transmission algorithm that the Data Acquisition System Transmitter (DAST) follows. The DAST emulates receiving data from wind turbine parameters mentioned in Table 2.1 and then they are sent primarily through the PLC; the

3.2. COMMUNICATION SYSTEM SETUP

Figure 3.2 illustrates the complete communication system with the two communication prototypes.



The microcontroller (PIC16F873A) or DAS serial interface (refer to Appendix E for full DAST schematic) is connected to a gate controlled TTL buffer (SN74ABT125) setup that allows the DAS to administrate the desired transmission link (see Figure 3.3). While the AC4790 needs RS232 protocol (MAX232ACPE), the PLC modem (Netgear XE102) needs TCP/IP, so a Serial-to-Ethernet adaptor (XPORT XP1001000-03) is used to connect the buffer setup to the XE102, this enhances the DAS-MPCB link with independent protocols for the two communication carriers. The AC4790 receives the data through RS232, adjust the signal with a FHSS FSK modulation, and sends it to the MPCBR. On the other hand, the Xport adaptor receives the data using the RS232 serial

interface (CMOS Asynchronous, 5V Tolerant), and sends to the XE102 modem using TCP/IP protocol. Please refer to Appendix E for DAST's schematic diagram, each stage is explained in subsequent sections.

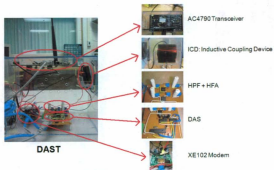


Figure 3.3. Data Acquisition System Transmitter Prototype Setup [42]

3.2.1. DAST's Microcontroller Pin Configuration

Table 3.1 describes the purpose and application for each of the PIC16F873A pins considering the following classification: NC: Not Connected; I: Input; O: Output; TTL: Transistor-Transistor Logic Input/Output; ST: Schmitt Trigger Input/Output; P: Power.

Table 3.1. DAST's Microcontroller PIC16F873A Pin Configuration

Name	Pin #	Type (I/O/P)	Buffer Type	Description
MCLR/Vpp	1			RESET
RA0/AN0	2	-	TTL	NC
RA1/AN1	3	-	TTL	NC
RA2/AN2/Vref-/CVref	4	-	TTL	NC
RA3/AN3/Vref+	5	-	TTL	NC
RA4/T0CKI/C1OUT	6	-	ST	NC
RA5/AN4/SS/C2OUT	7	-	TTL	NC
Vss	8	P	-	GND
OSC1/CLKI	9	I		Crystal oscillator
OSC2/CLKO	10	O		Crystal oscillator
RC0/T1OSO/T1CKI	11	-	ST	NC
RC1/T1OSI/CCP2	12	-	ST	NC
RC2/CCP1	13	-	ST	NC
RC3/SCK/SCL	14	-	ST	NC
RC4/SDI/SDA	15	-	ST	NC
RC5/SDO	16	-	ST	NC
RC6/TX/CK	17	O	ST	Serial Tx
RC7/RX/DT	18	I	ST	Serial Rx
Vss	19	P	-	GND
VDD	20	P	-	5V
RB0/INT	21	-	TTL/ST	NC
RB1	22	O	TTL	PCL High frequency buffer control
RB2	23	O	TTL	Wireless High frequency buffer control
RB3/PGM	24	O	TTL	LED control – Green
RB4	25	O	TTL	LED control – Red
RB5	26	-	TTL	NC
RB6/PGC	27	-	TTL/ST	NC
RB7/PGD	28	-	TTL/ST	NC

3.2.2. Serial-to-Ethernet Adaptor (XPORT XP1001000-03)

Lantronix, Inc. "XPort Embedded Device Server" is used to link DAST's PIC16F873A to the XE102, its function is to adjust microcontroller's TTL data to TCP/IP protocol and transmit them to the PCL modem. Even though this device is relatively small (33.9mm long, 16.25mm wide, 13.5mm tall), it comprises a 4Mb flash memory, a 25MHz crystal

oscillator, circuit reset feature, 5V serial interface, embedded UART (compatible with 300-921600bps transmissions), Ethernet technology up to 100Mbps, and an external RJ-45 jack connected to a UTP cable (See Appendix D for detail technical data) [43].

Once the XPORT is connected to a Local Area Network (LAN), a fixed IP address is assigned to it using the "DeviceInstaller" software, and finally Telnet or a Hypertextual application is used for the pos-configuration process (UART setup for example).

The XPORT package comes with an extra tool called "Redirector" which can be used to create virtual ports for easier data access while programming the User Graphic Interface mention in the subsequent section 3.3.1.

3.2.3. Inductive Coupling Stage

According to the analyzed power distribution system at Ramea, the WM15S Wind Turbines generate 480V which is then converted to 4160V with a step-up transformer. A coupling stage is needed to allow a successful connection between the PLC modems and the 4.16kV power line. Note in Figure 3.2 that the coupling is performed after the 480:4.16kV step-up transformer in order to avoid transmission instability. V. Krishnan "Transformer Bypass Circuit" study on Power Line Communication applications, capacitive and inductive coupling methods for PLC modules and power line cables, are the baseline for The DAST and MPCBR setup with an active filter (High Pass Filter (HPF), plus High Frequency Amplifier (HFA)) and an Inductive Coupling Device (ICD)

to ensure low frequency signal discrimination and proper signal propagation [44]. Refer to section 3.2.3.1, 2 & 3 for full HPF, HFA and LCD analysis. After the MPCBR recognizes the data the acknowledgement signal is sent back through the power line closing the bilateral communication cycle.

3.2.3.1. High Pass Filter (HPF)

One of the designs for active high pass filters are based on passive HPF followed by an HFA, first order Resistance & Capacitance ($R&C$ or RC) filters (Figure 3.4) are designed to attenuate low frequency signals including the induced AC from the 4.16kVAC plus noise signals remaining only high frequency signals from the XE102 modem.



Figure 3.4. High Pass Filter

Measures and analysis from several samples of XE102 output demonstrated that its lowest frequencies are above 5MHz, as an example Figure 3.5 & 3.6 shows an instance of the sampled signal.

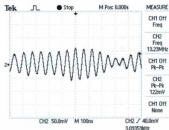


Figure 3.5. 1st Sample of Data Signal

Following high pass filter mathematical formulas found on A. S. Sedra & K. C. Smith "Microelectronic Circuits", the R & C values are based on a passive first order HPF with a -3db gain, which guarantees that low frequency signals are properly discriminated [45]. Cutoff frequency (f_c) of 1MHz is enough to acquire acceptable results:

$$\text{Assuming } \omega = \omega_0 (\omega : \text{angular frequency}; \omega_0 : \text{cutoff frequency}) \quad (1)$$

$$\text{Where } \omega = 2 * \pi * f (f : \text{frequency}) \quad (2)$$

$$\text{For a first order circuit } \omega_0 = \frac{1}{RC} \Rightarrow 2 * \pi * f = \frac{1}{RC} \quad (3)$$

$$f = \frac{1}{(2 * \pi * R * C)} \quad (4)$$

Substituting $C = 0.47 \mu\text{F}$ and $R = 3\Omega$

$$f = \frac{1}{(2 * \pi * 3\Omega * 0.047 \mu\text{F})} \approx 1\text{MHz} \quad (5)$$

3.2.3.2. High Frequency Amplifier (HFA)

After the high frequency signal passes the HPF a percentage is attenuated as seen in Figure 3.6. With the intention of matching the input signal shape while increasing the output, the High Frequency Amplifier seen in Figure 3.7 will correct the attenuation in order to have proper signal propagation by the ICD.

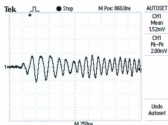


Figure 3.6. 2nd Sample of Data Signal

The HFA design is based on the LM6171, a high speed low power low distortion voltage feedback amplifier necessary for circuit requirements (datasheet on Appendix D); operates with 100MHz bandwidth, a supply voltage range of $\pm 36V$ and $\pm 5V$, and scope gain of 20-200.

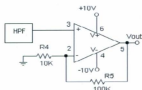


Figure 3.7. High Frequency Amplifier

3.2.3.3. Inductive Coupling Device (ICD)

In the late 1820s, Michael Faraday discovered that voltage is induced through a conductor moving through a magnetic field, or a magnetic field moving around a conductor. His law states that Voltage (V induced) is equal to the wire's number (N) of turns times magnetic flux over current (I) or:

$$V = N \frac{\Phi}{I} \quad (6)$$

The School of Physics in Sydney, Australia, states in their "Transformers" multimedia archive that Faraday's principle is followed if two coils are inductively coupled, converting ac power at a certain voltage level to ac power at a different level but same frequency; if there is a current change in one coil an ElectroMagnetic Field (EMF) is induced in other [46]. A high voltage pulse transformer was preliminary considered for the ICD to allow an interface between the low voltage devices and the 4.16kV power line, but lab tests showed that implementing the same transformer's concept to a less

expensive iron core with a AWG 32 wire can work as the ICD induce the necessary signal for the coupling system to send/receive data through the power line. As shown in Figure 3.8, the high voltage cable passes through an iron core with an AWG 32 cable with 200 turns. From transformer's design we get the induction ratio (r):

$$r = \frac{V_s}{V_p} = \frac{N_s}{N_p} = \frac{200}{1} = 200 \quad (7)$$

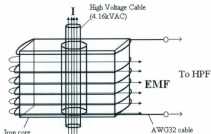


Figure 3.8. Inductive Coupling Device Diagram

The reason for the “high voltage cable pass through” design instead of spiraling it around the core is to model a non invasive ICD that will avoid disconnecting the power cable from its original installation, same principle as an inductive clamp.

As a counter measure to prevent unwanted signals passing to and from the inductive coupling stage, an inverted HPF was connected to the PLC modem input and ICD input as seen in Figure 3.9, therefore guarantying uncontaminated communication between the devices. Please refer to Appendix E for full DAST schematic.

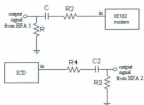


Figure 3.9. Inverted HPF

3.3. COMMUNICATION SYSTEM PROTOTYPES

Figure 3.10 shows the prototypes of above communication system; the DAST (left) has the wireless LaridTech AC4790 transceiver on top, PLC Netgear XE102 modem on the bottom left corner, and the ICD on the top right; the MPCBR has the wireless transceiver on top, PLC modem on the bottom right corner, the ICD on the top right, and a small cooling fan for heat removal purposes.

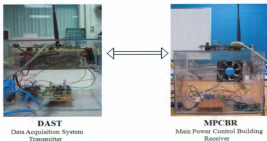


Figure 3.10. Communication System Prototypes

3.3.1. Graphic User Interface (GUI)

A Visual Basic GUI is designed to be operated by the user for data control and communication path supervision between the DAST and MPBCR. As seen from Figure 3.11 the user is capable to manually start/stop all transmissions or enable/disable each communication link individually, but there is an automatic background process which constantly scans for new incoming data, evaluates which comm. system was used, displays incoming data in real time, and transmits the acknowledgment signal through the same comm. link.

Since the DAST PLC modem is directly connected to the XPORT Serial-to-Ethernet adaptor, a TCP/IP virtual port is necessary for Power Line Communications while the computer serial port is used for wireless transmissions. Appendix C contains the Visual Basic source code.

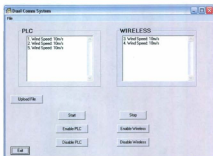


Figure 3.11. Graphic User Interface

For lab experimentation it is necessary to setup the DAST and MPCBR to an emulated 4.16kVAC power line so both ICD systems have to be coupled to a high voltage cable connected to four 120V-2kVAC transformers in series, two for each side. The GUI must be carefully supervised to display which communication medium was used for data transmission/reception and broadcast the acknowledgment signal through the same medium.

Going through above engineering design we have the PIC16F873A following its own algorithm which not only emulates receiving wind turbines parameters but will also controls the high frequency buffer configuration; the buffers are connected to the XPORT module and the MAX232, this last communicates with the AC4790 transceiver; the XPORT transmits the data to the XE102 modem which sends the data through an HPF,

HFA, an inverted HPF, and finally through the ICD which induces the signal into the 4.16kVAC cable. To close the communication loop the GUI will use the MPCBR to acknowledge transmission as soon as it receives and displays wind turbine parameter data. Now the designed Communication System for the Remote Hybrid Power System in Ramea, NL is ready for experimental testing. Next chapter provides some experimental results.

CHAPTER 4. EXPERIMENTAL RESULTS

The microcontroller's algorithm, transmission synchronization, induced data reconstruction, acknowledgment of new acquired data and sub-stages were tested in sequence in order to isolate and resolve possible difficulties with the DAST, MPCBR, and GUI. Challenging comadrums like transmission synchronization with the high frequency buffers command controls as well as signal coupling, filtering and amplification were deeply examined in order to achieve optimal results.

Experimental testing results confirmed a successful DAS – MPCB communication as expected. Studies of these outcomes in addition to prototypes' cost analysis are documented as such:

- After testing numerous versions of the microcontroller's algorithm to solve synchronization difficulties with PLC-Wireless transmissions, it was necessary to first configure the microcontroller's USART and delay the primary transmission for 8s to let the XPORT module initialize, as well as creating a sub-routine that decontaminates the Rx USART buffer before transmitting through wireless as seen in Figure 4.1. Full source code can be found in Appendix B.

```

...
USART_init(57600);           // initialize USART module
                             // (8 bit, 57600 baud rate, no parity bit...)
PORTB = 0;                  // Initialize PORT
TRISB = 0;                  // Configure PORTB as output
v = 1;                      // validate send / receive data
Delay_ms(8000);             // Delay of 8s to let XPORT initialize
...

//-----Start Empty trash can
if (USART_Data_Ready())     // if trash data is received
{
    trash_ = USART_Read();  // read the received trash data
}
//-----Finish Empty trash can

```

Figure 4.1. Microcontroller's Algorithm XPORT initialization + Buffer Decontamination

Laboratory tests determined that with above sub-routines the DAST can successfully communicate with the MPCBR and record data on a terminal computer via Ethernet without the loss of characters. Wireless and PLC signals had no instability and satisfactory transmission synchronization.

- As shown in Figure 4.2, the high pass filter, high frequency amplifier, and the 4.16kVAC inductive coupling overall performance is acceptable for an ideal PLC communication. The Inductive Coupling Device transfers the high (Data) and low (60Hz power AC voltage at lower scale) frequency signals to the active high pass filter (HPF+HFA), 60Hz sine wave is discriminated and only the data signal is amplified, then processed by the PLC modem, converted to TCP/IP and last the parameter is displayed on the GUI.



Figure 4.2. ICD & HPF+HFA Signal

Transmission rate analysis under laboratory conditions shows that it can reach up to 1Mb/20s which meets the necessary scan rate requirement predetermined by wind turbine parameters on Table 2.1.

4.1. COST – BENEFIT ASSESSMENT

Taking into consideration what is mentioned in Chapter 1.2, paragraph 4 about not using low cost transceivers with a 2.4GHz transmission which is vulnerable to atmospheric attenuation, plus Newfoundland Hydro's fiber optic initial expense of CAN\$19,380.00 mentioned in Chapter 2.1; comparing it to what is shown in Table 4.1, a total hardware cost of CAN\$443.60 can initially satisfy the low budget cost-effective goal of the project.

Table 4.1. Hardware Cost

Unit	Price (\$CAN)
AC4790	\$62.5(x2)
XE102	\$99.00(x2)
PIC16F873A	\$4.00

Unit	Price (\$CAN)
MAX232	\$0.50
SN74ABT125	\$0.90
LM6171	\$2.80(x4)
ICD	<\$2.00(x2)
Miscellaneous	\$100.00
TOTAL	\$443.60

Considering that first prototype expense costs are always higher than the next ones, these modules can become even more economically attractive by reducing manufacturing expenditures if the DAST & MPCBR are to be conceived as mass production products for different kinds of hybrid power systems, a very convenient aspect for power companies.

4.1.1. Benefits

There are fundamental benefits which determine the feasibility, advantage, and purpose of this project such as:

- Establishing a new and efficient approach to supervise wind turbine performance without compromising existing hybrid power system infrastructure.
- Reducing expenses by adding a second purpose to existing power cabling currently installed.

- Minimizing communication failures attributable to hazardous weather conditions by establishing a redundant PLC-Wireless transmission.
- Limiting onsite travel to a minimum.
- A new incentive for engineers to innovate new practical products for current & future generation of hybrid power systems.
- Possibility for a new market in the hybrid power communication system industry.

Taking into account the benefits that this communication system provides, it creates a new innovative approach to today's hybrid power systems market.

CHAPTER 5: CONCLUSIONS AND RECOMMENDATIONS

The design of a Communication System for the Remote Hybrid Power System in Ramea, NL was not only challenging but insightful, studying the different types of hybrid power systems and their communication technologies provided us with a preliminary design that later on was engineered into an unconventional approach to communicate the different power systems. Hybrid communication for hybrid power systems combines the advantages of two different technologies working as one. Insights on these advantages are described below:

- The usefulness of implementing a half duplex transmission agreement with PLC and RF technologies combined is to assure the redundancy necessary for a constant and stable communication. A trustworthy remote transmission opens the possibility for automated systems to become more independent. Currently at Ramea the remote control is limited to a collective Enable/Disable of all wind turbines but future enhancements in wind turbine control's robustness will become possible with constant remote communication regardless of present weather conditions.
- Advantages like minimizing constant weather limitations will provide technicians with a reliable communication system for potential upgrades not only in remote supervision and control but faster technical response time on extraordinary circumstances like wind turbines malfunction, power cabling detachment, and data error transmissions.

- Implementing PLC modems and low RF transceivers to our system is not only an economically feasible approach to hardware communication expenses but can also reduce budget spending without allocating dedicated mediums to remote communication systems. Preserving Ramea's current power infrastructure will minimize system's downtime installation processes.
- Wireless enhancements to remote transmissions in addition to include extra tasks to existing power cabling with PLC will limit onsite travel to a minimum, therefore reducing fuel consumption, ground transportation maintenance, and traffic misfortunes.
- The Data Acquisition System Transmitter (DAST) was designed with the purpose of emulating the compilation of wind turbine parameter readings and resourcefully but yet efficiently transmit the data with low budget expenditure.
- Using a Serial-to-Ethernet XPORT adaptor allowed the microcontroller's TTL signal adaptation to TCP/IP corresponding to XE102 PLC modem's Ethernet protocol compatibility.
- A high frequency buffer arrangement was implemented for the DAST as a matter to synchronize two communication technologies attached to a single data acquisition system. The master control for the buffer arrangement was successfully programmed

in the microcontroller which its inverse TTL outputs of pins 22 & 23 dictates which transmission is suppressed while enabling the other at the same time.

- The synchronization algorithm implemented to DAST's master transmission control was not only designed to be fully automatic but simple enough to be a recursive function with the limited amount of memory available in the microcontroller.
- Calibrating high pass filters and amplifiers for the inductive coupling stage was an overwhelming assignment with remarkable results that allowed the iron core induction device to send and/or receive suitable quality data. The retrieved signal was reconstructed with enough rigor to be duplicated in the Main Power Control Building Receiver (MPCBR) employing an equivalent circuitry.
- XE102 PLC modems were essential not only for data transmission through power lines but adding a special feature to the MPCBR, remote supervision anywhere in the Local Area Network. With proper routing network configuration the MPCBR data could be retrieved any where throughout the Worldwide Web.
- The Graphic User Interface (GUI) was designed to remotely recognize which communication method is currently been used for transmission, monitor and display the wind turbines parameters in real time as well as having user friendly features for communication control.

- Matters like weather insulation, overheating protection, and power overloads must be taken into consideration for future upgrades to the prototypes with the purpose of avoiding environmental, structural and personal hazards, otherwise the system can become a mayor safety risk to the infrastructure.

5.1. FUTURE WORK

Various recommendations are reported in this thesis for future improvement of the "Communication System For The Remote Hybrid Power System In Ramca Newfoundland" in order to adjust the prototypes to multiple hybrid power system infrastructure configurations:

- A battery backup system and power management algorithms must be designed to take advantage of a semi-independent feature like having a constant communication in case the power system is switched off for maintenance or cabling detachment from the main power network. For future references, on Table 4.2 below you will find the theoretical load consumption of each DAST device in order to maintain a wireless connection with the MPCBR:

Table 4.2. Load Consumption

Component	
AC4790	68mA
PIC16F873A	250mA
MAX232	8mA
SN74ABT125	64mA
Total Power Consumption:	2.12W

- Implementing a transformer bypass will eliminate the PLC constraint and transmit signal even if the DAST is connected before a main power transformer. An optical approach might be the solution to overcome this limitation, a low budget laser point at one side of the transformer can be modified to be used as a transmitter while a light-receiving device or diode is attached to the other side of the transformer, and with filters, amplifiers and ICDs, the signal can be re-adapted for PLC transmission. The light transmitter and receiver must be encapsulated on a dark/black cylindrical non metal tube to avoid losing data packages or transmission errors.
- Future studies on how to interface the prototypes with hybrid power system's centralized supervisory controller to analyze compatibility challenges.
- Implementation of a compatible encryption algorithm for the DAST and GUI to avoid a potential system cracking or data theft.
- Include a Log file for the GUI which automatically records date, time, source, communication path, and type of incoming data.
- Improve GUI to display all information from the Log file.
- Secure Routing configuration for data recording through the Internet.
- Modification to the prototypes' encapsulation boxes for easier transportation, smaller dimensions, and easier user friendly installation features.

BIBLIOGRAPHY AND REFERENCES

- [1] T. Ackerman, "*Wind Power in Power Systems*". Chichester, West Sussex UK: John Wiley & Sons Ltd, 2005, pp. 299 – 316. [Online]. Available: <http://books.google.ca/books?id=f7MDGCiOgiMC&printsec=frontcover#v=onepage&q&f=false>
- [2] Meridian Energy (2010, Jan 11). "*The Ross Island Wind Energy – Stage 1 Project*". [Online]. Available: <http://www.meridianenergy.co.nz/OurProjects/The+Ross+Island+Wind+Energy+%E2%80%93+Stage+1+Project.htm>
- [3] S. Bennett, "Ross Island Wind Energy – Stage 1 Project, Building the World's Southern Most Wind Farm", project update presented at the New Zealand Wind Energy Conference, Mar 2010. [Online]. Available: <http://windenergy.org.nz/documents/conference10/sbennett.pdf>
- [4] Renewable Energy Alaska Project (2010, Nov 15). "Hybrid Power Systems and Integration". [Online]. Available: <http://alaskarenewableenergy.org/wp-content/uploads/2010/09/Hybrid-power-systems-and-integration-111010.pdf>

- [5] Renewable Energy Alaska Project (2010, Nov 15). "2010 Alaska Wind Project Updates". [Online]. Available:
<http://alaskarenewableenergy.org/wp-content/uploads/2010/09/Annual-Wind-Working-Group-Narratives.pdf>
- [6] National Renewable Energy Laboratory (2010, Feb 06). "US Virgin Island Energy Workshop". [Online]. Available:
http://www.edinenergy.org/pdfs/ee_workshop2010_gould_elliott.pdf
- [7] J. Zimmerman and C. Loone, "Session Three: Renewable Energies in the Remote Areas and the Top End", presented at the Regional Forum: Electrical Engineering in the Top End 2009 – IDC Technologies. [Online]. Available:
http://www.idc-online.com/pdf/Papers/Juergen_Zimmerman.pdf
- [8] D. Clarke (2011, Jan 20). "Wind farms in Western Australia". [Online]. Available:
http://ramblingsdc.net/Australia/WindWA.html#Denham_Wind_Farm
- [9] P. Lundsager et al. (2010, Mar 13) "Isolated Systems with Wind Power Main Report". [Online]. Available:
<http://130.226.56.153/rispubl/VEA/veapdf/ris-r-1256.pdf>

- [10] J. Macgillivray, "Northern Wind Project Evolution- Tuktoyaktuk," in CanWEA 26th Annual Conference and Exhibition, 2010 © Canadian Wind Energy Association.
- [11] Cleveland Live (2009, Sep 05). "In Canada's tiny Tuktoyaktuk, they confront climate change up close as permafrost thaws". [Online]. Available:
http://www.cleveland.com/world/index.ssf/2009/09/in_canadas_tiny_tuktoyaktuk_1.html
- [12] CBC News (2010, Apr 10). "Tuktoyaktuk harnesses northern wind farm idea". News Report [Online]. Available:
<http://www.cbc.ca/canada/north/story/2007/04/10/nwt-wind.html>
- [13] CBC News (2010, Apr 10). "Tuktoyaktuk to get 4 wind turbines by 2011". News Report [Online]. Available:
<http://www.cbc.ca/canada/north/story/2009/06/02/tuk-wind-turbines.html>
- [14] T. M. Weis and A. Ilianca, "The Utility of Energy Storage to Improve the Economics of Wind-Diesel Power Plants in Canada", *ScienceDirect*, Renewable Energy 33, pp. 1544 – 1557, Oct. 2007.

- [15] PEI Energy Corporation (2010, Nov 21). "PEI Wind-Hydrogen Village". [Online]. Available: <http://www.windh2.ca/projectdesc.php>
- [16] B. Saulnier and R. Gagnon, "High Penetration No-Storage Wind Diesel study by Hydro Quebec in Quaqtaq, QC", in Wind Diesel Workshop, 2002 © Hydro-Quebec Research Institute. [Online]. Available: <http://www.docstoc.com/docs/16388181/Wind-Diesel-Hybrid-System>
- [17] Canadian Wind Energy Association (CANWEA) (2010, Jan 17). "Canada's current wind installed capacity table". [Online]. Available: http://www.canwea.ca/farms/index_e.php
- [18] Canadian Wind Energy Association (CANWEA) (2010, Jan 17). "Canada's planned or under construction wind energy projects". [Online]. Available: <http://www.canwea.ca/pdf/Proposed%20projects.pdf>
- [19] Newfoundland Hydro (2009, Feb 25). "Ramea Wind-Hydrogen Diesel Project". [Online]. Available: <http://www.env.gov.nl.ca/env/ENV/EA%202001/Project%20info/1357.htm>

- [20] Nalcor Energy (2010, Jul 03), "Ramea Report". [Online]. Available: <http://www.nalcorenergy.com/publications.asp>
(Winter 2010 report of Ramea's Wind-Hydrogen-Diesel project done by Nalcor Energy (<http://www.nalcorenergy.com/>))
- [21] Cirronet, Inc. (2009, Nov 09). "HN-210D User's Guide" [Online]. Available: <http://www.cirronet.com/07cdcatalog/cirronet/hn210 Ug.pdf>
"Cirronet HN-210" Datasheet.
- [22] A. Pereira "Modular supervisory controller for hybrid power systems", Ph.D. dissertation, Dept. of Automation, Lyngby, Technical University of Denmark (DTU), Risø National Laboratory, Roskilde, 2000.
(Also available at <http://130.226.56.153/rispubl/VEA/veapdf/ris-r-1202.pdf>)
- [23] R. Sebastian, M. Castro, E. Sancristobal, F. Yeves, J. Peire, J. Quesada, "Approaching hybrid wind-diesel systems and Controller Area Network", *IECON 02 Industrial Electronics Society, IEEE 2002 28th Annual Conference*, pp. 2300-2305, Nov. 2002.
- [24] H. Kirkham, A. R. Johnston, G. D. Allen, "Design Considerations For A Fiber Optic Communications Network For Power Systems", *IEEE Transactions on Power Delivery*, Vol. 9, No. 1, pp. 510-518, Jan. 1994.

- [25] Mary Bellis, About.com, Inventors (2010, Jan 22) "The birth of fiber optics". [Online]. Available: <http://inventors.about.com/library/weekly/aa980407.htm>
- [26] Home Theater Accessories Resource (2010, Jan 22) "How Optical Cable Works". [Online]. Available: <http://www.home-theater-accessories-resource.com/connectingcomponents/optical-cable.html>
- [27] A. Akbulut, H. Gokhan Ilk, F. Ari, "Design, Availability and Reliability Analysis on an Experimental Outdoor FSO/RF Communication System", *Transparent Optical Networks, 2005, Proceedings of 2005 7th International Conference*, Vol.1, pp. 403-406, Jul. 2005.
- [28] Renesas Electronics Cooperation (2010, Apr 04). "Introduction to CAN". [Online]. Available: http://documentation.renesas.com/eng/products/mgumcu/ugm/rej05b0804_m16cap.pdf
- [29] Intel Corporation (2010, Jan 25) "Helping Define 802.11n and other Wireless LAN Standards". [Online]. Available: http://www.intel.com/standards/case/case_802_11.htm

- [30] Inter Corporation (2010, Jan 25) "How WIMAX works". [Online]. Available:

http://www.intel.com/technology/wimax/demo/works/demo.htm?iid=tech_wimax+demo

- [31] Dr. J. Takei, Intel Corporation (2009, Jan 25). "Digital Wireless Communication Basics: Overview of basic concepts". [Online]. Available:

<http://www.soi.wide.ad.jp/class/20070044/slides/01/>

- [32] D. D. Bois, Energy Business (2009, Jan 25). "Broadband over Powerlines (BPL) in a Nutshell". [Online]. Available:

http://energypriorities.com/entries/2004/12/broadband_over_1.php

- [33] Home Automation Directory (2009, Jan 25). "Home Automation". [Online]. Available:

<http://home-automation.org/>

- [34] NETGEAR (2009, Jan 25). "NETGEAR Powerline and Coax products". [Online]. Available:

<http://www.netgear.com/home/products/powerline-and-coax/>

- [35] X10 (2009, Jan 25). "Transmission theory over X-10 signals". [Online]. Available:

<http://www.eurox10.com/Content/X10SignalTheory.htm>

- [36] Echelon Corporation (2009, Jan 25). "LonWorks Technology Overview". [Online]. Available:
<http://www.echelon.com/communities/energycontrol/developers/lonworks/>
- [37] Smart Labs Inc. (2009, Jan 25). "INSTEON Technology". [Online]. Available:
<http://www.insteon.net/about-home.html>
- [38] L. Brackmann, ATICON Home Automation GmbH, "Power line applications with European Home Systems (EHS)", presented at the International Symposium on Powerline Communication and its Applications, Essen, Germany, 1997.
- [39] KNX (2009, May 22). "KNX PL 110 Communication Media". [Online]. Available:
<http://www.knx.org/knx-standard/communication-media/>
- [40] AeroComm, Inc. (2009, Sep 17). "AC4790 Transceiver datasheet" [Online]. Available: http://www.aerocomm.com/docs/Datasheet_AC4790_H1.pdf
- [41] J. F. Acevedo, M. T. Iqbal, "Communication System for the Remote Hybrid Power System in Ramea Newfoundland", Electrical and Computer Engineering (CCECE), 2010 23rd Canadian Conference, pp. 1-4, May 2010.

- [42] J. F. Acevedo, M. T. Iqbal "Dual Communication System for Ramea's Remote Power System", in CanWEA 26th Annual Conference and Exhibition, 2010 © Canadian Wind Energy Association.
- [43] Lantronix, Inc. (2009, Mar 15). "XPort Embedded Device Server" [Online]. Available: http://www.lantronix.com/pdf/XPort_PB.pdf
- [44] V. Krishnan, "Transformer Bypass Circuit", *Power Line Communications and Its Applications, 2005 International Symposium*, pp. 275-277, Apr. 2005.
- [45] A. S. Sedra and K. C. Smith, "Microelectronic Circuits", fifth edition, New York, Oxford: Oxford University Press, 2004, pp. 64-122, 1084-1101.
- [46] School of Physics, Sydney, Australia (2010, Jan 12). "Transformers". [Online]. Available: <http://www.animations.physics.unsw.edu.au/jw/transformers.html>
- [47] U. Abdulwahid et al., "Development of a dynamic control communication system for hybrid power systems", *Renewable Power Generation, IET*, Vol. 1 No. 1, pp. 70-80, Apr. 2007.

- [48] V. Chunduru and N. Subramanian, "*Effects of Power Lines on Performance of Home Control System*", Power Electronics, Drives and Energy Systems, 2006. PEDES '06. International Conference, pp. 1-6, December 2006.
- [49] O. Bilal et al., "Design of Broadband Coupling Circuits for Power line Communication", presented at the 7th ISPLC Proceedings, 2004.

**APPENDIX A. RAMEA WIND-HYDROGEN-DIESEL PROJECT,
REALISTIC POINT COUNT FOR EMS GROUP – ST. JOHN'S**

14-015 PLC				
14-016 PLC				
14-017 PLC				
14-018 PLC				
14-019 PLC				
14-020 PLC				
14-021 PLC				
14-022 PLC				
14-023 PLC				
14-024 PLC				
14-025 PLC				
14-026 PLC				
14-027 PLC				
14-028 PLC				
14-029 PLC				
14-030 PLC				
14-031 PLC				
14-032 PLC				
14-033 PLC				
14-034 PLC				
14-035 PLC				
14-036 PLC				
14-037 PLC				
14-038 PLC				
14-039 PLC				
14-040 PLC				
14-041 PLC				
14-042 PLC				
14-043 PLC				
14-044 PLC				
14-045 PLC				
14-046 PLC				
14-047 PLC				
14-048 PLC				
14-049 PLC				
14-050 PLC				
14-051 PLC				
14-052 PLC				
14-053 PLC				
14-054 PLC				
14-055 PLC				
14-056 PLC				
14-057 PLC				
14-058 PLC				
14-059 PLC				
14-060 PLC				
14-061 PLC				
14-062 PLC				
14-063 PLC				
14-064 PLC				
14-065 PLC				
14-066 PLC				
14-067 PLC				
14-068 PLC				
14-069 PLC				
14-070 PLC				
14-071 PLC				
14-072 PLC				
14-073 PLC				
14-074 PLC				
14-075 PLC				
14-076 PLC				
14-077 PLC				
14-078 PLC				
14-079 PLC				
14-080 PLC				
14-081 PLC				
14-082 PLC				
14-083 PLC				
14-084 PLC				
14-085 PLC				
14-086 PLC				
14-087 PLC				
14-088 PLC				
14-089 PLC				
14-090 PLC				
14-091 PLC				
14-092 PLC				
14-093 PLC				
14-094 PLC				
14-095 PLC				
14-096 PLC				
14-097 PLC				
14-098 PLC				
14-099 PLC				
14-100 PLC				
14-101 PLC				
14-102 PLC				
14-103 PLC				
14-104 PLC				
14-105 PLC				
14-106 PLC				
14-107 PLC				
14-108 PLC				
14-109 PLC				
14-110 PLC				
14-111 PLC				
14-112 PLC				
14-113 PLC				
14-114 PLC				
14-115 PLC				
14-116 PLC				
14-117 PLC				
14-118 PLC				
14-119 PLC				
14-120 PLC				
14-121 PLC				
14-122 PLC				
14-123 PLC				
14-124 PLC				
14-125 PLC				
14-126 PLC				
14-127 PLC				
14-128 PLC				
14-129 PLC				
14-130 PLC				
14-131 PLC				
14-132 PLC				
14-133 PLC				
14-134 PLC				
14-135 PLC				
14-136 PLC				
14-137 PLC				
14-138 PLC				
14-139 PLC				
14-140 PLC				
14-141 PLC				
14-142 PLC				
14-143 PLC				
14-144 PLC				
14-145 PLC				
14-146 PLC				
14-147 PLC				
14-148 PLC				
14-149 PLC				
14-150 PLC				
14-151 PLC				
14-152 PLC				
14-153 PLC				
14-154 PLC				
14-155 PLC				
14-156 PLC				
14-157 PLC				
14-158 PLC				
14-159 PLC				
14-160 PLC				
14-161 PLC				
14-162 PLC				
14-163 PLC				
14-164 PLC				
14-165 PLC				
14-166 PLC				
14-167 PLC				
14-168 PLC				
14-169 PLC				
14-170 PLC				
14-171 PLC				
14-172 PLC				
14-173 PLC				
14-174 PLC				
14-175 PLC				
14-176 PLC				
14-177 PLC				
14-178 PLC				
14-179 PLC				
14-180 PLC				
14-181 PLC				
14-182 PLC				
14-183 PLC				
14-184 PLC				
14-185 PLC				
14-186 PLC				
14-187 PLC				
14-188 PLC				
14-189 PLC				
14-190 PLC				
14-191 PLC				
14-192 PLC				
14-193 PLC				
14-194 PLC				
14-195 PLC				
14-196 PLC				
14-197 PLC				
14-198 PLC				
14-199 PLC				
14-200 PLC				

APPENDIX B. MICROCONTROLLER (DAS) SOURCE CODE

```

char i;
char trash_;
int v = 0;

void main()
{
    USART_init(57600);           // initialize USART module
                                // (8 bit, 57600 baud rate, no parity bit...)
    PORTB = 0;                  // Initialize PORTB
    TRISB = 1;                  // Configure PORTB as output
    v = 1;                      // validate send / receive data
    Delay (8000);               //Delay of 8s to let XPORT initialize
    while (1)
    {
        if (v == 1)            //Trying Tx through XPORT
        {
            PORTB = 12;        //Enable XPORT / green light / Disable Wireless
            USART_Write("Wind speed: 10m/s"); //send data via USART
            Delay_ms (1);       //delay of 1ms
            if (USART_Data_Ready()) // if data is received
            {
                i = USART_Read(); // read the received data
                if (i == 'X')      //acknowledgment Xport
                {
                    v = 1;
                }
                else
                {
                    v = 2;
                }
            }
            else
            {
                v = 2;
            }
        }
        if (v == 2)            //Trying Tx through wireless
        {
            PORTB = 18;        //Enable Wireless / red light / Disable XPORT
            //-----Start Empty trash can
            if (USART_Data_Ready()) // if trash data is received

```



```

{
    trash_ = USART_Read();           // read the received trash data
}
//-----Finish Empty trash can
USART_Write("Wind speed: 10m/s"); //send data via USART
Delay_ms(1);                       //delay of 1ms
if(USART_Data_Ready())              // if data is received
{
    i = USART_Read();               // read the received data
    if (i == 'w')                   //acknowledgment Wireless
    {
        v = 1;
    }
    else
    {
        v = 3;
    }
}
else
{
    v = 3;
}
}
if (v == 3)                          //Tx Failure
{
    PORTB = 6;                      //Disable Wireless / Disable XPORT / No light
    v = 1;
}
Delay(6000);                         //delay of 6s
}
}

```

APPENDIX C. GRAPHIC USER INTERFACE SOURCE CODE

```

Option Explicit
Dim xport_rx As String
Dim wireless_rx As String
Dim m As String
Dim n As String
Dim temp As Integer
Dim numfile As Integer
Dim numfile2 As Integer
Dim LineaDeTexto As String
Dim TodoElTexto As String
Dim moda As String

Private Sub StopCommand_Click()
    Text1.Text = ""
    Text2.Text = ""
    If MSComm1.PortOpen = True Then
        MSComm1.PortOpen = False
    End If
    If MSComm3.PortOpen = True Then
        MSComm3.PortOpen = False
    End If
End Sub

Private Sub StartCommand_Click()
    m = "e"
    Text1.Text = ""
    Text2.Text = ""
    m = "ex"
    n = "cw"
    MSComm1.PortOpen = True
    MSComm3.PortOpen = True
    Do
        DoEvents
        If MSComm3.InBufferCount > 0 Then
            xport_rx = MSComm3.Input
            Text1.Text = Text1.Text + xport_rx
            xport_rx = ""
            If m = "ex" Then
                MSComm3.Output = xport_rx
            End If
            numfile = numfile + 1
            Label2.Caption = "XPORT: " + numfile
        End If
        If MSComm1.InBufferCount > 0 Then
            wireless_rx = MSComm1.Input

```

```

Text2.Text = Text2.Text + wireless_rx
wireless_rx = ""
If n = "ew" Then
    MSComm1.Output = wireless_rx
End If
' numfile2 = numfile2 + 1
' Label2.Caption = "Wireless: " + numfile2
End If
Loop Until m = "s"
MSComm3.PortOpen = False
MSComm1.PortOpen = False
End Sub

Private Sub ExitCommand_Click()
    m = "s"
    If MSComm1.PortOpen = True Then
        MSComm1.PortOpen = False
    End If
    If MSComm3.PortOpen = True Then
        MSComm3.PortOpen = False
    End If
End
End Sub

Private Sub DisablePLCCommand_Click()
    m = "dx" 'disable XPORT
End Sub

Private Sub DisableWCommand_Click()
    n = "dw" 'disable Wireless
End Sub

Private Sub EnablePLCCommand_Click()
    m = "ex" 'Enable XPORT
End Sub

Private Sub EnableWCommand_Click()
    n = "ew" 'Enable Wireless
End Sub

Private Sub Form_Load()
    MSComm1.InputLen = 1024
    MSComm3.InputLen = 1024
End Sub

```

**APPENDIX D. COMPONENTS' DATASHEETS USED FOR THIS
PROJECT**

LM6171

High Speed Low Power Low Distortion Voltage Feedback Amplifier

General Description

The LM6171 is a high speed unity-gain stable voltage feedback amplifier. It offers a high slew rate of 3600V/ μ s and a unity-gain bandwidth of 100 MHz while consuming only 2.5 mA of supply current. The LM6171 has very impressive AC and DC performance which is a great benefit for high speed signal processing and video applications.

The ± 15 V power supplies allow for large signal swings and give greater dynamic range and signal-to-noise ratio. The LM6171 has high output current drive, low ISFDR and THD , ideal for ADC/DAC systems. The LM6171 is specified for ± 15 V operation for portable applications.

The LM6171 is built on National's advanced VFP^{TM} II (Vertically Integrated PNP) complementary bipolar process.

Features

(Typical Unless Otherwise Noted)

- Easy-To-Use Voltage Feedback Topology
- Very High Slew Rate: 3600V/ μ s
- Wide Unity-Gain-Bandwidth Product: 100 MHz
- -3dB Frequency @ $A_v = +2$: 62 MHz
- Low Supply Current: 2.5 mA
- High CMRR: 110 dB
- High Open-Loop Gain: 90 dB
- Specified for ± 15 V and ± 5 V Operation

Applications

- Multimedia Broadcast Systems
- Line Drivers, Switches
- Video Amplifiers
- NTSC, PAL and SECAM Systems
- ADC/DAC Buffers
- HDTV Amplifiers
- Pulse Amplifiers and Peak Detectors
- Instrumentation Amplifier
- Active Filters

Typical Performance Characteristics

Closed Loop Frequency Response, Supply Voltage
($A_v = +1$)



Large Signal Pulse Response
 $A_v = +1$, $V_{cc} = \pm 15$



Connection Diagram



Ordering Information

Package	Temperature Range	Transport Media	NSC Drawing
	Industrial -40°C to +85°C		
8-Pin Molded DIP	LM6171AIM LM6171BIN	Reels	NOB
8-Pin Small Outline	LM6171AIM, LM6171BIM LM6171AIMX, LM6171BIMX	Reels 2.5k Units Tape and Reel	MOA

Absolute Maximum Ratings (Note 1)

If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/Distributors for availability and specifications.

ESD Tolerance (Note 2)	2.5 kV
Supply Voltage ($V^+ - V^-$)	36V
Differential Input Voltage	$\pm 10V$
Common-Mode Voltage Range	$V^+ + 0.3V$ to $V^- - 0.3V$
Input Current	$\pm 10mA$
Output Short Circuit to Ground (Note 3)	Continuous
Storage Temperature Range	$-65^\circ C$ to $+150^\circ C$
Maximum Junction Temperature (Note 4)	$150^\circ C$

Soldering Information

Infused or Convection Reflow (20 sec.)	$235^\circ C$
Wave Soldering Lead Temp (10 sec.)	$260^\circ C$

Operating Ratings (Note 1)

Supply Voltage	$5.5V \leq V_{DS} \leq 34V$
Operating Temperature Range (LM171SAI, LM171SB)	$-40^\circ C$ to $+85^\circ C$
Thermal Resistance ($R_{\theta JA}$)	
N Package, 8-Pin Molded DIP	$106^\circ C/W$
M Package, 8-Pin Surface Mount	$172^\circ C/W$

 $\pm 15V$ DC Electrical Characteristics

Unless otherwise specified, all limits guaranteed for $T_J = 25^\circ C$, $V^+ = +15V$, $V^- = -15V$, $V_{CM} = 0V$, and $R_L = 1 k\Omega$. Boldface limits apply at the temperature extremes.

Symbol	Parameter	Conditions	Typ (Note 5)	LM171SAI Limit (Note 6)	LM171SB Limit (Note 6)	Units
V_{OS}	Input Offset Voltage		1.5	3	6	mV max
TC V_{OS}	Input Offset Voltage Average Drift		6			$\mu V/^\circ C$
I_B	Input Bias Current		1	3	3	μA max
I_{OS}	Input Offset Current		0.60	2	2	μA max
R_{in}	Input Resistance	Common Mode	40			$M\Omega$
		Differential Mode	4.5			
R_o	Open Loop Output Resistance		14			Ω
CMRR	Common Mode Rejection Ratio	$V_{CM} = \pm 10V$	110	80	75	dB min
PSRR	Power Supply Rejection Ratio	$V_{DS} = \pm 15V$ to $\pm 5V$	85	85	80	dB min
V_{CM}	Input Common-Mode Voltage Range	CMRR ≥ 60 dB	± 13.5			V
A_v	Large Signal Voltage Gain (Note 7)	$R_L = 1 k\Omega$	90	80	80	dB min
		$R_L = 100\Omega$	80	70	70	dB min
V_{O1}	Output Swing	$R_L = 1 k\Omega$	13.3	12.5	12.5	V min
			-13.3	-12.5	-12.5	V max
		$R_L = 100\Omega$	11.6	9	9	V min
			-11.6	-9	-9	V max
	Continuous Output Current (Open Loop) (Note 8)	Sourcing, $R_L = 100\Omega$	116	90	90	mA min

The fastest way to wireless.

High-performance AC4790 transceivers utilize AeroComm's "masterless" protocol, allowing each transceiver to communicate with any other in-range transceiver for true peer-to-peer operation.

Using field-proven 900MHz FHSS technology that needs no additional site licensing*, AC4790s reject interference, enable co-located system operation, increase output power and maintain data integrity.

AC4790's protocol features a dynamic addressing scheme, which simplifies node-to-node communication. The transceiver enables identification of the most efficient transmission path, so OEMs can design routing sequences that optimize the RF network. This makes AC4790 ideal for a wide variety of industrial applications that must rely on smooth, constant data flow.

Developer tools and integration support back every transceiver line. Let AeroComm help you find the best fit for your application.



AC4790 Highlights

- True peer-to-peer protocol
- Ultra-low duty time (25 msec)
- Small form factor: 1.45 x 3.9 inches
- API commands to control packet routing
- Software-controlled sensitivity
- Network node discovery
- Variable output power: 50mW to 1000mW

Applications



- Commercial Buildings**
- Security & fire alarm
 - Lighting control
 - Access control
 - Building automation
 - Video systems



- Public Works/Infrastructure**
- Traffic management
 - Toll monitoring
 - Safety alerts



- Industrial Management**
- Automated field testing
 - Load testing, inventory
 - Data collection
 - Temperature data
 - Machine output



- Recreation/Active**
- Field data tracking
 - Game scoring
 - Game stats
 - League rankings
 - Scoreboard updates



- Fleet Telemetry**
- Vehicle tracking
 - Cargo data
 - Driver behavior
 - Maintenance logs
 - Mapping

Specifications

PARAMETER	AC4790-200	AC4790-1000
Interface	20-pin FIM connector	20-pin FIM connector
Frequency (software selectable)	902.000 MHz - 902.975 MHz	902.000 MHz - 902.975 MHz
Modulation	FHSS FSK	FHSS FSK
Serial interface options	32 or 50 TTY	32 TTY
Serial interface baud rate	Up to 192,000 bps	Up to 192,000 bps
Output power (at 50% duty)	200mW (variable)	1000mW (variable)
Power consumption†	50 mW typical	500 mW typical
Dimensions	1.45 x 3.9 x 0.75"	1.45 x 3.9 x 0.75"
Connectivity	One-to-one, simplex, RT, SISO	One-to-one, simplex, RT, SISO
Standard antenna (included)	5.0' (1.5m) whip	5.0' (1.5m) whip
Range (line of sight)	1.6 to 4 miles (up to 6.5 km) with external antenna	Up to 20 miles (up to 32 km) with high gain antenna
Temperature	-40° to +85°C	-40° to +85°C
Humidity (non-condensing)	0% to 95%	0% to 95%
Clearance time	1.50 x 1.50 x 0.20 inches	1.50 x 1.50 x 0.20 inches
Weight	0.05 to 0.15 lbs	0.05 to 0.15 lbs
Antenna	Integrated or external option*	Integrated option*

*The 900MHz frequency band is approved for the license and hardware for an external antenna system subject to approval by FCC.

†Power consumption and specifications subject to change. For complete, please contact AeroComm directly.

* Power consumption assumes 70% transmitter output.

* High gain antenna option.



17401 Sanger Drive • Irvine, CA 92614 Phone 949.457.3330 Fax 949.457.3332 <http://www.aerocomm.com>

Flexible RF Protocol

AeroComm's RF202™ embedded transparent protocol simplifies the OEM's integration process by allowing for drop-in installation. As each transceiver receives raw data, it manages over-the-air protocol to assure successful communication. Headers, data packet length, and CRCs are not needed.

AC4700's flexible "masterless" topology supports simple cable replacement up to complex peer-to-peer configurations. Broadcast communication to all transceivers or address packets to a specific destination using unique MAC addresses embedded in each transceiver.



Protocol Features

RF PROTOCOL MODES

- a) Communication
 - Circuit (one-to-one addressing)
 - Broadcast (one-to-many addressing)
- b) Acknowledgment mode (ACK)
 - API with hardware and/or software ACK indication
- c) Ultra-fast sync time
 - Up to 20 simultaneous conversations
 - Intelligent call-extending session time
 - Requires only one 20 msec sync
- d) Remote over-the-air configuration
- e) Standby/lost
 - Software controlled RF deactivation
 - Warns of interference
- f) Random back-off
- g) Network mode discovery
- h) Dynamic radio data table
 - Passes data from up to 8 transceivers

INTERFACE PROTOCOL

- a) On-the-fly transceiver configuration
 - Full API Control
 - Distribution address
 - RF transmit power
 - RF Channel
 - Broadcast address
- b) Raw data or transparent API
- c) Long range mode
 - Enables variability modes
- d) AID, Data generic IDs
- e) Variable baud rate
- f) RF packet size, timeout control
- g) Onboard temperature sensor
- h) Handshaking
 - CTS/RTS
- i) In range indicator
- j) Error detection
 - Different CRC
 - Duplicate packet filtering
- k) Data encryption standard (DES)

ARCHITECTURE



Peer-to-peer

Placing Orders

Select features from the list below to identify the appropriate part number. More product lines are available for industrial & commercial applications. Contact AeroComm Sales for details. Toll free 1-800-450-0000, email sales@aerocomm.com

PART NUMBERS

AC4700-280M

800MHz transceiver, 3.2V-5.5V, TTL serial, 0-100MHz, -40° to +80° C, 9MMX antenna

AC4700-280A

800MHz transceiver, 3.2V-5.5V, TTL serial, 0-100MHz, -40° to +80° C, integral antenna

AC4700-1900M

900MHz transceiver, 3.2V-5.5V, TTL serial, 0-100MHz, -40° to +80° C, 9MMX antenna

AC4700-1x1

See AC4700-1x1 datasheet.



SN54ABT125, SN74ABT125 QUADRUPLE BUS BUFFER GATES WITH 3-STATE OUTPUTS

SCDS100 – FEBRUARY 1987 – REVISED AUGUST 2000

- Typical V_{OLP} (Output Ground Source) $<1\text{ V}$ at $V_{CC} = 5\text{ V}$, $T_A = 25^\circ\text{C}$
- High-Drive Outputs ($\sim 32\text{-mA}$ I_{OL} , 64-mA I_{OL})
- I_{LH} and Power-Up 3-State Support Hot Insertion
- Latch-Up Performance Exceeds 500 mA Per JEDEC Standard JESD-17
- ESD Protection Exceeds JEDEC 22 – 2000-V Human-Body Model (A114-A) – 200-V Machine Model (A115-A)

SN54ABT125 ... J OR W PACKAGE
SN74ABT125 ... Q, SN, N, NS,
OR PW PACKAGE



SN54ABT125 ... REY PACKAGE
(TOP VIEW)



SN54ABT125 ... FK PACKAGE
(TOP VIEW)



NC – No internal connection

description/ordering information

The 'ABT125 quadruple bus buffer gates feature independent line drivers with 3-state outputs. Each output is disabled when the associated output-enable (OE) input is high.

These devices are fully specified for hot-insertion applications using I_{LH} and power-up 3-state. The I_{LH} circuitry disables the outputs, preventing damaging current backflow through the devices when they are powered down. The power-up 3-state circuitry places the outputs in the high-impedance state during power up and power down, which prevents driver conflict.

To ensure the high-impedance state during power up or power down, OE should be tied to V_{CC} through a pullup resistor; the minimum value of the resistor is determined by the current-sinking capability of the driver.

ORDERING INFORMATION

T_A	PACKAGE	ORDERABLE PART NUMBER	TOP-SEE MARKINGS
-40°C to 85°C	PDP – N	Tube	SN54ABT125N
	QFN – REY	Tape and reel	SN54ABT125RQYR
	SOIC – D	Tube	SN54ABT125D
		Tape and reel	SN54ABT125DR
	SOP – NS	Tape and reel	SN74ABT125NSR
	SSOP – DB	Tape and reel	SN74ABT125DBR
-50°C to 125°C	TSSOP – FW	Tape and reel	SN74ABT125FWR
	COF – J	Tube	SN54ABT125J
	COF – W	Tube	SN54ABT125W
	LOGIC – FK	Tube	SN54ABT125FK

¹ Package drawings, standard packing quantities, thermal data, symbolization, and PCB design guidelines are available at www.ti.com/package.



Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.

REVISIONS: This document is subject to change without notice. The latest revision of this document is the only one that should be used. The revision history is located at the end of this document.



POST OFFICE BOX 655505 • DALLAS, TEXAS 75265

Copyright © 2000, Texas Instruments Incorporated. All rights reserved. This document is the property of Texas Instruments and is not to be distributed outside of the company.

SN54ABT125, SN74ABT125
QUADRUPLE BUS BUFFER GATES
WITH 3-STATE OUTPUTS

DS0152D – FEBRUARY 1987 – REVISED NOVEMBER 2002

FUNCTION TABLE
 (each buffer)

INPUTS		OUTPUT	
OE	A	Y	
L	H	H	
L	L	L	
H	X	Z	

logic diagram (positive logic)



Pin numbers shown are for the D, DB, J, N, NS, PW, RGY, and W packages.

absolute maximum ratings over operating free-air temperature range (unless otherwise noted)[†]

Supply voltage range, V_{CC}	–0.5 V to 7 V
Input voltage range, V_I (see Note 1)	–0.5 V to 7 V
Voltage range applied to any output in the high or power-off state, V_O	–0.5 V to 5.5 V
Current into any output in the low state, I_{OL} SN54ABT125	96 mA
SN74ABT125	128 mA
Input clamp current, I_{IK} ($V_I < 0$)	–18 mA
Output clamp current, I_{OK} ($V_O < 0$)	–50 mA
Package thermal impedance, θ_{JA} (see Note 2): D package	86°C/W
(see Note 2): DB package	96°C/W
(see Note 2): N package	86°C/W
(see Note 2): NS package	76°C/W
(see Note 2): PW package	113°C/W
(see Note 2): RGY package	47°C/W
Storage temperature range, T_{stg}	–65°C to 150°C

[†] Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute maximum-rated conditions for extended periods may affect device reliability.

- NOTES: 1. The input and output negative-voltage ratings may be exceeded if the input and output clamp current ratings are observed.
 2. The package thermal impedance is calculated in accordance with JEDEC J-15-7.
 3. The package thermal impedance is calculated in accordance with JEDEC J-15-5.



POST OFFICE BOX 655800 • DALLAS, TEXAS 75265

XPort™ Data Sheet

General Description

The XPort™ is the most compact, integrated solution available to web-enable any device with a serial interface. By simply adding XPort™ to a product design, device manufacturers cut their design cycle by as much as 80% and are able to offer Ethernet connectivity in record time.



The XPort offers the highest level of integration available in a device server. Within a compact RJ45 package is a D5Tn-EX 186 controller, memory, 10/100 Ethernet transceiver, high-speed serial port, status/diagnostic LEDs, and 3 programmable I/O pins. In the space that is normally consumed by a connector, the XPort provides a complete networking interface.

To enable access to a local network or the Internet, the XPort integrates a fully developed TCP/IP network stack and OS. The XPort also includes an embedded web server used to remotely configure, monitor, or troubleshoot the attached device.



Where there's a need for custom user interfaces and a desire to use common and familiar tools, the XPort can serve web pages to a web browser. The XPort becomes a conduit between you and your device over the network or Internet.

The Windows™-based configuration software, DeviceInstaller, simplifies installation and setup. The XPort can also be set up locally through its serial port, or remotely over a network using Telnet or a web browser. Flash memory provides for maintenance-free nonvolatile storage of web pages, and allows future system software upgrades.

Using our highly integrated hardware and software platform, you will add profit to your bottom line by significantly reducing product development time, risk, and cost.

Key Features

- The only complete, integrated solution in an RJ45 form factor
- Complete integrated solution
- Embedded web server
- 10/100Mbit Ethernet – Auto-Sensing
- Stable, field proven TCP/IP protocol suite and web-based application framework
- Easy configuration through a web interface
- Easy customization of HTML web pages and configuration screens
- Interactive web pages through the use of Java applets
- E-mail
- 128-, 192-, or 256-bit AES Rijndael encryption (Optional)
- EM tested and compliant
- Extended operating temperature:
 - 40 to +85° C normal mode
 - 40 to +75° C high-performance mode
- High-performance processor (12 MIPS at 48 MHz; 22 MIPS at 88 MHz)
- Network overhead handled by XPort
- Password protection
- Upgrade XPort's firmware over the network
- 3.3V power
- Serial-to-10/100 Ethernet conversion
- 921,600 baud serial speed

Hardware & Software Description

The XPort is a complete solution (hardware and software) for web-enabling your edge devices. Packed into an RJ45 connector smaller than your thumb, this powerful device server comes with a 10BASE-T/100BASE-TX Ethernet connection, a reliable and proven operating system stored in flash memory, an embedded web server, a full TCP/IP protocol stack, and standards-based (AES) encryption.

The XPort software runs on a DSTn-EX controller which has 256 KB of SRAM, 16 KB of boot ROM, and a MAC with integrated 10/100BASE-TX PHY. The XPort communicates to the edge device through a 3.3V serial interface and three general-purpose programmable I/O pins. 512 KB of flash memory is included for storing firmware and web pages. The XPort runs on 3.3V, and has a built-in voltage supervisory circuit that will trigger a reset if the supply voltage drops to unreliable levels (2.7V). A built-in 1.8V regulator drives the processing core of the EX controller.

An RJ45 Ethernet cable connects directly into an XPort. Ethernet magnetics, status LEDs, and shielding are built in. The XPort was designed to meet class B emissions levels, which makes the electromechanical integration very simple.



PCB Interface

The 8-pin PCB interface consists of 3.3V CMOS Serial In/Out, 3 Flow Control/Handshake/PRO pins, reset input, +3.3V power, and signal ground. Signal pins Data In, Data Out and CPs are 5V tolerant.

Table 1 - PCB Interface Signals

Signal Name	Pins	Function
GND	1	Circuit Ground
VCC	2	+3.3V Power In
Reset (in)	3	External Reset In
Data OUT	4	Serial Data Out
Data IN	5	Serial Data In
CP0	6	CP1 can be configured as follows: <ul style="list-style-type: none"> • Flow control: RTS (Request to Send) output driven by DSTn's built-in UART for connection to CTS of attached device. • Programmable input/output: CP1 can be driven or read through software control, independent of serial port activity.
		CP2 can be configured as follows: <ul style="list-style-type: none"> • Modem control: DTR (Data Terminal Ready) output driven by DSTn's built-in UART for connection to DCD of attached device. • Programmable input/output: CP2 can be driven or read through software control, independent of serial port activity.
CP1	7	CP2 can be configured as follows: <ul style="list-style-type: none"> • Flow control: CTS (Clear to Send) input read by DSTn's built-in UART for connection to RTS of attached device. • Modem control: DCD (Data Carrier Detect) input read by DSTn's built-in UART for connection to DTR of attached device. • Programmable input/output: CP2 can be driven or read through software control, independent of serial port activity.
CP2	8	CP3 can be configured as follows: <ul style="list-style-type: none"> • Flow control: CTS (Clear to Send) input read by DSTn's built-in UART for connection to RTS of attached device. • Modem control: DCD (Data Carrier Detect) input read by DSTn's built-in UART for connection to DTR of attached device. • Programmable input/output: CP3 can be driven or read through software control, independent of serial port activity.

Ethernet Interface

The 10/100 Ethernet magnetics, network status LEDs, and RJ45 connector are integrated into the XPort.

Table 2 - Ethernet Interface Signals

Signal Name	Dir	Count	Primary Function
TX+	Out	1	Transmit Data +
TX-	Out	2	Transmit Data -
RX+	In	3	Receive Data +
RX-	In	4	Receive Data -
Not Used		5	Terminated
Not Used		6	Terminated
Not Used		7	Terminated
Not Used		8	Terminated
SHIELD			Chassis Ground

Protocol Support

The XPort uses Internet Protocol (IP) for network communications and Transmission Control Protocol (TCP) to assure that no data is lost or duplicated, and that everything sent arrives correctly at the target.

Other suggested protocols are listed below:

- ARP, UDP, TCP, ICMP, Telnet, TFTP, AutoP, DHCP, HTTP, and SMTP for network communications.
- TCP, UDP, and Telnet for connections to the serial port.
- TFTP for firmware updates.
- IP for addressing, routing, and data block handling over the network.
- User Datagram Protocol (UDP) for typical datagram applications in which devices interact with other devices without maintaining a point-to-point connection.

* For a complete discussion of protocol support, see the XPort user manual.

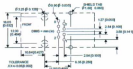
LEDs

The device contains two bi-color LEDs built into the front of the XPort connector. (See dimension drawing for location.)

Link LED (Left Side)		Activity LED (Right Side)	
Color	Meaning	Color	Meaning
Off	No Link	Off	No Activity
Amber	10 Mbps	Amber	Half-Duplex
Green	100 Mbps	Green	Full-Duplex

Recommended PC Board Layout

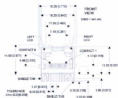
The hole pattern and mounting dimensions for the XPort are shown in the following drawing:



For proper heat dissipation, the PCB should have approximately 1 square inch of copper attached to the shield tabs. The shield tabs are an important source of heat sinking for the device.

Discussion

The XPort dimensions are shown in the following drawings:



Executive View

Side View



Note: PADS and PROTEL design files are included with the XPort development kit.

XPort Technical Data

Category	Description
CPU/Memory	Lantronix DET+ EX 186 CPU, 256 KB zero-wait state SRAM, 512 KB Flash, 16 KB Boot ROM
Timers	Upgradable via TFTP and serial port
Reset Circuit	Internal 200ms power-up reset pulse. Power-drop reset triggered at 2.8V. External reset input causes an internal 200ms reset
Serial Interface	CMOS (Asynchronous) 3.3V-level signals Rate is software selectable (300 bps to 921600 bps)
Serial Line Formats	7 or 8 data bits, 1-2 Stop bits, Parity: odd, even, none
Modem Control	DSR/DTR, CTS, RTS
Flow Control	XON/XOFF (software), CTS/RTS (hardware), none
Programmable I/O	3 PIO pins (software selectable) sink or source 4mA max.
Network Interface	PLAS Ethernet 10BASE-T or 100BASE-TX (auto-sensing)
Compatibility	Ethernet Version 2 IEEE 802.3
Protocols Supported	ARP, UDP/IP, TCP/IP, Telnet, ICMP, SNMP, DHCP, BOOTP, TFTP, Auto IP, and HTTP
LEDs	10BASE-T & 100BASE-TX Link Activity, Full/half duplex. Software generated status & diagnostic signals can optionally drive external LEDs through GPI & GPO (see I/O Guide)
Management	Internal web server, SNMP, Serial login, Telnet login
Security	Password protection, locking features, optional 160bit, 128-, 160-, or 256-bit encryption
Internal Web Server	Serves web pages Storage capacity: 384 KB
Weight	9.6 grams (0.34 oz)
Material	Metal shell, thermoplastic case
Temperature	Operating range: Commercial Temp RoHS-product: 0°C to +70°C (32°F to 158°F) Extended Temp RoHS-product: -40°C to +85°C (-40°F to 185°F) Storage range: -40°C to +85°C (-40°F to 185°F)
Relative Humidity	Operating: 5% to 95% non-condensing
Shock/Vibration	Non-operational shock: 500 g's. Non-operational vibration: 20 g's
Warranty	2-year limited warranty
Included Software	Windows™ 98/NT/2000/XP-based DeviceInstaller configuration software and Windows™-based Comm Port Redirector
EMI Compliance	Radiated & conducted emissions - complies with Class B limits of EN 55022:1998 Direct & indirect ESD - complies with EN55024:1998 RF Electromagnetic Field Immunity - complies with EN55024:1998 Electrical Fast Transient/Burst Immunity - complies with EN55024:1998 Power Frequency Magnetic Field Immunity - complies with EN55024:1998 RF Common Mode Conducted Susceptibility - complies with EN55024:1998

**APPENDIX E. DATA ACQUISITION SYSTEM TRANSMITTER
SCHEMATIC**

